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### SMITHSONIAN

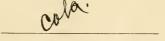
# MISCELLANEOUS COLLECTIONS.

VOL. I.



"EVERY MAN IS A VALUABLE MEMBER OF SOCIETY WHO BY HIS OBSERVATIONS, RESEARCHES,

AND EXPERIMENTS PROCURES KNOWLEDGE FOR MEN."—SMITHSON.



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### ADVERTISEMENT.

The present series, entitled "Smithsonian Miscellaneous Collections," is intended to embrace all the publications issued directly by the Smithsonian Institution in octavo form; those in quarto constituting the "Smithsonian Contributions to Knowledge." The quarto series includes memoirs embracing the records of extended original investigations and researches resulting in what are believed to be new truths, and constituting positive additions to the sum of human knowledge. The octavo series is designed to contain reports on the present state of our knowledge of particular branches of science; instructions for collecting and digesting facts and materials for research; lists and synopses of species of the organic and inorganic world; museum catalogues; reports of explorations; aids to bibliographical investigations, etc., generally prepared at the express request of the Institution, and at its expense.

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JOSEPH HENRY, Secretary S. I.



### SMITHSONIAN MISCELLANEOUS COLLECTIONS.

### DIRECTIONS

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### METEOROLOGICAL OBSERVATIONS,

AND THE

REGISTRY OF

PERIODICAL PHENOMENA.



WASHINGTON: SMITHSONIAN INSTITUTION. 1860.

PHILADELPHIA:
COLLINS, PRINTER, 705 JAYNE STREET.

### DIRECTIONS

FOR

### METEOROLOGICAL OBSERVATIONS,

### ADOPTED BY THE SMITHSONIAN INSTITUTION

The following directions were originally drawn up for the use of the observers in correspondence with the Smithsonian Institution, by Professor Guyot, of the College of New Jersey, Princeton, and are now reprinted, with a series of additions, for more general distribution. The additions are indicated by brackets, [ ].

SECRETARY S. I.

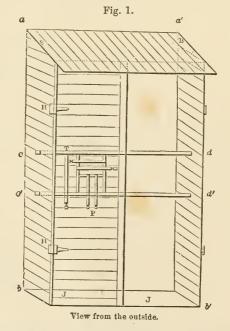
#### PLACING AND MANAGEMENT OF THE INSTRUMENTS.

#### THERMOMETER.

Placing.—Place the thermometer in the open air, and in an open space, out of the vicinity of high buildings, or of any obstacle that impedes the free circulation of the air. It should be so situated as to face the north, to be always in the shade, and be at least from nine to twelve inches from the walls of the building, and from every other neighboring object. The height from the ground may be from ten to fifteen feet, and, as far as possible, it should be the same at all the stations. The instrument should be protected against its own radiation to the sky, and against the light reflected by neighboring objects, such as buildings, the ground itself, and sheltered from the rain, snow, and hail. The following arrangement will fulfil these requirements (Fig. 1):—

Select a window situated in the first story, fronting the north, in a room not heated or inhabited; remove the lattice blinds, if there be any, and along the exterior jambs of the window place perpendicularly two pieces of board ( $a \ b-a' \ b'$ ), projecting to

a distance of from twenty to twenty-four inches from the panes. At half this distance, ten or twelve inches from the panes, and at the height of the eye of the observer, when in the chamber, pass from one piece of board to the other two small wooden transverse bars (c d, c' d'), each an inch broad, for the purpose of supporting the instruments. Upon the outer edge of the boards fasten, in the usual way (H H), the latticed blinds which were removed from the jambs, or two others provided for the purpose. That blind behind which the instruments are to be placed, is to serve as a screen, and must be fastened, almost entirely closed, so as to make a little more opening; the other will remain entirely open, to allow a free access of air and light, and is not to be closed except in great storms. The whole must be covered with a small inclined roof of boards (B E), placed at least fifteen or twenty inches above the instrument. The lower part (J J), or the basis, may remain open.



[The foregoing is a convenient arrangement by which the observations can be taken without exposing the observer to the

weather. To prevent radiation from the room, the windows during the intervals of observations may be closed with an inside wooden shutter. The outside of the lattice-work should be painted white, to reflect off the light and heat which may fall upon it.]

The thermometer must be placed exactly perpendicular, the middle of the scale being at the height of the eye against the

two small wooden bars, so that the top of the scale being fixed by a screw to the upper bar, the bulb may pass at least two or three inches beyond the lower bar. The instrument is attached to the last by a little metallic clasp. (Fig. 2.) It will thus be placed ten or twelve inches from the panes, from the screen, and the other parts of the window.

[In a later arrangement, a single transverse bar is used. This being placed at the necessary height, the thermometers are attached to it by small metal brackets, which support them at a distance from the bar of about two inches. The metal brackets are permanently screwed to the bar, and the thermometers are fastened to them by small finger-screws, by

Fig. 2.

which they can be detached at pleasure. The order of placing them is shown in the cut.]

Reading.—To read the thermometer, the eye must be placed

exactly at the same height as the column of mercury. Unless this precaution is taken, there is a liability to errors, the greater in proportion to the thickness of the glass of the stem and the shortness of the degrees. The reading should be made at all times, and especially in the winter, through the panes, and without opening the window; otherwise the temperature of the chamber will inevitably influence the thermometer in the open air. The degrees must be read, and the fractions carefully estimated in tenths of degrees. After having rapidly taken the observation, another should be made to verify it. If there are several other instruments to observe, and the thermometer is to be read first, the first reading may be made some minutes before the hour; the second, after the reading of the psychrometer; and if there is a difference, the mean number is to be entered in the journal. When, notwithstanding the shelter, the bulb of the thermometer is moistened by rain or fog, or covered with ice or snow, it is necessary to wipe it rapidly, and not to record the degree until the instrument has been allowed to acquire the true temperature of the air.

Verification.—Verify the zero point, at the beginning and end of winter. For this purpose, fill a vessel with snow, immerse the bulb of the thermometer in the middle of it, so as to be surrounded on every side by a layer of several inches of snow, slightly pressed around the instrument. The stem must be placed exactly perpendicular, and covered with snow as far up as the freezing-point on the scale. Let it stand so for half an hour or more, and then read it, taking great care to place the eve at the same height as the summit of the mercurial column. If the top of the column does not coincide with the freezingpoint of the scale, the exact amount of the difference must be ascertained, and the correction immediately applied. At the same time enter in the journal, under its appropriate head, the day on which the experiment is made, its quantity, and the hour at which the application of it was commenced. [It is necessary to add, that since the zero point of the thermometer is not that of the temperature of snow as it is frequently found when exposed to the atmosphere, but that of melting snow, the experiment must be made in a place above the temperature of freezing. Instead of snow, pounded ice may be employed.]

[Green's thermometers have an arrangement by which the tube can be slipped down the small quantity necessary to correct for this change. The end of the tube is fitted into a small plate of German silver, and this fastened by a screw to the scale. If, on testing the thermometer, the mercury be found to stand above 32°, free the screw one or two turns without taking it out, and push down the plate the necessary amount to bring the mercury to coincide. The thermometer must be handled with great care in making this adjustment, and it may be well, for additional security against accident, to loosen all the screws which fasten the bands around the tube; it will then slide in them more freely. After completing the adjustment, they may again be set moderately tight. The object of this adjustment being only to avoid the trouble of making a correction, it is not advisable to attempt it, if the observer thinks that he risks, in so doing, the safety of his instrument. As the tubes of these standard thermometers are kept for a considerable time before fixing the zero point, in most cases the moving will not be required. After the first year the zero point changes little, and practically, when exposed only to atmospheric influences, may be considered permanent.]

### SELF-REGISTERING THERMOMETERS.

Placing.—These two thermometers, indicating the maxima and minima, are to be placed beside the common thermometer, in a horizontal position, with the bulbs opposite and free, on two small perpendicular supports uniting the two bars, as shown in Fig. 1.

Reading.—For the reading, place the eye in such a position that the visual ray may be perpendicular to the extremity of the index; enter the indications with the fractions of degrees, if there are any, and, after having verified them again, bring back, by means of the magnet, the indexes of the two thermometers to the summit of their respective columns.

Verification.—Compare the indications of the two thermometers frequently, and especially the spirit thermometer, with those of the common thermometer; verify the zeros at least twice a year, and, if there is a difference, adjust the zero anew, if the instrument permits, to eliminate the correction, as has been stated above for the simple thermometer, or take this correction into account in the register.

[The maximum thermometer is subject to derangement by the mercury getting to the side of the steel index and wedging it fast. When such is the case, put the bulb in ice, if it is necessary to bring the mercurial column so low, or cool it sufficiently to get all the mercury down that will pass the index; then move the magnet along the tube with a slight knocking or jarring motion, and try to get the index into the chamber at the top of the stem. If you get the index free of the wedge, but with mercury above it, heat the bulb until all the disjointed mercury and index are driven into the chamber, then keep the index up by the magnet, and the mercury will go back as the bulb cools. The great point of attention is to get and keep the index free of the wedge. The mercury being above is of little consequence, as it can readily be heated up into the chamber; in doing this, most watchfulness is required in not suffering the index to wedge

by the driving mercury. If the index is so wedged that it cannot be moved by these methods, then grasp the thermometer firmly in the hand, and swing it quickly, as if you wished to throw the mercury into the chamber at the top; the index, with more or less mercury, will be found in the chamber: if not, repeat the swinging until it is there. Then heat up the bulb until the mercury joins that in the chamber, keep the index up by the magnet, and let the mercury, by cooling, go back in unbroken line.

Iu using the magnet to move the index up into contact with the mercury, care must be taken not to urge it too strongly, or it may *enter* the mercury.

In using the spirit-thermometer, the same care is necessary as with the mercurial, since the index may sometimes be forced out of the spirit, entangling the vapor and the alcohol. When this is the case, the thermometer must be taken down and held vertically; a few taps or jars will bring the spirit together. The spirit-thermometer requires attention, also, in the following particular. The vapor above the column is apt, in time, to condense at the end of the tube, commonly at the very end. When the spirit-thermometer stands lower than the mercurial one, this may be suspected and looked for. When so found, the thermometer should be taken down and shaken until the alcohol runs down: it should then be kept in an upright position for some time, to drain. If it is found difficult to shake down the condensed vapor. the end of the tube may be carefully and slowly heated with a small lamp, or a small rod of heated iron held at a short distance, keeping the bulb and lower part as cold as possible; the alcohol by vaporization will then condense at the surface of the spirit in connection with the bulb. Occasionally, in cold climates, spiritthermometers are deranged by the air absorbed by the alcohol becoming free in the bulb at a low temperature. When this occurs, bring the thermometer to as low a temperature as may be convenient; then hold it in such a position that the air-bubble comes to the juncture of the bulb and tube, warm the bulb till all the air is in the tube; then, by shaking the thermometer, or by gentle knocking, the spirit will flow down, and the air speck come to the top.

This does not occur in spirit-thermometers that are closed with a vacuum, and the spirit at the time well freed from air.

In this case, however, the above-named difficulty from vaporization takes place more readily than when closed with air. These derangements of the spirit-thermometer are readily rectified, and only require occasional examination to detect them.

Both the maximum and minimum thermometers may be adjusted without the magnet, by raising one end sufficiently to allow the index to slide down by its own weight.\*

The ordinary maximum thermometer (Rutherford's) not working well, even in the hands of many careful observers, has occasioned several attempts to make one without an index.

Mr. Green has lately contrived one. The object is effected by inclosing in the bulb a glass valve, which is floated by the mercury to the juncture of the bulb and tube. On an increase of heat the mercury from the bulb passes this valve, but on contraction from a decreasing temperature, the portion in the column is obstructed, and remains stationary, indicating the maximum point attained.

To set the instrument for another observation, it is held bulb downwards, and with a gentle jerk the mercury falls and joins that in the bulb; it is then placed horizontal in the usual way.

A movable valve-piece is introduced rather than a fixed obstruction or stricture, as in a new and ingenious maximum thermometer by Messrs. Negretti and Zambra, of London, in expectation that the observer will find greater ease and satisfaction in readjusting the instrument for observation.

Professor Phillips, of England, has also devised one. His plan is to cut off a portion of the column of mercury by an intervening small bubble of air. An increase of heat drives this detached portion forward, and leaves it there on a decrease of heat.

This form is also made by Mr. Green, and possesses some advantages peculiar to it; but, until experience decide otherwise, we doubt if it can be put in order after accidental derangement, by every observer. The former plans are not open to this objection.]

<sup>\*</sup> The index of the spirit-thermometer is frequently made of a small cylinder of enamel, which cannot be moved by the magnet.

<sup>†</sup> These thermometers being new in plan, particular instructions in regard to suspending and setting them will be given with each instrument by the maker, Mr. James Green, New York.

#### PSYCHROMETER.

Placing.—The psychrometer, or wet-bulb thermometer, must be situated under the same conditions as the thermometer. It should be placed on the same wooden bars, several inches off, and outside of the thermometer. (See Fig. 1.)

The bulbs should also be entirely free, and at a distance from the bars.

In case of violent winds, the instrument may be sheltered by the movable blind, which may also serve as a fan to promote evaporation when the air is too still.

The cloth which surrounds the bulb ought to be of medium fineness, not too coarse; it should form a covering of equal thickness on all sides, and should not be drawn too closely upon the glass. Linen is preferable to cotton, which retains the dust. The covering should be changed every two or three months, and the bulb cleaned. [The linen may be washed, without removal, by means of a jet of clean water from a small syringe.]

Observation.—For the observation, take first a small vessel full of water, which should be left on the window, that the water may be at the temperature of the air; bring it near to the bulb, and immerse the bulb several times into the water. All the space between the bulb and the bottom of the scale must be wet, and care must be taken that the wrapping is thoroughly moistened, without, however, a too large drop remaining suspended at the bulb. The water used must be pure; the best is rain-water, filtered, because it does not hold any salt in solution, which might incrust the cloth after evaporation.

[In some arrangements of the psychrometer, the wet-bulb is kept constantly wet by conducting water to it from a small vessel, by capillary attraction, along a string of cotton wick. A series of comparative observations was made at this Institution, last summer, on these two modes of wetting the bulb, which gave the same result within a fraction of a degree from the mean of the records of a month. The observers connected with the Coast Survey prefer the method of dipping the covered bulb.]

After wetting the bulb, shut the window, and leave the psychrometer for a time.

While the wet bulb is slowly acquiring the temperature of

evaporation, the observer is occupied with other observations, though watching the psychrometer to make sure of the moment when it has become stationary. In summer, from four to ten minutes are needed for this, according to the size of the bulb; but in winter, when the water freezes on the bulb, it must be moistened from fifteen to thirty minutes before the observation, which should not be made until the ice around the bulb is quite formed and dry. The best way is to keep round the bulb a layer of ice, constant and uniform, which should be neither too thick nor too thin; then the observation may take place immediately. When the temperature is in the neighborhood of the freezing-point, the observation of the psychrometer requires very peculiar care; the reason of which we have elsewhere explained. During a fog, the wet-bulb thermometer may sometimes be higher than the dry-bulb; then the air is over-saturated, and contains, besides the vapor at its maximum of tension, water suspended in a disseminated liquid state. This is, however, not a frequent occurrence.

If the air is very still, it is well to increase the evaporation by setting the air in motion by a fan. If the wind is too strong, the instrument should be protected by the movable blind. The reading must be made rapidly, and, as much as possible, at a distance, and without opening the window; for the proximity of the observer, either by the heat radiating from his body, or by his breath, as well as the temperature and the hygrometrical state of the air issuing from the chamber, which is always different from that of the external air, especially in winter, would infallibly act upon the instruments, and would falsify the observation.

Verification.—The two thermometers must be carefully compared from time to time, and if a difference is found, the instruments must be adjusted, or it must be taken into the account, and the observations corrected when entered in the journal.

#### BAROMETER.

Placing.—The barometer should be placed in a room, of a temperature as uniform as possible; not heated, nor too much exposed to the sun. The instrument must be suspended at the height of the eye, near a window, in such a manner as to be lighted perfectly, without exposure either to the direct rays of

the sun, or to the currents of the air, which always take place at the joinings of the windows. When the barometer has to be fixed to the wall, as is the case with all the common stationary and wheel barometers, care must be taken to secure the tube in a position perfectly vertical, regulating it by the plumb-line, first in front, then at the sides, at least in two vertical planes cutting

Fig. 3. w 20

each other at right angles. When the instrument is so constructed as to take its equilibrium itself, as the Fortin barometers and those of J. Green, recently made under the direction of the Smithsonian Institution, it is enough to hang it on a strong hook. These conditions being fulfilled, the rest of the arrangement may be varied according to the nature of the localities. For the Fortin and Green barometers, the following arrangement is convenient, and may be almost everywhere adopted. (See Fig. 3.)\*

A small oblong box  $(a \ b)$ , some inches longer than the barometer, and a little broader than its eistern, is firmly set against the wall (w w'), near the window, in such a manner as to open in a direction parallel to the panes; at the summit (a) it has a strong hook (h h'), which extends beyond the box about two or three inches, and on which the barometer is suspended. The instrument remains generally in the box, which is closed by a movable cover, and which protects it from external injuries, from dust, and from the direct radiation of warm bodies, or the currents of air from the window, and diminishes the effect of the too sudden variations of temperature. When it is to be observed, the barometer is taken by the upper end of the tube, and the suspending ring is made to slide towards the end of the

<sup>\*</sup> The standard barometer at the Smithsonian Institution is stationary and inclosed within a narrow case, the front and two sides of which open out by means of hinges so as fully to expose the instrument at the time of the observation.

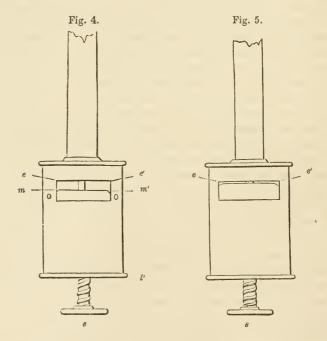
hook. The instrument is then in the full light of the window, in front of which the observer places himself; the summit of the mercurial column, as well as the surface of the mercury in the cistern, are completely lighted, and the reading becomes easy and certain. Moreover, the slight oscillating movement impressed on the instrument, by changing its place, breaks the adherence of the mercury to the glass, and thus prepares a good observation. After the reading, the barometer is again slipped gently into the box, and this is closed.

Observation.—The different operations of the barometer of constant level should be made in the following order:—

- a. Before all, incline the instrument gently, so as to render the mercurial column very movable; then, after having restored it to rest, strike several slight blows upon the easing, in such a manner as to impress on the mercury gentle vibrations. The adherence of the mercury to the glass will thus be destroyed, and the column will take its true equilibrium.
- b. Note the degree and the tenths of degrees of the thermometer attached to the instrument; for it will be seen that the heat of the observer's body soon makes it rise.
- c. Bring, by means of the adjusting screw (Fig. 4), the surface of the mercury to its constant level. In Green's first barometers, the metallic envelop of the cistern is pierced through  $(o\ o')$ , and allows the surface of the mercury contained in the glass cistern to be seen. The plane which passes through the upper edge  $(e\ e')$  of this opening is the true level, or the zero of the scale, to which the surface of the mercury must be restored.

For this, take hold, with the left hand, of the lower edge of the cistern  $(l\ l')$ , taking great care not to disturb its vertical position; apply the right hand to the adjusting screw (s), and, turning it gently, bring by degrees the level surface of the mercury to the upper edge  $(e\ e')$  of the opening of the cistern, until there remains between the two only an almost imperceptible line of light, as in the Fig. 5  $(e\ e')$ . Then leave the instrument to itself, to re-establish its verticality, if it had been accidentally deranged, and placing the eye exactly at the height of the mercury, examine whether the contact is exact. For this operation, it is important to have a good light; the cistern ought to be placed higher than the lower edge of the window, so that the light may reach it directly. It is necessary also to take care

not to confound the slight line of light which marks the opposite edge of the cistern, with the light reflected by the surface of the mercury against the inner walls; the former is always sharp and well defined; the latter vague and indefinite. When, before adjusting the level, the mercury is higher than the upper edge, it is necessary to begin by lowering it beneath the level (see Fig. 4), so as to leave an interval of light, which is then gradually shut out, as has been described. When the observation is to be made in the night, place the lamp before, and not behind, the instrument, and somewhat higher than the eye; and if the wall itself is not light enough, place behind the cistern, or the top of the column, a viece of white paper, which reflects the light.



In the barometers with an ivory point, as the Fortin, Newman, and Green barometers, the extremity of this point is the zero of the scale, which must be brought into exact contact with the surface of the mercury. We commonly judge that this takes place when we see the actual rounded summit of the point co-

incide exactly with its image reflected below by the mercury. This method may be very good when the surface of the mercury is perfectly pure and brilliant; but this is very rare. It is generally dimmed by a slight layer of oxide, which makes the coincidence of the point with its image uncertain. It is safer to judge of the contact in a different manner. From the moment when the point does more than touch the surface, it forms around itself. by capillary action, a small depression, which, breaking the direction of the reflected rays, becomes immediately very easy to discover. It is enough, then, to raise the mercury so as slightly to immerse the point; then to lower it gradually until the little depression disappears. If care is taken to make a good light fall on that portion of the mercury which is under the point, and to use the aid of a magnifier, the adjustment of the point thus made becomes not only easy, but very certain, and the errors to which we are liable are almost insensible, for they do not exceed two or three hundredths of a millimetre, or a thousandth of an inch.

d. The level being thus adjusted to the zero of the scale, we proceed to observe the height of the summit of the column. Take hold of the instrument with the left hand, above the attached thermometer, without moving it from the vertical; strike several slight blows in the neighborhood of the top of the column; then, by means of the screw, lower the slide which carries the vernier, until the plane passing through the two lower opposite edges of it is exactly tangent to the summit of the meniscus—that is, the convexity which terminates the column. We know that this is the case when, placing the eye exactly at the height of the summit of the column, we still see the summit of the column, without there being any trace of light between the summit and the edge of the ring. To convince ourselves that the barometer has remained quite vertical during its operation. we leave it to itself, and when it is at rest, we look again to see whether the ring has remained tangential to the summit of the column. If it has not, the verticality has been disturbed; it must be adjusted anew. It is necessary, at the same time, to examine if the adjustment of the surface of the mercury in the cistern has remained the same. The attached thermometer will also be read anew, and if it indicates a temperature noticeably higher than at the commencement of the observation, a mean

value between the two indications must be adopted. An exact observer can never dispense with these verifications.

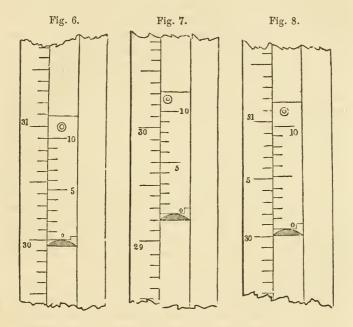
e. Nothing more, then, remains than to read the instrument. In the English barometers, the inches and tenths of inches are read directly on the scale, the hundredths and thousandths on the vernier. In the French barometers, with the metrical scale, the centimetres and millimetres are read on the scale, and the fractions of millimetres on the vernier. We begin by reading on the scale the number of inches and tenths of an inch, or of millimetres, there are, as far up as the line which corresponds to the lower edge of the vernier, and which marks the summit of the column. In the Green barometers, this line marks at the same time the zero of the vernier. If this line does not coincide with one of the divisions of the scale, we read the fraction of the following division on the vernier:—

The principle of the vernier is very simple. If we wish to obtain tenths, we divide into ten parts a space on the vernier comprising nine parts of the scale (see Fig. 6); each division of the vernier is thus found shorter by a tenth than each division of the scale. Now, if we start from the point where the zero of the vernier and its tenth division coincide exactly with the first and the ninth division of the scale, and if we cause the vernier to move gradually from the ninth to the tenth division of the scale, we shall see the first, the second, the third, and the other divisions of the vernier as far as the tenth, coincide successively with one of the divisions of the scale. Now, the divisions of the scale to which those of the vernier correspond, being equal parts, it follows that the space in question has been successively divided into ten parts, or tenths, by these successive coincidences. If the scale bears millimetres, the vernier will give tenths of millimetres; if it has tenths of an inch, the vernier will give hundredths. By changing the proportions, it may be made to indicate by the vernier smaller fractions, as twentieths of millimetres. or five-hundredths of an inch, &c.

To read the vernier, we must look out for the line that coincides with one of the divisions of the scale; the number of this division of the vernier, proceeding from zero, indicates the number of tenths of millimetres, or of hundredths of an inch, which must be added to the whole number given by the scale. If none of the divisions of the scale coincides exactly, we estimate by

the eye, in decimals, the quantity by which the vernier must be lowered to obtain a coincidence, and this is added to the fraction already obtained. This will be hundredths of millimetres in the metrical barometer, and thousandths of inches in the English barometers.

The following figures will serve as an example; the instrument is an English barometer.



In Fig. 6 the regulating line, which is the lower edge of the vernier ring, coincides exactly with the line of thirty inches on the scale. The zero and the tenth division of the vernier are also in exact coincidence; that is to say, there is no fraction. We shall read then 30.000 inches.

In Fig. 7 the regulating line does not fall upon any of the divisions of the scale, but between twenty-nine inches and two-tenths and twenty-nine inches and three-tenths of an inch. There is then a fraction which must be read on the vernier. Seeking which of these divisions coincides with that of the scale, we find that it is the fifth; we shall write then 29.250 inches.

In Fig. 8 we see that the height falls between thirty inches

and thirty inches and one-tenth; no line of the vernier also coincides exactly; but the line 7 is a little above, the line 8 is a little below, one of the lines of the scale; the fraction falls, then, between seven and eight hundredths. Estimating in tenths the distance the vernier passes over between the coincidence of seven and that of eight, we thus obtain the tenths of an hundredth, or the thousandths. In this latter case, the distance above seven is less than the half; we shall then read 30.073. It will always be easy to indge whether the top approaches nearer the upper coincidence than the lower coincidence; in the former case, the fraction is greater than .005; in the latter it is smaller than .005. The error which will be committed in this estimate will remain less than .005; with practice and a little skill, it will hardly ever exceed .002, always supposing the scale is well graduated. For this reading, as well as for the others, it is particularly important to have the eye exactly at the height of the line to be determined.

The same process of reading is applied to the metrical scale; the vernier then gives tenths directly, and by estimate, the hundredths of millimetres. In the English instruments, the inches must be separated by a (.) and three decimals written, even when the last is a zero; e. g. 30.250, and not 30.25; the zero indicates that the thousandths have been taken into account, but that there are none. In the metrical scale put the (.) after the millimetres, and admit two decimals, e. g. 761.25.\*

During the whole time of the observation of the barometer, the observer must endeavor to protect it as much as possible from the heat which radiates from his body. But the best way is to learn to observe rapidly. All the operations of which we have just spoken take longer to describe than to execute; one or two minutes, if the instrument be in place, three minutes if it is to be taken from its case and put back again, are sufficient for a practised observer to make a good observation

Altitude.—The height of the barometer above the ground, or above some fixed point, which may serve as an invariable point of reference, ought to be exactly determined. Such a point, for instance, may be the base of a public edifice, the level of low

<sup>\*</sup> For the method of reading the vernier of Green's standard barobeter, see the description of the instrument, page 54.

water of a neighboring river, the ordinary level of the surfacewater of a canal, the upper part of a wharf in mason-work, &c. If the barometer has changed place, it is again necessary to measure exactly its height above the same point of reference; the latter will serve to fix the height of the barometer and of the station above the level of the ocean; this datum being of the greatest importance. Every change of this nature should be carefully noted in the journal.

It is greatly to be desired that the place of the barometer, once determined, should not be changed, either from one story to another, or from one house to another. If circumstances compel this to be done, we should begin, before taking it from its place, by raising the mercury in the cistern by means of the screw, so as to fill the cistern and the tube; it must then be gently taken from the hook, turned upside down, and carried with the cistern up, taking great care not to strike it against anything. If it were transported without these precautions, even from one chamber to another, great risk would infallibly be run of breaking it, or letting in air, and thus rendering it useless.

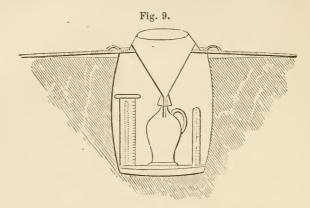
Verification.—From time to time the barometer should be so inclined as to cause the mercury to strike gently against the top of the tube. If it gives a dry and clear sound, it is free from air, and the instrument is in good condition. If the sound is flat and muffled, there is a little air in the barometric vacuum; and the fact should be noticed in the journal. Every occasion should be seized to compare it anew with a standard barometer, to ascertain whether it has undergone any change.

### OMBROMETER.

Placing.—The ombrometer, or rain-gage, is a funnel, accompanied by a graduated cylindrical glass vessel, and by a reservoir. It should be placed in an open space. Trees, high buildings, and other obstacles, if too near, may have a considerable influence in increasing or diminishing the quantity of rain which falls into the funnel. The surface of the receiver should be placed horizontally about six inches above the ground. The most simple mode of establishing it is the following:—

Place in the ground a cask or barrel (Fig. 9), water-tight, the

top rising above the ground about three inches; cover it with boards slightly inclined in the form of a roof, which project on all sides beyond the edge of the barrel at least a foot. A circular opening in the middle receives the funnel, the borders of



which rest on the board. At the bottom of the barrel, to receive the water, is an earthen or metallic vessel, with a narrow neck, (an ordinary earthen jug will answer,) in which is placed the end of the funnel, exactly filling the opening. It must contain two or three quarts. The funnel is fastened by means of two clasps to the board, which must be covered up with sod, to make it like the ground itself. If circumstances render it necessary to place the ombrometer higher, the height must be carefully noted in the journal. If it is placed upon a sloping roof, it should be on the top, and not at the edges, or at the angles, and must be raised several feet above the roof itself.

Observation.—To make the observation, remove the funnel, and pour the water from the jug into the large graduated glass cylinder. The opening of the funnel being one hundred square inches, one inch of rain in depth gives one hundred cubic inches of water; and each division of the glass containing a cubic inch of water, each of them represents a hundredth of an inch of rain fallen into the ombrometer. These degrees are large enough to permit us to estimate the thousandths of an inch. The divisions of the smaller graduated glass cylinder will measure directly the thousandths of an inch, and it may serve, in case of accident, as a substitute for the larger one. The two glass vessels may be

placed in the barrel itself, if it is of sufficient size. They must be placed in a reversed position, on two upright pegs, to let them drip out. As soon as the observation is made, it should be noted in pencil, not trusted to the memory; and written in the journal upon entering the house.

### SNOW-GAGE.

Observation.—The snow-gage should be supported vertically, in an open place, between three short wooden posts, its opening being about two feet from the ground. It should be employed in the following manner:—

When only a very small quantity of snow falls, or of snow alternating with rain, or of dry and fine snow, driven by the wind, it should be collected in the snow-gage, as would be done in the ombrometer. But when the snow falls in a sufficient quantity to cover the ground more than an inch deep, the vessel must be emptied, and plunged, mouth downwards, into the snow, until the rim reaches the bottom. A plate of tinned iron, or a small board, may then be passed between the ground and the mouth of the gage, and the whole reversed. In this way a cylinder of snow, of which the base is snperficially one hundred inches, will be cut out, and received into the vessel. The operation may be facilitated by placing on the ground a platform of strong board or plank, two or three feet square, on which the snow is received.

The place selected for this purpose must be one where the snow has not been heaped up, or swept away by the wind, and where it presents, as near as possible, the mean depth of the layer that has fallen. In order to take only the snow which may fall in the interval between two observations, the board should be swept after each measurement, and the place designated by stakes.

Reading.—In the reading of the graduated vessels, the general surface of the liquid must be considered as the true height, and not the edges, which are always raised along the walls of the vessel by capillary attraction.

The collected snow must be melted by placing the gage, covered with a board, to prevent evaporation, in a warm room;

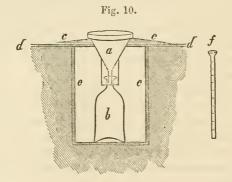
and the quantity of water produced measured by pouring it into the glass cylinder. It need hardly be said, that if rain and snow fall the same day, no account will be taken except of what the snow-gage receives, unless the ombrometer has been observed separately after the rain, and the snow-gage after the snow. Care must be taken, in these cases, not to count twice the same quantity of fallen water.

The rain-water and melted snow-water must be separately entered in the journal in the columns reserved for each.

During abundant rain-falls, it is well to measure the water more than once a day, or at least immediately after the rain; and the quantity of the rain fallen, together with the time it has lasted, is to be noted separately in the column of remarks.

When it freezes, it will be necessary to protect the receiver by filling in the interior of the barrel with straw.

[A series of observations have been made at the Smithsonian Institution with rain-gages of different sizes and different forms, the result of which, as far as the observations have been carried, is to induce a preference for the smallest gages. The one which was first distributed by the Institution and the Patent Office to the observers, is represented in Fig. 10. It consists of the



funnel  $\alpha$ , terminated above by a cylindrical brass ring, bevelled into a sharp edge at the top, turned perfectly round in a lathe, and of precisely five inches diameter. The rain which falls within this ring is conducted into a two-quart bottle, b, placed below to receive it. To prevent any water which may run down on the outside of the funnel from entering the bottle, a short

tube is soldered on the lower part of the former and encloses the neck of the latter. The funnel and bottle are placed in a box or small cask e, e, sunk to the level of the ground, which is covered with a board d, d, having a circular hole in its centre to receive and support the funnel. To prevent the rain-drops which may fall on this board from spattering into the mouth of the funnel, some pieces of old cloth or carpet, e, e, may be tacked upon it.

The object of placing the receiving ring so near the surface of the earth, is, to avoid eddies caused by the wind, which might disturb the uniformity of the fall of rain.

In the morning, or after a shower of rain, the bottle is taken up and its contents measured in the graduated tube f, and the quantity in inches and parts recorded in the register. The gage, or tube, which was first provided for this purpose, will contain, when full, only one-tenth of an inch of rain, the divisions indicating hundredths and thousandths of an inch. As this, however, is found to be too small for convenience, another gage, which will contain an inch of rain, and indicating tenths and hundredths, will be sent to observers.

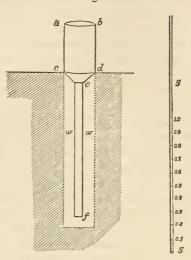
Another and simpler form of the gage has since been adopted by the Institution and the Patent Office, to send by mail to distant observers. It is one of those which have been experimented on at the Institution, and is a modification of a gage which was received from Scotland, and which has been recommended by Mr. Robert Russell.

It consists of-

- 1. A large brass cylinder a, b, c, d, two inches in diameter, to catch the rain.
- 2. A smaller brass cylinder e, f, for receiving the water and reducing the diameter of the column, to allow of greater accuracy in measuring the height.
- 3. A whalebone scale s, s, divided by experiment, so as to indicate tenths and hundredths of an inch of rain.
- 4. A wooden cylinder w, w, to be inserted permanently in the ground for the protection and ready adjustment of the instrument.

To facilitate the transportation, the larger cylinder is attached to the smaller by a screw-joint at e.

Fig. 11.



Directions for use.—To put up this rain-gage for use: 1. Let the wooden cylinder be sunk into the ground in a level unsheltered place until its upper end is even with the surface of the earth. 2. Screw the larger brass cylinder on the top of the brass tube and place the latter into the hole in the axis of the wooden cylinder, as shown in the figure, and the arrangement is completed.

The depth of rain is measured by inserting the scale into the gage and noting the height to which it has been wetted by the water when it is withdrawn. In order, however, that the water may wet the scale, the superficial grease should be removed by rubbing it with a moist cloth, previous to use. In case the water cannot be made to adhere to the scale, a slip of pine or other wood may be made of the same size of the scale, and this inserted in its stead. The quantity of water may then be measured by applying the slip of wood to the scale.

Should the fall of rain be more than sufficient to fill the smaller tube, then the excess must be poured out into another vessel, and the whole measured in the small tube in portions.

Care should be taken to place the rain-gage in a level field or open space, sufficiently removed from all objects which would prevent the free access of rain, even when it is falling at the most oblique angle during a strong wind. A considerable space also around the month of the funnel should be kept free from plants, as weeds or long grass, and the ground so level as to prevent the formation of eddies or variations in the velocity of the wind.

To ascertain the amount of water produced from snow, a column of the depth of the fall of snow, and of the same diameter as the mouth of the funnel, should be melted and measured as so much rain.

The simplest method of obtaining a column of snow for this purpose is to procure a tin tube, about two feet long, having one end closed, and precisely of the diameter of the mouth of the gage.

With the open end downward, press this tube perpendicularly into the snow until it reaches the ground or the top of the ice, or last preceding snow; then take a plate of tin, sufficiently large, to cover it, pass it between the mouth of the tube and the ground, and invert the tube. The snow contained in the tube, when melted, may be measured as so much rain. When the snow is adhesive, the use of the tin plate will not be necessary.

From measurements of this kind, repeated in several places when the depth of the snow is unequal, an average quantity may be obtained.

As a general average, it will be found that about ten inches of snow will make one of water.]

Mr. Guest, of Ogdensburgh, N. Y., recommends, from an experience of six years, the following as the best plan for ascertaining the amount of melted snow. Procure a cylindrical tin tube of the exact diameter of the mouth of the rain-gage and two or three feet long, so that the snow cannot be blown out. Place this vertically in a properly exposed position, and firmly secure it against the action of the wind, which would otherwise blow it over in a violent storm. After the snow has ceased to fall, bring the vessel with its contents into the house, near a fire, which will gradually melt the snow, and afterwards measure the water produced by means of the rain-gage.

### WIND-VANE.

Placing.—The wind-vane should be set in a place as free and open as possible, away from every obstacle, and especially from high buildings. It should exceed in elevation, by at least eight or ten feet, the neighboring objects. To facilitate observations at night, the following arrangement may be adopted:—

The wind-vanc is composed of a leaf of zinc about three feet in length, in the form of a butterfly's wing, exactly counterbalanced by a leaden ball. It is carried upon a cylindrical axis of pine wood, or of any other light and strong material, two inches in diameter, which, if possible, passes down through the roof into the observer's chamber, otherwise along the exterior wall of the building to a window. The axis terminates by a steel pivot turning freely on a cast-iron plate. This plate supports a dial divided into degrees, besides indicating the eight principal points of the compass. The axis carries an index placed in the same plane as the feather of the wind-vane, which enables us to read upon the dial, as well by night as by day, the direction of the wind. The whole rests on a strong wooden shelf, firmly fastened to the window by supports. Above, the rod is firmly fixed to a strong upright staff, or, better, on the roof, with strong braces, by means of a piece of wood containing friction rollers, which allow the shaft to turn freely and without effort. Similar pieces with friction rollers, placed at different distances along the wall, keep the axis vertical.

Great care must be taken to secure the perfect verticality of the shaft, and to this end it is necessary to fix it by a plumb-line in two different planes cutting each other at right angles. The index at the foot of the rod should be placed on the same side with the point of the wind-vane, and in the same plane as the feather. The pivot should turn very freely in the hole that receives it, and into which a drop of oil should be poured.

Finally, we must carefully adjust the points of the dial, which is supported with the iron plate, upon a board fastened upon a shelf by means of a strong screw. In making this adjustment by means of a compass, the magnetic variation of the locality must be taken into account; each observer should have the line of the true north traced on his window.

If the dial is exposed to the open air, it must be protected against the snow and ice, which would impede the play of the pivot and of the index. A small ring of wood placed around the pole, under one of the friction rollers, will prevent the windvane from being raised, and the pivot from being displaced during the most viclent winds.

[As a flat vane is always in a neutral line, a more accurate and sensitive one is made by fastening two plates together at an angle of about ten degrees, forming a long wedge. Thus,

The longer the vane, the shorter the pulsations, and the steadier the action will be. For a small sized vane, it may be ten or twelve inches wide, and four feet long.]

Observation.—The observation of this instrument demands some care. In winds of considerable strength the vane is never at rest, or fixed in the same direction; it oscillates incessantly, and its oscillations increase in amplitude with certain winds, and with the violence of the wind. We must then note the mean direction between the extremes. When the wind is very feeble. perhaps it may not have sufficient force to set the vane in motion; in this case, as when the air is calm, great mistakes might be made by registering the direction marked by the index; for its position indicates, not the direction of the existing wind, but that of the last wind that had the power to set the instrument in motion. When the index is immovable, and there is no oscillation, we must give up its indications, and refer to the movement of light bodies, as that of the leaves of trees and the smoke of chimneys, to determine the direction of these feeble currents of During the night the direction of the wind may be easily ascertained by raising the hand in the air, with one finger wet. The least motion in the air increases evaporation, and a sensation of cold is experienced on the side of the finger turned towards the wind.

The direction of the wind must be noted, following the eight principal points of the compass—north, northeast, east, southeast, south, southwest, west, and northwest. For the additional observations during storms, the degrees may be indicated, in order to follow more exactly the rotation of the wind, or at least

sixteen points of the compass, viz: N. NNE. NE. ENE. E. ESE. SE. SSE. S. SSW SW. WSW. W. WNW. NW. NNW.

The lower, or surface wind, often has a different direction from that which prevails in the upper regions of the atmosphere, and this is generally the case when the wind turns, and the weather is going to change, also during storms and great atmospheric movements. The direction, then, of the lower and the higher layers of clouds must be separately noted in the several columns of the journal reserved for this purpose. If the direction is the same in the whole extent of the atmosphere, the same letters will be marked in the three columns. If the absence of clouds does not permit us to judge how the wind is above, a dash must be substituted for the letter, indicating that the observation has been made. A blank always signifies an observation omitted.

To avoid an error in the estimate of the direction of the clouds, it will be well to observe their course between two fixed points, as a window frame, the fixed lines of which will facilitate the observation. Another very convenient method is to place a small mirror horizontally, with lines traced on it indicating the points of the compass; the image of the clouds passing over these will indicate their direction.

The manner in which the wind turns, or rather the order in which the winds succeed each other in the course of the day, must be watched very carefully. It will be seen that they commonly follow in regular order; they pass from the east by the south to the west, and from the west, by the north, to the east. Nevertheless, they sometimes go back in the opposite direction, particularly during storms. A little memorandum, summing up in a few words at the end of each day this course of the wind, together with the hours of the wind's changes, is very valuable. It may be entered in the column of remarks.

The force of the wind must be estimated as nearly as possible according to the following degrees:—

0. A perfect calm.

The simple initial letter of the wind, for instance N. (north), indicating its direction without any number, means a slight movement of the air hardly to be called a wind, and only just sufficient to allow an estimate of its direction.

- 1. A light breeze which moves the foliage, and sometimes fans the face.
- 2. A wind which moves the branches of the trees, somewhat retards walking, and causes more or less of a slight rustling sound in the open air.
- 3. A wind which causes strong boughs and entire trees to rock, makes walking against it difficult; which causes a stronger rustling sound to be heard, and which often blows in gusts, and carries light bodies up into the air.
- 4. A storm-wind, during which the trees are in constant motion; branches and boughs covered with foliage are broken off, and in a violent sterm sometimes even entire trees are broken, or uprooted; leaves, dust, &c., are continually borne up and carried far away; during which time there is an uninterrupted loud rustling sound, with strong gusts; walking windward is extremely difficult, and now and then chimneys, fences, &c., are thrown down, windows broken in, &c.

These degrees correspond nearly to the following numbers of Beaufort's scale, which is generally used among seamen:—

1. the same as 1. Light breeze,
2. " " 4. Moderate breeze,
3. " " 8. A fresh gale,
scale.

4. " " 11. A storm-wind,

[The force of the wind is now estimated and registered according to the direction on the blank forms.]

### SKY.

The blue color of the sky has an intimate connection with the hygrometrical state and the electrical tension of the air; it may be noted by the expressions, dark, light, and grayish.

Haze and dry mist.—The transparency of the air is often disturbed by a kind of vapor, which gives a whitish tint to the sky and dims the rays of the sun. This phenomenon, known in Europe under different names, appears frequently after long droughts; in this country it seems to characterize the Indian summer. In Europe, and elsewhere, an intensely dry mist, which is, probably, a different phenomenon, sometimes follows great earthquakes or volcanic eruptions. The observer will carefully

enter phenomena of this kind, and the circumstances under which they appear or disappear. If he has an opportunity, as in a high station, he should endeavor to ascertain if there is an upper limit, and what is the thickness of the layer of haze or dry mist. Observations made in the Alps prove that the atmosphere is often entirely free from it at a height of two thousand feet, when it is very intense in the plain. Does a thunder-storm or rain always cause it to disappear? Do the prairie fires have any relation with kindred phenomena? Does it appear more frequently in certain seasons than in others?

## HYDRO-METEOROLOGICAL PHENOMENA.

## DEW.

The dews, especially when they are abundant, and
The white frosts, or frozen dew, particularly the first and last
of the year, and their intensity, must be entered.

## FOG.

Fog.—The moment must be noted when it forms and when it dissipates, as falling fog, rising fog; its density, as dense fog, slight fog.

Mists hanging over forests, moors, meadows, rivers, or the like.

Notice must be carefully taken of the time of their appearance or disappearance; these are the most important facts in regard to them.

These fogs must not be confounded with the dry fog, which belongs to another class of phenomena, which have been spoken of above.

### CLOUDS.

For noting these the observer must go out to a place entirely free, in case his residence has too confined a horizon.

The cloudiness or the quantity of clouds, after some practice,

CLOUDS. 29

can be easily estimated, in accordance with the following scale. Thus, we understand by—

- 0. A clear sky, entirely free from clouds;
- 10. The whole sky covered with clouds, or a dense fog, or rain; and by 1, 2, 3, 4, 5, 6, 7, 8, 9, the different degrees of cloudiness which lie between these:
- 1. Denotes, for instance, nine times as much blue sky as clouds;
- 5. An equal amount of clouds and blue sky;
- 9. Nine times more clouds than blue sky.

If, on account of the locality, it is impossible for the observer to estimate the quantity of clouds in this way, he can make use of the following expressions, which will mark at the same time the medium character of the aspect of the sky during each day:

Wel. Wholly clear; a sky entirely free from clouds.

- Cl. Clear; when at least two-thirds of the sky is unclouded.
- M. Medium; the clouded part of the sky nearly equal to the blue.
  - C. Cloudy; a larger part cloudy than clear.
  - Ov. Overcast; the clouds rarely broken.
  - Cov. Covered sky; without any visible spot of blue.

The form of the clouds will be indicated by the terminology of Howard.

According to this, they are distinguished by their external forms into three kinds: the *cirrus*, *cumulus*, and the *stratus*, to which belong four transition forms, the *cirro-cumulus*, the *cirro-stratus*, the *cumulo-stratus*, and the *nimbus*. The most remarkable of these forms may be characterized in the following manner:—

The *cirrus*, or cat-tail of the sailors, is composed of loose filaments, the whole of which sometimes resembles a pencil, sometimes curly hair, sometimes a fine net, or a spider's web.

The cumulus, or summer cloud, the cotton-bale of the sailors, often shows itself under the form of a hemisphere resting on a horizontal base. Sometimes these half spheres are piled upon one another, forming those large accumulated clouds in the horizon which resemble, at a distance, mountains covered with snow.

The *stratus* is a horizontal band, which is formed at sunset and disappears at sunrise.

The cirro-cumulus are those small rounded clouds, which are

often called fleecy; when the sky is covered with clouds of that kind it is said to be mottled.

The cirro-stratus is composed of small bands, formed of closer filaments than those of the cirrus, for the rays of the sun often find it difficult to penetrate them. These clouds form horizontal beds, which, at the zenith, seem composed of a great number of loose clouds, while at the horizon a long and very narrow band is seen.

The *cumulo-stratus* is a mass of heaped up and dense cumuli. At the horizon they often assume a dark or bluish tint, and pass into the condition of *nimbi*, or rain clouds.

The *nimbus* is distinguished by its uniform gray tint, its fringe and indistinct edges; the clouds composing it are so blended that it is impossible to distinguish them.

But besides these principal forms, there are several intermediate, to which it is difficult to assign a name. They must be referred to the form which they most resemble.

They may be entered in the journal by means of the following abbreviations:—

St.	i. e.	Stratus.
Cu.	66	Cumulus.
Cir.	"	Cirrus.
Cir. st.	4.6	Cirro-stratus.
Cu. st.	"	Cumulo-stratus.
Cir. cu.	66	Cirro-cumulus.
Nim.	"	Nimbus.

If several of these forms are visible, the most frequent should be underlined, and the others should follow the order of their frequency. The distribution of the clouds in the sky should be noted, whether they are dispersed or accumulated in a special region of the heavens, in the horizon, at the zenith, &c

### RAIN.

It is necessary to note as accurately as possible the hour at which the rain begins and ends; if it is a continued rain, or at intervals and in showers; if it is general or only partial, preceded, followed, or accompanied by fogs; the size of the drops and the force of the rain should be also noted. For these different cases, the following designations may be adopted:—

Rainy, when the fall of some drops and the appearance of the weather is such as to indicate the approach of rain.

Continued rain.

Interrupted rain.

Shower, which lasts not more than a quarter of an hour.

General rain, which prevails over the whole extent of the horizon.

Partial rain, which falls from the clouds that pass over only a small extent of country.

The force of the rain may be indicated by the following gradations:—

Drizzling rain, which falls in very small drops, almost like those of mist.

Slight or fine rain.

Moderate rain,

Heavy rain.

Violent rain, heavy and strong pelting rain.

The size of the drops seems to depend chiefly upon the height of the clouds, and consequently upon the seasons and the circumstances of the temperature.

The snow.—The period of the first and last snow, the size of the flakes, their forms.

Sleet, which consists in small balls of snow, white and opaque, commonly without a crust of ice, like the opaque nucleus found within hail-stones, falling more frequently in spring and in autumn.

Frozen rain drops should be distinguished from the preceding forms; they make little balls of transparent ice.

Hail.—Indicate the size, form and average weight of the hail-stones. The number of different strata observed in the larger stones. Whether any of them contain particles of sand or any other foreign matter. The extent and course of the phenomenon.

#### THUNDER-STORMS.

The time of beginning and ending of the storm must be indicated as exactly as possible; the point of the horizon whence it rises, the direction of the clouds, of the wind and its variations, and, if possible, the quantity of rain before and during the storm;

of hail, &c., which falls; note if it passes over the place of the observation, or at a distance; if it is accompanied, or not, with strong electrical detonations and numerous lightnings. It will be well to ascertain the state of the meteorological instruments every five minutes during the storm, especially of the barometer and the thermometer.

[At the Institution the barometer generally sinks during the coming on of a storm, and rises suddenly at the first fall of rain.]

In the journal, the occurrence of a storm will be indicated on the opposite page of the blank, with the hour when it took place. If special observations have been made with the instruments, they will also be entered on the opposite side of the sheet, taking care to note the day and the hour. If the observations require a more detailed description, it may be made on a separate sheet.

## TORNADOES AND LAND-SPOUTS.

These whirlwinds, or violent and circumscribed storms, give rise to very complex phenomena, which are difficult to observe. All the meteorological circumstances, however, should be minutely noted; among others the following:—

The course of the barometer, which almost always sinks much and rapidly; that of the thermometer, which usually indicates an elevation of temperature; the region of the heavens in which the thunder-storm frequently accompanying them is formed; the form and color of the clouds; the direction and intensity of the wind; the frequency, the size, and the form of the lightnings; finally, the apparent shape of the land-spout, its variations, its course, and its effects upon the trees and upon the ground.\*

## ADDITIONAL OBSERVATIONS DURING STORMS.

Everybody knows the importance of a knowledge of the laws of those great movements of the atmosphere which embrace almost the whole extent of the continent. It is only in following them, step by step; by observing their different phases at different

<sup>\*</sup> For more detailed instructions upon the observations of land-spouts, see the Annuaire Météorol. de France, 1849, p. 225.

places, and by combining the facts obtained, that the meteorologist can be enabled to discover the laws which preside over these great phenomena. For this, the three regular observations a day are insufficient; it is then earnestly recommended to observers, who desire to contribute effectually to the solution of this great problem, not to content themselves with the prescribed number, but to add as many more as possible during the continuance of remarkable storms; noting not only the state of the instruments from hour to hour, if possible, but following with attention all the meteorological changes. These observations must be entered on the reverse of the sheet, under the head of Casual Phenomena, which is particularly reserved for this purpose.

The principal points to which attention should be directed are the following:—

The barometer announces by a considerable fall the approach of a storm. Then it begins to rise during its continuance, and only resumes its nominal equilibrium after its close. Remark especially the following points:—

Was the storm preceded by a noticeable or sudden rise previous to the fall;

Note the state of the barometer, and the time when the fall becomes more rapid;

Its state, and the time, when it is lowest and when the rise begins;

The highest point which it reaches during, or immediately after the storm.

If alternations of rising and falling take place, the fact should be mentioned and the time noted.

The thermometer.—The fluctuations of the thermometer in the same time as those of the barometer should also be noted, and their connection with the changes of the wind be observed.

The wind.—It is of the greatest importance to observe the course of the winds through the entire height of the atmosphere during the whole continuance of the storm, by means of the windvane and of the clouds in the different layers of the atmosphere.

The hour when the wind begins, and the direction whence it comes;

The moment of its greatest violence;

The instant it changes its direction, and when it takes the direction it keeps to the end of the storm.

It should be stated if the wind blows in a continuous manner or in squalls, and what is its force.

If there should be one or more moments of calm, the hour and duration will be indicated.

Great care must be taken at each observation to note also the direction of the different layers of clouds, which will very often be found different from that of the wind below, for the whole duration of the storm.

The clouds.—Are there certain forms of clouds which announce the approach of a storm? It is necessary, in this connection, to watch the formation of the cirrus, the cirro-cumulus, cirro-stratus, their arrangement in parallel lines, their course, and their directions. Note the quarter of the sky first covered with clouds; the moment when it is entirely covered; if there are later clear spots or not; the moment when the sky clears off.

The rain.—Note the hour at which the rain or the snow begins and ends; measure the quantity fallen while the storm lasts.

#### ACCIDENTAL METEORIC PHENOMENA.

These will be entered in the tables, in the place reserved for this purpose on the opposite side of the sheet. If the space is not sufficient for the description to be given, the phenomenon should be simply noted, and reference made to a separate account for details. Thus:—

The solar and lunar haloes—that is, the colored circles sometimes observed round the sun and moon. Distinguish the small ones, the ring of which measures only a few degrees, from the large or real haloes, the ring of which has a diameter of about forty-four degrees. It must be stated whether they are connected with other circles, as is sometimes the case. Care must be taken not to mistake a part of a grand halo for a rainbow. Note whether these appearances are, or are not, ordinarily followed by rain.

The Parhelia and Paraselenes (mock-suns and moons).—Describe exactly their forms and the state of the heavens at the moment of their appearance.

Rainbows, simple or double.

An extraordinary redness of the sky, either in the morning or

evening; the particular color of the sun and of the moon at their rising, especially in fair days.

Heat lightnings without thunder, and sometimes without clouds; indicate their direction and the aspect of the clouds in their neighborhood.

The Aurora Borealis, or northern light, for the observation of which the special instructions, page 48, must be followed.

Shooting-stars.—The observer must be particularly attentive to their frequency, during the periods near the 10th and 11th of August, and the 10th and 15th November, in which it is supposed that they are more numerous than at any other time. He will designate the quarter of the heavens from which they seem to issue, and their direction.

Fireballs.—Describe their aspect, their size, their course in the heavens, and note the exact hour of their appearance.

All the other luminous phenomena, which present any extraordinary appearance, should be noted down.

These descriptions should be made in simple and well-defined terms. The observer will take great care to enter scrupulously what he sees without drawing any conclusion, or attempting any explanation of the phenomenon. He ought to reflect that, in order to make a good observation, he must keep his mind in a state of perfect freedom in respect of any preconceived theory, and to consider the phenomenon before him as being one of the data for the foundation of the science, and that the knowledge of the truth will depend upon the fidelity of his observation.

### TIME OF OBSERVATIONS.

The time of observations will be the mean time at each station The observations will be made three times daily, viz:—

The mean of these three hours will be very nearly the true mean, as it would be obtained by observation made every hour of the day and night.

The rain gage will be observed only once a day, unless very abundant rains should make a second measurement necessary.

The best time will be 2 o'clock p. m., the observation being made daily; if another hour is selected, it should, when once fixed, remain the same.

The maxima and minima thermometers will be read once a day, always at the same hour. The most suitable hour will be 9 o'clock in the evening.

If an observer desires to examine the daily oscillations of the barometer, he will also observe at 10 a. m. and 4 p. m., which give the daily maximum and minimum. It will be well to note also, at the same time, the state of the hygrometer.

If he desires to complete the data upon the diurnal course of the temperature, he will add observations of the thermometer at 10 a.m. and 6 p.m. In all cases it is desirable that, if an observer has leisure to increase the number of the hours of observations, he should fix them at equal intervals between the principal hours indicated above.

Besides these observations at regular hours, additional observations ought to be made during remarkable storms, as has been remarked above.

It is very important that the observations should be made at the exact hour, fixed by a well regulated watch. All the instruments should be read rapidly, so that the observations may be as simultaneous as possible.

The order in which they are to be observed will be as follows:-

A few minutes before the hour, observe the thermometer before opening the window; then wet the psychrometer. While it is taking the temperature of evaporation, note the height of the barometer, observe the wind, the course of the clouds, their quantity, the aspect of the sky, &c.; then read the temperature of the psychrometer.

The observations must be recorded for each instrument at the moment when they are made, without trusting anything to the memory. A strict rule should be laid down for one's self, to note exactly the indications of the instruments, without subjecting them mentally to any corrections or any reductions; these should not be applied until all the elements are at hand.

If the observer has been unavoidably hindered from making the observations at the exact hour, he will note in the column of hours the number of minutes of the delay. If he is obliged to procure a substitute, he must choose one accustomed to this kind of observation; but before entering his records, he will carefully examine them. To distinguish the observations made by his substitute, he will enter them in red ink.

As it is of the greatest importance that the series of observations should not be interrupted, and that there should be no omissions, each observer will do well to instruct beforehand one or more substitutes, who may be able upon occasion to take his place. If, in spite of these precautions, the observation has necessarily been omitted, its place will be left blank in the journal. In this case the observer must never fill up these blanks with calculations, according to his judgment; he should consider the conscientious observance of this rule indispensable to truth and good faith. He should remember, besides, that if he acts differently, he not only lessens the value of these results, but brings into doubt and disfavor the fidelity of his other observations, and takes from them what constitutes their greatest value for science—confidence.

#### THE REGISTER.

In the register the first page is devoted to regular observations; the second to additional observations, to periodical or extraordinary phenomena, and to monthly recapitulations. The headings of the columns indicate clearly the use of each.

For each instrument the columns follow each other in the order in which the observations are to be made, and one column is reserved to enter the observation just as it is made, and before any correction or reduction. As each sheet is to be regarded as an independent document, it should carry with it all that is necessary to correct the observations therein contained, and to render them authentic. Thus, the date of the year, the month, the precise locality, the latitude and longitude, the elevation of the instruments from the ground and above the sea, the nature and condition of the instruments which have been employed, and the amount of their corrections; finally, the signature of the observer should be repeated on every leaf. It will be sufficient, for this, to fill the blank spaces left after the different printed titles in the blank forms. The observer should the less neglect this important duty, as it is an affair of only a few strokes of the pen each

month, without which his labor would run the hazard of losing its value.

Barometer.—The degree of the attached thermometer and the observed height of the barometer will be inscribed in the first two columns. This height will be reduced to freezing-point, or 32° Fahrenheit, or zero Centigrade, by means of tables, and the whole correction of the instrument will be applied to it. It will then be inscribed in the third column, entitled corrected height at freezing-point. These corrected heights, and never any others, must be employed to form the mean, which will be inscribed in the fourth column.

Thermometer.—In the thermometrical observations the quantities above zero will be always written without a sign; the negative quantities will be all individually marked with the sign minus (—), whether they follow each other or are isolated. In the first column, entitled daily mean, will be inscribed the mean of the three observations of the day, i. e. their sum divided by 3, admitting two decimals.

Psychrometer.—In the first two columns will be entered the indications of the dry and wet thermometer, after having applied to each of them the correction of the instruments, if there be any. By means of the psychrometrical tables will be found the force of the vapor and the degree of relative moisture, each of which has its column.

We have indicated above the manner of noting the direction of the winds.

As to the force of the surface wind, which alone can be estimated with some degree of precision, it will be expressed by adding to the letter which designates the direction, the figure indicating its force: e. g., N, without a figure, signifies a slight air, hardly perceptible, coming from the north;  $N_1$ , a slight breeze;  $N_3$ , a strong wind, &c. The other two columns will have only letters, or a dash (—) if the observation has not been possible.

The quantity of clouds, or the *cloudiness* estimated from zero, or a perfectly clear sky, to 10, sky entirely overcast, has a separate column.

It is the same with rain and melted snow, which will be separately entered. A third column is reserved for the total quantity

of both. The thickness of the layer of fallen snow may be indicated in inches and tenths.

As to the broad column for Casual Phenomena, although it is desirable, considering the small space the form of the table allows, to employ abbreviations to express the state of the sky and the different meteorological phenomena; nevertheless, we must limit ourselves to a small number, chosen from among the expressions which most frequently occur, such as those found at the bottom of the blank forms. If abbreviations are too much multiplied, we lose in clearness and certainty what we gain in conciseness. A meteorological journal should not resemble a page of algebra, where a badly formed letter or a misplaced sign renders the expression unintelligible.

For the additional observations the same rule should be followed.

In the space mentioned above, periodical and extraordinary phenomena will be inscribed, with their dates and the hour of their appearance.

Every change of position, or in the condition of the instruments, should be carefully entered, with the precise date at which it took place. If there has been none, instruments all in order will be entered. By the side of the indication of the correction of the instruments will be placed, correction applied or correction not applied, according as the observations contained in the sheet shall have been corrected or not. The finished sheet will be signed by the observer.

The reductions, the corrections, and the calculations of means, must be made day by day and at the end of each month with the greatest punctuality. The necessary tables will be placed at hand by the side of the journal, and each observation reduced, and the correction, if any, applied immediately.

This is not only the least troublesome method, but the only one which permits the observer to control the observations and the reductions, and to discover the accidental errors of the pen and of the reading in the record.

The observer cannot be too thoroughly convinced that a meteorological journal which contains only rough observations, is only half made; in this condition it is wholly unfit to serve any scientific purpose. The observations cannot be compared rigorously with each other, nor with those of other stations. The

only means for the observer to give its true value to his labor, is to make the corrections, the reductions, and the calculations of the means himself. It is for want of having thus been elaborated that voluminous collections of observations, the fruits of long years of toil, remain useless and forgotten in the dust of libraries, because the meteorologist finds it impossible to make use of them without first undertaking those calculations, the amount of which absolutely transcends the powers of an individual, and would discourage the most ardent zeal, while they would have cost the observer only an instant each day, if he had made them at the time of the observations.

The calculations desirable are as follows:-

- 1. Each barometrical observation must be reduced immediately to the temperature of zero Centigrade, or 32° Fahrenheit, by means of the tables, and the total correction of the barometer, if there is any, will be applied.
- 2. The diurnal means of the several instruments, resulting from the sum of the three observations made at these different hours, divided by three, must be entered each day in the respective columns, after the observation of 9 p. m. It is needless to say that these means should be drawn solely from observations reduced and corrected.
- 3. The monthly means for each hour separately—that is, the monthly mean of the observations of 7 a.m., and that of 2 p.m., and of the observations of 9 p.m.
- 4. The monthly means drawn from the means of each day; the monthly extremes of the instruments; the monthly amount of the rain, hail, or snow; the mean cloudiness of the sky; the prevailing wind, &c.
- 5. The annual means and amounts, and the respective extremes for the eivil year.

It will be interesting to calculate, also, if the observer is so disposed, the mean of the seasons of the meteorological year, which begins December 1, to November 30, of the following civil year.

The meteorological seasons are, then:-

Winter—December, January, February.

Spring-March, April, May.

Summer-June, July, August.

Autumn-September, October, November.

In calculating all these different results, we should take, in order to be very exact, the means of the sums of all the observations during the period of time in question, by reason of the inequality of the length of the months.

The sums which form the basis of all these means should be inscribed in the tables in the place reserved for them.

The preceding calculations, after a little practice, will not appear difficult, and may be quickly performed; but it can hardly be too often urged upon the observer to make them without delay; otherwise, this task, which is slight if accomplished daily, would become very heavy, if left to accumulate for several months. It is only by making the correction himself that the observer can institute his own comparisons, and really study the course of the meteorological phenomena. His interest will increase still more with the feeling that he is coöperating in a great work, which concerns at once his whole country and the science of the world, and the success of which depends upon the accuracy, fidelity, and devotion of all who take part in it.

A copy of the observations of each month must be forwarded during the first week of the following month. It should be carefully collated by two persons, one of whom reads the figures aloud. Each observer will receive for this purpose a double series of blank forms, one of which will be retained by him.

Many of the phenomena connected with the state of the atmosphere are of great interest for comparative climatology, especially in a practical point of view. The periodical phenomena of vegetation and of the animal kingdom, such as the epoch of the appearance and the fall of the leaves, of the flowering and ripening of the more generally cultivated fruits; the seed time and harvest of plants; the coming and going of migratory birds; the first cry of the frogs, the appearance of the first insects, &c.; the moment of the closing of rivers, lakes, and canals by ice, and of their opening; the temperature of springs at different periods of the year; the temperature in the sun compared to that observed in the shade; that of the surface, and that below the surface of the ground. All observations of this kind are valuable.

The observer will find it very instructive to project curves which indicate the diurnal, monthly, or annual variations of tem-

peratures, of atmospheric pressure, of moisture, &c., as well as thermometrical, barometrical compasses, or circles, &c.

These graphic representations are of the greatest utility for the comparisons, speaking to the eye more clearly than simple figures.

Besides the above directions for keeping an ordinary Meteorological Journal, more special instructions for the study of peculiar meteorological phenomena are prepared by the Smithsonian Institution; as on

Thunder-storms, Tornadoes, and Water-spouts, Aurora Borealis, Parhelia, Parasalenes, Haloes, Rainbows, Temperature of the soil, Periodical phenomena of the vegetable and animal kingdoms, Graphic representations of meteorological phenomena, &c. If any observer should feel inclined to devote himself to the study of any one of these physical problems, he may receive, on application, the special instructions relating to the point which he wishes to investigate. [These instructions now form a part of this pamphlet.]

[The directions given in the preceding article are not intended to supersede those printed on the sheet of blank forms issued jointly by the Smithsonian Institution and the Patent Office, but to impart additional instruction, particularly to those who are furnished with a full set of instruments and desire to attain as much precision as possible.]

# SPECIAL DIRECTIONS

TO THE

## METEOROLOGICAL OBSERVERS

OF THE

## SMITHSONIAN INSTITUTION.

In the reduction of the meteorological records presented to this Institution, much additional labor has resulted from the occasional omission in the registers, of some important facts, and in a want of perfect uniformity in noting the phenomena. We beg, therefore, to call attention to the following remarks:—

- 1. Failure to record latitude and longitude, name and station of the observer, and date on each sheet; the observer probably supposing it sufficient to insert them once on the first sheet sent, and so omitting them afterwards. This often renders it necessary to search back through all the series of registers to some one that contained them—perhaps in a former year. They should be inserted on every sheet.
- 2. Designating the same place by different names, thus rendering it impossible to distinguish whether it were one place or two, unless by accidentally noticing the similarity in the name of the observer or in the latitude and longitude. Such changes of name should be avoided when practicable, and when necessarily made special attention should be called to it.
  - 3. Diversity in the mode of recording the Barometer, as follows:
    - (a) Integers recorded in full, thus 29.35. (This is the proper mode.)
    - (b) Integers omitted when the same as in the entry next above, thus 38.
    - (c) Integers omitted when the same as in the entry next to the left.

- (d) Integers omitted when the same as in the entry next preceding in the order of time.
- (e) Integers omitted except where they are different from the usual ones at the place of observation.
- (f) Integers inserted occasionally and apparently without any system whatever.
- (g) A constant suppressed, and the excess or deficiency recorded, as + or -.

The proper mode is that indicated by (a).

- 4. Diversity in the mode of recording the Thermometer, when it is below zero, as follows:—
  - (a) Indicated by the sign minus placed before it, thus —16°. (This is the proper mode.)
  - (b) Indicated by the same sign placed after it, thus 160-.
  - (c) Indicated by writing it under a zero—thus  $\frac{0}{16^{\circ}}$ .
  - (d) Indicated by writing it after a zero, with a comma between, thus 0,16°.
  - (e) Indicated by the word 'below,' or the abbreviation b written before or after it—thus 16° below, 16° b, b 16°, or below 16°.

The first (a) is the proper mode.

- 5. Departure from the printed instructions in recording the degree of cloudiness, some observers reversing the figures and using 10 to denote a clear sky and 0, one entirely overcast; and others omitting the record altogether in the columns of cloudiness when the sky is clear, and in place of it sometimes inserting the word "clear" in the columns of "Remarks," or elsewhere. Both lead to error, and should be avoided—the zero should always be inserted "in the narrow column," as directed, when the sky is clear.
- 6. Diversity in the use of the character zero (0) in recording the motion of the clouds, as follows:—
  - (a) Used to signify a calm, or that there is no perceptible motion. (This is the correct use.)
  - (b) Used to signify that the sky is clear, instead of inserting it in the proper column.
  - (c) Used to signify that no observation was taken.

(d) Used to signify that the direction in which the upper current was moving could not be determined on account of the sky being either perfectly clear or entirely overcast.

The first (a) is the correct use.

- 7. Want of full and proper records of the direction of the wind, some observers recording the direction only after each change, and then omitting it so long as it continues the same, merely inserting a figure to denote the force. It is better to make the record in full. Other observers record the direction towards which the wind or clouds are moving instead of indicating that from which they come. A wind from the North, or clouds moving from the North, are to be denoted by N, and from the Sonth by S, &c.
- 8. Different kinds of thermometers or different exposures used for the dry and wet-bulb thermometers, so that the observations are not comparable readily, if at all.
  - 9. Diversity in the use of the dash and the sign (") as follows:—
    - (a) To signify that the entry next above is to be repeated.
    - (b) To signify that the entry next to the left is to be repeated.
    - (c) To signify that the entry next preceding in the order of time is to be repeated.
- (d) To signify nothing at all, but merely to fill a blank. The use of these characters has caused much trouble in the reduction, and the true remedy would be to avoid them altogether, by making each record complete in itself.
- 10. Illegibility of the records, either from defective chirography or from being entered in pencil marks and partially erased.

# CIRCULAR RELATIVE

TO

## EARTHQUAKES.

The Smithsonian Institution is desirous of collecting information in reference to all phenomena having a bearing on the physical geography of this continent; and, in behalf of the Board of Regents, it is respectfully requested that you will furnish us with any information which you may possess, or be able to obtain, in regard to the earthquake which lately occurred in your neighborhood.

It will be interesting to determine the geographical limits of the disturbance, and to ascertain whether it was confined to any particular geological formation. If the direction of the shock was observed at a few places, the centre of commotion could be determined; and if the time were accurately known at different points, the velocity of the earth-wave could be calculated. Hence, an answer is requested to the following questions, viz:—

- 1. Was the agitation felt by yourself, or by any other person in your vicinity?
  - 2. What was the approximate time of the occurrence?
  - 3. What was the number, and duration, of the shocks?
  - 4. What was the direction of the motion?

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- 5. What was the character of the disturbance? was it vertical, horizontal, or oblique? was it an actual oscillation? an upheaval and depression, or a mere tremor?
- 6. Was there any noise heard? and if so, what was its character?
- 7. Was the place of observation on soft ground, or on a hard foundation near the underlaying rocks of the district?

- 8. Were any facts observed having apparently an immediate or remote bearing on this phenomenon?
- 9. What was the intensity of the force in reference to producing motion in bodies and cracks in walls?

Note.—Please reply to the *first* question, if to no other—for an answer to it is necessary, in order to determine the limits of the commotion.

The direction of the impulse may have been ascertained by observing the direction in which molasses, or any viscid liquid, was thrown up against the side of a bowl. The remains of the liquid on the side of a vessel would indicate the direction some time after the shock occurred.

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# INSTRUCTIONS FOR OBSERVATIONS

OF THE

## AURORA.\*

#### GENERAL REMARKS.

Though the aurora borealis has received attention during a considerable portion of the last two centuries, definite information is still wanting on several points which may serve as the basis of a sound induction as to its cause. These relate particularly to the actual frequency of the appearance of the meteor; its comparative frequency in the different months of the year and different hours of the day; the connection of the appearance of the meteor with other atmospherical phenomena; the elevation and extent of visibility of the arch; and whether the same or different phases are presented to individuals at different stations at the same moment of time; finally, the precise influence of the arches, streams, &c., on the magnetic condition of the earth; and whether any unusual electrical effects can be observed during the appearance of the meteor.

Auroral phenomena may be divided into the following classes:-

- 1. A faint light in the north, without definite form or boundary.
  - 2. A diffused light, defined by an arch below.
  - 3. Floating patches of luminous haze—sometimes striated.
- 4. One or more arches, resembling the rainbow, of uniform white color, retaining the same apparent position for a considerable time, and varying in luminosity.

<sup>\*</sup> These instructions are principally adopted from those used in the Observatory at Toronto, Canada.

- 5. A dark segment, appearing under the arch.
- 6. Beams, rays, streamers, waves, transverse and serpentine bands, interrupted or checkered arches, frequently tinged with color, and showing rapid changes in form, place, and color.
  - 7. Auroral corona, or a union of beams south of the zenith.
  - 8. Dark clouds accompanying the diffuse light.
  - 9. Sudden appearance of haze over the whole face of the sky.

The following may serve as a scale of brightness:-

1. Faint. 2. Moderate. 3. Bright. 4. Very bright.

### GENERAL DIRECTIONS.

- 1. Make a regular practice of looking for auroras every clear evening, from 8 to 10 o'clock, or later. Record the result, whether there be an aurora or not.
- 2. Note the time of observation, and compare the watch used with a good clock, as soon after as is convenient.
  - 3. Make a return of the latitude and longitude of the station.
  - 4. Note the class to which the auroral phenomenon belongs.
- 5. If it be an arch, note the time when the convex side reaches any remarkable stars, when it passes the zenith, disappears, &c.
- 6. If the arch be stationary for a time, mark its position among the stars on the accompanying map, so that its altitude may be determined.
- 7. If it be a streamer or beam, mark its position on the map, and the time of its beginning and ending.
- 8. If motion be observed in the beams, note the direction, whether vertically or horizontally, to the east or west.
- 9. Note the time of the formation of a corona, and its position among the stars.
- 10. Note the time of the appearance of any black clouds in the north near the aurora; also, if the sky be suddenly overcast with a mist at any time during the auroral display.
  - 11. Give the direction and force of the wind at the time.
  - 12. Note if any electrical effects are observed.
- 13. Note the effect upon a delicately suspended magnetic needle.

### USE OF THE MAP.\*

- 1. To define the place and the extent of the aurora, the observer should familiarize himself with the relative position of the stars in the northern sky, by frequent inspection of the accompanying map, or a celestial globe.
- 2. Let the observer place the map before him, with the constellations in the positions in which they actually appear at the time of the observation. This may be done by holding up a plumb-line between the eye and the pole star, noticing the stars which it cuts; then a light pencil drawn through these stars and the pole on the map will be the centre of the heavens, or place of the meridian at the moment.
- 3. Mark carefully the place among the stars of the arch of the aurora, and show its width by parallel curved lines. Make a note of the time.
- 4. Draw a light curved line, following, as nearly as can be judged, the outline of the arch down to the horizon, on each side.
- 5. If the arch changes its position, mark its new places at intervals, noting the time of each observation.
- 6. Letter each position A, B, C, &c., and note the time and other particulars on the back or margin of the map, or in the register.
- 7. Beams or cornscations, or streamers of white or colored light, may be marked by lines at right angles to the above, with arrow heads pointing towards the place among the stars to which they tend, or where they would meet, if prolonged.
- 8. To aid in the estimation of angular distances the spaces between certain conspicuous stars have been marked on the map, which will furnish a scale to assist the eye, when actual measurement may be impracticable.
- 9. The course of brilliant meteors, when they fall within the portion of the heavens included on the map, may be marked by a line, the length of which will show the path of the meteor; the course should be indicated by an arrow, and the time recorded.

The map, when filled, together with any written observations,

<sup>\*</sup> Copies of the map will be furnished by the Institution.

may be returned to the Smithsonian Institution, indorsed Meteorology.

### MAGNETIC APPARATUS.

Few observers will probably be furnished with a regular set of magnetical instruments. A temporary apparatus may, however, be fitted up at comparatively little expense and trouble. For this purpose a steel plate, such as was used a few years since for ladics' busks, may be magnetized, and suspended edgewise in the vertical plane, by a few fibres of untwisted silk, in a box to prevent agitation by the air, furnished with a glass window on one side, through which observations may be made. To render the motions perceptible, a small mirror should be cemented on the side of the magnet opposite the window. In front of this mirror, and at the distance of ten or fifteen feet, an ordinary spyglass is fastened to a block, and under the glass, to the same block, a graduated scale, with arbitrary divisions marked upon it, is attached. The arrangement is such that the divisions of the scale may be seen through the telescope, reflected from the mirror, and consequently the slightest motion of the needle, and of the mirror cemented to it, gives a highly magnified apparent motion to the scale. The mirror may be formed of a flat piece of steel, highly polished by means of calcined magnesia; or, in default of a mirror of this kind, a piece of plate looking-glass may be employed, provided one can be procured sufficiently true. The suspension threads should be three or four feet long. The instrument should not be placed very near large masses of iron, and care should be taken not to change the position of any articles of iron which are within the distance of fifteen or twenty feet, otherwise a change in the position of the needle will be produced. For a similar reason the box should be constructed without iron nails. The above described instrument will indicate changes in the direction of the magnetic meridian. similar instrument, deflected at right angles to the magnetic meridian by the torsion of two suspended threads, will furnish an apparatus for indicating changes of horizontal magnetic force.

### ELECTRICAL APPARATUS.

To ascertain whether any change takes place in the electrical state of the atmosphere during the appearance of an aurora, the end of a long insulated wire, suspended from two high masts or two chimneys by means of silk threads, may be placed in connection with a delicate gold leaf electrometer. Any change in the electrical state of the atmosphere, simultaneous with the aurora, will be indicated by the divergence of the leaves. Two slips of gold-leaf attached by a little paste to the lower end of a thick wire, passing through a cork in a four-ounce vial, will answer for this purpose. The arrangement of the leaves will be best made by a bookbinder, who is expert in the management of gold-leaf.

[A continuous series of photographic registers of the motion of the magnetic needle is now kept up at the joint expense of the Coast Survey and this Institution, which will serve for comparison with any observations which may be made on the aurora.]

Prof. Olmsted, in a recent paper published by the Smithsonian Institution, classifies different auroras as follows:—

"CLASS I. This is characterized by the presence of at least three out of four of the most magnificent varieties of form, namely, arches, streamers, corona, and waves. The distinct formation of the corona is the most important characteristic of this class; yet, were the corona distinctly formed, without auroral arches or waves, or crimson vapor, it could not be considered as an aurora of the first class.

"Class II. The combination of two or more of the leading characteristics of the first class, but wanting in others, would serve to mark class the second. Thus the exhibition of arches and streamers, both of superior brilliancy, with a corona, while the waves and crimson columns were wanting, or of streamers with a corona, or of arches without a corona, without streamers or columns (if such a case ever occurs), we should designate as an aurora of the second class.

"Class III. The presence of only one of the more rare characteristics, either streamers or an arch, or irregular cornscations, but without the formation of a corona, and with but a

moderate degree of intensity, would denote an aurora of the third class.

"CLASS IV. In this class we place the most ordinary forms of the aurora, as a mere northern twilight, or a few streamers, with none of the characteristics that mark the grander exhibitions of the phenomenon."

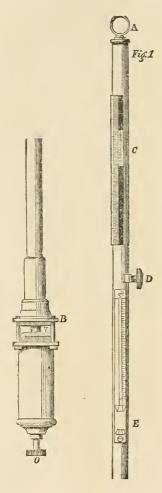
The same author remarks:-

"On the evening of the 27th of August, 1827, after a long absence of any striking exhibition of the aurora borealis, there commenced a series of these meteors, which increased in frequency and magnificence for the ten following years, arrived at a maximum during the years 1835, 1836, and 1837, and, after that period, regularly declined in number and intensity until November, 1848, when the series appeared to come to a close. The recurrence, however, of three very remarkable exhibitions of the meteor in September, 1851, and of another of the first class as late as February 19th, 1852, indicates that the close was not so abrupt as was at first supposed; but still there was a very marked decline in the number of great auroras after 1848, and there has been scarcely one of the higher class since 1853.

"A review of the history of the foregoing series of auroras appears to warrant the conclusion that it constituted a definite period, which I have ventured to call the "Secular Period," having a duration of little more than twenty years; increasing in intensity pretty regularly for the first ten years, arriving at its maximum about the middle of this period, and as regularly declining during the latter half of the same period."

If this view be correct, it would appear that but few brilliant displays of the aurora may be expected for a number of years to come.

## GREEN'S STANDARD BAROMETER.

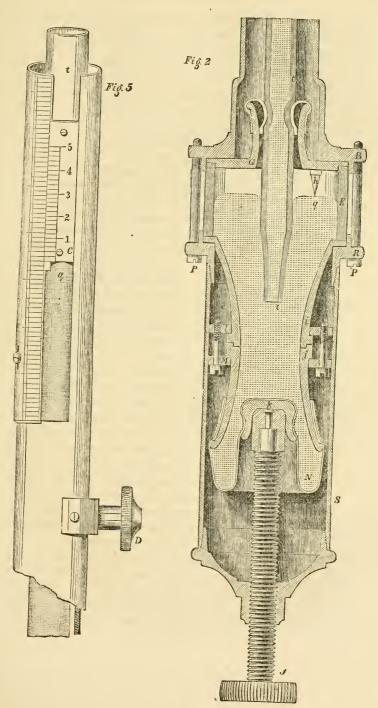


THE following is an account of Green's improved standard barometer, adopted by the Smithsonian Institution, for observers of the first class.

The barometer consists of a brass tube, (Fig. 1) terminating at top in a ring A, for suspension, and at bottom in a flange B, to which the several parts forming the cistern are attached.

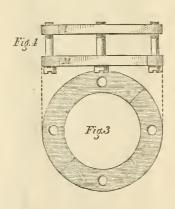
The upper part of this tube is cut through so as to expose the glass tube and mercurial column within, seen in Fig. 5. Attached at one side of this opening is a scale, graduated in inches and parts; and inside this slides a short tube c, connected to a rack-work arrangement, moved by a milled head D: this sliding tube carries a vernier in contact with the scale, which reads off to  $\frac{1}{500}$  (.002) of an inch.

In the middle of the brass tube is fixed the thermometer E, the bulb of which being externally covered, but inwardly open, and nearly in contact



with the glass tube, indicates the temperature of the mercury in the barometer tube, not that of the external air. This central position of the thermometer is selected that the mean temperature of the whole column may be obtained; a matter of importance, as the temperature of the barometric column must be taken into account in every scientific application of its observed height.

The cistern (Fig. 2) is made up of a glass cylinder F, which allows the surface of the mercury q to be seen, and a top plate G, through the neck of which the barometer-tube t passes, and to which it is fastened by a piece of kid leather, making a strong but flexible joint. To this plate, also, is attached a small ivory point h, the extremity of which marks the commencement or zero of the scale above. The lower part, containing the mercury, in which the end of the barometer-tube t is plunged, is formed of two parts i j, held together by four screws and two divided rings l m, in the manner shown in the Figures 2, 3, and



4. To the lower piece j is fastened the flexible bag N, made of kid leather, furnished in the middle with a socket k, which rests on the end of the adjusting-screw O. These parts, with the glass cylinder F, are clamped to the flange B by means of four long screws P and the ring R; on the ring R screws the cap S, which covers the lower parts of the cistern, and supports at the end the adjusting-screw R. R, R, R, are of boxwood; the

other parts of brass or German silver. The screw O serves to adjust the mercury to the ivory point, and also, by raising the bag, so as to completely fill the cistern and tube with mercury, to put the instrument in condition for transportation.

In Fortin's barometer, and also Delcro's modification of it, a cement is used to secure the mercury against leakage at the joints. This, sooner or later, is sure to give way; and tested under the extremes of the thermometrical and hygrometrical range of this climate especially, has made this defect more evi-

dent. This was removed by the substitution of iron in the place of wood; but it was soon found impracticable, in this form of cistern, to prevent damage from rust. These objections led to the present plan of construction, which effectually secures the joints without the use of any cement. The surfaces concerned are all made of a true figure, and simply clamped together by the screws, a very thin leather washer being interposed at the joints. This would not be permanent, however, but for the especial care taken in preparing the boxwood. The boxwood rings are all made from the centres of the wood, and concentric with its growth. They are worked thin and then toughened, as well as made impervious to moisture, by complete saturation with shellac. This is effected by immersing them in a suitable solution in vacuo. The air being withdrawn from the pores of the wood, is replaced by the lac. This, however, with the after-drying or baking, requires care; but when properly done, the wood is rendered all but unchangeable.

Another peculiarity consists in making the scale adjustable to correct for capillarity, so that the barometer may read exactly with the adopted standard, without the application

of any correction; and this, too, without destroying the character of the barometer as an original and standard instrument. Near the 30 inches line, Figure 6, is a line v, on the main tube; this last line is distant exactly thirty inches from the tip of the ivory point; therefore, when these lines coincide, or make one line, the scale is in true measurement position; or the 30 mark is exactly thirty inches from the tip of the ivory point in the cistern. In this position, the amount of correction due to capillarity being ascertained, the scale is then moved that quantity and clamped firm. The barometer will now give the readings



corrected for capillarity, and thus avoid at once the labor of applying a correction, and the risk of error from an accidental neglect of it.

It must be borne in mind that this correction applies only to the particular tube, and while preserved in good condition.

If this tube is injured and again used, or another tube put in its place, the scale should then be moved until the lines coincide,

the amount of correction for the repaired or the new tube being estimated until a good comparison can be made directly or intermediately with the Smithsonian standard.

The connecting the parts i and j by rings and screws, Figs. 2, 3, and 4, rather than by a single screw cut on the edge, is an improvement, as the single wood-screw is apt, after a time, to adhere so firmly that it is often difficult, and sometimes impossible, with safety to the parts, to separate it.

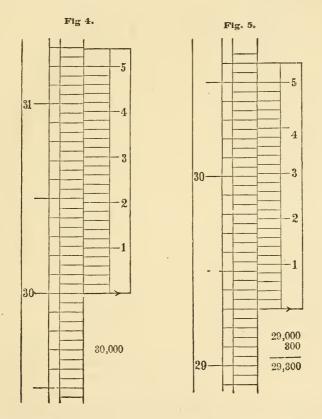
It is not advisable to disturb the cistern, unless it becomes difficult, from the oxide of mercury which gradually forms, to make the adjustment of the mercury to the ivory point, as there is more or less risk in doing so. Any one accustomed to such mechanical affairs, with due attention to the plan, can, however, take out the mercury from the cistern, refilter, clear the parts of adhering oxide, and replace them; the instrument all the time being kept vertical, with the cistern at top, as the mercury must not be allowed to come from the tube.

To insure a good vacuum by the complete expulsion of all air and moisture, the boiling of the mercury in the tube is done in vacuo; and care should be taken to preserve it in good condition.

To put up the barometer for observation, suspend the barometer by the ring A in a good light, near to and at the left side of a window, and, when practicable, in a room not liable to sudden variations of temperature. Record the temperature, and then, by the screw O, lower the mercury in the cistern until the surface is in the same plane with the extremity of the ivory point. As this extremity of the point is the zero of the scale, it is necessary, at each observation, to perfect this adjustment. It is perfect when the mercury just makes visible contact. If the surface is lowered a little, it is below the point; and if raised a small amount, a distinct depression is seen around the point. This depression is reduced to the least visible degree. A few trials will show that this adjustment can always be made to a thousandth of an inch.

The adjustment effected, bring the lower edge of the vernier C, Fig. 5, by means of the milled head D, into the same plane with the convex summit of the mercury in the tube. Looking through the opening, with the eye on a level with the top of the mercury in the tube, when the vernier tube is too low, the light

is cut off; when too high, the light is seen above the top of the mercury. It is right when the light is just cut off from the summit, the edge making a tangent to the curve. A piece of white paper placed behind, and also at the cistern, will be found to give a more agreeable light by day, and is, besides, necessary for night observations; the lamp being placed before the instrument and above the eye, to reflect the light.

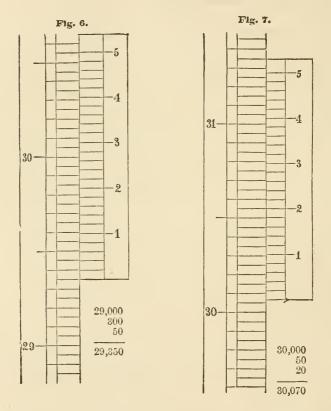


The method of reading off will perhaps be best explained by a few examples. Suppose, after completing the adjustments, the scale and vernier to be in the position shown in Fig. 4, on this page, it will be seen that the lowest or index line of the vernier coincides exactly with the line marked 30 on the scale. The reading, therefore, is 30.000 inches.

If, as in Fig. 5, we find the line of the vernier coinciding with the third line of the tenths above 29, we read 29.300.

If, as in Fig. 6, on this page, we find the index at 29 inches 3 tenths and 5 hundredths, we read 29.350.

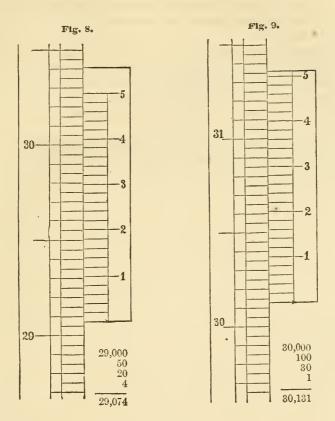
If, as in Fig. 7, we find the index at 30 inches no tenths 5 hundredths and something more, this additional quantity we



shall find by looking up the vernier scale, until we come to some one line on it, coinciding with a line on the other scale. In this instance it is the line marked 2, and indicates 2 hundredths, to be added to the other numbers, making 30.070.

If, as in Fig. 8, we find 29 inches no tenths 5 hundredths, and on the vernier the second line above that marked 2, is found to coincide with the scale, each of these short lines indicates 2

thousandths—consequently, are so counted; the reading s therefore 29.074.



Or it may be, as in Fig. 9, where we have 30 inches 1 tenth, and the line on the vernier mark 3 coinciding nearly, but not perfectly, with a line on the scale, it is a little too high; the 2 thousandth short line next above is, however, a like quantity too low; so the true reading must be the number between them—that is, 1 thousandth, making together 30.131.

These examples include all the combinations the scale allows. A little practice with the barometer, with reference to the examples, will soon enable the learner to read off the scale with facility. At first it will be best to write down the inches and

parts in full, as in the diagrams, not trusting the memory with the whole, until experience shall have given confidence.

Be careful never to lower the mercury in the cistern much below the necessary quantity, as it increases the risk of air entering the tube.

When the barometer is to be removed for transportation, or change of position, before taking it down, the mercury is to be screwed up until the cisteru and tube are just full. If it is screwed more than this, the mercury may be forced through the joints of the cistern. It should then be inverted, and carried cistern-end upwards.

This instrument is well adapted for service as a mountain barometer, and when used as such, is packed in a leather case, with suitable straps for convenient carriage.

## REGISTRY OF PERIODICAL PHENOMENA.

The Smithsonian Institution, being desirous of obtaining information with regard to the periodical phenomena of animal and vegetable life in North America, respectfully invites all persons who may have it in their power, to record their observations, and to transmit them to the Institution. These should refer to the first appearance of leaves and of flowers in plants; the dates of appearance and disappearance of migratory or hybernating animals, as mammals, birds, reptiles, fishes, insects, &c.; the times of nesting of birds, of moulting and littering of mammals, of utterance of characteristic cries among reptiles and insects, and anything else which may be deemed noteworthy.

The Smithsonian Institution is also desirous of obtaining detailed lists of all the animals and plants of any locality throughout this continent. These, when practicable, should consist of the scientific names, as well as of those in common use; but when the former are unknown, the latter may alone be given. It is in contemplation to use the information thus gathered, in deducing general laws relating to the geographical distribution of species of the animal and vegetable kingdoms of North America. Any specimens of natural history will also be acceptable. Directions for their preservation have been published by the Institution, and will be sent to all who may wish them.

The points in the phenomena of plants, to which attention should be directed, are:—

- 1. Frondescence, or leafing.—When the buds first open and exhibit the green leaf.
  - 2. Flowering.—When the anther is first exhibited:
    - a. In the most favorable location;
    - b. General flowering of the species.

- 3. Fructification.—When the pericarp splits spontaneously in dehiscent fruits, or the indehiscent fruit is fully ripe.
  - 4. Fall of leaf.—When the leaves have nearly all fallen.

The dates of these various periods should be inserted in their appropriate columns.

When the observations for the year are complete, they should be returned to the Institution, with the locality and observer's name inserted in the blank at the head of the sheet.

# PLANTS.

, and the second	fing.	Flow	ering.	cation	leaf.
List of Plants.	Frondescence or leafing.	a.	ъ.	Fructification	Fall of leaf
Acer rubrum, L.—Red, or soft maple.  Acer dasycarpum, Ehrh.—White, or silver maple  Acer saccharinum, L.—Sugar maple  Achillea millefolium, L.—Millefoil, or yarrow  Actæa rubra, Willd.—Red baneberry  Actæa alba, Bigelow.—White baneberry;  necklace weed  Esculus hippocastanum, L.—Horse chestnut  Esculus glabru, Willd.—Ohio buckeye  Asculus glabru, Willd.—Ohio buckeye  Asculus gladru, Ait.—Yellow buckeye  Ailantus glandulosa.—Tree of heaven; ailanthus  Amelanchier canadensis.—Shad bush; service  berry  Amorpha fruticosa, L.—False indigo  Amygdalus nana, L.—Flowering almond  Anemone nemorosa, L.—Wind flower; wood  anemone  Aquilegia canadensis, L.—Wild columbine  Arctostaphylos uva-ursi, Spreng.—Bearberry  Asclepias cornuti, Decaisne.—Milkweed  Asimina triloba, Dunal.—Papaw  Azalea nudiflora, L.—Common red honey- suckle  Bignonia (Tecoma) radicans, Juss.—Trumpet creeper  Castanea vesca, L.—Chestnut  Carya alba.—Shag-bark, or shell-bark hickory Cercis canadensis, L.—Red bud; Judas tree  Cerasus virginiana, DC.—Chokeberry  Cerasus virginiana, DC.—Chokeberry  Cerasus virginiana, DC.—Chokeberry  Chionanthus virginica, L.—Fringe tree  Cimicifuga racemosa, Ell.—Black-snake root; rattlesnake root  Claytonia virginica, L.—Spring beauty  Clettra alnifolia.—White alder, or sweet pepper bush  Cornus florida, L.—Flowering dogwood*  Cratægus crus-galli, L.—Cockspur thorn  Cratægus crus-galli, L.—Coc					

<sup>\*</sup> The time of the expansion of the real flower, not of the white involucre.

## PLANTS-Continued.

	cence,	Flow	ering.	ation.	eaf.
List of Plants.	Frondescence or leafing.	a.	ъ.	Fructification	Fall of leaf.
Gaylussacia resinosa, Torr. and Gray.—Black					
huckleberry					
Houstonia cærulea, Hook.—Bluets; innocence,					
Hypericum perforatum, L.—St. John's wort  Iris versicolor, L.—Large blue flag					
Kalmia latifolia, L.—Mountain laurel Laurus benzoin, L.—(Benzoin odoriferum, Nees.)  Spice bush; Benjamin bush					
Leucanthemum vulgare, Lam.—Ox-eye daisy; white weed					
Lobelia cardinalis, L.—Red cardinal flower . Lonicera tartarica, L.—Fereign spurs					
Lupinus perennis, L.—Wild lupine Liriodendron tulipifera, L.—Tulip tree; American poplar					
Magnolia glauca, L.—Small or laurel magno-					
lia; sweet bay					
Morus rubra, L.—Red mulberry					
lily					
Pontederia cordata, L.—Pickerel weed Pogonio ophioglossoides, Nutt.—Adder's tongue Pyrus communis, L.—Common pear-tree					
Pyrus malus, L.—Common apple-tree					
Rhododendron maximum, L.—Great laurel					
Robinia viscosa, Vent.—Clammy locust					
Sambucus canadensis, L.—Common elder					
Sarracenia purpurea, L.—Side-saddle flower					
Smilacina bifolia, Ker.—Two-leaved Solomon- seal					
Syringa vulgaris, L.—Lilac					
lime, or linden					

#### BIRDS

Birds.	Arrival in spring.	Commencement of nesting.	Commencement of incubation.	Appearance of young.	Departure in autumn.
Acanthylis pelasgia, Boie.—Chimney-bird . Agelaius phæniceus, L.—Red-winged blackbird Anser canadensis, L.—Wild goose					

# Reptiles—first appearance, cries, and general peculiarities of habits.

Bufo americanus, and other species of toads.

Rana, the various kinds of frogs.

Hyla and Hylodes, the several kinds of tree-frogs.

Turtles, lizards, snakes.

FISHES—first appearance and spawning.

Salmo salar, L., salmon. Alosa, shad. Clupea, herring. Anguilla, eel. Acipenser, sturgeon.

INSECTS—their first appearance and cries.

Platyphyllum concavum, Harr., catydid. Cicada, locusts—the several kinds Ecanthus niveus, Harr., tree-crickets Grasshoppers, in their variety. Fire-flies.

#### GENERAL PHENOMENA OF CLIMATE.

Phenomena of a general character, of which the date of appearance cannot be mistaken, are very valuable. Series of years have in some cases been carefully observed, which would greatly add to the value of the current record, if forwarded with it. The following are of this class:—

- 1. Breaking up of ice in large rivers or bays.
- 2. Date of greatest rise and lowest fall of water in large rivers, especially when periodic, as in parts of the interior.
- 3. General leafing and fall of leaf in deciduous forests. In most parts of the North and interior these are well marked and easily designated periods.
- 4. Commencement of growth and the end of growth or destruction of grasses in general; as on plains or prairies.
- 5. First growth, flowering, and maturity, of important annual staples, with their period in days from the commencement to the end of vital action.

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# Psychrometrical Table:

FOR DETERMINING THE

# ELASTIC FORCE OF AQUEOUS VAPOR

AND THE

# RELATIVE HUMIDITY OF THE ATMOSPHERE

FROM

INDICATIONS OF THE WET AND THE DRY-BULB THERMOMETER FAHRENHEIT.

BY

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WASHINGTON:
PUBLISHED BY THE SMITHSONIAN INSTITUTION.
1856.

THE following table is based on the formulæ of Reginault, as used by Prof. Guyot, in the preparation of his Psychrometrical Tables, for the Smithsonian Institution viz.:—

$$x = f - \frac{.480 \ (t - t')}{610 - t'} h, \text{ for temperatures above the freezing-point,}$$
 and  $x = f - \frac{.480 \ (t - t')}{689 - t'} h$ , for those below;

in which h represents the height of the barometer, t the temperature indicated by the dry bulb centigrade thermometer, t' that indicated by the wet bulb thermometer, f the elastic force of aqueous vapor in a saturated air at the temperature t', and x the actual force at the time of the observation.

Adapting these formulæ to the Fahrenheit thermometer, the former will read

$$x = f - \frac{.480 \times \frac{5}{9} (t - t')}{610 - \frac{5}{9} (t' - 32)} h = f - \frac{.480 (t - t')}{1130 - t'} h,$$

and the latter,

$$x = f - \frac{.480 \times \frac{5}{9} (t - t')}{689 - \frac{5}{9} (t' - 32)} h = f - \frac{.480 (t - t')}{1240.2 - t'} h.$$

If we put h = 755 millimetres, = 29,725 English inches, these formulæ may be reduced for the latter measure to the following forms:—

$$x = f - \frac{14.268(t - t')}{1130 - t'}; \text{ and } x = f - \frac{14.268(t - t')}{1240.2 - t'}.$$

In using the table, look out the degree of the wet-bulb thermometer at the top, and the difference between the wet and dry bulb thermometers at the left. Under the former and opposite the latter, find, in their appropriate columns, the force of vapor, and the relative humidity.

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heit.		וע	EGREES	OF THE	WET B	ULB TI	ERMOME						
Fahren	8	31°	-8	80°	2	29°	2	S°	- 2	70	- 2	26°	
t - t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vaper, in inches.	Relative II umidity.	
00	·011 ·006	100 50 2	·012 ·006 ·001	100 52 6	·012 ·007 ·001	100 54 9	·013 ·007 ·002	100 55 12	·013 ·008 ·002	100 57 16	·014 ·008 ·003	100 59 19	
eit.		D	EGREES	OF TH	E WET	BULB '	THERMO	METER	—FAHRE	NHEIT			
ahrenb	-2	5°	2	40	2	23°	-2	22°	_2	21°	_ 2	20°	
t — t' Fabrenheit.	Force of Vapor, in iuches.												
0°   1/2   1   1/2	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $										·018 ·012 ·007 ·001	100 67 35 5	
It.		D	EGREES	OF TH	E WET	BULB ?	THERMO	METER.	—FAHRI	NHEIT			
direnhe	-1	9°	-1	s°	-1	70	-1	<b>6</b> °	-1	5°	-1	<b>4</b> °	
t t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	
$ \begin{array}{c c} \hline 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2 \end{array} $	·019 ·013 ·007 ·002	100 69 37 9	·020 ·014 ·008 ·003	100 70 40 12	·021 ·015 ·009 ·003	100 71 43 16	·022 ·016 ·010 ·004	100 72 45 19	·023 ·017 ·011 ·005	100 73 47 23	·024 ·018 ·012 ·006 ·001	100 74 49 26 3	
it.		DI	EGREES	OF TH	E WET	BULB 7	HERMON	IETER.	FAHRE	NHEIT			
Fabrenbeit.	-1	<b>3</b> °	-1	<b>2</b> °	-1	1°	-1	<b>0</b> °	-9	)°	-8	3°	
t t' E	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches,	Relative Humidity.	
$ \begin{array}{c c} \hline 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2\frac{1}{2} \end{array} $	·025 ·019 ·013 ·007 ·002	100 75 51 29 6	·026 ·020 ·014 ·009 ·003	100 76 53 31 10	·027 ·021 ·015 ·010 ·004	100 77 55 34 13	-028 -022 -017 -011 -005	100 78 57 36 17	·029 ·024 ·018 ·012 ·006 ·001	100 79 58 39 20 2	·031 ·025 ·019 ·013 ·008 ·002	100 80 60 41 23 6	

	1												
i.		:	DEGREES	S OF T	HE WET	BULB	THERM	OMETE:	R.—FAHI	RENHE	T.		
brenhe		7°		6°		5°		1°	_ :	3°	- 5	2°	
t — t' Fabrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	
$ \begin{array}{c c} 0^{\circ} \\ 1 \\ 1 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 3^{\circ} \end{array} $	·032 ·026 ·021 ·015 ·009 ·003	100 80 62 43 26 10	·033 ·028 ·022 ·016 ·011 ·005	100 81 63 46 29 13	·035 ·029 ·024 ·018 ·012 ·006 ·001	100 82 65 48 32 17 2	·036 ·031 ·025 ·019 ·014 ·008 ·002	100 83 66 50 34 20 5	·038 ·032 ·027 ·021 ·015 ·010 ·004	100 83 67 52 37 23 9	·040 ·034 ·028 ·023 ·017 ·011 ·006	100 84 68 53 39 26 12	
eit.		D	EGREES	OF TH	IE WET	BULB	THERMO	METER	.—FAHR	ENHEI'	г.		
ahrenh	1	1° 0° 1° 2° 3° 4°											
t — t' Fabrenbeit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	
$\begin{array}{c c} 0^{\circ} \\ 1 \\ 1 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 3 \\ 3 \\ 4 \\ \end{array}$	-042 -036 -030 -025 -019 -013 -008 -002	100 84 69 55 42 28 16 4	·044 ·038 ·032 ·026 ·020 ·015 ·009 ·003	100 85 70 56 43 30 18 6	·046 ·040 ·034 ·028 ·022 ·017 ·011 ·005	100 85 71 57 45 32 21	-048 -042 -036 -030 -024 -019 -013 -007 -001	100 86 72 59 47 35 23 12	·050 ·044 ·038 ·032 ·027 ·021 ·015 ·009 ·003	100 86 73 60 49 37 26 15 6	·052 ·046 ·041 ·035 ·029 ·023 ·017 ·012 ·006	100 87 74 61 51 39 29 19	
it.		· D	EGREES	OF TH	IE WET	BULB	THERMO	METER	.—FAHR	ENHEL	г.		
hrenbe	5		6	0	70	,	S		9	0	10	0	
t t' Fahrenheit,	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	
$\begin{array}{c c} 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2 \\ \frac{2}{1} \\ \frac{1}{2} \\ \frac{3}{2} \\ 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \end{array}$	008	100 87 75 62 52 42 82 22 13 4	057 051 045 040 034 028 022 017 011 005	100 87 76 64 54 44 35 25 16 7	·060 ·054 ·048 ·042 ·036 ·031 ·025 ·019 ·013 ·007 ·002	100 88 77 66 56 46 37 27 19 10 2	·062 ·057 ·051 ·045 ·039 ·033 ·028 ·022 ·016 ·010 ·004	100 88 77 68 57 48 39 30 21 13 6	-065 -059 -054 -048 -042 -036 -030 -025 -019 -013 -007 -001	100 89 78 69 59 49 41 32 24 16 9	·068 ·062 ·057 ·051 ·045 ·039 ·028 ·022 ·016 ·010 ·004	100 89 79 70 60 51 43 34 27 19 12 5	

			TODEES	OF TH	IF WET	DILID	THERMO	METER	_FAHRI	ENHEI	,	
t' Fahrenheit.	11		12		13	1	14	1	15		16	0
t — t' Fab	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c c} 0^{\circ} & \frac{1}{2} \\ 1 & 1 \\ 1 \\ \frac{1}{2} \\ 2 & 2 \\ \frac{1}{2} \\ 3 & 3 \\ \frac{1}{2} \\ 4 & 4 \\ \frac{1}{2} \\ 5 & 5 \\ \frac{1}{2} \\ 6 & 6 \\ \frac{1}{2} \\ 7 & 7 \\ \frac{1}{2} \\ \end{array}$	·071 ·066 ·060 ·054 ·048 ·042 ·037 ·031 ·025 ·019 ·019 ·007 ·002	100 90 80 71 62 53 45 87 29 22 15 8	·075 ·069 ·063 ·057 ·051 ·046 ·040 ·034 ·028 ·022 ·017 ·011 ·005	100 90 81 72 63 55 46 39 31 24 18 11 5	·078 ·072 ·067 ·061 ·055 ·049 ·038 ·032 ·026 ·020 ·014 ·008 ·003	100 91 81 73 64 56 48 41 34 27 20 13 8	·082 ·076 ·070 ·065 ·059 ·053 ·047 ·041 ·036 ·030 ·024 ·018 ·012 ·006 ·001	100 91 82 74 65 58 50 43 36 29 23 17 11 6	-086 -080 -074 -068 -068 -065 -057 -051 -045 -039 -034 -028 -022 -016 -010 -004	100 91 83 75 67 59 52 45 38 32 25 20 14 9	090 084 078 072 067 061 055 049 043 032 026 020 014 008 003	100 91 83 75 68 60 53 47 40 34 28 22 17 12 7
heit.		D	EGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEI	r.	
t — t' Fabrenbeit.	17	Yo	18	90	19	0	20	)°	21	l°	22	
t - t'	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in iuches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{ c c c c }\hline 0^{\circ} & \frac{1}{2} & \frac{1}{2} \\ \hline 1 & \frac{1}{2} & \frac{1}{2} \\ 2 & \frac{1}{2} & \frac{1}{2} \\ 3 & \frac{1}{2} & \frac{1}{2} \\ 4 & \frac{1}{2} & \frac{1}{2} \\ 5 & \frac{1}{2} & \frac{1}{2} \\ 6 & \frac{1}{2} & \frac{1}{2} \\ 6 & \frac{1}{2} & \frac{1}{2} \\ 8 & \frac{1}{2} & \frac{1}{2} \\ 9 & \frac{1}{2} & \frac{1}{2} \\ 10 & \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \\ \end{array}$	-094 -088 -082 -077 -071 -065 -059 -053 -042 -036 -030 -024 -012 -007 -001	100 92 84 76 69 62 55 48 42 36 31 25 20 15 10	-098 -093 -087 -081 -075 -069 -064 -058 -052 -046 -040 -034 -028 -028 -023 -017 -011 -005	100 92 84 77 70 63 56 50 44 38 33 27 22 17 12 8 4	-103 -097 -091 -085 -080 -074 -068 -062 -051 -044 -039 -033 -027 -021 -015 -010	100 92 85 78 71 64 58 52 46 40 35 29 24 20 15	·108 ·102 ·096 ·090 ·084 ·079 ·073 ·067 ·061 ·055 ·049 ·043 ·038 ·032 ·026 ·020 ·014 ·009 ·003	100 92 85 78 71 65 59 53 47 42 37 42 17 13 9 5	-113 -107 -101 -095 -089 -077 -071 -060 -054 -048 -042 -037 -031 -025 -019 -013 -007 -001	100 93 86 79 72 66 60 54 49 39 34 29 24 20 16 12 8	·118 ·112 ·106 ·100 ·094 ·088 ·082 ·077 ·071 ·065 ·059 ·053 ·042 ·036 ·030 ·024 ·012 ·006 ·001	100 93 86 79 73 67 61 56 51 40 36 31 27 22 18 14 11 7

23°   24°   25°   26°   27°   28°   25°   26°   27°   28°   25°   26°   27°   28°   25°	neit.		D	EGREES	OF TI	E WET	BULB	THERMO	METER	.—FAHRI	ENHEIT		
	ahrenl	23	0	24	Į°	25	0	26	3°	21	yo	28	0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	t — t' F	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
	$\begin{array}{c} \frac{1}{2} \\ 1 \\ 1 \\ \frac{1}{2} \\ 2 \\ 2 \\ \frac{1}{2} \\ 3 \\ \frac{1}{2} \\ 3 \\ \frac{1}{2} \\ 4 \\ 4 \\ \frac{1}{2} \\ 5 \\ 5 \\ \frac{1}{2} \\ 6 \\ 6 \\ \frac{1}{2} \\ 7 \\ 7 \\ \frac{1}{2} \\ 8 \\ 8 \\ \frac{1}{2} \\ 9 \\ 9 \\ \frac{1}{2} \\ 10 \\ 10 \\ \frac{1}{2} \\ 11 \\ 11 \\ \frac{1}{2} \\ \end{array}$	·123 ·117 ·111 ·105 ·100 ·094 ·088 ·082 ·076 ·070 ·065 ·059 ·047 ·041 ·035 ·023 ·017 ·011	100 93 86 80 74 68 62 57 52 47 42 37 33 29 25 21 17 13 10 6	·129 ·123 ·117 ·111 ·105 ·099 ·093 ·088 ·076 ·070 ·064 ·053 ·047 ·041 ·035 ·023 ·017 ·012	100 93 87 81 75 69 63 58 58 48 44 39 35 31 27 23 19 15 12 9	·135 ·129 ·123 ·117 ·111 ·105 ·099 ·093 ·087 ·082 ·076 ·070 ·064 ·058 ·052 ·046 ·041 ·035 ·029 ·029 ·017 ·011	100 93 87 82 75 70 64 50 45 41 37 33 29 25 21 18 14 11	·141 ·135 ·129 ·123 ·117 ·111 ·105 ·099 ·093 ·088 ·082 ·076 ·070 ·064 ·058 ·052 ·047 ·041 ·035 ·029 ·029 ·021	100 93 88 82 76 71 66 61 56 51 47 43 39 35 31 27 24 20 17 14	·147 ·141 ·135 ·129 ·123 ·117 ·111 ·106 ·094 ·088 ·082 ·076 ·076 ·076 ·059 ·053 ·047 ·041 ·039 ·029 ·023 ·017 ·011	100 93 88 82 77 72 67 62 57 53 49 44 40 87 29 26 22 19 16 13 10 8	·153 ·147 ·142 ·136 ·130 ·124 ·118 ·112 ·106 ·100 ·094 ·089 ·083 ·077 ·071 ·065 ·059 ·053 ·047 ·041 ·036 ·036 ·036 ·036 ·036 ·036 ·036 ·036	100 94 88 83 78 63 54 50 46 42 38 35 31 28 24 21 18 15 7

heit.		I	EGREES	OF TH	IE WET	BULB	THERMO	)METER	.—FAHR	ENHEL	г.	
- U Fahrenheit.	29	)°	30	)°.	31	Į°	32	0	38	3°	34	10
t – t	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	·160 ·154 ·148 ·142 ·136 ·130 ·125 ·119 ·113 ·107 ·101 ·095 ·089 ·083 ·077 ·072 ·066 ·060 ·054 ·048 ·042 ·036 ·030 ·024 ·013 ·007 ·001	100 94 89 84 78 74 69 64 60 56 51 48 44 40 36 33 30 26 23 21 18 15 12 10 7	·167 ·161 ·155 ·149 ·143 ·187 ·131 ·120 ·114 ·108 ·102 ·096 ·096 ·084 ·078 ·072 ·067 ·067 ·043 ·037 ·031 ·026 ·099 ·043 ·037 ·031 ·026 ·038 ·037 ·031 ·038 ·038 ·038 ·038 ·038 ·038 ·038 ·038	100 95 89 84 79 74 70 65 61 57 53 49 45 42 28 83 22 28 20 17 14 12 9	·174 ·168 ·162 ·156 ·150 ·144 ·138 ·133 ·127 ·121 ·115 ·109 ·009 ·074 ·085 ·079 ·074 ·068 ·062 ·056 ·050 ·044 ·038 ·032 ·026 ·020 ·015 ·009	100 95 89 85 80 75 71 66 62 58 54 51 47 43 40 87 22 19 17 14 12 10 7 5	·181 ·175 ·168 ·162 ·155 ·149 ·142 ·136 ·129 ·123 ·116 ·110 ·103 ·097 ·090 ·084 ·077 ·071 ·0648 ·051 ·045 ·038 ·032 ·025 ·019 ·012 ·006 ·····	100 94 89 84 79 74 70 65 61 57 53 49 41 38 34 31 28 25 22 19 16 14 11 9 6 4 4 2	188 182 175 169 162 156 149 143 136 123 117 110 104 097 091 084 078 071 065 058 052 045 039 032 026 019 013 006	100 95 89 84 80 75 71 66 62 58 54 50 46 43 89 36 83 80 27 24 21 18 16 13 11 8 6 4 2	196 190 183 177 170 164 157 151 144 138 131 124 118 111 105 098 092 085 079 072 066 059 053 046 040 033 027 020 014	100 95 90 85 80 76 71 67 63 59 55 51 48 44 41 37 34 31 28 20 18 15 13 11 8 6
14 14½ 15			1002	1	.003	1	*****	•••••	***************************************		·014 ·007 ·001	$\begin{vmatrix} 4\\2\\0 \end{vmatrix}$

eit		D	EGREES	OF TH	E WET	BULB	THERMO	METER	.—FAHR	ENHEI	2.	
t' Fahrenheit.	38	0	36	0	37	70	38	3° .	39	°	40	)°
t-4 E	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches,	Relative Humidity.	Force of Aapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{ c c c c c }\hline 0^{\circ} & \frac{1}{2} \\ 1 & \frac{1}{1} & \frac{1}{2} \\ 2 & 2 & \frac{1}{2} \\ 3 & \frac{1}{3} & \frac{1}{2} \\ 4 & 4 & \frac{1}{2} \\ 5 & 5 & \frac{1}{2} \\ 6 & 6 & \frac{1}{2} \\ 7 & 7 & \frac{1}{2} & \frac{1}{2} \\ 8 & 8 & \frac{1}{2} \\ 9 & \frac{1}{2} & 1 \\ 10 & 10 & \frac{1}{2} \\ 11 & 11 & \frac{1}{2} \\ 12 & 12 & \frac{1}{2} & \frac{1}{2} \\ 13 & 13 & \frac{1}{2} & \frac{1}{2} \\ 14 & 14 & \frac{1}{2} & \frac{1}{2} \\ 15 & 15 & \frac{1}{2} & \frac{1}{2} \\ 16 & 16 & \frac{1}{2} & \frac{1}{2} \\ 17 & 17 & \frac{1}{2} & \frac{1}{2} \\ 18 & 18 & \frac{1}{2} & \frac{1}{2} \\ \end{array}$	-204 -197 -191 -184 -178 -171 -165 -158 -152 -145 -139 -132 -126 -119 -113 -106 -100 -093 -087 -061 -067 -061 -054 -048 -041 -035 -028 -002	100 95 90 85 81 76 72 68 63 60 56 52 49 45 42 39 36 33 30 27 25 22 19 17 15 13 10 8 6 4 2 1	·212 ·206 ·199 ·193 ·186 ·180 ·173 ·167 ·160 ·154 ·147 ·140 ·134 ·127 ·121 ·114 ·108 ·095 ·069 ·069 ·069 ·049 ·043 ·036 ·030 ·023 ·016 ·010 ·003	100 95 90 86 81 77 73 68 64 61 57 53 50 47 43 40 37 32 29 26 24 21 19 16 14 12 10 8 6 4 3 1	-221 -214 -208 -201 -195 -188 -182 -175 -169 -162 -155 -149 -142 -137 -130 -124 -117 -111 -103 -097 -090 -083 -077 -070 -064 -057 -051 -044 -038 -031 -025 -018 -012 -005	100 95 91 86 82 77 73 69 65 61 58 54 42 39 30 28 25 23 20 18 16 14 12 10 8 6 5 3 1	·229 ·223 ·216 ·210 ·203 ·197 ·190 ·184 ·177 ·151 ·164 ·157 ·151 ·144 ·138 ·131 ·125 ·118 ·112 ·105 ·099 ·092 ·086 ·079 ·073 ·066 ·060 ·053 ·047 ·040 ·033 ·027 ·020 ·014 ·007 ·001	100 95 91 86 82 78 74 70 66 62 59 55 52 49 46 43 40 37 34 32 29 27 24 22 20 18 16 14 12 10 8 7 5 5 6 6 6 6 6 6 6 6 6 6 7 7 8 8 7 8 8 8 8 8 8 8 8 8 8 8 8 8	·238 ·232 ·225 ·219 ·212 ·206 ·199 ·193 ·186 ·180 ·173 ·166 ·160 ·152 ·146 ·139 ·133 ·126 ·120 ·113 ·107 ·101 ·094 ·088 ·062 ·055 ·049 ·042 ·036 ·029 ·023 ·016 ·010 ·003	100 95 91 87 82 78 74 71 67 63 60 56 53 50 47 44 41 39 36 33 31 28 26 24 17 15 14 12 10 9 7 5 8 8 10 10 10 10 10 10 10 10 10 10	·248 ·241 ·235 ·228 ·222 ·215 ·209 ·189 ·189 ·163 ·156 ·150 ·143 ·137 ·130 ·124 ·177 ·110 ·104 ·097 ·091 ·084 ·078 ·071 ·065 ·051 ·045 ·038 ·032 ·025 ·019 ·0106 ·0106	100 95 91 87 88 79 75 71 68 64 61 57 54 48 40 37 35 32 30 28 29 17 15 14 12 10 8 7 5 4 4 3 4 10 10 10 10 10 10 10 10 10 10

eit.		1	DEGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEIT	Γ.	
abrenb	41	L°	42	0	43	0	44	Įo	4.5	0	40	0
t - t' Fabrenbeit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c} 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2 \\ 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \\ 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \\ 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \\ 8 \\ 8\frac{1}{2} \\ 9 \\ 9\frac{1}{2} \\ 10 \\ 10\frac{1}{2} \end{array}$	·257 ·251 ·244 ·237 ·231 ·224 ·218 ·211 ·204 ·198 ·192 ·185 ·179 ·172 ·165 ·159 ·152 ·146 ·132 ·126 ·120	100 96 91 87 83 79 76 72 68 65 62 58 55 52 49 47 44 41 39 36 34 31	·267 ·261 ·254 ·248 ·241 ·234 ·228 ·221 ·215 ·208 ·202 ·195 ·189 ·182 ·175 ·169 ·162 ·156 ·149 ·142 ·136 ·130	100 96 92 88 84 80 76 72 69 66 62 59 50 48 45 42 40 37	·278 ·271 ·265 ·258 ·251 ·245 ·232 ·225 ·218 ·212 ·205 ·199 ·192 ·173 ·166 ·179 ·153 ·146 ·140	100 96 92 88 84 80 77 73 70 66 63 60 57 54 49 46 43 41 39 36 34	·289 ·282 ·275 ·269 ·262 ·256 ·249 ·242 ·236 ·229 ·223 ·216 ·210 ·203 ·196 ·190 ·163 ·177 ·170 ·163 ·157 ·151	100 96 92 88 84 81 77 74 70 67 64 61 58 55 52 50 47 45 42 40 38	-300 -293 -286 -280 -273 -260 -253 -247 -240 -234 -227 -214 -208 -201 -194 -188 -181 -175 -168 -162	100 96 92 88 85 81 78 74 71 68 65 62 59 56 53 51 48 46 43 41 39 37	**311 **305 **298 **291 **285 **272 **265 **252 **245 **239 **212 **206 **199 **193 **186 **179 **173	100 96 92 89 85 81 78 75 71 68 65 63 60 57 54 52 49 47 44 42 40 38
$\begin{array}{c} 11^1\\ 11^1_{\frac{1}{2}}\\ 12^1\\ 12^1_{\frac{1}{2}}\\ 13^1\\ 13^1_{\frac{1}{2}}\\ 14\\ 14^1_{\frac{1}{2}}\\ 15^1_{\frac{1}{2}}\\ 16\\ 16^1_{\frac{1}{2}}\\ 17\\ 17^1_{\frac{1}{2}}\\ 18\\ 18^1_{\frac{1}{2}}\\ 19\\ 19^1_{\frac{1}{2}}\\ 20\\ 20^1_{\frac{1}{2}}\\ 21^1_{\frac{1}{2}}\\ 22\\ 22^1_{\frac{1}{2}}\\ 23^1_{\frac{1}{2}}\\ 23^1_{\frac{1}{2}} \end{array}$	·113 ·106 ·100 ·093 ·087 ·080 ·073 ·061 ·054 ·041 ·034 ·021 ·015 ·008 ·001	29 27 25 23 21 19 17 15 13 12 10 9 7 6 4 3 2	·123 ·116 ·110 ·103 ·097 ·090 ·083 ·077 ·071 ·064 ·057 ·051 ·044 ·031 ·024 ·018 ·011 ·005	30 28 26 24 22 20 19 17 15 13 12 10 9 7 6 5 3 2	·133 ·127 ·120 ·113 ·107 ·100 ·094 ·087 ·081 ·074 ·068 ·061 ·054 ·041 ·035 ·028 ·021 ·015 ·009 ·002	32 30 28 26 24 22 20 18 17 15 13 12 10 9 7 6 5 4 2 1 0	·144 ·137 ·131 ·124 ·118 ·111 ·044 ·098 ·072 ·065 ·058 ·052 ·045 ·039 ·032 ·026 ·013 ·006	33 31 29 27 25 23 22 20 18 17 15 13 12 11 9 8 7 5 4 2 2	155 148 142 135 129 122 115 109 102 096 089 082 076 069 063 056 049 043 037 030 023 017	34 32 30 28 27 25 23 21 20 18 17 15 14 12 11 10 8 7 6 5 4 3 2	166 160 153 147 140 133 127 120 114 107 101 094 087 081 074 068 061 054 048 041 028 022 015 008	36 34 32 30 28 26 25 23 21 20 18 16 15 14 11 10 9 7 6 5 4 3 2

neit.		D	EGREES	OF TH	IE WET	BULB ?	THERMO:	METER	—FAHRI	ENHEIT		
ahren	47	10	48	0	49	0	50	0	51	0	52	,0
t — t' Fahrenheit.	Force of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	. Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c c} 0^{\circ} & & \\ \hline 1^{2} & & \\ 1 & 1^{\frac{1}{2}} & \\ 2 & & \\ 2^{\frac{1}{2}} & \\ 3 & & \\ 3^{\frac{1}{2}} & \\ 4 & \\ 4^{\frac{1}{2}} & \\ \end{array}$	•323 •316 •310 •303 •297 •290 •283 •277 •270 •264	100 96 92 89 85 82 78 75 72 69	·335 ·329 ·322 ·315 ·309 ·302 ·296 ·289 ·282 ·276	100 96 92 89 85 82 79 76	*348 *341 *335 *328 *321 *315 *308 *302 *295	100 96 93 89 86 83 79 76 73	361 354 348 341 334 328 321 315 308 301	100 96 93 89 86 83 80 77 74 71	·374 ·368 ·361 ·354 ·348 ·341 ·335 ·328 ·321	100 96 93 90 86 83 80 77 74	·388 ·382 ·375 ·369 ·362 ·355 ·349 ·342 ·336	100 96 93 90 87 84 81 78 75 72
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	204 ·257 ·251 ·244 ·237 ·231 ·224 ·218 ·211 ·204	66 63 60 58 55 52 50 48 45	·276 ·269 ·263 ·256 ·249 ·243 ·236 ·230 ·223 ·216	70 67 64 61 59 56 53 51 49 46	.288 .282 .275 .269 .262 .255 .249 .242 .236 .229	70 67 65 62 59 57 54 52 50 47	·295 ·288 ·282 ·275 ·268 ·262 ·255 ·249 ·242	68 65 63 60 58 55 53 51 48	·315 ·308 ·302 ·295 ·288 ·282 ·275 ·269 ·262 ·255	71 69 66 63 61 58 56 54 51 49	-329 -322 -316 -309 -302 -296 -289 -283 -276 -269	69 67 64 61 59 57 54 52 50
$\begin{array}{c c} 9\frac{1}{2} \\ 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \\ 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array}$	198 191 185 178 171 165 158 152 145	43 41 39 37 35 33 31 29 27	·210 ·203 ·197 ·190 ·183 ·177 ·170 ·164 ·157	44 42 40 38 36 34 32 30 29	·222 ·216 ·209 ·203 ·196 ·189 ·183 ·176 ·170	45 43 41 39 37 35 33 32 30	·235 ·229 ·222 ·216 ·209 ·202 ·196 ·189 ·182	46 44 42 40 38 36 35 33 31	·249 ·242 ·235 ·229 ·222 ·216 ·209 ·203 ·196	47 45 43 41 39 37 36 34 32	·263 ·256 ·249 ·248 ·236 ·230 ·223 ·216 ·210	48 46 44 42 40 38 37 35 33
$\begin{array}{ c c c }\hline 14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2} \\ 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \\ \end{array}$	·138 ·132 ·125 ·119 ·112 ·106 ·099 ·092	26 24 22 21 19 18 16 15	·150 ·144 ·137 ·131 ·124 ·118 ·111 ·104	27 25 24 22 21 19 18 16	·163 ·156 ·150 ·143 ·137 ·130 ·123 ·117	28 27 25 23 22 21 19 18	·176 ·169 ·163 ·156 ·149 ·143 ·136 ·130	29 28 26 25 23 22 21 19	·189 ·183 ·176 ·169 ·163 ·156 ·150 ·143	31 29 27 26 25 23 22 20	203 -197 -190 -183 -177 -170 -163 -157	32 30 29 27 26 24 23 22
$\begin{array}{c c} 18 \\ 18 \\ 19 \\ 19 \\ 19 \\ 20 \\ 20 \\ 21 \\ 21 \\ 22 \\ 22 \end{array}$	.086 .079 .073 .066 .059 .053 .046 .040	14 12 11 10 9 8 7 6 4	.098 .091 .085 .078 .071 .065 .058 .052	15 14 13 11 10 9 8 7 6	·110 ·104 ·097 ·090 ·084 ·077 ·071 ·064 ·057	17 15 14 13 12 11 10 8 7	123 116 110 103 097 090 083 077	18 17 15 14 13 12 11 10 9	.136 .130 .123 .117 .110 .103 .097 .090 .083	19 18 17 16 14 13 12 11 10	150 ·144 ·137 ·130 ·124 ·117 ·110 ·104 ·097	20 19 18 17 16 15 13 12 11
$\begin{bmatrix} 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \\ 24\frac{1}{2} \\ 24\frac{1}{2} \\ 25 \end{bmatrix}$	·027 ·020 ·013 ·007 ·001	3 2 2 1 0	038 032 025 019 012 005	4 4 3 2 1 0	·057 ·051 ·044 ·038 ·031 ·024 ·018	6 5 5 4 3 2	•070 •064 •057 •050 •044 •037 •030	8 7 6 5 4 3	.083 .077 .070 .064 .057 .050 .044	9 8 7 6 6 5	·097 ·091 ·084 ·077 ·071 ·064 ·057	11 10 10 9 8 7 6

eit.		1	EGREES	OF TI	IE WET	BULB	THERMO	METER	R.—FAHR	ENHEI	r.	
— t' Fahrenheit.	53	0	54	0	55	,0	.56	0	57	70	58	0
t — t' F	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•403	100	·418	100	·433	100	·449	100	•466	100	•483	100
	•396	96	·411	97	·427	97	·443	97	•459	97	•476	97
	•390	93	·405	94	·420	94	·436	94	•452	94	•469	94
	•383	90	·398	90	·413	90	·429	91	•446	91	•462	91
$ \begin{array}{c c} 2 \\ 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \end{array} $	•376	87	·391	87	·407	87	·423	88	·489	88	•456	88
	•370	84	·385	84	·400	84	·416	85	·433	85	•449	85
	•363	81	·378	81	·394	82	·410	82	·426	82	•442	83
	•357	78	·372	78	·387	79	·403	79	·419	80	•436	80
4	·350	75	·365	76	·380	76	•396	76	·413	77	·429	77
4½	·343	72	·358	73	·374	73	•390	74	·406	74	·422	75
5	·337	70	·352	70	·367	71	•383	71	·399	72	·416	72
5½	·330	67	·345	68	·360	68	•376	69	·392	69	·409	70
$\begin{array}{c c} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \end{array}$	·323	65	•338	65	·354	66	•370	66	·386	67	•403	67
	·317	62	•332	63	·347	64	•363	64	·379	65	•396	65
	·310	60	•325	61	·340	61	•356	62	·373	62	•389	63
	·304	57	•319	58	·334	59	•350	60	·366	60	•383	61
8	·297	55	*312	56	·327	57	·343	57	·359	58	·376	59
8½	·290	53	*305	54	·321	55	·337	55	·353	56	·369	56
9	·284	51	*299	52	·314	53	·330	53	·346	54	·362	55
9½	·277	49	*292	50	·307	51	·323	51	·340	52	·356	53
$ \begin{array}{c c} 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \end{array} $	·270	47	•285	48	·301	49	*316	49	·333	50	·349	51
	·264	45	•279	46	·294	47	*310	48	·326	48	·343	49
	·257	43	•272	44	·287	45	*303	46	·319	47	·336	47
	·251	41	•265	42	·281	43	*296	44	·313	45	·329	46
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	·244	39	•259	40	·274	41	·290	42	·306	43	·323	44
	·237	38	•252	39	·268	40	·283	41	·300	41	·316	42
	·231	36	•246	37	·261	38	·277	39	·293	40	·309	41
	·224	34	•239	35	·254	36	·270	37	·286	38	·303	39
14	·218	33	•232	34	·248	35	•263	36	·280	37	·296	38
14½	·211	31	•226	32	·241	33	•257	34	·273	35	·289	36
15	·204	30	•219	31	·234	32	•250	33	·266	34	·283	35
15½	·198	28	•212	29	·228	30	•243	31	·259	32	·276	33
$ \begin{array}{ c c c c c } \hline 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \\ \hline 18 \\ \end{array} $	·191	27	·206	28	·221	29	·237	30	·253	31	·270	32
	·184	25	·199	27	·214	28	·230	29	·246	30	·263	31
	·178	24	·193	25	·208	26	·223	27	·240	28	·256	29
	·171	23	·186	24	·201	25	·217	26	·233	27	·249	28
$ \begin{array}{c c} 18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \\ 20 \end{array} $	·165 ·158 ·151 ·145	22 20 19 18	·179 ·173 ·166 ·160	23 22 20 19	·195 ·188 ·181 ·175 ·168	24 23 22 20	·210 ·204 ·197 ·190	25 24 23 21	·226 ·220 ·213 ·207	26 25 24 22	·243 ·236 ·229 ·223 ·216	27 26 25 23 22
$ \begin{array}{ c c c c c } \hline 20 \\ 20 \\ 21 \\ 21 \\ 22 \end{array} $	·138 ·131 ·125 ·118 ·112	17 16 15 14 13	·153 ·146 ·139 ·133 ·126	18 17 16 15	·168 ·161 ·155 ·148	19 18 17 16 15	·183 ·177 ·170 ·164 ·157	20 19 18 17 16	·200 ·193 ·186 ·180 ·173	21 20 19 18 17	·216 ·210 ·203 ·196 ·190	21 20 19 18
$ \begin{array}{c c} 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \\ 24 \end{array} $	·105 ·098 ·092 ·085	12 11 10	·120 ·120 ·113 ·106 ·100	13 12 11 10	·135 ·128 ·122 ·115	14 13 12 12	·157 ·150 ·144 ·137 ·131	15 14 14 14	·167 ·160 ·153 ·147	16 16 15	·183 ·176 ·169	18 17 16 15
24 241 25	·079 ·072	9 8 7	·100 ·093 ·086	10 10 9	·108 ·101	11 11 10	·131 ·124 ·117	12 11	·147 ·140 ·133	14 13 12	·163 ·156 ·150	16 14 13

eit.		D	EGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEI	Γ.	
U Fahrenheit.	59	0	60	0	. 61	0	62	30	68	0	64	f <sub>o</sub>
t - V E	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 12 1 1 1 1 2	·500	100.	·518	100	•537	100	•556	100	·576	100	·596	100
	·493	97	·511	97	•530	97	•549	97	·569	97	·590	97
	·487	94	·505	94	•523	94	•543	94	·563	94	·583	94
	·480	91	·498	91	•517	91	•536	92	·556	92	·576	92
$\begin{bmatrix} 2 \\ 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \end{bmatrix}$	·473	88	·491	88	·510	88	·529	89	•549	89	•570	89
	·466	85	·485	86	·503	86	·523	86	•542	87	•563	87
	·460	83	·478	83	·497	83	·516	84	•586	84	•556	84
	·453	80	·471	81	·490	81	·509	81	•529	82	•550	82
$ \begin{array}{c c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \end{array} $	·446	77	•464	77	·483	78	·502	78	•522	79	•543	79
	·440	75	•458	75	·476	75	·496	77	•516	77	•536	77
	·433	78	•451	73	·470	73	·489	75	•509	75	•529	75
	·427	71	•444	71	·463	71	·483	72	•502	72	•523	72
$\begin{bmatrix} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \\ 9 \end{bmatrix}$	·420 ·413 ·407 ·400	68 66 63 61	·438 ·431 ·425 ·418	68 66 64 62	·457 ·450 ·443 ·437	69 67 65 63	·476 ·469 ·462 ·456	69 67 65 63 61	·496 ·490 ·482 ·476 ·469	70 68 66 64 62	*516 *509 *503 *496 *489	70 68 66 64 62
8 8½ 9 9½	•393 •386 •380 •373	59 57 56 54	·411 ·405 ·398 ·391	50 58 56 54	·430 ·423 ·416 ·410	61 59 57 55	·449 ·442 ·436 ·429 ·422	59 57 55 54	·462 ·455 ·449	60- 58 56	·483 ·476 ·469	61 59 57 56
10 10½ 11 11½	*367 *360 *353 *347	52 50 48 . 46	·385 ·378 ·371 ·365	53 51 49 47	·403 ·397 ·390 ·383	54 52 50 48	·416 ·409 ·402	52 50 49 48	·442 ·436 ·429 ·422	55 53 51 49	•463 •456 •449 •443	54 52 50 49
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	*340 *333 *327 *320	45 43 42 40	·358 ·351 ·345 ·338	46 44 42 41	•376 •370 •363 •356	47 45 43 42	·396 ·389 ·382 ·376	46 44 42	·415 ·409 ·402 ·395	48 46 45 43	•436 •429 •422 •416	47 46 44
$ \begin{array}{c c} 14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2} \end{array} $	·313	39	•331	39	·350	40	*369	41	·389	42	·409	43
	·306	37	•324	38	·343	39	*362	40	·382	40	·402	41
	·300	36	•318	37	·336	37	*356	38	·375	39	·396	40
	·293	35	•311	35	·330	36	*349	37	·369	38	·389	39
$ \begin{array}{c c} 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \end{array} $	·287	33	·305	34	*323	35	·342	36	·362	36	·382	37
	·280	32	·298	33	*316	34	·336	34	·355	35	·376	36
	·273	30	·291	31	*310	32	·329	33	·349	34	·369	35
	·267	29	·285	30	*303	31	·322	32	·342	33	·362	34
18	·260	28	·278	29	·296	30	·315	31	·335	32	·355	32
18½	·253	27	·271	28	·290	29	·309	30	·328	30	·349	31
19	·247	26	·264	27	·283	28	·302	28	·322	29	·342	30
19½	·240	25	·258	26	·276	26	·295	27	·315	28	·335	29
$ \begin{array}{c c} 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \end{array} $	·234	23	·251	24	·270	25	·289	26	·308	27	·329	28
	·227	22	·245	23	·263	24	·282	25	·302	26	·322	27
	·220	21	·238	22	·256	23	·275	24	·295	25	·315	26
	·213	20	·231	21	·250	22	·269	23	·288	24	·309	25
$ \begin{array}{c c} 22 \\ 221 \\ 23 \\ 231 \\ 24 \end{array} $	·207	19	·225	21	·243	22	·262	22	·282	23	·302	24
	·200	19	·218	20	·236	21	·255	22	·275	22	·295	23
	·193	18	·211	19	·230	20	·249	21	·268	22	·289	22
	·187	17	·205	18	·223	19	·242	20	·262	21	·282	22
$\begin{bmatrix} 24 \\ 24\frac{1}{2} \\ 25 \end{bmatrix}$	·180	16	·198	17	·216	18	·234	19	·255	20	·275	21
	·173	15	·191	16	·209	17	·228	18	·248	19	·268	20
	·167	14	·185	15	·203	16	·222	17	·241	18	·262	19

it.		D	EGREES	OF TH	E WET	BULB 1	HERMO	METER.	—FAHRI	ENHEIT		
— t' Fahrenheit.	65	0	66	0	67	•	68	0	69	0	70	0
t - t E	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of . Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$ \begin{array}{c c} 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \end{array} $	·618	100	·639	100	·662	100	·685	100	·708	.100	·733	100
	·611	97	·633	97	·655	97	·678	97	·702	97	·726	97
	·604	94	·626	95	·648	95	·671	95	·695	95	·720	95
	·598	92	·619	92	·642	92	·665	92	·688	92	·713	92
$\frac{2}{2\frac{1}{2}}$ $\frac{3}{3\frac{1}{2}}$	•591	89	·612	90	·635	90	·658	90	·682	90	·706	90
	•584	87	·606	88	·628	88	·651	88	·675	88	·700	88
	•577	85	·599	85	·621	85	·644	86	·668	86	·693	85
	•571	82	·592	83	·615	83	·638	83	·662	83	·686	83
$ \begin{array}{c c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \end{array} $	·564	79	•586	80	·608	80	·631	81	·655	81	·680	81
	·557	77	•579	78	·601	78	·624	79	·648	79	·673	79
	·551	75	•572	76	·595	76	·617	77	·641	77	·666	77
	·544	73	•566	74	·588	74	·611	75	·635	75	·659	75
$ \begin{array}{ c c c c c } \hline                                    $	•537	71	·559	72	·581	72	·604	73	·628	73	•652	73
	•530	69	·552	70	·574	70	·597	71	·621	71	•646	71
	•524	66	·545	67	·568	67	·591	68	·614	68	•639	69
	•517	64	·539	65	·561	65	·584	66	·608	67	•632	67
$ \begin{array}{c c} 8 \\ 8\frac{1}{2} \\ 9 \\ 9\frac{1}{2} \end{array} $	·510	63	•532	63	•554	64	·577	64	·601	65	·626	65
	·504	61	•525	61	•548	62	·571	63	·594	63	·619	64
	·497	• 59	•519	60	•541	60	·564	61	·588	62	·612	62
	·490	58	•512	58	•534	59	·557	59	·581	60	·606	60
$ \begin{array}{ c c c c c } \hline                                    $	·484	56	·505	56	·527	57	·550	58	·574	58	·599	59
	·477	54	·498	55	·521	55	·544	56	·567	57	·592	57
	·470	52	·492	53	·514	54	·537	54	·561	55	·585	56
	·463	51	·485	52	·507	52	·530	53	·554	53	·578	54
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	·457	49	·478	50	·501	51	·523	51	•547	52	·572	52
	·450	48	·472	48	·494	49	·517	50	•541	50	·565	51
	·443	46	·465	47	·487	48	·510	48	•534	49	·558	50
	·437	45	·458	46	·481	46	·503	47	•527	48	·552	48
$ \begin{array}{ c c c c } \hline 14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2} \end{array} $	·430	43	·452	44	·474	45	·497	45	*520	46	•545	47
	·423	42	·445	43	·467	43	·490	44	*514	45	•538	45
	·417	41	·438	41	·460	42	·483	43	*507	43	•531	44
	·410	39	·432	40	·454	41	·476	42	*500	42	•525	43
$ \begin{array}{ c c c c } \hline 16 \\ 16 \\ 17 \\ 17 \\ \hline 17 \\ \hline 2 \end{array} $	·403 ·396 ·390 ·383	38 37 36 34	·425 ·417 ·410 ·404	39 38 36 35	·447 ·440 ·433 ·427	38 37 36	·470 ·463 ·456 ·450	40 39 38 37	·493 ·487 ·480 ·473	41 40 39 38	•518 •511 •504 •498	42 41 39 38
$ \begin{array}{c c} 18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \end{array} $	•376	33	·397	34	·420	35	·443	36	·467	36	·491	37
	•370	32	·390	33	·413	34	·436	35	·460	35	·484	36
	•363	31	·384	32	·407	33	·429	33	·453	34	·478	35
	•356	30	·377	31	·400	32	·423	32	·446	33	·471	34
$ \begin{array}{ c c c c c } \hline 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \end{array} $	·350	29	·371	30	•393	31	·416	31	·440	32	·464	33
	·343	28	·364	29	•386	30	·409	30	·433	31	·457	32
	·336	27	·358	28	•380	29	·403	29	·426	30	·451	31
	·330	26	·351	27	•373	28	·396	29	·419	29	·444	30
$ \begin{array}{c c} 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \end{array} $	·323	25	·344	26	·366	27	·389	28	·413	28	·437	29
	·316	24	·338	25	·360	26	·382	27	·406	28	·430	28
	·309	24	·331	24	·353	25	·376	26	·399	27	·424	27
	·303	23	·324	23	·346	24	·369	25	·393	26	·417	27
$ \begin{array}{ c c c c c } \hline 24 \\ 241 \\ 25 \end{array} $	·296	22	·317	23	·340	23	·362	24	·386	25	·410	26
	·289	21	·311	22	·333	23	·356	23	·379	24	·404	25
	·283	20	·304	21	·326	22	·349	22	·372	23	·397	24

eit		D	EGREES	OF TH	E WET	BULB	THERMO	METER	.—FAHR	ENIIEIT		
- t' Fahrenheit.	71	Lº	17:	0	78	80	7.1	0	75	0	76	30
t-t/E	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, iu inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vaper, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 2	·759	100	·785	100	·812	100	·839	100	·868	100	·897	100
	·752	98	·778	98	·805	98	·833	98	·861	98	·890	98
	·745	95	·771	95	·798	95	·826	95	·854	95	·884	95
	·739	93	·765	93	·792	93	·819	93	·847	93	·877	93
21 12 3 12 3 12	·732	90	·758	90	·785	90	·812	91	·841	91	•870	91
	·725	88	·751	88	·778	88	·805	88	·834	88	•863	89
	·718	86	·745	86	·772	86	·799	86	·827	86	•856	87
	·712	83	·738	84	·765	84	·792	84	·820	84	•850	85
$ \begin{array}{c c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \end{array} $	·705	81	·731	81	·758	82	·785	82	·813	82	*843	83
	·698	79	·725	79	·751	80	·778	80	·807	80	*836	81
	·691	77	·717	77	·744	78	·772	78	·800	78	*829	79
	·685	75	·711	75	·738	76	·765	76	·793	76	*823	77
$\begin{bmatrix} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \end{bmatrix}$	·678	73	·704	73	·731	74	·758	74	·787	74	·816	75
	·671	71	·697	71	·724	72	·751	72	·780	73	·809	74
	·664	69	·691	69	·717	70	·745	70	·773	71	·802	72
	·658	67	·684	.67	·711	68	·738	69	·766	69	·795	70
8	·651	66	·677	66	·704	66	·731	67	·759	67	·789	68
8½	·644	64	·670	64	·697	65	·724	65	·753	66	·782	67
9	·638	62	·664	62	·691	63	·717	64	·746	64	·775	65
9½	·631	61	·657	61	·684	61	·711	62	·789	62	·768	63
$ \begin{array}{c c} 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \end{array} $	·624 ·617 ·610 ·604	59 58 56 54	·650 ·643 ·637 ·630	59 58 56 54	·677 ·670 ·663 ·657	58 57 55	·704 ·698 ·691 ·684	59 57 56	·783 ·726 ·719 ·712	59 58 56	·762 ·755 ·748 ·741	62 60 59 57
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	·597	53	·623	53	·650	54	·677	54	·705	55	·735	56
	·590	51	·616	51	·643	52	·670	53	·699	54	·728	55
	·584	50	·610	50	·637	51	·664	52	·692	52	·721	53
	·577	49	·603	49	·630	50	·657	50	·685	51	·714	52
$ \begin{array}{c c} 14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2} \end{array} $	·570	47	•596	47	·623	48	•650	49	·678	50	·707	51
	·564	46	•590	46	·616	47	•643	48	·671	48	·701	49
	·557	45	•583	45	·609	46	•637	47	·665	47	·694	48
	·550	43	•576	43	·603	45	•630	45	·658	46	·687	47
$ \begin{array}{c c} 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \end{array} $	·543	42	•569	42	•596	43	•623	44	·651	45	·680	46
	·536	41	•562	41	•589	42	•616	43	·645	44	·674	45
	·530	40	•556	40	•582	41	•610	42	·638	42	·667	43
	·523	39	•549	39	•576	40	•603	41	·631	41	·660	42
$ \begin{array}{c c} 18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \end{array} $	·516	38	•542	38	•569	39	•596	40	·624	40	·653	41
	·510	37	•536	37	•562	38	•589	39	·617	39	·646	40
	·503	36	•529	36	•556	37	•582	38	·611	38	·640	39
	·496	35	•522	35	•549	36	•576	37	·603	37	·633	38
$ \begin{array}{c c} 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \end{array} $	·489	34	•515	34	·542	35	*569	36	·597	36	*626	37
	·482	33	•508	33	·535	34	*562	35	·591	35	*620	36
	·476	32	•502	32	·528	33	*556	34	·584	34	*613	35
	·469	31	•495	31	·522	32	*549	33	·577	33	*606	34
22	·462	30	·488	31	•515	31	·542	32	·570	33	•599	33
22½	·456	29	·482	30	•508	30	·535	31	·563	32	•592	32
23	·449	28	·475	29	•502	29	·528	30	·557	31	•586	31
23½	·442	27	·468	28	•495	28	·522	29	·550	30	•579	30
$ \begin{array}{c c}  & 24 \\  & 24\frac{1}{2} \\  & 25 \end{array} $	·436	26	·461	27	·488	28	•515	28	·543	29	•572	29
	·429	26	·455	26	·481	27	•508	27	·586	28	•565	28
	·422	25	·448	25	·474	26	•502	26	·530	27	•559	27

beit.		D	EGREES	OF TI	IE WET	BULB	THERMO	)METEI	R.—FAHR	ENHEI	т.	
V Fahrenheit.	77	70	78	0	79	0	80	0	81	0	S	<b>2</b> °
t-1	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$ \begin{array}{c c} 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2 \end{array} $	·927 ·920 ·914 ·907 ·900	100 98 95 93 91	·958 ·951 ·945 ·938 ·931	100 98 95 93 91	·990 ·984 ·977 ·970 ·963	100 98 96 93 91	1.023 1.017 1.010 1.003 .996	100 98 96 93 91	1.057 1.050 1.044 1.037 1.030	100 98 96 93 91	1·092 1·085 1·079 1·072 1·065	100 98 96 94 91
$ \begin{array}{c c} 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \\ 4 \end{array} $	·893 ·886 ·880 ·873	89 87 85 83	•924 •918 •911 •904	89 87 85 83	•956 •950 •943 •936	89 87 85 83	·989 ·983 ·976 ·969	89 87 85 83	1.023 1.016 1.010 1.003	89 87 85 83	1.058 1.051 1.045 1.038	89 87 86
$ \begin{array}{c c}  & 4\frac{1}{2} \\  & 5 \\  & 5\frac{1}{2} \\  & 6 \end{array} $	·866 ·859 ·853 ·846	81 79 77 75	·897 ·891 ·884 ·877	81 79 77 75	·929 ·923 ·916 ·909	81 79 77 75	·962 ·955 ·949 ·942	81 79 78 76	•996 •989 •982 •976	81 80 78 76	1.031 1.024 1.017 1.010	84 82 80 78
$ \begin{array}{c c} 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \\ 8 \end{array} $	·839 ·832 ·825	73 72 70 68	·870 ·863 ·857 ·850	73 72 70 68	*902 *895 *889 *882	74 72 70 69	•935 •928 •921 •915	74 72 71 69	•969 •962 •955 •948	74 73 71 69	1.004 .997 .990 .983	76 75 73 71 70
8½ 9 9½ 10	·812 ·805 ·798 ·792	67 65 63 62	·843 ·836 ·829 ·823	67 65 63 62	·875 ·868 ·861 ·855	67 66 64 62	·908 ·901 ·894 ·887	68 66 64 63	•942 •935 •928 •921	68 66 65	·976 ·970 ·963 ·956	68 67 65 64
$ \begin{array}{c c} 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \\ 12 \end{array} $	·785 ·778 ·771 ·764	60 59 57 56	·816 ·809 ·802 ·796	60 59 57 56	·848 ·841 ·834 ·827	61 60 58 57	·881 ·874 ·867 ·860	61 60 59 57	•914 •908 •901 •894	62 60 59 58	·949 ·942 ·936 ·929	62 61 59 58
$ \begin{array}{c c} 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \\ 14 \end{array} $	·758 ·751 ·744 ·737	55 53 52 51	·789 ·782 ·775 ·768	55 53 52 51	·821 ·814 ·807 ·800	56 54 53 52	·854 ·847 ·840 ·833	56 55 53 52	·887 ·880 ·874 ·867	56 55 54 53	•922 •915 •908 •902	57 56 54 53
$ \begin{array}{ c c c c } \hline 141\\ 15\\ 15\frac{1}{2}\\ \hline 16\\ \end{array} $	·731 ·724 ·717	49 48 47 46	·762 ·755 ·748 ·741	50 48 47 46	·793 ·787 ·780 ·773	50 49 48 47	·826 ·820 ·813 ·806	51 50 49 47	·860 ·853 ·846 ·840	51 50 49	·895 ·888 ·881	52 51 50
$\begin{array}{ c c c }\hline 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \\ \end{array}$	·704 ·697 ·690	45 44 42	·734 ·728 ·721	45 44 43 42	·766 ·760 ·753	46 45 44	·799 ·792 ·786	46 45 44	·833 ·826 ·819	48 47 46 45	·874 ·867 ·861 ·854	48 47 46 45
$ \begin{array}{c c} 18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \\ 20 \end{array} $	·683 ·676 ·670 ·663	41 40 39 38	·714 ·707 ·700 ·694	41 40 39	·746 ·739 ·732 ·726	43 42 41 40	·779 ·772 ·765 ·758	43 42 41 40	·812 ·806 ·799 ·792	44 43 42 41	·847 ·840 ·833 ·827	44 43 42 41
$ \begin{array}{c c} 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \end{array} $	·656 ·649 ·643 ·636	37 36 36 35	·687 ·680 ·673 ·667	38 37 36 35	·719 ·712 ·705 ·698	39 38 37 36	·752 ·745 ·738 ·731	39 38 37 36	·785 ·778 ·772 ·765	40 39 38 37	·820 ·813 ·806 ·799	40 39 38 38
22 22½ 23 23½	·629 ·622 ·615 ·609	34 33 32 31	·660 ·653 ·646 ·639	34 33 33 32	·692 ·685 ·678 ·671	35 34 33 32	·724 ·718 ·711 ·704	35 35 34 33	·758 ·751 ·744 ·738	36 35 34 34	·793 ·786 ·779 ·772	37 36 35 34
$ \begin{array}{ c c c c c } \hline     24 \\     24 \\     \hline     25 \\ \hline \end{array} $	·602 ·595 ·588	30 29 28	·633 ·626 ·619	31 30 29	·664 ·658 ·651	32 31 30	·697 ·690 ·684	32 31 30	·731 ·724 ·717	33 32 31	·765 ·759 ·752	33 32 31

eit.		D	EGREES	OF TI	IE WET	BULB	гнекмо	METER	.—FAHR	ENHEI	r.	
ahrenh	83	0	84	Į°	<b>S</b> 5	0	80	°	87	10	88	30
t _ t Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{bmatrix} 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2 \\ 2\frac{1}{2} \\ 3 \end{bmatrix}$	1·128 1·121 1·114 1·108 1·101 1·094	100 98 96 94 91 90	1·165 1·158 1·151 1·145 1·138 1·131	100 98 96 94 92 90	1·203 1·196 1·189 1·183 1·176 1·169	100 98 96 94 92 90	1·242 1·235 1·228 1·222 1·215 1·208	100 98 96 94 92 90	1·282 1·275 1·269 1·262 1·255 1·249	100 98 96 94 92 90	1·324 1·317 1·310 1·303 1·296 1·290	100 98 96 94 92 90
$egin{array}{cccccccccccccccccccccccccccccccccccc$	1.087 1.080 1.074 1.067 1.060 1.053 1.046	88 86 84 82 80 78	1·124 1·117 1·111 1·104 1·097 1·090	88 86 84 82 80 79 77	1·162 1·155 1·149 1·142 1·135 1·128 1·121	88 86 84 82 80 79 77	1·201 1·194 1·188 1·181 1·174 1·167 1·160	88 86 84 82 81 79 77	$ \begin{array}{c cccc} 1 \cdot 241 \\ 1 \cdot 235 \\ 1 \cdot 228 \\ 1 \cdot 221 \\ 1 \cdot 214 \\ 1 \cdot 207 \\ 1 \cdot 200 \end{array} $	88 86 84 83 81 79 78	$ \begin{array}{c c} 1.283 \\ 1.276 \\ 1.269 \\ 1.262 \\ 1.255 \\ 1.248 \\ 1.242 \end{array} $	88 86 85 83 81 79 78
$ \begin{array}{c c} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \\ 8 \\ 8\frac{1}{2} \\ 9 \end{array} $	1.039 1.033 1.026 1.019 1.012 1.005	75 73 72 70 69 67	1.083 1.076 1.070 1.063 1.056 1.049 1.042	75 74 72 70 69 67	1·114 1·108 1·101 1·094 1·087 1·080	75 74 72 71 69 68	1·153 1·146 1·140 1·133 1·126 1·119	76 74 72 71 69 68	1·193 1·187 1·180 1·173 1·166 1·159	76 74 73 71 70 68	$\begin{array}{c} 1.235 \\ 1.228 \\ 1.221 \\ 1.214 \\ 1.208 \\ 1.201 \end{array}$	76 75 73 72 70 69
$ \begin{array}{c c} 9\frac{1}{2} \\ 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \\ 12 \end{array} $	•999 •992 •985 •978 •971 •965	66 64 63 61 60 58	1.036 1.029 1.022 1.015 1.008	66 64 63 62 60 59	1.074 1.066 1.060 1.053 1.046 1.039	66 65 63 62 61 59	1·112 1·105 1·099 1·092 1·085 1·078	66 65 64 62 61 60	1·153 1·145 1·139 1·132 1·125 1·118	67 65 64 63 61 60	1·194 1·187 1·180 1·173 1·166 1·159	67 66 64 63 61 60
12½ 13 13½ 14 14½ 15 15½	•958 •951 •944 •937 •931 •924 •917	57 56 55 54 52 51 50	•995 •998 •981 •974 •967 •960 •954	58 56 55 54 53 52 50	1.032 1.026 1.019 1.012 1.005 .998 .991	58 57 56 55 53 52 51	1.071 1.065 1.058 1.051 1.044 1.037 1.030	58 57 56 55 54 52 51	1·111 1·105 1·098 1·091 1·084 1·077 1·070	59 57 56 55 54 53 52	1.153 1.146 1.139 1.132 1.125 1.118 1.111	59 58 57 56 54 53 52
$ \begin{array}{ c c c c } \hline     16 \\     16 \\     17 \\     17 \\     17 \\     18 \\ \hline \end{array} $	·910 ·903 ·896 ·890 ·883	49 48 47 46 45	•947 •940 •933 •926 •920	49 48 47 46 45	·985 ·978 ·971 ·964 ·957	50 49 48 47 46	1.023 1.017 1.010 1.003 .996 .989	50 49 48 47 46 45	1.063 1.057 1.050 1.043 1.036 1.029	51 50 49 48 47 46	1·105 1·098 1·091 1·084 1·077 1·071	51 50 49 48 47 46
$ \begin{array}{c c} 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \\ 20 \\ 20\frac{1}{2} \\ 21\frac{1}{2} \end{array} $	*876 *869 *862 *855 *849 *842 *835	44 43 42 41 40 39 38	•913 •906 •899 •892 •885 •879 •872	44· 43 42 41 40 39 38	•951 •944 •937 •930 •923 •916 •910	45 44 43 42 41 40 39	•983 •976 •969 •962 •955 •948.	44 43 42 41 41	1.029 1.023 1.016 1.009 1.002 .995 .988	45 44 43 42 41 40	1.064 1.057 1.050 1.043 1.036 1.029	45 44 43 42 41 41
$ \begin{array}{c c} 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \\ 24 \end{array} $	-828 -821 -815 -808 -800	37 36 *35 34 34	-865 -858 -851 -845 -838	38 37 36 35 34	.903 .896 .889 .882	38 37 37 36 35	·942 ·935 ·928 ·921 ·914	39 38 37 36 36	·981 ·975 ·967 ·961 ·954 ·947	39 38 38 37 36 35	1.023 1.016 1.009 1.002 .995 .989	40 39 38 37 37 36
$\begin{bmatrix} 24\frac{1}{2} \\ 25 \end{bmatrix}$	·794 ·787	33 32	·831 ·824	33	·869 ·862	34 33	·908 ·900	35 34	947	35 35	989	35 35

eit.		· I	EGREES	OF TI	IE WET	BULB	THERMO	METEI	.—FAHR	ENHEI	r.	
ahrenh	89	0	90	0	91	0	92	0	93	°	94	o
t — t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.										
0° 1/2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1·366	100	1·410	100	1·455	100	1·501	100	1.548	100	1·597	100
	1·359	98	1·403	98	1·448	98	1·494	98	1.541	98	1·590	98
	1·352	96	1·396	96	1·441	96	1·487	96	1.535	96	1·583	96
	1·346	94	1·389	94	1·434	94	1·480	94	1.528	94	1·576	94
$ \begin{array}{c c} 2 \\ 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \end{array} $	1·339	92	1·382	92	1·427	92	1·473	92	1.521	92	1.569	92
	1·332	90	1·375	90	1·420	90	1·466	90	1.514	91	1.562	91
	1·325	88	1·368	88	1·413	88	1·459	89	1.507	89	1.556	89
	1·318	86	1·362	86	1·406	87	1·453	87	1.500	87	1.549	87
$\begin{array}{ c c c }\hline & 4 & \\ & 4\frac{1}{2} & \\ & 5 & \\ & 5\frac{1}{2} & \\ \hline \end{array}$	1·311	85	1.355	85	1·400	85	1.446	85	1.493	85	1.542	85
	1·304	83	1.348	83	1·393	83	1.439	83	1.486	84	1.535	84
	1·298	81	1.341	81	1·386	82	1.432	82	1.479	82	1.528	82
	1·291	80	1.334	80	1·379	80	1.425	80	1.473	80	1.521	80
$ \begin{array}{ c c c c } \hline 6 & 6\frac{1}{2} \\ 7 & 7\frac{1}{2} \end{array} $	1.284	78	1·327	78	1·372	78	1·418	79	1.466	79	1.514	79
	1.277	77	1·321	77	1·365	77	1·411	77	1.459	77	1.507	77
	1.270	75	1·314	75	1·358	75	1·405	75	1.452	76	1.500	76
	1.263	73	1·307	74	1·352	74	1·398	74	1.445	74	1.493	74
8	1.256	72	1·300	72	1.345	72	1·391	73	1·438	73	1·487	73
8½	1.249	70	1·293	71	1.338	71	1·384	71	1·431	71	1·480	72
9	1.243	69	1·286	69	1.331	69	1·377	70	1·424	70	1·473	70
9½	1.236	67	1·279	68	1.324	68	1·370	68	1·417	69	1·466	69
$ \begin{array}{c c} 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \end{array} $	1·229	66	1·273	66	1·317	67	1.363	67	1·411	67	1·459	67
	1·222	65	1·266	65	1·311	65	1.356	65	1·404	66	1·452	66
	1·215	64	1·259	64	1·304	64	1.350	64	1·397	65	1·445	65
	1·208	62	1·252	62	1·297	63	1.343	63	1·390	63	1·439	64
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	1·202	61	1·245	61	1·290	61	1.336	62	1·383	62	1·432	62
	1·195	59	1·238	60	1·283	60	1.329	60	1·376	61	1·425	61
	1·188	58	1·231	59	1·276	59	1.322	59	1·369	60	1·418	60
	1·181	57	1·224	57	1·269	58	1.315	58	1·363	59	1·411	59
14	1·174	56	1·217	56	1·262	57	1·308	57	1.356	58	1·404	58
14½	1·167	55	1·211	55	1·255	56	1·301	56	1.349	56	1·397	57
15	1·161	54	1·204	54	1·249	54	1·295	55	1.342	55	1·390	56
15½	1·154	53	1·197	53	1·242	53	1·288	54	1.335	54	1·383	55
16	1.147	51	1·190	52	1.235	52	1.281	53	1·328	53	1·377	54
161	1.140	50	1·183	51	1.228	51	1.274	52	1·321	52	1·370	53
17	1.133	49	1·176	50	1.221	50	1.267	51	1·314	51	1·363	52
171	1.126	48	1·170	49	1.214	49	1.260	50	1·308	50	1·356	51
$ \begin{array}{c c} 18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \end{array} $	1·119	47	1·163	48	1·207	48	1.253	49	1·301	49	1·349	50
	1·112	46	1·156	47	1·200	47	1.246	48	1·294	48	1·342	49
	1·105	45	1·149	•46	1·194	46	1.239	47	1·287	47	1·335	48
	1·099	44	1·142	45	1·187	45	1.233	46	1·280	46	1·328	47
$ \begin{array}{c c} 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \end{array} $	1.092	44	1·135	44	1.180	44	1·226	45	1·273	45	1·321	46
	1.085	43	1·129	43	1.173	44	1·219	44	1·266	44	1·315	45
	1.078	42	1·122	42	1.166	43	1·212	43	1·259	44	1·308	44
	1.071	41	1·115	41	1.159	42	1·205	43	1·253	43	1·301	43
$ \begin{array}{c c} 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \end{array} $	1.065	40	1·108	41	1·153	41	1·198	42	1·246	42	1·294	43
	1.058	39	1·101	40	1·146	40	1·191	41	1·239	41	1·287	42
	1.051	39	1·094	39	1·139	39	1·185	40	1·232	41	1·280	41
	1.044	38	1·087	38	1·132	39	1·178	39	1·225	40	1·273	40
$ \begin{array}{ c c c c } \hline 24 \\ 24 \\ 25 \\ \hline 25 \end{array} $	1.037	37	1.080	38	1·125	38	1·171	38	1·218	39	1.266	39
	1.030	36	1.073	37	1·118	37	1·164	38	1·211	38	1.259	39
	1.023	36	1.067	36	1·111	37	1·157	37	1·204	38	1.253	38

eit.		D	EGREES	OF TH	E WET	BULB !	THERMO	METER	—FAHRI	• ENHEIT	•	
- t Fahrenheit.	95	0	96	0	97	0	98	0	99	0	100	)°
t - t E	Force of Vapor, in inches.	Relative Humidity.										
0° 1/2 1 1/2	1·647	100	1.698	100	1.751	100	1.805	100	1·861	100	1.918	100
	1·640	98	1.691	98	1.744	98	1.798	98	1·854	98	1.911	98
	1·633	96	1.684	96	1.737	96	1.791	96	1·847	96	1.904	96
	1·626	94	1.677	94	1.730	94	1.784	95	1·840	95	1.897	95
2	1.619	92	1.671	92	1.723	92	1·777	93	1.833	93	1.890	93
2½	1.612	90	1.664	90	1.716	90	1·770	91	1.826	91	1.883	91
3	1.605	89	1.657	89	1.709	89	1·764	90	1.819	90	1.876	90
3½	1.598	87	1.650	87	1.703	87	1·757	88	1.812	88	1.870	88
$\begin{array}{ c c c }\hline & 4 \\ & 4\frac{1}{2} \\ & 5 \\ & 5\frac{1}{2} \\ \hline \end{array}$	1.592	85	1.643	85	1.696	85	1.750	86	1.805	86	1.863	86
	1.585	83	1.636	83	1.689	83	1.743	84	1.799	84	1.857	84
	1.578	82	1.629	82	1.682	82	1.736	83	1.791	83	1.849	83
	1.571	80	1.622	80	1.675	80	1.729	81	1.785	81	1.842	81
$ \begin{array}{ c c c c } \hline 6 & 6\frac{1}{2} \\ 7 & 7\frac{1}{2} \end{array} $	1.564	78	1.615	78	1.668	78	1·722	79	1.778	79	1.835	79
	1.557	77	1.608	77	1.661	77	1·715	78	1.771	78	1.828	78
	1.550	75	1.602	76	1.654	76	1·708	77	1.764	77	1.821	77
	1.543	73	1.595	74	1.647	74	1·701	75	1.757	76	1.814	76
8	1.536	72	1.588	73	1.640	73	1.694	74	1.750	74	1.807	74
8½	1.530	71	1.581	71	1.633	71	1.688	72	1.743	73	1.800	73
9	1.523	70	1.574	70	1.627	70	1.681	71	1.736	72	1.793	72
9½	1.517	69	1.567	69	1.620	69	1.674	70	1.729	70	1.786	70
$ \begin{array}{ c c c c } \hline 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \end{array} $	1.509	68	1.560	68	1.613	68	1.667	69	1.722	69	1.779	69
	1.502	66	1.553	66	1.606	66	1.660	67	1.715	67	1.772	67
	1.495	65	1.546	65	1.599	65	1.653	66	1.708	66	1.766	66
	1.488	63	1.539	63	1.592	64	1.646	64	1.702	65	1.759	65
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	1·481	62	1.532	62	1.585	63	1.639	63	1.695	64	1.752	64
	1·474	61	1.526	61	1.578	62	1.632	62	1.688	63	1.745	63
	1·468	60	1.519	60	1.571	61	1.625	61	1.681	62	1.738	62
	1·461	59	1.512	59	1.564	60	1.618	60	1.674	61	1.731	61
$ \begin{array}{c c} 14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2} \end{array} $	1·454 1·447 1·440 1·433	58 57 56 55	1.505 1.498 1.491 1.484	58 57 56 55	1.558 1.551 1.544 1.537	59 58 57 56	1.611 1.605 1.598 1.591	59 58 57 56	1.667 1.660 1.653 1.646	60 59 58 57	1.724 1.717 1.710 1.703	59 58 57
$ \begin{array}{c c} 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \end{array} $	1·426	54	1·477	54	1.530	55	1.584	55	1.639	56	1.696	56
	1·419	53	1·470	53	1.523	54	1.577	54	1.632	55	1.689	55
	1·412	52	1·464	52	1.516	53	1.570	53	1.625	54	1.682	54
	1·405	51	1·457	51	1.509	52	1.563	52	1.619	53	1.676	53
$ \begin{array}{ c c c c } \hline 18 \\ 18 \\ 19 \\ 19 \\ 19 \\ \hline 2 \end{array} $	1·399	50	1·450	50	1.502	51	1.556	52	1.612	52	1.669	53
	1·392	49	1·443	49	1.495	50	1.549	51	1.605	51	1.662	52
	1·385	48	1·436	48	1.488	49	1.542	50	1.598	50	1.655	51
	1·378	47	1·429	47	1.482	48	1.535	49	1.591	49	1.648	50
$ \begin{array}{c c} 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \end{array} $	1·371	46	1·422	47	1·475	47	1.528	48	1.584	48	1.641	49
	1·364	45	1·415	46	1·468	46	1.522	47	1.577	47	1.634	48
	1·357	45	1·408	45	1·461	45	1.515	46	1.570	46	1.627	47
	1·350	44	1·401	44	1·454	44	1.508	45	1.563	46	1.620	46
$ \begin{array}{c c} 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \end{array} $	1·343 1·337 1·330 1·323	42	1.395 1.388 1.381 1.374	44 43 42 42	1·447 1·440 1·433 1·426	44 43 42 42	1.501 1.494 1.487 1.480	43	1.556 1.549 1.542 1.536	45 44 43 43	1.613 1.606 1.599 1.593	46 45 44 43
$\begin{bmatrix} 24 \\ 24\frac{1}{2} \\ 25 \end{bmatrix}$	1·316 1·309 1·302	40	1·367 1·360 1·353	41 40 39	1·420 1·413 1·406	41 40 39	1·473 1·466 1·459	41	1.529 1.522 1.515	42 41 40	1.586 1.579 1.572	43 42 41

lejt.		DEGREES OF THE WET BULB THERMOMETER.—FAHRENHEIT.										
ahren	10	L°	109	2°	10	3°	104	1°	10	5°	10	6°
t — t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{ c c c c c }\hline 0° & \frac{1}{2} \\ 1 & \frac{1}{2} \\ 2 & \frac{1}{2} \\ 3 & \frac{1}{3} \\ \frac{1}{2} & \frac{1}{2} \\ 4 & \frac{4}{2} \\ 5 & \frac{1}{2} \\ 6 & \frac{6}{2} \\ 7 & \frac{1}{2} \\ 8 & \frac{8}{2} \\ 9 & \frac{1}{2} \\ 10 & \frac{10}{2} \\ 11 & \frac{11}{2} \\ 12 & \frac{1}{2} \\ 13 & \frac{1}{2} \\ 14 & \frac{1}{4} \\ 14 & \frac{1}{4} \\ 14 & \frac{1}{4} \\ \end{array}$	1.977 1.977 1.963 1.956 1.949 1.942 1.935 1.921 1.914 1.907 1.900 1.893 1.887 1.866 1.859 1.862 1.845 1.831 1.824 1.817 1.810 1.803 1.776	100 98 96 95 93 91 90 88 86 84 83 82 80 79 78 76 67 66 67 66 65 64 62 61 60 59	2·037 2·030 2·023 2·016 2·009 2·002 1·995 1·989 1·982 1·975 1·967 1·960 1·954 1·940 1·940 1·933 1·926 1·919 1·912 1·905 1·898 1·891 1·884 1·877 1·870 1·863 1·850 1·843 1·856	100 98 96 95 93 91 90 88 86 84 83 82 80 79 78 76 74 72 71 70 69 67 66 65 64 63 62 61 60	2·098 2·092 2·092 2·085 2·078 2·071 2·065 2·057 2·050 2·043 2·036 2·029 2·022 2·022 2·015 2·008 2·001 1·994 1·988 1·974 1·960 1·953 1·946 1·939 1·932 1·935 1·918 1·918 1·918 1·918 1·918 1·918	100 98 96 95 93 91 90 88 87 84 83 82 80 79 78 77 75 74 72 71 70 69 68 67 65 64 63 62 61 60	2·162 2·155 2·148 2·141 2·134 2·127 2·120 2·113 2·106 2·099 2·092 2·085 2·071 2·064 2·057 2·053 2·043 2·036 2·029 2·022 2·015 2·008 2·001 1·994 1·987 1·980 1·976 1·959	100 98 96 95 93 91 90 88 87 85 84 82 81 79 78 77 75 74 73 71 70 69 66 65 63 62 61 60	2.226	100	2.293	100
$ \begin{vmatrix} 15 \\ 15 \\ \frac{1}{2} \end{vmatrix} $ $ \begin{vmatrix} 16 \\ 16 \\ 16 \end{vmatrix} $ $ \begin{vmatrix} 17 \\ 17 \\ 18 \end{vmatrix} $ $ \begin{vmatrix} 18 \\ 18 \\ 19 \end{vmatrix} $ $ \begin{vmatrix} 19 \\ 20 \\ 21 \\ 21 \end{vmatrix} $ $ \begin{vmatrix} 22 \\ 22 \\ 22 \\ 23 \\ 23 \\ 24 \\ 24 \\ 25 \end{vmatrix} $	1.769 1.762 1.755 1.748 1.741 1.734 1.727 1.720 1.713 1.706 1.699 1.685 1.679 1.672 1.665 1.655 1.651 1.644 1.637 1.630	58 57 56 54 53 52 51 50 49 47 46 45 44 43 43 42 41	1·829 1·822 1·815 1·808 1·801 1·794 1·787 1·780 1·773 1·765 1·752 1·745 1·738 1·732 1·711 1·704 1·697 1·690	59 58 57 55 54 53 52 51 50 48 48 47 46 45 44 44 43 42 42	1·890 1·883 1·876 1·869 1·862 1·856 1·849 1·842 1·835 1·828 1·821 1·814 1·807 1·793 1·776 1·779 1·772 1·765 1·759 1·751	59 58 57 55 54 53 53 52 51 50 49 48 48 47 46 45 44 43 43	1.952 1.945 1.938 1.931 1.924 1.917 1.910 1.903 1.896 1.882 1.875 1.868 1.861 1.854 1.847 1.847 1.840 1.833 1.826 1.819	59 58 57 55 55 55 54 53 52 51 50 49 48 47 46 46 45 43				

beit.		D	EGREES	OF TH	E WET	BULB	THERMO	METER	.—FAHRI	ENHEI	г.	
Fahrenbeit	107°   108°   109°   110°   111°   112°											
t — t' F	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
00	2.360	100	2.429	100	2.500	100	2.572	100	2.646	100	2.721	100

# TABLES,

# METEOROLOGICAL AND PHYSICAL,

PREPARED FOR

### THE SMITHSONIAN INSTITUTION.

BY

### ARNOLD GUYOT, P.D., LL.D.,

PROFESSOR OF GEOLOGY AND PHYSICAL GEOGRAPHY, COLLEGE OF NEW JERSEY.

THIRD EDITION, REVISED AND ENLARGED.

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The Tables contained in this collection are divided into six series, as follows: —

- 1. Thermometrical Tables, marked A.
- II. Hygrometrical Tables, "B.
- III. Barometrical Tables, "C.
- IV. Hypsometrical Tables, "D.
- V. Meteorological Corrections, " E.
- VI. Miscellaneous Tables, "F.

Each series has an independent paging running through all the tables that it contains.

The letters A, B, C, D, E, F, at the bottom of each page, indicate the series, and the figure the folio of the series to which the page belongs.

The figure at the top of the page indicates the folio of the particular table of which the page is a part.

At the head of each series is found a detailed table of its contents.



# METEOROLOGICAL TABLES.

I.

THERMOMETRICAL TABLES.



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### PREFACE

#### TO THE FIRST EDITION.

To PROF. JOSEPH HENRY,

Secretary of the Smithsonian Institution.

SIR,

In compliance with your instructions, I have prepared the collection of Meteorological Tables contained in the following pages. I have endeavored to render it useful, not only to the observers engaged in the system of Meteorological Observations now in operation under the direction of the Smithsonian Institution, for whom it was immediately designed, but also to any Meteorologist who may desire to compare and to work out portions of the vast amount of Meteorological Observations already accumulated in the stores of science.

The reduction of the observations and the extensive comparisons, without which Meteorology can do but little, require an amount of mechanical labor which renders it impossible for most observers to deduce for themselves the results of their own observations. The difficulty is still further increased by the diversity of the thermometrical and barometrical scales which Meteorologists, faithful to old habits rather than to science and to reason, choose to retain, notwithstanding the additional labor they thus gratuitously assume to themselves. To relieve the Meteorologist of a great portion of this labor, by means of tables sufficiently extensive to render calculations and even interpolations unnecessary, is to save his time and his forces in favor of science itself, and thus materially contribute to its advancement. But most of the tables useful in Meteorology being scattered through many volumes, which are often not of easy access, this collection will be, it is hoped, acceptable to the friends of Meteorology, and will supply a want very much felt in this department of the physical sciences.

In the selection of the matter, I have been guided by the idea that the tables which I sought for my own use might also be those most likely to be wanted by others. But I wish the following to be considered as a first collection, containing only the tables most appropriate to the present purpose. They are, therefore, arranged in different and independent series, with distinct paging, but constituting together a frame-work into which any tables may be readily inserted when wanted, either to make the collection more complete, or to present a choice of tables calculated from somewhat different elements, or adapted to various methods of calculation.

The measurement of heights by means of the barometer being intimately connected with Meteorology, it was thought not inappropriate to admit into this collection Hypsometrical Tables, destined to render this kind of calculations more easy and more rapid, and thus to increase the taste for a method so useful in physical geography. I have preferred the tables of Delcros, as uniting in the greatest degree simplicity and accuracy. Those of Gauss, Bessel, and Baily may be given afterwards.

Every table contains directions for its use, when necessary; moreover, the indication of the elements used in its calculation, and of the source from which it has been taken. When no remark is made as to this last point, the table has been expressly calculated for this volume.

Very respectfully,

Your obedient servant,

A. GUYOT.

Cambridge, Mass., December 15th, 1851.

### PREFACE

### TO THE SECOND EDITION.

To PROF. JOSEPH HENRY,

Secretary of the Smithsonian Institution.

SIR, -

In sending to you the Meteorological Tables composing the first edition of this volume, published in 1852, I expressed the desire that they be considered as a first collection, containing the tables most needed at the time by the meteorological observers engaged in the system carried on under the supervision of the Smithsonian Institution, but destined to be increased. It was in that expectation, I remarked, that the tables had been arranged in independent series, as a kind of framework, into which a larger number could readily be inserted. It seemed, indeed, highly desirable to offer to the Meteorologist and Physical Geographer, not only the tables they daily need for working out the results of their observations, but also such a variety of tables, computed from different elements, or by different methods, or adapted to different measures, as to enable every one to choose among them those that he most approves, and at the same time properly to compare and to appreciate the results obtained by others.

Thanks to the congenial spirit with which the elevated views of the founder of the Smithsonian Institution are carried out, that character of general usefulness is not wanting in the present volume. With your agreement, the present edition contains more than three times as much matter as the first; and a rapid indication of the additions will suffice to justify them, and to show that, in selecting or calculating the new tables, the object just mentioned was constantly kept in view

As to the tables in the first edition, I must remark that, several of them having been printed in my absence, the copy prepared for the printer, in which decimals had to be left out, failed to give always the nearest value. Though these errors are too small to have any importance whatsoever in Meteorology, a careful revision of all the tables on the original computations was made, and they were corrected in the present edition. The few actual misprints which were discovered are indicated in a table of errata to the first edition.

In the Thermometrical series six small tables have been added; they were prepared for converting into each other differential results given in degrees of any one of the three thermometrical scales, irrespective of their zero point.

The Hygrometrical series has been entirely reorganized. It only contained five tables, all in French measures, and the Appendix. It is now composed of twenty-seven, arranged in three divisions. In the first are found ten tables, based on Regnault's hygrometrical constants, both in French and in English measures, in two corresponding sets, for the use of the psychrometer, the dew-point instruments, and for computing the weight of vapor in the air. The whole set in English measures, and Table V. in French measures, have been prepared for this edition. Being based on the best elements we now possess, they are given here for ordinary use. The second division contains the seven most important tables published in the Greenwich Observations, and Glaisher's extensive Psychrometrical Table. These tables being much used in England, and the results obtained by them exhibiting no inconsiderable differences from those derived from the preceding ones, they are indispensable for comparing these results. The third division, composed of ten miscellaneous tables, furnishes the means of comparing the different values of the force and the weight of vapor, especially those which have frequently been used in Germany, and also of reducing the indications of Saussure's Hair-Hygrometer to the ordinary seale of moisture. The Appendix has remained as in the first edition, but all the tables have been revised and corrected.

The Barometrical series, now in four divisions, has been increased from twelve to twenty-eight tables. Excepting three small tables for capillary action, all the new ones have been computed for this edition. The comparison, now so much needed, of the Russian barometer with the other scales, appears here for the first time.

The Hypsometrical series is almost entirely new. It contained only Deferos's table for barometric and Regnault's table for thermometric measurements, besides two auxiliary tables and the thirteen small tables of the Appendix. It now offers twenty-three tables for barometrical measurement of heights, in which all the principal formulæ and scales are represented; three for the measurement of heights by the thermometer, in French and in English measures; and a rich Appendix of forty-four tables, more extensive and convenient than those in the old set, which afford the means of readily converting into each other all the measures usually employed for indicating altitudes.

The series of Meteorological Corrections for periodic and non-periodic variations, for all parts of the world, mostly due to the untiring industry of Professor Dove, is an addition which will surely be appreciated by those who know how difficult access to the original tables is for most Meteorol-

ogists. A few tables have been added to Dove's collection, computed by Glaisher, Captain Lefroy, and by myself. Most of the tables refer to temperature, only two to moisture. Two tables of Barometrical Corrections have been placed in the Hypsometrical series, where they were needed, until they can be joined by others to make a set in this series, which still awaits new contributions, especially for these last two departments.

The Miscellaneous series is but begun. I have prepared a list of useful tables, which would be no doubt welcome to the lovers of Terrestrial Physics, and which may be published at some future occasion, if you should then

find it expedient.

The present collection being designed, not for the scientific only, but for the observers at large, the propriety of the explicit and popular form of the explanations which accompany the tables, and of the directions for using them, will readily be understood.

I close by the remark, that, in every instance, the works from which the tables were taken have been carefully noted, and due credit given to their authors. For all the tables without author's names, I am myself responsible.

I remain, Sir,

Very respectfully, yours,

A. GUYOT.

PRINCETON, N. J., December, 1857.

### PREFACE

#### TO THE THIRD EDITION.

A NEW series of Hygrometrical Tables, based on Regnault's Table of Elastic Forces of Vapor, has been published by Mr. Glaisher, in London, 1856. As, however, the Psychrometrical Table has not been computed from Regnault's formula, but by means of empirical factors, the results differ from those contained in Table VII. B. A table containing Glaisher's empirical factors, therefore, has been added, and will be found on page 144 B.

Table XVIII. of the Barometrical set, C, page 72, of the Second Edition, for reducing to the freezing point the Barometers with glass or wooden seales, copied from the Instructions of the Royal Society of London, and which is reprinted in most of the English works on Meteorology, having been found erroneous, a new table has been computed and substituted for it. As a large number of observers still use barometers with wooden scales, it was found advisable to enable them to make the needed interpolations at sight, by giving the corrections for every degree of the thermometer, from 0° to 100° Fahr., and for barometric heights ranging between 26 and 31 inches.

The small Table VI. D, page 48, of the Hypsometrical Tables by the writer, having been found useful for rapid computation of approximate results, a larger one of the same description, which allows to make at sight every interpolation, has been added, on page 92, as Table XIX'. The scientific traveller, wishing to determine, when ascending a mountain, the elevation of the physical or geological phenomena that he meets with, such as the stations of remarkable plants, limits of zones of vegetation,—the geologist who uses the aneroid barometer for geological sections,—the engineer who wishes to know, on the ground, approximately, his results,—will find it convenient to obtain the relative heights indicated by their instrument by a simple multiplication. The use of the table is explained page D 90.

Some of the decimals in the smaller Table VI. D, page 48, above mentioned, have been slightly altered in order to make both tables agree.

In set E of Meteorological Corrections, a table of corrections derived by Professor C. Dewey from the hourly observations of Professor Snell, at Amherst College, has been added, which will be of service especially to the numerous observers in New England and in the neighboring States.

The errata indicated in the Second Edition, and a few unimportant ones found since, have been corrected. No other changes have been made in this edition.

A. GUYOT.

I. – III.

### GENERAL COMPARISON

OF

## THE THERMOMETRICAL SCALES,

OR

### TABLES

showing the corresponding values of each full degree of fahrenheit's, centigrade, and reaumur's thermometers, from +212° to -39° fahrenheit.



#### COMPARISON OF THE THERMOMETRICAL SCALES.

The first three tables of this set give a simultaneous comparison of the three scales mostly used at present in Meteorology, and especially of the portion of the scales not comprised in the more extensive tables which follow them. They form thus a complement to these last tables; but as most of the temperatures contained in them do not occur in Meteorology, the comparison of the full degrees was found sufficient.

These three tables have been taken from E. L. Schubarth's Collection of Physical Tables. Berlin, 1836.

Tables IV. to IX. being more useful to the Meteorologist, the calculation has been carried out for every tenth of a degree. Tables VII. and IX. are from the *Annuaire Météorologique de France*; the others have been calculated.

A comparison of the Centigrade and Fahrenheit degrees near the boiling point, for every tenth of a degree, for the sake of the comparison of standard thermometers, will be found at the end of Table VI.

Tables X. to XV. will be found useful, for comparing differential results, such as ranges of temperature, and any relative amount expressed in degrees of different scales, without reference to their respective zeros.

### I. COMPARISON OF FAHRENHEIT'S THERMOMETRICAL SCALE WITH THE

### CENTIGRADE AND REAUMUR'S.

 $x^{\circ}$  Fahr. =  $(x^{\circ} - 32^{\circ}) \frac{5}{9}$  Centig. =  $(x^{\circ} - 32^{\circ}) \frac{4}{9}$  Reaum.

Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.
+212	+100.00	+80.00	+172	+77.78	+62.22	+132	+55.56	+44.44
211	99.44	79.56	171	77.22	61.78	131	55.00	44.00
210	98.89	79.11	170	76.67	61.33	130	54.44	43.56
209	98.33	78.67	169	76.11	60.89	129	53.89	43.11
208	97.78	78.22	168	75.56	60.44	128	53.33	42.67
207	97.22	77.78	167	75.00	60.00	127	52.78	42.22
206	96.67	77.33	166	74.44	59.56	126	52.22	41.78
205	96.11	76.89	165	73.89	59.11	125	51.67	41.33
204	95.56	76.44	164	73.33	58.67	124	51.11	40.89
203	95.00	76.00	163	72.78	58.22	123	50.56	40.44
202	94.44	75.56	162	72.22	57.78	122	50.00	40.00
201	93.89	75.11	161	71.67	57.33	121	49.44	39.56
200	93.33	74.67	160	71.11	56.89	120	48.89	39.11
199	92.78	74.22	159	70.56	56.44	119	48.33	38.67
198	92.22	73.78	158	70.00	56.00	118	47.78	38.22
197	91.67	73.33	157	69.44	55.56	117	47.22	37.78
196	91.11	72.89	156	68.89	55.11	116	46.67	37.33
195	90.56	72.44	155	68.33	54.67	115	46.11	36.89
194	90.00	72.00	154	67.78	54.22	114	45.56	36.44
193	89.44	71.56 71.11	153	67.22	53.78	113	45.00	36.00
192	88.89	70.67	152	66.67	53.33	112	44.44	35.56
191 190	88.33 87.78	70.22	151 150	66-11 65-56	52.89 52.44	111 110	43.89	35.11 $34.67$
189	87.22	69.78	149	65.00	52.44	109	43.33 42.78	34.22
188	86.67	69.33	148	64.44	51.56	109	42.78	33.78
187	\$6.11	68.89	147	63.89	51.11	103	41.67	33.33
186	85.56	68.44	146	63.33	50.67	106	41.11	32.89
185	85.00	68.00	145	62.78	50.22	105	40.56	32.44
184	84.44	67.56	144	62.22	49.78	104	40.00	32.00
183	83.89	67.11	143	61.67	49.33	103	39.44	31.56
182	83.33	66.67	142	61.11	48.89	102	38.89	31.11
181	82.78	66.22	141	60.56	48.44	101	38.33	30.67
180	82.22	65.78	140	60.00	48.00	100	37.78	30.22
179	81.67	65.33	139	59.44	47.56	99	37.22	29.78
178	81.11	64.89	138	58.89	47.11	98	36.67	29.33
177	80.56	64.44	137	58.33	46.67	97	36.11	28.89
176	80.00	64.00	136	57.78	46.22	96	35.56	28.44
175	79.44	63.56	135	57.22	45.78	95	35.00	28.00
174	78.89	63.11	134	56.67	45.33	94	34.44	27.56
173	78.33	62.67	133	56.11	44.89	93	33.89	27.11

 $x^{\circ}$  Fahr. =  $(x^{\circ} - 32^{\circ}) \frac{5}{9}$  Centig. =  $(x^{\circ} - 32^{\circ}) \frac{4}{9}$  Reaum.

Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.
+92	+33.33	+26.67	+48	+ 8.89	+ 7.11	+ 4	-15.56	-12.44
91	32.78	26.22	47	8.33	6.67	3	-16.11	-12.89
90	32.22	25.78	46	7.78	6.22	2	-16.67	-13.33
89	31.67	25.33	45	7.22	5.78	1	-17.22	-13.78
88	31.11	24.89	44	6.67	5.33	0	-17.78	-14.22
87	30.56	24.44	43	6.11	4.89	- 1	-18.33	-14.67
86	30.00	24.00	42	5.56	4.44	- 2 - 3	-18.89 -19.44	-15.11 -15.56
85	29.44	23.56	41	5.00	4.00 3.56	- 3 - 4	-19.44 -20.00	-16.00
84	28.89	23.11	39	4.44 3.89	3.11	- 4 - 5	-20.56	-16.44
83 82	28.33 27.78	22.67 22.22	38	3.33	2.67	- 6	-20.50 -21.11	-16.89
81	27.18	21.78	37	2.78	2.22	- 7	-21.11 $-21.67$	<b>-10.33</b>
80	26.67	21.33	36	2.22	1.78	- 8	-22.22	-17.78
79	26.11	20.89	35	1.67	1.33	- 9	-22.78	-18.22
78	25.56	20.44	34	1.11	0.89	-10	-23.33	-18.67
77	25.00	20.00	33	0.56	0.44	-11	-23.89	-19.11
76	24.44	19.56	32	0.00	0.00	-12	-24.44	-19.56
75	23.89	19.11	31	- 0.56	- 0.44	-13	-25.00	-20.00
74	23.33	18.67	30	- 1.11	- 0.89	-14	-25.56	-20.44
73	22.78	18.22	29	- 1.67	- 1.33	-15	-26.11	-20.89
72	22.22	17.78	28	- 2.22	- 1.78	-16	-26.67	-21.33
71	21.67	17.33	27	- 2.78	- 2.22	-17	-27.22	<b>-21.7</b> S
70	21.11	16.89	26	- 3.33	- 2.67	-18	-27.78	-22.22
69	20.56	16.44	25	- 3.89	- 3.11	-19	-28.33	-22.67
68	20.00	16.00	24	- 4.44	- 3.56	-20	-28.89	-23.11
67	19.44	15.56	23	- 5.00	- 4.00	-21	-29.44	-23.56
66	18.89	15.11	22	- 5.56	- 4.44	-22	-30.00	-24.00
65	18.33	14.67	21	- 6.11	- 4.89	-23	-30.56	-24.44
64	17.78	14.22	20	- 6.67	- 5.33	-24	-31.11	-24.89
63	17.22	13.78	19	7.22	- 5.78 - 6.22	-25 -26	-31.67 -32.22	-25.33 -25.78
62	16.67 16.11	13.33 12.89	18 17	- 7.78 - 8.33	-6.22 $-6.67$	-26 $-27$	-32.22 -32.78	-25.75 $-26.22$
61 60	15.56	12.59	16	- 8.89	- 0.07 - 7.11	-28 -28	-32.75 -33.33	-26.22 $-26.67$
59	15.00	12.44	15	- 9.44	- 7.11 - 7.56	-28 -29	-33.89	-20.07 -27.11
58	14.44	11.56	14	-10.00	- 8.00	-30	-34.44	-27.56
57	13.89	11.11	13	-10.56	- 8.44	-31	-35.00	-28.00
56	13.33	10.67	12	-11.11	- 8.89	-32	-35.56	-28.44
55	12.78	10.22	11	-11.67	- 9.33	-33	-36.11	-28.89
54	12.22	9.78	10	-12.22	- 9.78	-34	-36.67	-29.33
53	11.67	9.33	9	-12.78	-10.22	-35	-37.22	-29.78
52	11.11	8.89	8	-13.33	-10.67	-36	-37.78	-30.22
51	10.56	8.44	7	-13.89	-11.11	-37	-38.33	-30.67
50	10.00	8.00	6	-14-44	-11.56	-38	-38.89	-31-11
49	9.44	7.56	5	-15.00	-12.00	-39	-39.44	-31.56
	1		For the Co	ontinuation se	e Table IV. ar	nd V.		l

For the Continuation see Table IV. and V.

## II. COMPARISON OF THE CENTIGRADE THERMOMETER WITH REAUMUR'S AND FAHRENHEIT'S.

 $x^{\circ}$  Centig. =  $(32 + \frac{9}{5} x^{\circ})$  Fahr. =  $\frac{4}{5} x^{\circ}$  Reaum.

Centig.	Reaumur.	Fahrenheit.	Centig.	Reaumur.	Fahrenheit.	Centig.	Reaumur,	Fahrenheit.
+100	+80.0	+212.0	+83	+66.4	+181.4	+ 66	+52.8	+150.8
99	79.2	210.2	82	65.6	179.6	65	52.0	149.0
98	78.4	208.4	81	64.8	177.8	64	51.2	147.2
97	77.6	206.6	80	64.0	176.0	63	50.4	145.4
96	76.8	204.8	79	63.2	174.2	62	49.6	143.6
95	76.0	203.0	78	62.4	172.4	61	48.8	141.8
94	75.2	201.2	77	61.6	170.6	60	48.0	140.0
93	74.4	199.4	76	60.8	168.8	59	47.2	138.2
92	73.6	197.6	75	60.0	167.0	58	46.4	136.4
91	72.8	195.8	74	59.2	165.2	57	45.6	134.6
90	72.0	194.0	73	58.4	163.4	56	44.8	132.8
89	71.2	192.2	72	57.6	161.6	55	44.0	131.0
88	70.4	190.4	71	56.8	159.8	54	43.2	129.2
87	69.6	188.6	70	56.0	158.0	53	42.4	127.4
86	68.8	186.8	69	55.2	156.2	52	41.6	125.6
85	68.0	185.0	68	54.4	154.4	51	40.8	123.8
84	67.2	183.2	67	53.6	152.6	50	40.0	122.0

For the Continuation see Tables V. and VI.

# III. COMPARISON OF REAUMUR'S THERMOMETER WITH FAHRENHEIT'S AND THE CENTIGRADE.

 $x^{\circ}$  Reaum. =  $(32^{\circ} + \frac{9}{4} x^{\circ})$  Fahr. =  $\frac{5}{4} x^{\circ}$  Centig.

Reaumur.	Fahrenheit.	Centigrade.	Reaumur.	Fahrenheit.	Centigrade.	Reaumur.	Fahrenheit.	Centigrade.
+80	+212.00	+100.00	+66	+180.50	+82.50	+52	+149.00	+65.00
79	209.75	98.75	65	178.25	81.25	51	146.75	63.75
78	207.50	97.50	64	176.00	80.00	50	144.50	62.50
77	205.25	96.25	63	173.75	78.75	49	142.25	61.25
76	203.00	95.00	62	171.50	77.50	48	140.00	60.00
75	200.75	93.75	61	169.25	76.25	47	137.75	58.75
7.4	198.50	92.50	60	167.00	75.00	46	135.50	57.50
73	196.25	91.25	59	164.75	73.75	45	133.25	56.25
72	194.00	90.00	58	162.50	72.50	44	131.00	55.00
71	191.75	88.75	57	160.25	71.25	43	128.75	53.75
70	189.50	87.50	56	158.00	70.00	42	126.50	52.50
69	187.25	86.25	55	155.75	68.75	41	124.25	51.25
68	185.00	85.00	54	153.50	67.50	40	122.00	50.00
67	182.75	83.75	53	151.25	66.25	39	119.75	48.75

For the Continuation see Tables VIII. and IX.

IV. - V.

### COMPARISON

OF

## FAHRENHEIT'S THERMOMETER

WITH

THE CENTIGRADE AND WITH THAT OF REAUMUR,

OR

### TABLES

FOR CONVERTING THE DEGREES OF FAHRENHEIT INTO CENTIGRADE DEGREES AND INTO DEGREES OF REAUMUR;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM  $+122^{\circ}$  TO  $-76^{\circ}$  FAHRENHEIT.



Degrees of	Tenths of Degrees.											
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
1.100	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.		
+122 121	+50.00	+50.06	+50.11	+50.17	+50.22	+50.28	+50.33	+50.39	+50.44	+50.50		
121	49.44	49.50	49.56	49.61	49.67	49.72	49.78	49.83	49.89	49.94		
119	48.89	49.94	49.00	49.06	49.11	49.17	49.22	49.28	49.33	49.39		
118	48.33	48.39	48.44	48.50	48.56	48.61	48.67	48.72	48.78	48.83		
115	47.78	47.83	47.89	47.94	48.00	48.06	48.11	48.17	48.22	48.28		
117	47.22	47.28	47.33	47.39	47.44	47.50	47.56	47.61	47.67	47.72		
116	46.67	46.72	46.78	46.83	46.89	46.94	47.00	47.06	47.11	47.17		
115	46.11	46.17	46.22	46.28	46.33	46.39	46.44	46.50	46.56	46.61		
114	45.56	45.61	45.67	45.72	45.78	45.83	45.89	45.94	46.00	46.06		
113	45.00	45.06	45.11	45.17	45.22	45.28	45.33	45.39	45.44	45.50		
112	44.44	44.50	44.56	44.61	44.67	44.72	44.78	44.83	44.89	44.94		
111	43.89	43.94	44.00	44.06	44.11	44.17	44.22	44.28	44.33	44.39		
110	43.33	43.39	43.44	43.50	43.56	43.61	43.67	43.72	43.78	43.83		
109	42.78	42.83	42.89	42.94	43.00	43.06	43.11	43.17	43.22	43.28		
108	42.22	42.28	42.33	42.39	42.44	42.50	42.56	42.61	42.67	42.72		
107	41.67	41.72	41.78	41.83	41.89	41.94	42.00	42.06	42.11	42.17		
106	41.11	41.17	41.22	41.28	41.33	41.39	41.44	41.50	41.56	41.61		
105	40.56	40.61	40.67	40.72	40.78	40.83	40.89	40.94	41.00	41.06		
104	40.00	40.06	40.11	40.17	40.22	40.28	40.33	40.39	40.44	40.50		
103	39.44	39.50	39.56	39.61	39.67	39.72	39.78	39.83	39.89	39.94		
102	38.89	38.94	39.00	39.06	39.11	39.17	39.22	39.28	39.33	39.39		
101	38.33	38.39	38.44	38.50	38.56	38.61	38.67	38.72	38.78	38.83		
100	37.78	37.83	37.89	37.94	38.00	38.06	38.11	38.17	38.22	38.28		
99	37.22	37.28	37.33	37.39	37.44	37.50	37.56	37.61	37.67	37.72		
98	36.67	36.72	36.78	36.83	36.89	36.94	37.00	37.06	37.11	37.17		
97	36.11	36.17	36.22	36.28	36.33	36.39	36.44	36.50	36.56	36.61		
96	35.56	35.61	35.67	35.72	35.78	35.83	35.89	35.94	36.00	36.06		
95	35.00	35.06	35.11	35.17	35.22	35.28	35.33	35.39	35.44	35.50		
94	34.44	34.50	34.56	34.61	34.67	34.72	34.78	34.83	34.89	34.94		
93	33.89	33.94	34.00	34.06	34.11	34.17	34.22	34.28	34.33	34.39		
0.0	00.00	00.00										
92	33.33	33.39	33.44	33.50	33.56	33.61	33.67	33.72	33.78	33.83		
91	32.78	32.83	32.89	32.94	33.00	33.06	33.11	33.17	33.22	33.28		
90 89	32.22	32.28	32.33	32.39	32.44	32.50	32.56	32.61	32.67	32.72		
88	31.67	31.72	31.78	31.83	31.89	31.94	32.00	32.06	32.11	33.17		
03	31.11	31.17	31.22	31.28	31.33	31.39	31.44	31.50	31.56	31.61		
87	30.56	30.61	30.67	30.72	30.78	30.83	30.89	30.94	31.00	31.06		
86	30.00	30.06	30.11	30.17	30.22	30.28	30.33	30.39	30.44	30.50		
85	29.44	29.50	29.56	29.61	29.67	29.72	29.78	29.83	29.89	29.94		
84 .	28.89	28.94	29.00	29.06	29.11	29.17	29.22	29.28	29.33	29.39		
83	28.33	28.39	28.44	28.50	28.56	28.61	28.67	28.72	28.78	28.83		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

Degrees of					Tenths o	f Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
+82	Centig. +27.78	Centig. +27.83	Centig. +27.89	Centig. +27.94	Centig. +28.00	Centig. +28.06	Centig. +28.11	Centig. +28.17	Centig. +28.22	Centig. +28.28
81	27.22	27.28	27.33	27.39	27.44	27.50	27.56	27.61	27.67	27.72
80	26.67	26.72	26.78	26.83	26.89	26.94	27.00	27.06	27.11	27.17
79	26.11	26.17	26.22	26.28	26.33	26.39	26.44	26.50	26.56	26.61
78	25.56	25.61	25.67	25.72	25.78	25.83	25.89	25.94	26.00	26.06
77	25.00	25.06	25.11	25.17	25.22	25.28	25.33	25.39	25.44	25.50
76	24.44	24.50	24.56	24.61	24.67	24.72	24.78	24.83	24.89	24.94
75	23.89	23.94	24.00	24.06	24.11	24.17	24.22	24.28	24.33	24.39
74	23.33	23.39	23.44	23.50	23.56	23.61	23.67	23.72	23.78	23.83
73	22.78	22.83	22.89	22.94	23.00	23.06	23.11	23.17	23.22	23.28
72	22.22	22.28	22.33	22.39	22.44	22.50	22.56	22.61	22.67	22.72
71	21.67	21.72	21.78	21.83	21.89	21.94	22.00	22.06	22.11	22.17
70 69	21.11	21.17 $20.61$	$21.22 \\ 20.67$	$21.28 \\ 20.72$	21.33 $20.78$	21.39 20.83	21.44	21.50 20.94	21.56	21.61
68	20.00	20.06	20.07	20.12	20.78	20.33	20.33	20.39	21.00 20.44	21.06 20.50
67	19.44	19.50	19.56	19.61	19.67	19.72	19.78	19.83	19.89	19.94
66	18.89	18.94	19.00	19.06	19.11	19.17	19.22	19.28	19.33	19.39
65	18.33	18.39	18.44	18.50	18.56	18.61	18.67	18.72	18.78	18.83
64	17.78	17.83	17.59	17.94	18.00	18.06	18.11	18.17	18.22	18.28
63	17.22	17.28	17.33	17.39	17.44	17.50	17.56	17.61	17.67	17.72
62	16.67	16.72	16.78	16.83	16.89	16.94	17.00	17.06	17.11	17.17
61	16.11	16.17	16.22	16.28	16.33	16.39	16.44	16.50	16.56	16.61
60	15.56	15.61	15.67	15.72	15.78	15.83	15.89	15.94	16.00	16.06
59	15.00	15.06	15.11	15.17	15.22	15.28	15.33	15.39	15.44	15.50
58	14.44	14.50	14.56	14.61	14.67	14.72	14.78	14.83	14.89	14.94
57	13.89	13.94	14.00	14.06	14.11	14.17	14.22	14.28	14.33	14.39
56	13.33	13.39	13.44	13.50	13.56	13.61	13.67	13.72	13.78	13.83
55 54	12.78 12.22	12.83 12.28	12.89 12.33	12.94 12.39	13.00 12.44	13.06 12.50	13.11 12.56	13.17	13.22 12.67	13.28 12.72
53	11.67	11.72	11.78	11.83	11.89	11.94	12.00	12.06	12.07	12.17
52	11.11	11.17	11.22	11.28	11.33	11.39	11.44	11.50	11.56	11.61
51	10.56	10.61	10.67	10.72	10.78	10.83	10.89	10.94	11.00	11.01
50	10.00	10.06	10.11	10.17	10.22	10.28	10.33	10.39	10.44	10.50
49	9.44	9.50	9.56	9.61	9.67	9.72	9.78	9.83	9.89	9.94
48	8.89	8.94	9.00	9.06	9.11	9.17	9.22	9.28	9.33	9.39
47	8.33	8.39	8.44	8.50	8.56	8.61	8.67	8.72	8.78	8.83
46	7.78	7.83	7.89	7.94	8.00	8.06	8.11	8.17	8.22	8.28
45	7.22	7.28	7.33	7.39	7.44	7.50	7.56	7.61	7.67	7.72
44	6.67	6.72	6.78	6.83	6.89	6.94	7.00	7.06	7.11	7.17
43	6.11	6.17	6.22	6.28	6.33	6.39	6.44	6.50	6.56	6.61
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of Fahren					Tenths o	f Degrees.				
heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
+42	Centig. +5.56	Centig. +5.61	Centig. +5.67	Centig. +5.72	Centig. +5.78	Centig. +5.83	Centig. +5.89	Centig. +5.94	Centig. +6.00	Centig. +6.06
41	5.00	5.06	5.11	5.17	5.22	5.28	5.33	5.39	5.44	5.50
40	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.83	4.89	4.94
39	3.89	3.94	4.00	4.06	4.11	4.17	4.22	4.28	4.33	4.39
38	3.33	3.39	3.44	3.50	3.56	3.61	3.67	3.72	3.78	3.83
37	2.78	2.83	2.89	2.94	3.00	3.06	3.11	3.17	3.22	3.28
36	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72
35	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.17
34	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61
33	0.56	0.61	0.67	0.72	0.78	0.83	0.89	0.94	1.00	1.06
32	0.00	0.06	0.11	0.17	0.22	0.28	0.33	0.39	0.44	0.50
31	- 0.56	- 0.50	- 0.44	- 0.39	- 0.33	- 0.28	- 0.22	- 0.17	- 0.11	- 0.06
30	- 1.11	- 1.06	- 1.00	- 0.94	- 0.89	- 0.83	- 0.78	- 0.72	- 0.67	- 0.61
29	- 1.67	- 1.61	- 1.56	- 1.50	- 1.44	- 1.39	- 1.33	- 1.28	- 1.22	- 1.17
28	- 2.22	- 2.17	- 2.11	- 2.06	- 2.00	- 1.94	- 1.89	- 1.83	- 1.78	1.72
27	- 2.78	- 2.72	- 2.67	- 2.61	- 2.56	- 2.50	- 2.44	- 2.39	- 2.33	- 2.28
26	- 3.33	- 3.28	- 3.22	- 3.17	- 3.11	- 3.06	- 3.00	- 2.94	- 2.89	- 2.83
25	- 3.89	- 3.83	- 3.78	- 3.72	- 3.67	- 3.61	- 3.56	- 3.50	- 3.44	- 3.39
24	- 4.44	- 4.39	- 4.33	- 4.28	- 4.22	- 4.17	- 4.11	- 4.06	- 4.00	- 3.94
23	- 5.00	- 4.94	- 4.89	- 4.83	<b>- 4.7</b> 8	- 4.72	- 4.67	<b>-</b> 4.61	- 4.56	<b>-</b> 4.50
22	- 5.56	- 5.50	- 5.44	- 5.39	- 5.33	- 5.28	- 5.22	- 5.17	- 5.11	- 5.06
21	- 6.11	- 6.06	- 6.00	- 5.94	- 5.89	- 5.83	- 5.78	- 5.72	- 5.67	- 5.61
20	- 6.67	- 6.61	- 6.56	- 6.50	- 6.44	- 6.39	- 6.33	- 6.28	- 6.22	- 6.17
19	- 7.22	- 7.17	- 7.11	- 7.06	- 7.00	- 6.94	- 6.89	- 6.83	- 6.78	- 6.72
18	<b>- 7.7</b> 8	- 7.72	- 7.67	- 7.61	<b>-</b> 7.56	<b>- 7.50</b>	- 7.44	- 7.39	- 7.33	<b>- 7.28</b>
17	- 8.33	- 8.28	- 8.22	- 8.17	- 8.11	- 8.06	- 8.00	- 7.94	<b>- 7.89</b>	- 7.83
16	- 8.89	- 8.83	- 8.78	- 8.72	- S.67	- 8.61	- 8.56	- 8.50	- 8.44	- 8.39
15	- 9.44	- 9.39	- 9.33	<b>-</b> 9.28	- 9.22	- 9.17	- 9.11	- 9.06	- 9.00	- 8.94
14	-10.00	- 9.94	<b>- 9.</b> 89	- 9.83	- 9.78	- 9.72	- 9.67	- 9.61	- 9.56	- 9.50
13	-10.56	-11.50	-10.44	-10.39	<b>-1</b> 0.33	-10.28	-10.22	-10.17	-10.11	-10.06
12	-11.11	-11.06	-11.00	-10.94	-10.89	-10.83	-10.78	-10.72	-10.67	-10.61
11	-11.67	-11.61	-11.56	-11.50	-11.44	-11.39	-11.33	-11.28	-11.22	-11.17
10	-12.22	-12.17	-12.11	-12.06	-12.00	-11.94	-11.89	-11.83	-11.78	-11.72
9	-12.78	-12.72	-12.67	-12.61	-12.56	-12.50	-12.44	-12.39	-12.33	-12.28
8	-13.33	-13.28	-13.22	-13.17	-13.11	-13.06	-13.00	-12.94	-12.89	-12.83
7	-13.89	-13.83	-13.78	-13.72	-13.67	-13.61	-13.56	-13.50	-13.44	-13.39
6	-14.44	-14.39	-14.33	-14.28	-14.22	-14.17	-14.11	-14.06	-14.00	-13.94
5	-15.00	-14.94	-14.89	-14.83	-14.78	-14.72	-14.67	-14.61	-14.56	-14.50
4	-15.56	-15.50	-15.44	-15.39	-15.33	-15.28	-15.22	-15.17	-15.11	-15.06
3	-16.11	-16.06	-16.00	-15.94	-15.89	-15.83 	-15.78	-15.72	-15.67	-15.61 
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	Tenths of Degrees.											
Degrees of Fahren- heit.		1		1	1	1	1	1	I	1		
nert.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.		
+ 2	-16.67 $-17.22$	-16.61 $-17.17$	-16.56 $-17.11$	$\begin{bmatrix} -16.50. \\ -17.06 \end{bmatrix}$	-16.44 $-17.00$	-16.39 $-16.94$	-16.33 $-16.89$	-16.28 -16.83	-16.22 $-16.78$	-16.17 16.72		
0	-17.22 $-17.78$	-17.17 $-17.72$	-17.11 $-17.67$	-17.61	-17.56	-17.50	-17.44	-17.39	-10.78 -17.33	-17.28		
- 0	-17.78	-17.83	-17.89	-17.94	-18.00	-18.06	-18.11	-18.17	-18.22	-18.28		
- 1	-18.33	-18.39	-18.44	-18.50	-18.56	-18.61	-18.67	-18.72	-18.78	-18.S3		
- 2	-18.89	-18.94	-19.00	-19.06	-19.11	-19.17	-19.22	-19.28	-19.33	-19.39		
- 3	-19.44	-19.50	-19.56	-19.61	-19.67	-19.72	-19.78	-19.83	-19.89	-19.94		
- 4	-20.00	-20.06	-20.11	-20.17	-20.22	-20.28	-20.33	-20.39	-20.44	-20.50		
- 5	-20.56	-20.61	-20.67	-20.72	-20.78	-20.83	-20.89	-20.94	-21.00	-21.06		
- 6	-21.11	-21.17	-21.22	-21.28	-21.33	-21.39	-21.44	-21.50	-21.56	-21.61		
- 7	-21.67	-21.72	-21.78	-21.83	-21.89	-21.94	-22.00	-22.06	-22.11	-22.17		
- 8	-22.22	-22.28	-22.33	-22.39	-22.44	-22.50	-22.56	-22.61	-22.67	-22.72		
- 9	-22.78	-22.83 -23.39	-22.89 $-23.44$	-22.94 $-23.50$	-23.00 $-23.56$	-23.06 -23.61	-23.11 $-23.67$	-23.17 $-23.72$	-23.22 $-23.78$	-23.28 -23.83		
-10 -11	-23.33 -23.89	-23.39 $-23.94$	-23.44 $-24.00$	-23.50 $-24.06$	-23.30 $-24.11$	-23.01 $-24.17$	-23.67 $-24.22$	-23.72 $-24.28$	-23.78 $-24.33$	-23.83 $-24.39$		
-11	-20.00	-20.04	24.00	-24.00			-24.22	-24.20	-24.00	-24.00		
-12	-24.44	-24.50	-24.56	-24.61		24.72	-24.78	-24.83	-24.89	-24.94		
-13	-25.00	-25.06	-25.11	-25.17	-25.22	-25.28	-25.33	-25.39	-25.44	-25.50		
-14	-25.56	-25.61	-25.67	-25.72	-25.78	-25.83	-25.89	-25.94	-26.00	-26.06		
-15	-26.11	-26.17	-26.22 $-26.78$	-26.28	-26.33	-26.39	-26.44	-26.50	-26.56	-26.61		
-16	-26.67	-26.72	-26.78	-26.83	-26.89	-26.94	-27.00	-27.06	-27.11	-27.17		
-17	-27.22	-27.28	-27.33	-27.39	-27.44	-27.50	-27.56	-27.61	-27.67	-27.72		
-18	-27.78	<b>-27.</b> S3	-27.89	-27.94	-28.00	-28.06	-28.11	-28.17	-28.22	-28.28		
-19	-28.33	-28.39	-28.44	-28.50	-28.56	-28.61	-28.67	-28.72	-28.78	-28.83		
-20	-28.89	-28.94	-29.00	-29.06	-29.11	-29.17	-29.22	-29.28	-29.33	-29.39		
-21	-29.44	-29.50	-29.56	-29.61	-29.67	-29.72	-29.78	-29.83	-29.89	-29.94		
-22	-30.00	-30.06	-30.11	-30.17	-30.22	-30.28	-30.33	-30.39	-30.44	-30.50		
-23	-30.56	-30.61	-30.67	-30.72	-30.78	-30.83	-30.89	-30.94	-31.00	-31.06		
-24 -25	-31.11 -31.67	-31.17 -31.72	-31.22 -31.78	-31.28 -31.83	-31.33 -31.89	-31.39 -31.94	-31.44 $-32.00$	-31.50 -32.06	-31.56 -32.11	-31.61 -32.17		
-25 -26	-32.22	-31.72 $-32.28$	-32.33	-32.39	-32.44	-32.50	-32.56	-32.61	-32.11 $-32.67$	-32.77		
20		4	02.00	32.00			02.00		02.01	02.12		
-27	-32.78	-32.83	-32.89	-32.94	-33.00	-33.06	-33.11	-33.17	-33.22	-33.28		
-28	-33.33	-33.39	-33.44	-33.50	-33.56	-33.61	-33.67	-33.72	-33.78	-33.83		
-29	-33.89	-33.94	-34.00	-34.06	-34.11	-34.17	-34.22	-34.28	-34.33	-34.39		
-30 -31	-34.44 -35.00	-34.50 -35.06	-34.56 -35.11	-34.61 -35.17	-34.67 $-35.22$	-34.72 -35.28	-34.78 -35.33	-34.83 -35.39	-34.89 -35.44	-34.94 -35.50		
-31	-55,00	-99,00	-99.11	-00.17	-50.22	-50.45	-00.00	-55.39	-55.44	-00.00		
-32	-35.56	-35.61	-35.67	-35.72	-35.78	-35.83	-35.89	-35.94	-36.00	-36.06		
-33	-36.11	-36.17	-36.22	-36.28	-36.33	-36.39	-36.44	-36.50	-36.56	-36.61		
-34	-36.67	-36.72	-36.78	-36.S3	-36.89	-36.94	-37.00	-37.06	-37.11	-37.17		
-35	-37.22	-37.28	-37.33	-37.39	-37.44	-37.50	-37.56	-37.61	-37.67	-37.72		
-36	-37.78	<del>-37.83</del>	-37.89	-37.94	-3S.00 	-38.06 	-38.11 	-38.17 	-38.22	-38.28		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

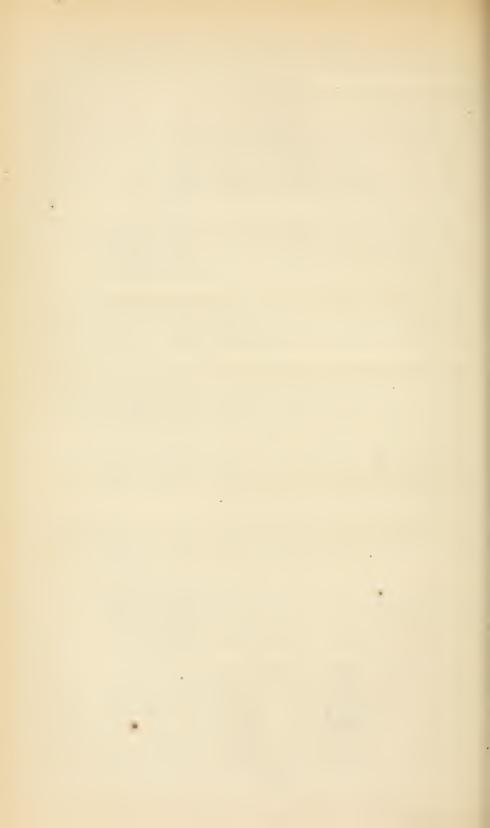
Degrees of	Tenths of Degrees.											
Degrees of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.		
-37	-38.33	-38.39	-38.44	-38.50	-38.56	-38.61	-38.67	-38.72	-38.78	-38.S3		
-38 -39	-38.89	-38.94	-39.00	-39.06	-39.11	-39.17	-39.22	-39.28	-39.33	-39.39		
-39 -40	-39.14 $-40.00$	-39.50	-39.56 -40.11	-39.61	-39.67	-39.72	-39.78	-39.83	-39.89	-39.94		
-40 -41	-40.00 $-40.56$	-40.06 $-40.61$	-40.11	-40.17	-40.22	-40.28 -40.83	-40.33	-40.39	-40.44	-40.50		
-41	-40.50	-40.61	-40.67	-40.72	-40.78	-40.53	-40.89	-40.94	-41.00	-41.06		
-42	-41.11	-41.17	-41.22	-41.28	-41.33	-41.39	-41.44	-41.50	-41.56	-41.61		
-43	-41.67	-41.72	-41.78	-41.83	-41.89	-41.94	-42.00	-42.06	-42.11	-42.17		
-44	-42.22	-42.28	-42.33	-42.39	-42.44	-42.50	-42.56	-42.61	-42.67	-42.72		
-45	-42.78	-42.93	-42.89	-42.94	-43.00	-43.06	-43.11	-43.17	-43.22	-43.28		
-46	-43.33	-43.39	-43.44	-43.50	-43.56	-43.61	-43.67	-43.72	-43.78	-43.S3		
-47	-43.89	-43.94	-44.00	-44.06	-44.11	-44.17	-44.22	-44.28	-44.33	-44.39		
-48	-44.44	-44.50	-44.56	-44.61	-14.67	-44.72	-44.78	-44.83	-44.89	-44.94		
-49	-45.00	-45.06	-45.11	-45.17	-45.22	-45.28	-45.33	-45.39	-45.44	-45.50		
-50	-45.56	-45.61	-45.67	-45.72	-45.78	-45.83	-45.89	-45.94	-46.00	-46.06		
-51	-46.11	-46.17	-46.22	-46.28	-46.33	-46.39	-46.44	-46.50	-46.56	-46.61		
-52	-46.67	-46.72	-46.78	-46.83	-46.89	-46.94	-47.00	-47.06	-47.11	-47.17		
-53	-47.22	-40.72 $-47.28$	-47.33	-47.39	-47.44	-47.50	-47.56	-47.61	-47.67	-47.72		
-54	-47.78	-47.83	-17.89	-47.94	-48.00	-48.06	-48.11	-48.17	-48.22	-48.28		
-55	-48.33	-48.39	-48.44	-48.50	-48.56	-48.61	-48.67	-48.72	-48.78	-48.83		
-56	-48.89	-48.94	-49.00	-49.06	-49.11	-49.17	-49.22	-49.28	-49.33	-49.39		
~~	10.11		40.50	10.01	40.00	10 #0	40.00	40.00	40.00	40.04		
-57 -58	-49.44 $-50.00$	-49.50 $-50.06$	-49.56 -50.11	-49.61 $-50.17$	-49.67 -50.22	-49.72 -50.28	-49.78 -50.33	-49.83 -50.39	-49.89 -50.44	-49.94 $-50.50$		
-59	-50.56	-50.61	-50.67	-50.72	-50.78	-50.83	-50.89	-50.94	-51.00	-51.06		
<b>-60</b>	-51.11	-51.17	-51.22	-51.28	-51.33	-51.39	-51.44	-51.50	-51.56	-51.61		
-61	-51.67	-51.72	-51.78	-51.83	-51.89	-51.94	-52.00	-52.06	-52.11	-52.17		
				02.00								
-62	-52.22	-52.28	-52.33	-52.39	-52.44	-52.50	-52.56	-52.61	-52.67	-52.72		
-63	-52.78	-52.83	-52.89	-52.94	-53.00	-53.06	-53.11	-53.17	-53.22	-53.28		
-64	-53.33	-53.39	-53.44	-53.50	-53.56	-53.61	-53.67	-53.72	-53.78	-53.83		
-65 -66	-53.89	-53.94	-54.00 -54.56	-54.06	-54.11	-54.17 $-54.72$	-54.22	-54.28	-54.33 -54.89	-54.39		
-00	-54.44	-54.50	-54.56	-54.61	-54.67	-54.72	-54.78	-54.83	-94.59	-54.94		
-67	-55.00	-55.06	-55.11	-55.17	-55.22	-55.28	-55.33	-55.39	-55.44	-55.50		
-68	-55.56	-55.61	-55.67	-55.72	-55.78	-55.83	-55.S9	-55.94	-56.00	-56.06		
-69	-56.11	-56.17	-56.22	-56.28	-56.33	-56.39	-56.44	-56.50	-56.56	-56.61		
-70	-56.67	-56.72	-56.78	-56.83	-56.89	-56.94	-57.00	-57.06	-57.11	-57.17		
-71	-57.22	-57.28	-57.33	-57.39	-57.44	-57.50	-57.56	-57.61	-57.67	-57.72		
	-57.78	-57.83	-57.89	-57.94	-58.00	-58.06	-58.11	-58.16	-58.22	-58.28		
-72 -73	-57.78 -58.33	-58.39	-58.44	-57.54 -58.50	-58.56	-58.61	-58.67	-58.72	-58.22 -58.78	-58.28 -58.83		
-73 -74	-58.89	-58.94	-59.00	-59.06	-59.11	-59.17	-59.22	-59.28	-59.33	-59.39		
-74 -75	-59.44	-59.50	-59.56	-59.61	-59.67	-59.72	-59.78	-59.83	-59.89	-59.94		
<b>-76</b>	-60.00	-60.06	-60.11	-60.17	-60.22	-60.28	-60.33	-60.39	-60.44	-60.50		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

Degrees of		Tenths of a Degree.											
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
. 100	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.		Reaumur.	Reaumur. +40.31		Reaum			
+122	+40.00	+40.04	+40.09	+40.13	+40.18	+40.22	+40.27	1	+40.36	+40.4			
121	39.56	39.60	39.64	39.69	39.73	39.78	39.82	39.87	39.91	39.9			
120	39.11	39.16	39.20	39.24	39.29	39.33	39.38	39.42	39.47	39.5			
119	38.67	38.71	38.76	38.80	38.84	38.89	38.93	38.98	39.02	39.0			
118	38.22	38.27	38.31	38.36	38.40	38.44	38.49	38.53	38.58	38.6			
117	37.78	37 82	37.87	37.91	37.96	38.00	38.04	38.09	38.13	38.1			
116	37.33	37.38	37.42	37.47	37.51	37.56	37.60	37.64	37.69	37.7			
115	36.89	36.93	36.98	37.02	37.07	37.11	37.16	37.20	37.24	37.2			
114	36.44	36.49	36.53	36.58	36.62	36.67	36.71	36.76	36.80	36.8			
113	36.00	36.04	36.09	36.13	36.18	36.22	36.27	36.31	36.36	36.4			
112	35.56	35.60	35.64	35.69	35.73	35.78	35.82	35.87	35.91	35.9			
111	35.11	35.16	35.20	35.24	35.29	35.33	35.38	35.42	35.47	35.5			
110	34.67	34.71	34.76	34.80	34.84	34.89	34.93	34.98	35.02	35.0			
109	34.22	34.27	34.31	34.36	34.40	34.44	34.49	34.53	34.58	34.6			
108	33.78	33.82	33.87	33.91	33.96	34.00	34.04	34.09	34.13	34.1			
107	33.33	33.38	33.42	33.47	33.51	33.56	33.60	33.64	33.69	33.7			
106	32.89	32.93	32.98	33.02	33.07	33.11	33.16	33.20	33.24	33.2			
105	32.44	32.49	32.53	32.58	32.62	32.67	32.71	32.76	32.80	32.8			
104	32.00	32.04	32.09	32.13	32.18	32.22	32.27	32.31	32.36	32.4			
103	31.56	31.60	31.64	31.69	31.73	31.78	31.82	31.87	31.91	31.9			
102	31.11	31.16	31.20	31.24	31.29	31.33	31.38	31.42	31.47	31.5			
101	30.67	30.71	30.76	30.80	30.84	30.89	30.93	30.98	31.02	31.0			
100	30.22	30.27	30.31	30.36	30.40	30.44	30.49	30.53	30.58	30.6			
99	29.78	29.82	29.87	29.91	29.96	30.00	30.04	30.09	30.13	30.1			
98	29.33	29.38	29.42	29.47	29.51	29.56	29.60	29.64	29.69	29.7			
97	28.89	28.93	28.98	29.02	29.07	29.11	29.16	29.20	29.24	29.2			
96	28.44	28.49	28.53		28.62			28.76	28.80				
,				28.58		28.67	28.71			28.8			
95	28.00	28.04	28.09	28.13	28.18	28.22	28.27	28.31	28.36	28.4			
94	27.56	27.60	27.64	27.69	27.73	27.78	27.82	27.87	27.91	27.9			
93	27.11	27.16	27.20	27.24	27.29	27.33	27.38	27.42	27.47	27.5			
92	26.67	26.71	26.76	26.80	26.84	26.89	26.93	26.98	27.02	27.0			
91	26.22	26.27	26.31	26.36	26.40	26.44	26.49	26.53	26.58	26.6			
90	25.78	25.82	25.87	25.91	25.96	26.00	26.04	26.09	26.13	26.1			
89	25.33	25.38	25.42	25.47	25.51	25.56	25.60	25.64	25.69	25.7			
88	24.89	24.93	24.98	25.02	25.07	25.11	25.16	25.20	25.24	25.2			
87	24.44	24.49	24.53	24.58	24.62	24.67	24.71	24.76	24.80	24.8			
86	24.00	24.04	24.09	24.13	24.18	24.22	24.27	24.31	24.36	24.4			
85	23.56	23.60	23.64	23.69	23.73	23.78	23.82	23.87	23.91	23.9			
84	23.11	23.16	23.20	23.24	23.29	23.33	23.38	23.42	23.47	23.5			
83	22.67	22.71	22.76	22.80	22.84	22.89	22.93	22.98	23.02	23.0			
82	22.22	22.27	22.31	22.36	22.40	22.44	22.49	22.53	22.58	22.6			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

Degrees of					Tenths of	a Degree.				
Fahren- heit.	0.	<sub>-</sub> 1.	2.	3.	4.	5.	6.	7.	8.	9.
		Reaumur.		Reaumur.				l .		
+81	+21.78	+21.82	+21.87	+21.91	+21.96	+22.00	+22.04	+22.09	+22.13	+22.18
80	21.33	21.38	21.42	21.47	21.51	21.56	21.60	21.64	21.69	21.73
79	20.89	20.93	20.98	21.02	21.07	21.11	21.16	21.20	21.24	21.29
78	20.44	20.49	20.53	20.58	20.62	20.67	20.71	20.76	20.80	20.84
77	20.00	20.04	20.09	20.13	20.18	20.22	20.27	20.31	20.36	20.40
76	19.56	19.60	19.64	19.69	19.73	19.78	19.82	19.87	19.91	19.96
75	19.11	19.16	19.20	19.24	19.29	19.33	19.38	19.42	19.47	19.51
74	18.67	18.71	18.76	18.80	18 84	18.89	18.93	18.98	19.02	19.07
73	18.22	18.27	18.31	18.36	18.40	18.44	18.49	18.53	18.58	18.62
72	17.78	17.82	17.87	17.91	17.96	18.00	18.04	18.09	18.13	18.18
71	17.33	17.38	17.42	17.47	17.51	17.56	17.60	17.64	17.69	17.73
70	16.89	16.93	16.98	17.02	17.07	17.11	17.16	17.20	17.24	17.29
69	16.44	16.49	16.53	16.58	16.62	16.67	16.71	16.76	16.80	16.84
68	16.00	16.04	16.09	16.13	16.18	16.22	16.27	16.31	16.36	16.40
67	15.56	15.60	15.64	15.69	15.73	15.78	15.82	15.87	15.91	15.96
66	15.11	15.16	15.20	15.24	15.29	15.33	15.38	15.42	15.47	15.51
65	14.67	14.71	14.76	14.80	14.84	14.89	14.93	14.98	15.02	15.07
64	14.22	14.27	14.31	14.36	14.40	14.44	14.49	14.53	14.58	14.62
63	13.78	13.82	13.87	13.91	13 96	14.00	14.04	14.09	14.13	14.18
62	13.33	13.38	13.42	13.47	13.51	13.56	13.60	13.64	13.69	13.73
61	12.89	12.93	12.98	13.02	13.07	13.11	13.16	13.20	13.24	13.29
60	12.44	12.49	12.53	12.58	12.62	12.67	12.71	12.76	12.80	12.84
59	12.00	12.04	12.09	12.13	12.18	12.22	12.27	12.31	12.36	12.40
58	11.56	11.60	11.64	11.69	11.73	11.78	11.82	11.87	11.91	11.96
57	11.11	11.16	11.20	11.24	11.29	11.33	11.38	11.42	11.47	11.51
56	10.67	10.71	10.76	10.80	10.84	10.89	10.93	10.98	11.02	11.07
55	10.22	10.27	10.31	10.36	10.40	10.44	10.49	10.53	10.58	10.62
54	9.78	9.82	9.87	9.91	9.96	10.00	10.04	10.09	10.13	10.18
53	9.33	9.38	9.42	9.47	9.51	9.56	9.60	9.64	9.69	9.73
52	8.89	8.93	8.98	9.02	9.07	9.11	9.16	9.20	9.24	9.29
51	8.44	8.49	8.53	8.58	8.62	8.67	8.71	8.76	8.80	8.84
50	8.00	8.04	8.09	8.13	8.18	8.22	8.27	8.31	8.36	8.40
49	7.56	7.60	7.64	7.69	7.73	7.78	7.82	7.87	7.91	7.96
48	7.11	7.16	7.20	7.24	7.29	7.33	7.38	7.42	7.47	7.51
47	6.67	6.71	6.76	6.80	6.84	6.89	6.93	6.98	7.02	7.07
46	6.22	6.27	6.31	6.36	6.40	6.44	6.49	6.53	6.58	6.62
45	5.78	5.82	5.87	5.91	5.96	6.00	6.04	6.09	6.13	6.18
44	5 33	5.38	5.42	5.47	5.51	5.56	5.60	5.64	5.69	5.73
43	4.89	4.93	4.98	5.02	5.07	5.11	5.16	5.20	5.24	5.29
42	4.44	4.49	4.53	4.58	4.62	4.67	4.71	4.76	4.80	4.84
41	4.00	4.04	4.09	4.13	4.18	4.22	4.27	4.31	4.36	4.40
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of	Tenths of a Degree.									
Degrees of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Reaumur	Reaumur.	Reaumur.		Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.
+40	+ 3.56	+ 3.60	+ 3.64	+ 3.69	+ 3.73	+ 3.78	+ 3.82	+ 3.87	+ 3.91	+ 3.96
39	3.11	3.16	3.20	3.24	3.29	3.33	3.38	3.42	3.47	3.51
38	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07
37	2.22	2.27	2.31	2.36	2.40	2.44	2.49	2.53	2.58	2.62
36	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.13	2.18
35	1.33	1.38	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.73
34	0.89	0.93	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29
33	0.44	0.49	0.53	0.58	0.62	0.67	0.71	0.76	0.80	0.84
32	0.00	0.04	0.09	0.13	0.18	0.22	0.27	0.31	0.36	0.40
31	- 0.44	- 0.40	- 0.36	- 0.31	- 0.27	- 0.22	- 0.18	- 0.13	- 0.09	- 0.04
30	- 0.89	- 0.84	- 0.80	- 0.76	- 0.71	- 0.67	- 0.62	- 0.58	- 0.53	- 0.49
29	- 1.33	- 1.29	- 1.24	- 1.20	- 1.16	- 1.11	- 1.07	- 1.02	- 0.98	- 0.93
28	<b>- 1.78</b>	- 1.73	- 1.69	- 1.64	- 1.60	- 1.56	- 1.51	- 1.47	- 1.42	- 1.38
27	- 2.22	- 2.18	- 2.13	- 2.09	- 2.04	- 2.00	- 1.96	- 1.91	- 1.87	- 1.82
26	- 2.67	- 2.62	- 2.5S	- 2.53	- 2.49	- 2.44	- 2.40	- 2.36	- 2.31	- 2.27
25	- 3.11	- 3.07	- 3.02	- 2.98	- 2.93	- 2.89	- 2.84	- 2.80	- 2.76	- 2.71
24	- 3.56	- 3.51	- 3.47	- 3.42	- 3.38	- 3.33	- 3.29	- 3.24	→ 3.20	- 3.16
23	- 4.00	- 3.96	- 3.91	- 3.87	- 3.82	- 3.78	- 3.73	- 3.69	- 3.64	- 3.60
22	- 4.44	- 4.40	- 4.36	- 4.31	- 4.27	-4.22	<b>- 4.18</b>	- 4.13	- 4.09	- 4.04
21	- 4.89	- 4.84	<b>- 4.</b> S0	- 4.76	- 4.71	- 4.67	<b>→</b> 4.62	- 4.58	- 4.53	- 4.49
20	- 5.33	- 5.29	- 5.24	- 5.20	- 5.16	<b>→</b> 5.11	- 5.07	- 5.02	- 4.98	- 4.93
19	- 5.78	- 5.73	- 5.69	- 5.64	- 5.60	- 5.56	- 5.51	- 5.47	→ 5.42	<b>→</b> 5.38
18	- 6.22	- 6.18	- 6.13	- 6.09	- 6.04	- 6.00	- 5.96	- 5.91	- 5.S7	- 5.82
17	- 6.67	- 6.62	- 6.58	- 6.53	- 6.49	- 6.44	- 6.40	- 6.36	- 6.31	- 6.27
16	- 7.11	- 7.07	7.02	- 6.98	- 6.93	- 6.89	→ 6.84	- 6.80	- 6.76	- 6.71
15	- 7.56	- 7.51	- 7.47	- 7.42	- 7.38	- 7.33	- 7.29	- 7.24	- 7.20	- 7.16
14	→ 8.00	- 7.96	- 7.91	- 7.87	- 7.82	<b>- 7.7</b> 8	- 7.73	- 7.69	- 7.64	- 7.60
13	- 8.44	- 8.40	- 8.36	- 8.31	- 8.27	- 8.22	- 8.18	- 8.13	- 8.09	- 8.04
12	- 8.89	- 8.84	- 8.80	- 8.76	- 8.71	- 8.67	- 8.62	- 8.58	- 8.53	- 8.49
11	- 9.33	- 9.29	- 9.24	- 9.20	- 9.16	- 9.11	- 9.07	- 9.02	- 8.98	- 8.93
10	- 9.78	- 9.73	- 9.69	- 9.64	- 9.60	- 9.56	- 9.51	- 9.47	- 9.42	- 9.38
9	-10.22	-10.18	-10.13	-10.09	-10.04	-10.00	- 9.96	- 9.91	- 9.87	- 9.82
8	-10.67	-10.62	-10.58	-10.53	-10.49	-10.44	-10.40	-10.36	-10.31	-10.27
7	-11.11	-11.07	-11.02	-10.98	-10.93	-10.89	-10.84	-10.80	-10.76	-10.71
6	-11.56	-11.51	-11.47	-11.42	<b>-11.</b> 38	-11.33	-11.29	-11.24	-11.20	-11.16
5	-12.00	-11.96	-11.91	-11.87	-11.82	-11.78	-11.73	-11.69	-11.64	-11.60
4	-12.44	-12.46	-12.36	-12.31	-12.27	-12.22	-12.18	-12.13	-12.09	-12.04
3	-12.89	-12.84	-12.80	-12.76	-12.71	-12.67	-12.62	-12.58	-12.53	-12.49
2	-13.33	-13.29	-13.24	-13.20	-13.16	-13.11	-13.07	-12.02	-12.98	-12.93
1	-13.78	-13.73	-13.69	-13.64	-13.60	-13.56	-13.51	-13.47	-13.42	-13.38
+ 0	-14.22	-14.18	-14.13 	-14.09	-14.04	-14.00	<del>-13.96</del>	-13.91 	-13.87 	-13.82 
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of										
Fahren- he it.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Reaumur.	Reaumur.	Reaumur.	Reaumur.						
- 0	-14.22	-14.27	-14.31	-14.36	-14.40	-14.44	-14.49	-14.53	-14.58	-14.62
- 1	-14.67	-14.71	-14.76	-14.80	-14.84	-14.89	-14.93	-14.98	-15.02	-15.07
- 2	-15.11	-15.16	-15.20	-15.24	-15.29	-15.33	-15.38	-15.42	-15.47	-15.51
- 3	-15.56	-15.60	-15.64	-15.69	-15.73	-15.78	-15.82	-15.87	-15.91	-15.96
- 4	-16.00	-16.04	-16.09	-16.13	-16.18	-16.22	-16.27	-16.31	-16.36	-16.40
- 5	-16.44	-16.49	-16.53	-16.58	-16.62	-16.67	-16.71	-16.76	-16.80	-16.84
- 6	-16.89	-17.93	-16.98	-17.02	-17.07	-17.11	-17.16	-17.20	-17.24	-17.29
- 7	-17.33	-17.38	-17.42	-17.47	-17.51	-17.56	-17.60	-17.64	-17.69	-17.73
- 8	-17.78	-18.82	-17.87	-17.91	-17.96	-18.00	-18.04	-18.09	-18.13	-18.18
- 9	-18.22	-18.27	-18.31	-18.36	-18.40	-18.44	-18.49	-18.53	-18.58	-18.62
-10	-18.67	-18.71	-18.76	-18.80	-18.84	-18.89	-18.93	-18.98	-19.02	-19.07
-11	-19.11	-19.16	-19.20	-19.24	-19.29	-19.33	-19.38	-19.42	-19.47	-19.51
-12	-19.56	-19.60	-19.64	-19.69	-19.73	-19.78	-19.82	-19.87	-19.91	-19.96
-13	-20.00	-20.04	-20.09	-20.13	-20.18	-20.22	-20.27	-20.31	-20.36	-20.40
-14	-20.44	-20.49	-20.53	-20.58	-20.62	-20.67	-20.71	-20.76	-20.80	-20.84
-15	-20.89	-20.93	-20.98	-21.02	-21.07	-21.11	-21.16	-21.20	-21.24	-21.29
-16	-21.33	-21.38	-21.42	-21.47	-21.51	-21.56	-21.60	-21.64	-21.69	-21.73
-17	-21.78	-21.82	-21.87	-21.91	-21.96	-22.00	-22.04	-22.09	-22.13	-22.18
-18	-22.22	-22.27	-22.31	-22.36	-22.40	-22.44	-22.49	-22.53	-22.58	-22.62
-19	-22.67	-22.71	-22.76	-22.80	-22.84	-22.89	-22.93	-22.98	-23.02	-23.07
-20	-23.11	-23.16	-23.20	-23.24	-23.29	-23.33	-23.38	-23.42	-23.47	-23.51
-21	-23.56	-23.60	-23.64	-23.69	-23.73	-23.78	<b>-23.82</b>	-23.87	-23.91	-23.96
-22	-24.00	-24.04	-24.09	-24.13	-24.18	-24.22	-24.27	-24.31	-24.36	-24.40
-23	-24.44	-24.49	-24.53	-24.58	-24.62	-24.67	-24.71	-24.76	-24.80	-24.84
-24	-24.89	-24.93	-24.98	-25.02	-25.07	-25.11	-25.16	-25.20	-25.24	-25.29
-25	-25.33	-25.38	-25.42	-25.47	-25.51	-25.56	-25.60	-25.64	-25.69	-25.73
-26	-25.78	-25.82	-25.87	-25.91	-25.96	-26.00	-26.04	-26.09	-26.13	-26.18
-27	-26.22	-26.27	-26.31	-26.36	-26.40	-26.44	-26.49	-26.53	-26.58	-26.62
-28	-26.67	-26.71.	-26.76	-26.80	-26.84	-26.89	<b>-26.9</b> 3	-26.98	-27.02	-27.07
-29	-27.11	-27.16	-27.20	-27.24	-27.29	-27.33	<b>-27.3</b> 8	-27.42	-27.47	-27.51
-30	-27.56	-27.60	-27.64	-27.69	-27.73	-27.78	-27.82	-27.87	-27.91	-27.96
-31	-28.00	-28.04	-28.09	-28.13	-28.18	-28.22	-28.27	-28.31	-28.36	-28.40
-32	-28 44	-28.49	-28.53	-28.58	-28.62	-28.67	-28.71	-28.76	-28.80	-28.84
-33	-28.89	-28.93	-28.98	-29.02	-29.07	-29.11	-29.16	-29.20	-29.24	-29.29
-34	-29.33	-29.38	-29.42	-29.47	-29.51	-29.56	-29.60	-29.64	-29.69	-29.73
-35	-29.78	-29.82	-29.87	-29.91	-29.96	-30.00	-30.04	-30.09	-30.13	-30.18
-36	-30.22	-30.27	-30.31	-30.36	-30.40	-30.44	-30.49	-30.53	-30.58	-30.62
-37	-30.67	-30.71	-30.76	-30.80	-30.84	-30.89	-30.93	-30.98	-31.02	-31.07
-38	-31.11	-31.16	-31.20	-31.24	-31.29	-31.33	-31.38	-31.42	-31.47	-31.51
-39	-31.56	-31.60	-31.64	-31.69	-31.73	-31.78	-31.82	-31.87	-31.91	-31.96
-40	-32.00	-30.04	-30.09	-30.13	-30.18	-30.22	-30.27	-30.31	-30.36	-30.40
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.



### VI.-VII.

### COMPARISON

OF

### THE CENTIGRADE THERMOMETER

WITH

THE THERMOMETERS OF FAHRENHEIT AND OF REAUMUR,

OR

### TABLES

FOR CONVERTING CENTIGRADE DEGREES INTO DEGREES OF FAHRENHEIT

AND OF REAUMUR;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM  $+50^{\circ}$  TO  $-54^{\circ}$  CENTIGRADE.



	Tenths of Degrees.									
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
+50	+122.00	+122.18	+122.36	+122.54	+122.72		+123.08	+123.26	+123.44	+123.62
49	120.20	120.38	120.56	120.74	120.92	121.10	121.28	121.46	121.64	121.82
48	118.40	118.58	118.76	118.94	119.12	119.30	119.48	119.66	119.84	120.02
47	116.60	116.78	116.96	117.14	117.32	117.50	117.68	117.86	118.04	118.22
46	114.80	114.98	115.16	115.34	115.52	115.70	115.88	116.06	116.24	116.42
45	113.00	113.18	113.36	113.54	113.72	113.90	114.08	114.26	114.44	114.62
44	111.20	111.38	111.56	111.74	111.92	112.10	112.28	112.46	112.64	112.82
43	109.40	109.58	109.76	109.94	110.12	110.30	110.48	110.66	110.84	111.02
42	107.60	107.78	107.96	108.14	108.32	108.50	108.68	108.86	109.04	109.22
41	105.80	105.98	106.16	106.34	106.52	106.70	106.88	107.06	107.24	107.42
40	104.00	104.18	104.36	104.54	104.72	104.90	105.08	105.26	105.44 103.64	105.62
39	102.20	102.38	102.56	102.74	102.92	103.10 101.30	103.28	103.46	103.64	103.82 102.02
38	100.40	100.58	100.76	100.94	101.12 99.32	99.50	101.48	101.66 99.86	100.04	102.02
37	98.60	98.78	98.96	99.14			99.68		98.24	98.42
36	96.80	96.98	97.16	97.34	97.52	97.70	97.88	98.06		
35	95.00	95.18	95.36	95.54	95.72	95.90	96.08	96.26	96.44	96.62
34	93.20	93.38	93.56	93.74	93.92	94.10	94.28	94.46	94.64	94.82
33	91.40	91.58	91.76	91.94	92.12	92.30	92.48	92.66	92.84	93.02
32	89.60	89.78	89.96	90.14	90.32	90.50	90.68	90.86	91.04	91.22
31	87.80	87.98	88.16	88.34	88.52	88.70	88.88	89.06	89.24	89.42
30	86.00	86.18	86.36	86.54	86.72	86.90	87.08	87.26	87.44	87.62
29	84.20	84.38	84.56	84.74	84.92	85.10	85.28	85.46	85.64	85.82
28	82.40	82.58	82.76	82.94	83.12	83.30	83.48	83.66	83.84	84.02
27	80.60	80.78	80.96	81.14	81.32	81.50	81.68	81.86	82.04	82.22
26	78.80	78.98	79.16	79.34	79.52	79.70	79.88	80.06	80.24	80.42
25	77.00	77.18	77.36	77.54	77.72	77.90	78.08	78.26	78.44	78.62
24	75.20	75.38	75.56	75.74	75.92	76.10	76.28	76.46	76.64	76.82
23	73.40	73.58	73.76	73.94	74.12	74.30	74.48	74.66	74.84	75.02
22	71.60	71.78	71.96	72.14	72.32	72.50	72.68	72.86	73.04	73.22
21	69.80	69.98	70.16	70.34	70.52	70.70	70.88	71.06	71.24	71.42
20	68.00	68.18	68.36	68.54	68.72	68.90	69.08	69.26	69.44	69.62
19	66.20	66.38	66.56	66.74	66.92	67.10	67.28	67.46	67.64	67.82
18	64.40	64.58	64.76	64.94	65.12	65.30	65.48	65.66	65.84	66.02
17	62.60	62.78	62.96	63.14	63.32	63.50	63.68	63.86	64.04	64.22
16	60.80	60.98	61.16	61.34	61.52	61.70	61.88	62.06	62.24	62.42
15	59.00	59.18	59.36	59.54	59.72	59.90	60.08	60.26	60.44	60.62
14	57.20	57.38	57.56	57.74	57.92	58.10	58.28	58.46	58.64	58.82
13	55.40	55.58	55.76	55.94	56.12	56.30	56.48	56.66	56.84	57.02
12	53.60	53.78	53.96	54.14	54.32	54.50	54.68	54.86	55.04	55.22
11	51.80	51.98	52.16	52.34	52.52	52.70	52.88	53.06	53.24	53.42
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		Tenths of Degrees.											
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.			
+10	+50.00	+50.18	+50.36	+50.54	+50.72	+50.90	+51.08	+51.26	+51.44	+51.62			
9	48.20	48.38	48.56	48.74	48.92	49.10	49.28	49.46	49.64	49.82			
8	46.40	46.58	46.76	46.94	47.12	47.30	47.48	47.66	47.84	48.02			
7	44.60	44.78	44.96	45.14	45.32	45.50	45.68	45.86	46.04	46.22			
6	42.80	42.98	43.16	43.34	43.52	43.70	43.88	44.06	44.24	44.42			
5	41.00	41.18	41.36	41.54	41.72	41.90	42.08	42.26	42.44	42.62			
4	39.20	39.38	39.56	39.74	39.92	40.10	40.28	40.46	40.64	40.82			
3	37.40	37.58	37.76	37.94	38.12	38.30	38.48	38.66	38.84	39.02			
2	35.60	35.78	35.96	36.14	36.32	36.50	36.68	36.86	37.04	37.22			
1	33.80	33.98	34.16	34.34	34.52	34.70	34.88	35.06	35.24	35.42			
0	32.00	32.18	32.36	32.54	32.72	32.90	33.08	33.26	33.44	33.62			
- 0	32.00	31.82	31.64	31.46	31.28	31.10	30.92	30.74	30.56	30.38			
- 1	30.20	30.02	29.84	29.66	29.48	29.30	29.12	28.94	28.76	28.58			
- 2	28.40	28.22	28.04	27.86	27.68	27.50	27.32	27.14	26.96	26.78			
- 3	26.60	26.42	26.24	26.06	25.88	25.70	25.52	25.34	25.16	24.98			
- 4	24.80	24.62	24.44	24.26	24.08	23.90	23.72	23.54	23.36	23.18			
- 5	23.00	22.82	22.64	22.46	22.28	22.10	21.92	21.74	21.56	21.38			
- 6	21.20	21.02	20.84	20.66	20.48	20.30	20.12	19.94	19.76	19.58			
- 7	19.40	19.22	19.04	18.86	18.68	18.50	18.32	18.14	17.96	17.78			
- 8	17.60	17.42	17.24	17.06	16.88	16.70	16.52	16.34	16.16	15.98			
- 9	15.80	15.62	15.44	15.26	15.08	14.90	14.72	14.54	14.36	14.18			
-10	14.00	13.82	13.64	13.46	13.28	13.10	12.92	12.74	12.56	12.38			
-11	12.20	12.02	11.84	11.66	11.48	11.30	11.12	10.94	10.76	10.58			
-12	10.40	10.22	10.04	9.86	9.68	9.50	9.32	9.14	8.96	8.78			
-13	8.60	8.42	8.24	8.06	7.88	7.70	7.52	7.34	7.16	6.98			
-14	6.80	6.62	6.44	6.26	6.08	5.90	5.72	5.54	5.36	5.18			
-15	5.00	4.82	4.64	4.46	4.28	4.10	3.92	3.74	3.56	3.38			
-16	3.20	3.02	2.84	2.66	2.48	2.30	2.12	1.94	1.76	1.58			
-17	1.40	1.22	1.04	0.86	0.68	0.50	0.32	0.14	- 0.04	- 0.22			
-18	- 0.40	- 0.58	- 0.76	- 0.94	- 1.12	- 1.30	- 1.48	- 1.66	- 1.84	- 2.02			
-19	- 2.20	- 2.38	- 2.56	- 2.74	- 2.92	- 3.10	- 3.28	- 3.46	- 3.64	- 3.82			
20	4.00				1.00	4.00	F 00	<b>.</b>		<b>-</b> 00			
-20	- 4.00	- 4.18	- 4.36	- 4.54	- 4.72	- 4.90	- 5.08	- 5.26	- 5.44	- 5.62			
-21	- 5.80	- 5.98	- 6.16	- 6.34	- 6.52	- 6.70	- 6.88	- 7.06	- 7.24	- 7.42			
-22	- 7.60	<b>- 7.7</b> 8	- 7.96	- 8.14	- 8.32	- 8.50	- 8.68	- 8.86	- 9.04	- 9.22			
-23 -24	-9.40 $-11.20$	- 9.58 -11.38	- 9.76 -11.56	-9.94 $-11.74$	-10.12 $-11.92$	-10.30 $-12.10$	-10.48 -12.28	-10.66 $-12.46$	-10.84 -12.64	-11.02 $-12.82$			
		11.00	22.00		11.05	12.10	12.20	12.10	22.01	12.02			
-25	-13.00	-13.18	-13.36	-13.54	-13.72	-13.90	-14.08	-14.26	-14.44	-14.62			
-26	-14.80	-14.98	-15.16	-15.34	-15.52	-15.70	-15.88	-16.06	-16.24	-16.42			
-27	-16.60	-16.78	-16.96	-17.14	-17.32	-17.50	-17.68	-17.86	-18.04	-18.22			
-28	-18.40	-18.58	-18.76	-18.94	-19.12	-19.30	-19.48	-19.66	-19.84	-20.02			
-29	-20.20	-20.38	-20.56	-20.74	-20.92	-21.10	-21.28	-21.46	-21.64	-21.82			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

					Tenths of	Degrees.				
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
-30	-22.00	-22.18	-22.36	-22.54	-22.72	-22.90	-23.08	-23.26	-23.44	-23.62
-31	-23.80	-23.98	-24.16	-24.34	-24.52	-24.70	-24.88	-25.06	-25.24	-25.42
-32	-25.60	<b>-25.7</b> 8	-25.96	-26.14	-26.32	-26.50	-26.68	-26.86	-27.04	-27.22
-33	-27.40	-27.58	-27.76	-27.94	-28.12	-28.30	-28.48	-28.66	-28.84	-29.02
-34	-29.20	-29.38	-29.56	-29.74	-29.92	-30.10	-30.28	-30.46	-30.64	-30.82
			:							02.02
-35	-31.00	-31.18	-31.36	-31.54	-31.72	<b>-31.90</b>	-32.08	-32.26	-32.44	-32.62
-36	-32.80	<b>-32.98</b>	-33.16	-33.34	-33.52	-33.70	-33.SS	-34.06	-34.24	-34.42
-37	-34.60	-34.78	-34.96	-35.14	-35.32	-35.50	-35.68	-35.S6	-36.04	-36.22
-38	-36.40	-36.58	-36.76	-36.94	-37.12	-37.30	-37.48	-37.66	-37.84	-38.02
-39	-38.20	-38.38	-38.56	-38.74	-38.92	-39.10	-39.28	-39.46	-39.64	-39.82
							00	47.00	17.44	47.00
-40	-40.00	-40.18	-40.36	-40.54	-40.72	-40.90	-41.08	-41.26	-41.44	-41.62
-41	<b>-41.</b> S0	-41.98	-42.16	-42.34	<b>-42.52</b>	-42.70	-42.88	-43.06	-43.24	-43.42
-42	-43.60	-43.78	-43.96	-44.14	-44.32	-44.50	-44.68	-44.86	-45.04	-45.22
-43	-45.40	-45.58	-45.76	-45.94	-46.12	-46.30	-46.48	-46.66	-46.84	-47.02
-44	-47.20	-47.38	-47.56	-47.74	47.92	-48.10	-48.28	-48.46	-48.64	-48.82
	40.00	10.70	40.00	-49.54	-49.72	-49.90	-50.08	-50.26	-50.44	-50.62
-45	-49.00	-49.18	-49.36 -51.16	-51.34	-49.72 $-51.52$	-45.50 -51.70	-50.05 -51.88	-50.20 $-52.06$	-52.24	-52.42
-46	-50.80	-50.98		-53,14	-51.52 -53.32	-51.70 -53.50	-53.68	-53.86	-54.04	-54.22
-47	-52.60	-52.78	-52.96			-55.30	-55.48	-55.66	-55.84	-56.02
-48	-54.40	-54.58	-54.76	-54.94	-55.12	-57.10	-57.28	-57.46	-57.64	-57.82
-49	-56.20	-56.38	-56.56	-56.74	-56.92	-57.10	-31.23	-57.40	-37.04	37.02
-50	-58.00	-58.18	-58.36	-58.54	-58.72	-58.90	-59.08	-59.26	-59.44	-59.62
-51	-59.80	-59.98	-60.16	-60.34	-60.52	-60.70	-60.88	-61.06	-61.24	-61.42
-52	-61.60	-61.78	-61.96	-62.14	-62.32	-62.50	-62.68	-62.86	-63.04	-63.22
-53	-63.40	-63.58	-63.76	-63.94	-64.12	-64.30	-64.48	-64.66	-64.84	-65.02
-54	-65.20	-65.38	-65.56	-65.74	-65.92	-66.10	-66.28	-66.46	-66.64	-66.82
0.1	00.20	00.00	00.00	00.71	00.02		1 00.20			

TABLE FOR COMPARING THE CENTIGRADE AND FAHRENHEIT'S THERMOMETERS NEAR THE BOILING POINT.

Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.									
100	212.00	212.18	212.36	212.54	212.72	212.90	213.08	213.26	213.44	213.62
99	210.20	210.38	210.56	210.74	210.92	211.10	211.28	211.46	211.64	211.82
98	208.40	208.58	208.76	208.94	209.12	209.30	209.48	209.66	209.84	210.02
97	206.60	206.78	206.96	207.14	207.32	207.50	207.68	207.86	208.04	208.22
96	204.80	204.98	205.16	205.34	205.52	205.70	205.88	206.06	206.24	206.42
95	203.00	203.18	203.36	203.54	203.72	203.90	204.08	204.26	204.44	204.62
94	201.20	201.38	201.56	201.74	201.92	202.10	202.28	202.46	202 64	202.82
93	199.40	199.58	199.76	199.94	200.12	200.30	200.48	200 66	200.84	201.02
92	197.60	197.78	197.96	198.14	198.32	198.50	198.68	198.86	199.04	199.22
91	195.80	195.98	196.16	196.34	196.52	196.70	196.88	197.06	197.24	197.42
90	194.00	194.18	194.36	194.54	194.72	194.90	195.08	195.26	195.44	195.62
89	192.20	192.38	192.56	192.74	192.92	193.10	193.28	193.46	193.64	193.82

	1								<u> </u>	
Centigrade					Tenths of	Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Reaum.	Reaum.	Reaum.	Reaum.	Reaum.	Reaum.	Reaum.	Reaum.	Reaum.	Reaum.
+40	+32.00	±32.08	+32.16	+32.24	+32.32	+32.40	+32.48	+32.56	+32.64	±32.72
39	31.20	31.28	31.36	31.44	31.52	00.18	31.68	31.76	31.84	31.92
38	30.40	30.48	30.56	30.64	30.72	30.80	30.88	30.96	31.04	31.12
37	29.60	29.68	29.76	29.84	29.92	30.00	30.08	30.16	30.24	30.32
36	28.80	28.88	28.96	29.04	29.12	29.20	29.28	29.36	29.44	29.52
35	28.00	28.08	28.16	28.24	28.32	28.40	28.48	28.56	28.64	28.72
34	27.20	27.28	27.36	27.44	27.52	27.60	27.68	27.76	27.84	27.92
33	26.40	26.48	26.56	26.64	26.72	26.80	26.88	26.96	27.04	27.12
32	25.60	25.68	25.76	25.84	25.92	26.00	26.08	26.16	26.24	26.32
31	24.80	24.88	24.96	25.04	25.12	25.20	25.28	25.36	25.44	25.52
30	24.00	24.08	24.16	24.24	25.32	24.40	24.48	24.56	24.64	24.72
29	23.20	23.28	23.36	23.44	23.52	23.60	23.68	23.76	23.84	23.92
28	22.40	22.48	22.56	22.64	22.72	22.80	22.88	22.96	23.04	23.12
27	21.60	21.68	21.76	21.84	21.92	22.00	22.08	22.16	22.24	22.32
26	20.80	20.88	20.96	21.04	21.12	21.20	21.28	21.36	21.44	21.52
25	20.00	20.08	20.16	20.24	20.32	20.40	20.48	20.56	20.64	20.72
24	19.20	19.28	19.36	19.44	19.52	19.60	19.68	19.76	19.84	19.92
23	18.40	18.48	18.56	18.64	18.72	18.80	18.88	18.96	19.04	19.12
22	17.60	17.68	17.76	17.84	17.92	18.00	18.08	18.16	18.24	18.32
21	16.80	16.88	16.96	17.04	17.12	17.20	17.28	17.36	17.44	17.52
20	16.00	16.08	16.16	16.24	16.32	16.40	16.48	16.56	16.64	16.72
19	15.20	15.28	15.36	15.44	15.52	15.60	15.68	15.76	15.84	15.92
18	14.40	14.48	14.56	14.64	14.72	14.80	14.88	14.96	15.04	15.12
17	13.60	13.68	13.76	13.84	13.92	14.00	14.08	14.16	14.24	14.32
16	12.80	12.88	12.96	13.04	13.12	13.20	13.28	13.36	13.44	13.52
15	12.00	12.08	12.16	12.24	12.32	12.40	12.48	12.56	12.64	12.72
14	11.20	11.28	11.36	11.44	11.52	11.60	11.68	11.76	11.84	11.92
13	10.40	10.48	10.56	10.64	10.72	10.80	10.88	10.96	11.04	11.12
12 11	9.60	9.68	9.76	9.84 9.04	9.92	10.00 9.20	10.08	10.16 9.36	10.24 9.44	10.32 9.52
11	8.80	8.88	8.96	9.04	9.12	9.20	9.28	9.36	9.44	9.32
10	8.00	8.08	8.16	8.24	8.32	8.40	8.48	8.56	8.64	8.72
9	7.20	7.28	7.36	7.44	7.52	7.60	7.68	7.76	7.84	7.92
8	6.40	6.48	6.56	6.64	6.72	6.80	6.88	6.96	7.04	7.12
7	5.60	5.68	5.76	5.84	5.92	6.00	6.08	6.16	6.24	6.32
6	4.80	4.88	4.96	5.04	5.12	5.20	5.28	5.36	5.44	5.52
5	4.00	4.08	4.16	4.24	4.32	4.40	4.48	4.56	4.64	4.72
4	3.20	3.28	3.36	3.44	3.52	3.60	3.68	3.76	3.84	3.92
3	2.40	2.48	2.56	2.64	2.72	2.80	2.88	2.96	3.04	3.12
2	1.60	1.68	1.76	1.84	1.92	2.00	2.08	2.16	2.24	2.32
1	0.80	0.88	0.96	1.04	1.12	1.20	1.28	1.36	1.44	1.52
0	0.00	0.08	0.16	0.24	0.32	0.40	0.48	0.56	0.64	0.72
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
1		1.	2.	3.	4.	٠.	0.	•	3.	3.

## VIII.-IX.

## COMPARISON

OF

## REAUMUR'S THERMOMETER

WITH

THE THERMOMETER OF FAHRENHEIT AND THE CENTIGRADE THERMOMETER,

OB

## TABLES

FOR CONVERTING DEGREES OF REAUMUR INTO DEGREES OF FAHRENHEIT

AND INTO CENTIGRADE DEGREES;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM +40° TO --40° REAUMUR.

					Tenths of	f Degrees.		<del></del>	0	
Degrees of Reaumur.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren. +122.67	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
+40	+122.00 119.75	+122.22 119.97	+122.45 $120.20$	120.42	120.65	+123.12 $120.87$	+123.35 121.10	+123.57 $121.32$	121.55	+124.02
39 38	117.50	117.72	117.95	118.17	118.40		118.85	119.07	119.30	121.77 119.52
37	115.25	115.47	115.70	115.92	116.15	116.37	116.60	116.82	117.05	117.27
36	113.00	113.22	113.45	113.67	113.90	114.12	114.35	114.57	114.80	115.02
35	110.75	110.97	111.20	111.42	111.65	111.87	112.10	112.32	112.55	112.77
34	108.50	108.72	108.95	109.17	109.40		109.85	110.07	110.30	110.52
33	106.25	106.47	106.70	106.92	107.15	107.37	107.60	107.82	108.05	108.27
32	104.00	104.22	104.45	104.67	104.90	105.12	105.35	105.57	105.80	106.02
31	101.75	101.97	102.20	102.42	102.65	102.87	103.10	103.32	103.55	103.77
30	99.50	99.72	99.95	100.17	100.40	100.62	100.85	101.07	101.30	101.52
29	97.25	97.47	97.70	97.92	98.15	98.37	98.60	98.82	99.05	99.27
28	95.00	95.22	95.45	95.67	95.90	96.12	96.35	96.57	96.80	97.02
27	92.75	92.97	93.20	93.42	93.65	93.87	94.10	94.32	94.55	94.77
26	90.50	90.72	90.95	91.17	91.40	91.62	91.85	92.07	92.30	92.52
25	88.25	88.47	88.70	88.92	89.15	89.37	89.60	89.82	90.05	90.27
24	86.00	86.22	86.45	86.67	86.90	87.12	87.35	87.57	87.80	88.02
23	83.75	83.97	84.20	84.42	84.65	84.87	85.10	85.32	85.55	85.77
22	81.50	81.72	81.95	82.17	82.40	82.62	82.85	83.07	83.30	83.52
21	79.25	79.47	79.70	79.92	80.15	80.37	80.60	80.82	81.05	81.27
20	77.00	77.22	77.45	77.67	77.90	78.12	78.35	78.57	78.80	79.02
19	74.75	74.97	75.20	75.42	75.65	75.87	76.10	76.32	76.55	76.77
18	72.50	72.72	72.95	73.17	73.40	73.62	73.85	74.07	74.30	74.52
17	70.25	70.47	70.70	70.92	71.15	71.37	71.60	71.82	72.05	72.27
16	68.00	68.22	68.45	68.67	68.90	69.12	69.35	69.57	69.80	70.02
15	65.75	65.97	66.20	66.42	66.65	66.87	67.10	67.32	67.55	67.77
14	63.50	63.72	63.95	64.17	64.40	64.62	64.85	65.07	65.30	65.52
13	61.25	61.47	61.70	61.92	62.15	62.37	62.60	62.82	63.05	63.27
12 11	59.00 56.75	59.22 56.97	59.45 57.20	59.67 57.42	59.90 57.65	60.12 57.87	60.35 58.10	60.57 58.32	60.S0 58.55	61.02 58.77
11	90.79	30.97	97.20	91.42	97.09	31.31	55.10	93.92	90.99	90.11
10	54.50	54.72	54.95	55.17	55.40	55.62	55.85	56.07	56.30	56.52
θ	52.25	52.47	52.70	52.92	53.15	53.37	53.60	53.82	54.05	54.27
8	50.00	50.22	50.45	50.67	50.90	51.12	51.35	51.57	51.80	52.02
7	47.75	47.97	48.20	48.42	48.65	48.87	49.10	49.32	49.55	49.77
6	45.50	45.72	45.95	46.17	46.40	46.62	46.85	47.07	47.30	47.52
5	43.25	43.47	43.70	43.92	44.15	44.37	44.60	44.82	45.05	45.27
4	41.00	41.22	41.45	41.67	41.90	42.12	42.35	42.57	42.80	43.02
3	38.75	38.97	39.20	39.42	39.65	39.87	40.10	40.32	40.55	40.77
2	36.50	36.72	36.95	37.17	37.40 25.15	37.62	37.85	38.07	38.30 36.05	38.52 36.27
	34.25	34.47	34.70	34.92	35.15	35.37	35.60	35.82		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

					Tenths o	f Degrees.	·			
Degrees of Reaumur.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
J+ 0	+32.00	+32.22	+32.45	+32.67	+32.90	+33.12	+33.35	+33.57	+33.80	+34.02
- 0	32.00	31.77	31.55	31.32	31.10	30.87	30.65	30.42	30.20	29.97
- 1	29.75	29.52	29.30	29.07	28.85	28.62	28.40	28.17	27.95	27.72
- 2	27.50	27.27	27.05	26.82	26.60	26.37	26.15	25.92	25.70	25.47
- 3	25.25	25.02	24.80	24.57	24.35	24.12	23.90	23.67	23.45	23.22
- 4	23.00	22.77	22.55	22.32	22.10	21.87	21.65	21.42	21.20	20.97
- 5	20.75	20.52	20.30	20.07	19.85	19.62	19.40	19.17	18.95	18.72
- 6	18.50	18.27	18.05	17.82	17.60	17.37	17.15	16.92	16.70	16.47
- 7	16.25	16.02	15.80	15.57	15.35	15.12	14.90	14.67	14.45	14.22
- 8	14.00	13.77	13.55	13.32	13.10	12.87	12.65	12.42	12.20	11.97
- 9	11.75	11.52	11.30	11.07	10.85	10.62	10.40	10.17	9.95	9.72
-10	9.50	9.27	9.05	8.82	8.60	8.37	8.15	7.92	7.70	7.47
-11	7.25	7.02	6.80	6.57	6.35	6.12	5.90	5.67	5.45	5.22
-12	5.00	4.77	4.55	4.32	4.10	3.87	3.65	3.42	3.20	2.97
-13	2.75	2.52	2.30	2.07	1.85	1.62	1.40	1.17	0.95	0.72
-14	0.50	0.27	0.05	- 0.17	- 0.40	- 0.62	- 0.85	- 1.07	- 1.30	- 1.52
-15	- 1.75	- 1.97	- 2.20	- 2.42	- 2.65	- 2.87	- 3.10	- 3.32	- 3.55	- 3.77
-16	- 4.00	- 4.22	- 4.45	- 4.67	- 4.90	- 5.12	- 5.35	- 5.57	- 5.80	- 6.02
-17	- 6.25	- 6.47	- 6.70	- 6.92	- 7.15	- 7.37	- 7.60	- 7.82	- 8.05	- 8.27
-18	- 8.50	- 8.72	- 8.95	- 9.17	- 9.40	-9.62	- 9.85	-10.07	-10.30	-10.52
-19	-10.75	-10.97	-11.20	-11.42	-11.65	-11.87	-12.10	-12.32	-12.55	-12.77
-20	-13.00	-13.22	-13.45	-13.67	-13.90	-14.12	-14.35	-14.57	-14.80	-15.02
-21	-15.25	-15.47	-15.70	-15.92	-16.15	-16.37	-16.60	-16.82	-17.05	-17.27
-22	-17.50	-17.72	-17.95	-18.17	-18.40	-18.62	-18.85	-19.07	-19.30	-19.52
-23	-19.75	-19.97	-20.20	-20.42	-20.65	-20.87	-21.10	-21.32	-21.55	-21.77
-24	-22.00	-22.22	-22.45	-22.67	-22.90	-23.12	-23.35	-23.57	-23.80	-24.02
-25	-24.25	-24.47	-24.70	-24.92	-25.15	-25.37	-25.60	-25.82	-26.05	-26.27
-26	-26.50	-26.72	-26.95	-27.17	-27.40	-27.62	-27.85	-28.07	-28.30	-28.52
-27	-28.75	-28.97	-29.20	-29.42	-29.65	-29.87	-30.10	-30.32	-30.55	-30.77
-28	-31.00	-31.22	-31.45	-31.67	-31.90	-32.12	-32.35	-32.57	-32.80	-33.02
-29	-33.25	-33.47	-33.70	-33.92	-34.15	-34.37	-34.60	-34.82	-35.05	-35.27
-30	-35.50	-35.72	-35.95	-36.17	-36.40	-36.62	-36.85	-37.07	-37.30	-37.52
-31	-37.75	-35.72 -37.97	-38.20	-38.42	-38.65	-38.87	-39.10	-39.32	-37.50 $-39.55$	-37.32 $-39.77$
-31 -32	-40.00	-37.97 $-40.22$	-40.45	-40.67	-40.90	-41.12	-41.35	-39.52 $-41.57$	-41.80	-39.77 $-42.02$
-33	-42.25	-40.22 $-42.47$	-40.45 $-42.70$	-40.07 $-42.92$	-43.15	-43.37	-43.60	-43.82	-41.05	-44.27
-34	-44.50	-44.72	-44.95	-45.17		-45.62	-45.85	-46.07	-46.30	-46.52
-35	-46.75	-46.97	-47.20	-47.42	-47.65	-47.87	-48.10	-48.32	-48.55	-48.77
-36	-49.00	-49.22	-49.45	-49.67	-49.90	-50.12	-50.35	-50.57	-50.80	-51.02
-37	-51.25	-51.47	-51.70	-51.92	-52.15	-52.37	-52.60	-52.82	-53.05	-53.27
-38 -39	-53.50 -55.75	-53.72 -55.97	-53.95 -56.20	-54.17 $-56.42$	-54.40 -56.65	-54.62 $-56.87$	-54.85 -57.10	-55.07 -57.32	-55.30 $-57.55$	-55.52 -57.77
	-00.10	-00.01	-50.20		-50.05		-57.10			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

					Tenths of	Degrees.				
Degrees of Reaumur.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
+ 10	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
±40	+50.00	+50.13	±50.25	±50.38	±50.50 49.25	±50.63	+50.75	±50.88	±51.00	±51.13 49.88
39 38	48.75	48.88	49.00	49.13 47.88	48.00	49.38 48.13	49.50 48.25	49.63	49.75	48.63
37	46.25	46.38	46.50	46.63	46.75	46.88	48.25	47.13	47.25	47.38
36	45.00	45.13	45.25	45.38	45.50	45.63	45.75	45.88	46.00	46.13
30	45.00	45.15	49.29	43.35	49.50	40.03	49.75	49.88	40.00	40.15
35	43.75	43.88	44.00	44.13	44.25	44.38	44.50	44.63	44.75	44.88
34	42.50	42.63	42.75	42.88	43.00	43.13	43.25	43.38	43.50	43.63
33	41.25	41.38	41.50	41.63	41.75	41.88	42.00	42.13	42.25	42.38
32	40.00	40.13	40.25	40.38	40.50	40.63	40.75	40.88	41.00	41.13
31	38.75	38.88	39.00	39.13	39.25	39.38	39.50	39.63	39.75	39.88
30	37.50	37.63	37.75	37.88	38.00	38.13	38.25	38.38	38.50	38.63
29	36.25	36.38	36.50	36.63	36.75	36.88	37.00	37.13	37.25	37.38
28	35.00	35.13	35.25	35.38	35.50	35.63	35.75	35.88	36.00	36.13
27	33.75	33.88	34.00	34.13	34.25	34.38	34.50	34.63	34.75	34.88
26	32.50	32.63	32.75	32.88	33.00	33.13	33.25	33.38	33.50	33.63
25	31.25	31.38	31.50	31.63	31.75	31.88	32.00	32.13	32.25	32.38
24	30.00	30.13	30.25	30.38	30.50	30.63	30.75	30.88	31.00	31.13
23	28.75	28.88	29.00	29.13	29.25	29.38	29.50	29.63	29.75	29.88
22	27.50	27.63	27.75	27.88	28.00	28.13	28.25	28.38	28.50	28.63
21	26.25	26.38	26.50	26.63	26.75	26.88	27.00	27.13	27.25	27.38
20	25.00	25.13	25.25	25.38	25.50	25.63	25.75	25.88	26.00	26.13
19	23.75	23.88	24.00	24.13	24.25	24.38	24.50	24.63	24.75	24.88
18	22.50	22.63	22.75	22.88	23.00	23.13	23.25	23.38	23.50	23.63
17	21.25	21.38	21.50	21.63	21.75	21.88	22.00	22.13	22.25	22.38
16	20.00	20.13	20.25	20.38	20.50	20.63	20.75	20.88	21.00	21.13
										70.00
15	18.75	18.88	19.00	19.13	19.25	19.38	19.50	19.63	19.75	19.88
14	17.50	17.63	17.75	17.88	18.00	18.13	18.25	18.38	18.50	18.63
13	16.25	16.38	16.50	16.63	16.75	16.88	17.00	17.13	17.25	17.38
12 11	15.00 13.75	15.13 13.88	15.25 14.00	15.38 14.13	15.50 14.25	15.63 14.38	15.75 14.50	15.88 14.63	16.00 14.75	16.13 14.88
10	12.50	12.63	12.75	12.88	13.00	13.13	13.25	13.38	13.50	13.63
9	11.25	11.38	11.50	11.63	11.75	11.88	12.00	12.13	12.25	12.38
8	10.00	10.13	10.25	10.38	10.50	10.63	10.75	10.88	11.00	11.13
7 6	8.75 7.50	8.88 7.63	9.00 7.75	9.13 7.88	9.25 8.00	9.38 8.13	9.50 8.25	9.63 8.38	9.75 8.50	9.88 8.63
5	6.25	6.38	6.50	6.63	6.75	6.88	7.00	7.13	7.25	7.38
4	5.00	5.13	5.25	5.38	5.50	5.63	5.75	5.88	6.00	6.13
3 2	3.75	3.88	4.00	4.13	4.25	4.38	4.50	4.63	4.75	4.88 3.63
1	2.50 1.25	2.63 1.38	2.75 1.50	2.88 1.63	3.00 1.75	3.13 1.88	3.25 2.00	3.38 2.13	3.50 2.25	2.38
0	0.00	0.13	0.25	0.38	0.50	0.63	0.75	0.88	1.00	1.13
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

X. - XV.

TABLES

FOR

## COMPARING THERMOMETRICAL DIFFERENCES

EXPRESSED IN DEGREES OF DIFFERENT SCALES,

IRRESPECTIVE OF THEIR ZERO POINT.

## X. NUMBER OF DEGREES OF FAHRENHEIT = NUMBER OF CENTIGRADE DEGREES.

4° Reaumur = 5° Centigrade = 9° Fahrenheit.

Degrees					Tenths of	a Degree.				
of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
0	0.00	0.06	0.11	0.17	0.22	0.28	0.33	0.39	0.44	0.50
1	0.56	0.61	0.67	0.72	0.78	0.83	0.89	0.94	1.00	1.06
2	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61
3	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.22
4	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72
5	2.78	2.83	2.89	2.94	3.00	3.06	3.11	3.17	3.22	3.28
6	3.33	3.39	3.44	3.50	3.56	3.61	3.67	4.72	3.78	3.83
7	3.89	3.94	4.00	4.06	4.11	4.17	4.22	4.28	4.33	4.39
8	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.83	4.89	4.94
9	5.00	5.06	5.11	5.17	5.22	5.28	5.32	5.39	5.44	5.50

### XI. NUMBER OF DEGREES OF FAHRENHEIT = NUMBER OF DEGREES OF REAUMUR.

Degrees					Tenths of	a Degree.		<del>,</del>		
of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Reaumur.	Reaumur.	Reaumur	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.
0	0.00	0.04	0.09	0.13	0.18	0.22	0.27	0.31	0.36	0 40
1	0.44	0.49	0.53	0.58	0.62	0.67	0.71	0.76	0.80	0.84
2	0.89	0.93	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29
3	1.33	1.38	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.73
4	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.13	2.18
5	2.22	2.27	2.31	2.36	2.40	2.44	2.49	2.53	2.58	2.62
6	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07
7	3.11	3.16	3.20	3.24	3.29	3.33	3.38	3.42	3.47	3.51
8	3.56	3.60	3.64	3.69	3.73	3.78	3.82	3.87	3.91	3.96
9	4.00	4.04	4.09	4.13	4.18	4.22	4.27	4.31	4.36	4.40

### XII. NUMBER OF CENTIGRADE DEGREES = NUMBER OF DEGREES OF REAUMUR.

					Tenths of	a Degree.				
Centig. Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Reaumur.	Reaumur	Reaumur.	Reaumur.	Reaumur	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.
0	0.00	0.08	0.16	0.24	0.32	0.40	0.48	0.56	0.64	0.72
1	0.80	0.88	0.96	1.04	1.12	1.20	1.28	1.36	1.44	1.52
2	1.60	1.68	1.76	1.84	1.92	2.00	2.08	2.16	2.24	2.32
3	2.40	2.48	2.56	2.64	2.72	2.80	2.88	2.96	3.04	3.12
4	3.20	3.28	3.36	3.44	3.52	3.60	3.68	3.76	3.84	3.92
5	4.00	4.08	4.16	4.24	4.32	4.40	4.48	4.56	4.64	4.72
6	4.80	4.88	4.96	5.04	5.12	5.20	5.28	5.36	5.44	5.52
7	5.60	5.68	5.76	5.84	5.92	6.00	6.08	6.16	6.24	6.32
8	6.40	6.48	6.56	6.64	6.72	6.80	6.88	6.96	7.04	7.12
9	7.20	7.28	7.36	7.44	7.52	7.60	7.68	7.76	7.84	7.92

XIII. NUMBER OF CENTIGRADE DEGREES — NUMBER OF DEGREES OF FAHRENHEIT.

4° Reaumur = 5° Centigrade = 9° Fahrenheit.

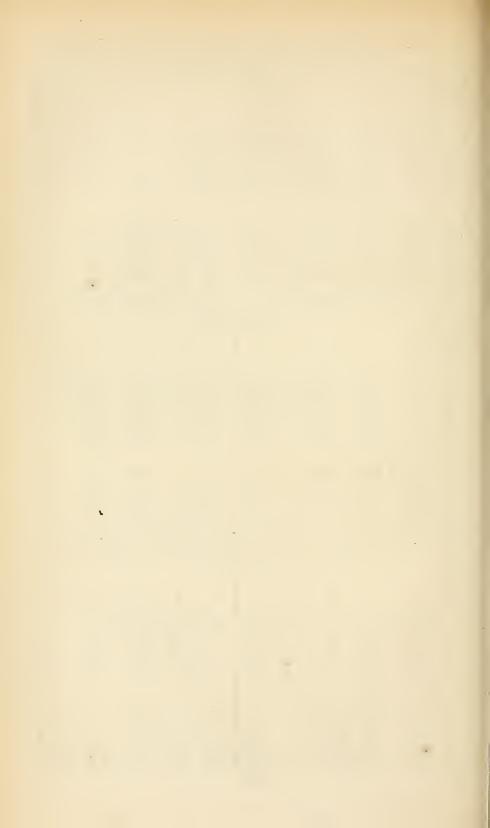
					Tenths of	a Degree.				
Centig. Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.
0	0.00	0.18	0.36	0.54	0.72	0.90	1.08	1.26	1.44	1.62
1	1.80	1.98	2.16	2.34	2.52	2.70	2.88	3.06	3.24	3.42
2	3.60	3.78	3.96	4.14	4.32	4.50	4.68	4.86	5.04	5.22
3	5.40	5.58	5.76	5.94	6.12	6.30	6.48	6.66	6.84	7.02
4	7.20	7.38	7.56	7.74	7.92	8.10	8.28	8.46	8.64	8.82
5	9.00	9.18	9.36	9.54	9.72	9.90	10.08	10.26	10.44	10.62
6	10.80	10.98	11.16	11.34	11.52	11.70	11.88	12.06	12.24	12.42
7	12.60	12.78	12.96	13.14	13.32	13.50	13.68	13.86	14.04	14.22
8	14.40	14.58	14.76	14.94	15.12	15.30	15.48	15.66	15.84	16.02
9	16.20	16.38	16.56	16.74	16.92	17.10	17.28	17.46	17.64	17.82

#### XIV. NUMBER OF DEGREES OF REAUMUR - NUMBER OF CENTIGRADE DEGREES.

D					Tenths of	a Degree.				
Degrees of Reaum.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
0	0.00	0.12	0.25	0.37	0.50	0.62	0.75	0.87	1.00	1.12
1	1.25	1.37	1.50	1.62	1.75	1.87	2.00	2.12	2.25	2.37
2	2.50	2.62	2.75	2.87	3.00	3.12	3.25	3.37	3.50	3.62
3	3.75	3.87	4.00	4.12	4.25	4.37	4.50	4.62	4.75	4.87
4	5.00	5.12	5.25	5.37	5.50	5.62	5.75	5.87	6.00	6.12
5	6.25	6.37	6.50	6.62	6.75	6.87	7.00	7.12	7.25	7.37
1									1	8.62
6	7.50	7.62	7.75	7.87	8.00	8.12	8.25	8.37	8.50	
7	8.75	8.87	9.00	9.12	9.25	9.37	9.50	9.62	9.75	9.87
8	10.00	10.12	10.25	10.37	10.50	10.62	10.75	10.87	11.00	11.12
9	11.25	11.37	11.50	11.62	11.75	11.87	12.00	12.12	12.25	12.37

### XV. NUMBER OF DEGREES OF REAUMUR = NUMBER OF DEGREES OF FAHRENHEIT.

	Tenths of a Degree.												
Degrees of Reaum.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.			
0	0.00	0.22	0.45	0.67	0.90	1.12	1.35	1.57	1.80	2.02			
1	2.25	2.47	2.70	2.92	3.15	3.37	3.60	3.82	4.05	4.27			
2	4.50	4.72	4.95	5.17	5.40	5.62	5.85	6.07	6.30	6.52			
3	6.75	6.97	7.20	7.42	7.65	7.87	8.10	8.32	8.55	8.77			
4	9.00	9.22	9.45	9.67	9.90	10.12	10.35	10.57	10.80	11.02			
5	11.25	11.47	11.70	11.92	12.15	12.37	12.60	12.82	13.05	13.27			
6	13.50	13.72	13.95	14.17	14.40	14.62	14.85	15.07	15.30	15.52			
7	15.75	15.97	16.20	16.42	16.65	16.87	17.10	17.32	17.55	17.77			
8	18.00	18.22	18.45	18.67	18.90	19.12	19.35	19.57	19.80	20.02			
9	20.25	20.47	20.70	20.92	21.15	21.37	21.60	21.82	22.05	22.27			



# METEOROLOGICAL TABLES.

II.

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## HYGROMETRICAL TABLES.

HYGROMETERS, or instruments used for determining the amount of aqueous vapor present in the air, are of three classes. In the first, we find the hygrometers based on the absorption of moisture by hygroscopic substances, the best of which is Saussure's Hair-Hygrometer; in the second class, the Psychrometer, or wet-bulb thermometer, which gives the temperature of evaporation; in the third, the various instruments designed for ascertaining the temperature of the dew-point. From the data furnished by each of these instruments, and a table of the elastic forces of vapor at different temperatures, the humidity of the air can be deduced with more or less accuracy.

The use of the hygroscopic substances as hygrometers having been nearly given up on account of the inaccuracy of the results, the variability of the instruments, and the difficulty, if not impossibility, of making them comparable, the psychrometer and the dew-point instruments represent the two methods now usually employed in Meteorology. The following set, therefore, contains extensive tables, in French and English measures, for deducing the hygrometrical condition of the atmosphere from the indications of the Psychrometer and of the dew-point instruments, to which have been added tables of the weight of vapor, in a given space, at different temperatures,—an element often needed in Meteorology.

As, however, the results deduced from the same data furnished by the observations may considerably differ, according to the values of the elastic force of vapor, and the formulæ used in the computation, the tables have been arranged in two series.

The first series contains Regnault's table of the elastic forces of vapor, with tables of the three kinds above mentioned, together with a corresponding set in English measures. Tables V. to X. have been computed for this volume.

The second series gives the table of elastic forces of vapor deduced from Dalton's experiments, and adopted in the Greenwich Observations, together with the various tables based on it.

B

#### HYGROMETRICAL TABLES.

A third series of miscellaneous tables furnishes the means of comparing the different values of the elastic force and weight of vapor determined by various physicists, as well as the results of Saussure's Hair-Hygrometer, with those obtained by other methods.

An Appendix, containing tables for comparing the quantity of rain-water indicated in different measures, closes the set.

Though the first series of tables, based on Regnault's table of tensions, is recommended for ordinary use, as being derived from the determinations which seem to deserve the greatest degree of confidence, it was thought expedient to give also the Greenwich tables, which have been, and still are, so extensively used in England, in order to enable meteorologists to judge of the differences which exist between the results obtained by them and those deduced from the constants of Regnault and others.

# PRACTICAL TABLES,

IN

FRENCH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

B



### TABLE

OF

### THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES,

BY REGNAULT.

This table contains the elastic forces of vapor corresponding to every tenth of a degree of temperature between —35° and +40° Centigrade, as determined by the experiments of V. Regnault, made by order of the French government, for the purpose of establishing the numerical value of the elements which enter into the computations concerning the steam-engine. These results are generally considered as the most accurate science possesses at present. They are published in the Mémoires de l'Institut, Tom. XXI.; and more correctly in Regnault's Etudes sur l'Hygrométrie, in the Annales de Chimie et de Physique. In Vol. XV. Regnault gives the table of elastic forces for every tenth of a degree from —10° to +35° Centigrade, which is reprinted in Table I. The numbers below —10° and above +35°, in the same table, have been taken from another table for every full degree, previously published in Vol. XI. p. 333 of the same periodical, and in the same volume of the Mémoires de l'Institut, extending from —32° to +230°.

It should be remarked, however, that the numbers below zero, in the two tables just mentioned, having been computed from different formulas of interpolation, slightly disagree. In order to establish a continuity, therefore, the numbers in Table I. corresponding to full degrees from  $-10^{\circ}$  to  $-35^{\circ}$  have been formed by starting from the value due to  $-10^{\circ}$  in the larger table of Regnault, and subtracting from it the difference between  $-10^{\circ}$  and  $-11^{\circ}$  in the other table, in order to find the value of  $-11^{\circ}$ , and so on, by subtracting successively the corresponding differences to  $-35^{\circ}$ . For the fractions of degrees below  $-10^{\circ}$ , the mean values have been adopted as sufficiently accurate for meteorological purposes.

B

## I. ELASTIC FORCE OF AQUEOUS VAPOR,

## EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

#### BY REGNAULT.

Tempera-					Tenths of	Degrees.				
ture Centigrade.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
-35	0.221	0.219	0.216	0.214	0.211	0.209	0.207	0.204	0.202	0.199
-34	0.247	0.244	0.242	0.249	0.237	0.234	0.231	0.229	0.226	0.224
-33	0.275	0.272	0.269	0.267	0.264	0.261	0.258	0.255	0.253	0.250
-32	0.305	0.302	0.299	0.296	0.293	0.290	0.287	0.284	0.281	0.278
-31	0.337	0.334	0.331	0.327	0.324	0.321	0.318	0.315	0.311	.0.308
-30	0.371	0.368	0.364	0.361	0.357	0.354	0.351	0.347	0.344	0.340
-29	0.409	0.405	0.401	0.398	0.394	0.390	0.386	0.382	0.379	0.375
-28	0.449	0.445	0.441	0.437	0.433	0.429	0.425	0.421	0.417	0.413
-27	0.493	0.489	0.484	0.480	0.475	0.471	0.467	0.462	0.458	0.453
-26	0.540	0.535	0.531	0.526	0.521	0.516	0.512	0.507	0.502	0.498
-25	0.590	0.585	0.580	0.575	0.570	0.565	0.560	0.555	0.550	0.545
-24	0.645	0.639	0.634	0.628	0.623	0.617	0.612	0.606	0.601	0.595
-23	0.704	0.698	0.692	0.686	0.680	0.674	0.669	0.663	0.657	0.651
-22	0.768	0.762	0.755	0.749	0.742	0.736	0.730	0.723	0.717	0.710
-21	0.838	0.831	0.824	0.817	0.810	0.803	0.796	0.789	0.782	0.775
-20	0.912	0.905	0.897	0.890	0.882	0.875	0.868	0.860	0.853	0.845
-19	0.993	0.985	0.977	0.969	0.961	0.952	0.944	0.936	0.928	0.920
-18	1.080	1.071	1.063	1.054	1.045	1.036	1.028	1.019	1.010	1.002
-17	1.174	1.165	1.155	1.146	1.136	1.127	1.118	1.108	1.099	1.089
-16	1.275	1.265	1.255	1.245	1.235	1.224	1.214	1.204	1.194	1.184
-15	1.385	1.374	1.363	1.352	1.341	1.330	1.319	1.308	1.297	1.286
-14	1.503	1.491	1.479	1.468	1.456	1.444	1.432	1.420	1.409	1.397
-13	1.631	1.618	1.605	1.593	1.580	1.567	1.554	1.541	1.529	1.516
-12	1.768	1.754	1.741	1.727	1.713	1.699	1.686	1.672	1.658	1.645
-11	1.918	1.903	1.888	1.873	1.858	1.843	1.828	1.813	1.798	1.783
-10	2.078	2.062	2.046	2.030	2.014	1.998	1.982	,1.966	1.950	1.934
- 9	2.261	2.242	2.223	2.204	2.186	2.168	2.150	2.132	2.114	2.096
- 8	2.456	2.436	2.416	2.396	2.376	2.356	2.337	2.318	2.299	2.280
- 7	2.666	2.645	2.624	2.603	2.582	2.561	2.540	2.519	2.498	2.477
- 6	2.890	2.867	2.844	2.821	2.798	2.776	2.754	2.732	2.710	2.688
- 5	3.131	3.106	3.082	3.058	3.034	3.010	2.986	2.962	2.938	2.914
- 4	3.387	3.361	3.335	3.309	3.283	3.257	3.231	3.206	3.181	3.156
- 3	3.662	3.634	3.606	3.578	3.550	3.522	3.495	3.468	3.441	3.414
- 2	3.955	3.925	3.895	3.865	3.836	3.807	3.778	3.749	3.720	3.691
- 1	4.267	4.235	4.203	4.371	4.140	4.109	4.078	4.047	4.016	3.985
- 0	4.600	4.565	4.531	4.497	4 463	4.430	4.397	4.364	4.331	4.299
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centigrade					Tenths of	f Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 4.600	Millim. 4.633	Millim. 4.667	Millim. 4.700	Millim. 4.733	Millim.	Millim. 4.801	Millim. 4.836	Millim. 4.871	Millim. 4.905
1	4.940	4.975	5.011	5.047	5.082	5.118	5.155	5.191	5.228	5.265
2	5.302	5.340	5.378	5.416	5.454	5.491	5.530	5.569	5.608	5.647
3	5.687	5.727	5.767	5.807	5.848	5.889	5.930	5.972	6.014	6.055
4	6.097	6.140	6.183	6.226	6.270	6.313	6.357	6.401	6.445	6.490
5	6.534	6.580	6.625	6.671	6.717	6.763	6.810	6.857	6.904	6.951
6	6.998	7.047	7.095	7.144	7.193	7.242	7.292	7.342	7.392	7.442
7	7.492	7.544	7.595	7.647	7.699	7.751	7.804	7.857	7.910	7.964
8	8.017	8.072	8.126	8.181	8.236	8.291	8.347	8.404	8.461	8.517
9	8.574	8.632	8.690	8.748	8.807	8.865	8.925	8.985	9.045	9.105
10	9.165	9.227	9.288	9.350	9.412	9.474	9.537	9.601	9.665	9.728
11	9.792	9.857	9.923	9.989	10.054	10.120	10.187	10.255	10.322	10.389
12	10.457	10.526	10.596	10.665	10.734	10.804	10.875	10.947	11.019	11.090
13	11.162	11.235	11.309	11.383	11.456	11.530	11.605	11.681	11.757	11.832
14	11.908	11.986	12.064	12.142	12.220	12.298	12.378	12.458	12.538	12.619
15	12.699	12.781	12.864	12.947	13.029	13.112	13.197	13.281	13.366	13.451
16	13.536	13.623	13.710	13.797	13.885	13.972	14.062	14.151	14.241	14.331
17	14.421	14.513	14.605	14.697	14.790	14.882	14.977	15.072	15.167	15.262
18	15.357	15.454	15.552	15.650	15.747	15.845	15.945	16.045	16.145	16.246
19	16.346	16.449	16.552	16.655	16.758	16.861	16.967	17.073	17.179	17.285
20	17.391	17.500	17.608	17.717	17.826	17.935	18.047	18.159	18.271	18.383
21	18.495	18.610	18.724	18.839	18.954	19.069	19.187	19.305	19.423	19.541
22	19.659	19.780	19.901	20.022	20.143	20.265	20.389	20.514	20.639	20.763
23	20.888	21.016	21.144	21.272	21.400	21.528	21.659	21.790	21.921	22.053
24	22.184	22.319	22.453	22.588	22.723	22.858	22.996	23.135	23.273	23.411
25	23.550	23.692	23.834	23.976	24.119	24.261	24.406	24.552	24.697	24.842
26	24.988	25.138	25.288	25.438	25.588	25.738	25.891	26.045	26.198	26.351
27	26.505	26.663	26.820	26.978	27.136	27.294	27.455	27.617	27.778	27.939
28	28.101	28.267	28.433	28.599	28.765	28.931	29.101	29.271	29.441	29.612
29	29.782	29.956	30.131	30.305	30.479	30.654	30.833	31.011	31.190	31.369
30	31.548	31.729	31.911	32.094	32.278	32.463	32.650	32.837	33.026	33.215
31	33.406	33.596	33.787	33.980	34.174	34.368	34.564	34.761	34.959	35.159
32	35.359	35.559	35.760	35.962	36.165	36.370	36.576	36.783	36.991	37.200
33	37.410	37.621	37.832	38.045	38.258	38.473	38.689	38.906	39.124	39.344
34	39.565	39.786	40.007	40.230	40.455	40.680	40.907	41.135	41.364	41.595
35	41.827	42.059	42.293	42.527	42.763	43.000	43.238	43.477	43.717	43.959
36	44.201	44.445	44.690	44.936	45.183	45.431	45.681	45.932	46.184	46.437
37	46.691	46.947	47.203	47.462	47.721	47.981	48.243	48.506	48.770	49.035
38	49.302	49.570	49.839	50.110	50.382	50.655	50.929	51.205	51.481	51.759
39	52.039	52.320	52.602	52.885	53.170	53.456	53.743	54.032	54.322	54.613
40	54.906	55.200	55.496	55.793	56.091	56.391	56.692	56.994	<b>57.29</b> 8	57.603
	0.	1.	2.	3.	4.	5.	6.	7.	S.	9.

### PSYCHROMETRICAL TABLES.

GIVING IMMEDIATELY THE FORCE OF AQUEOUS VAPOR AND THE RELATIVE HUMIDITY FROM THE INDICATIONS OF THE PSYCHROMETER.

CALCULATED BY M. T. HAEGHENS.

In his Etudes sur l'Hygrométrie,\* M. V. Regnautt discusses the theoretical bases of the formula of the Psychrometer, given by M. August, which was,

$$x = f' - \frac{0.568 (t - t')}{640 - t'} h,$$

in which h represents the height of the barometer; t the temperature of the air given by the dry-bulb thermometer; t' the temperature of the wet-bulb thermometer; f' the force of aqueous vapor in the saturated air at a temperature equal to t'; x the elastic force of aqueous vapor which exists in the air at the time of the observation.

After having modified some of the numerical values, which form the coefficients, M. Regnault adopted this formula,

$$x = f' - \frac{0.429 (t - t')}{610 - t'} h.$$

But comparative experiments, made by himself, showed that by substituting the coefficient 0.480 for that of 0.429, the calculated results, and those obtained by direct observation, agree perfectly in the fractions of saturation, which are greater than 0.40. This formula thus modified, or

$$x = f' - \frac{0.480(t-t')}{610-t'} h$$

has been used for calculating the following tables. In that part of the tables which supposes the wet-bulb to be covered with a film of ice, or below the freezing point, the value 610 — t', which represents the latent heat of aqueous vapor, has been changed into this: 610 + 79 - t' = 689 - t'.

The only hypothesis made, is that of a mean barometric pressure h, equal to 755 millimetres. If we take into account the causes of errors inherent to the psychrometer, and to the tables of the force of vapor, by means of which the absolute force of vapor is calculated, as well as to the differences of these tensions, taken at temperatures differing only by one tenth of a degree, it will be obvious that the correction due to the variations of barometric pressure can almost always be neglected. Nevertheless, a separate table has been calculated, giving the correction to be applied to the numbers in the Psychrometrical Tables for the heights of the barometer between 650 and 800 millimetres. It will be found at the end of the tables.

The disposition of the tables is the following: —

The temperatures are noted in centigrade degrees; the elastic force of vapor in the air, or its pressure on the barometer, is expressed in millimetres of mercury; the rel-

<sup>\*</sup> Etudes sur l'Hygrométrie, par M. V. Regnault. Annales de Chimie et de Physique, 3<sup>me</sup> Série, Tom XV., 1845. B

#### PSYCHROMETRICAL TABLES.

ative humidity is indicated in per cent. of the full saturation of the air at the corresponding temperature of the dry-bulb thermometer t.

The first vertical column contains the indications of the wet-bulb thermometer t', beginning with the temperatures below the freezing point, when the bulb is covered with ice, from  $-35^{\circ}$ , and continuing from the freezing point up to  $+35^{\circ}$  centigrade, the bulb being simply wet.

The second column gives the differences of the force of vapor for each tenth (0°.1) of a degree, between each full degree of the first column. It enables the observer to find out the correction for any fraction of a degree of the wet-bulb thermometer.

The following double columns give immediately the force of vapor and the relative humidity, corresponding to each degree of the wet-bulb, placed in the first column, on the same horizontal line, and to differences of the two thermometers, or to t-t', taken at every two tenths of a degree.

The horizontal column at the bottom indicates the mean difference, for each tenth of a degree, of the force of vapor contained in the same horizontal line. It gives the correction for the intermediate differences of the thermometers; 0.1, 0.3, 0.5, 0.7, 0.9, &c., &c.

To meet the wants arising from the extreme climate of North America, the tables of Mr. Haeghens have been extended from -15° to -35° centigrade, and from +30° to +35° of temperature of the wet-bulb, and to +40° of temperature of the dry-bulb thermometer. The forces of aqueous vapor of Regnault, as given in Table I., have been used for the calculations.

## Use of the Tables.

Enter the tables with the difference of the two thermometers, or t-t', and with the temperature of the wet-bulb thermometer t', taking the first three pages, when the temperature of the wet-bulb is below the freezing point; and the following ones when it is above the freezing point.

Seek first the column at the head of which you find the difference of the thermometers; go down as far as the horizontal line, at the beginning of which you see the temperature of the wet-bulb thermometer; there you find the force of vapor, and the relative humidity corresponding to your observation.

Two corrections for fractions may be required for a complete calculation of the force of vapor; one for the fractions of degrees of the wet-bulb thermometer; another for the intermediate differences of the two thermometers, viz. for 0.1, 0.3, 0.5, 0.7, &c.

The first correction for fractions of degrees of the wet-bulb thermometer is found by multiplying the decimal fraction by the number placed in the second vertical column next to the whole degree, which number is the value of a tenth of a degree. The product must be *added* to the value of the full degree given in the table, when the temperature of the wet-bulb is above the freezing point; it must be *subtracted* when the temperature is below the freezing point, and receives the sign —. This correction is too important to be neglected.

The second correction, less important, for the intermediate differences of the ther-

### PSYCHROMETRICAL TABLES.

mometers, which are greater by one tenth than those indicated in the tables, is given in the horizontal column at the bottom of the page. It is constant and always subtractive.

## Examples of Calculation.

Difference of thermometers, or  $t - t' = 0^{\circ}.8$ .

Temperature of the wet-bulb thermometer,  $t' = 11^{\circ}.0$ .

We find, page 18, for t-t', fifth double column; and for t', first column,

The force of vapor in the air =  $9^{mm}$ .31.

Relative humidity,

= 90.

Difference of thermometers, or t-t', = 7°.2.

Wet-bulb thermometer, or t', = 17°.9.

We find, page 24, for  $t - t' = 7^{\circ}.2$ , and  $t' = 17^{\circ}.0$ , force of vapor  $10^{\text{mm}}.02$ .

Additive correction for fraction 0°.9, or  $9 \times 0.09 = 0$  .81.

Force of vapor in the air = 10 .83.

Relative humidity, 46

Difference of thermometers,  $t-t'=6^{\circ}.5$ .

Wet-bulb thermometer,  $t' = 23^{\circ}.6$ .

We find, page 23, for  $t' = 23^{\circ}.0$ , and t - t', or difference,  $= 6^{\circ}.4$ , force of vapor  $16^{\text{mm}}.94$ ; applying immediately the correction found at the bottom of the page for one tenth more difference, or  $6^{\circ}.4 + 0.1 = 6^{\circ}.5$ , we have,

Force of vapor =  $16^{mm} \cdot .94 - 0.06$ , or

16mm.88.

Additive correction for fraction 0.6 of the wet-bulb,  $6 \times 0.13 = 0$  .78.

Force of vapor in the air = 17 .66.

Relative humidity,

56.

The wet-bulb thermometer covered with ice.

Difference of thermometers,  $t - t' = 2^{\circ}.8$ .

Wet-bulb thermometer (ice),  $t' = -8^{\circ}.5$ .

Page 17 gives for  $t-t'=2^{\circ}.8$ , and  $t'=-8^{\circ}.0$ , force of vapor =  $1^{\text{mm}}.0$ . Subtractive correction for fraction 0.5 of wet-bulb,  $5 \times 0.019 = -0$  .1.

Force of vapor in the air = 0 .9.

Relative humidity,

30.

### II. PSYCHROMETRICAL TABLES.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

	$\mathbf{t}-\mathbf{t}'$ , Difference of Wet and Dry Bulb Thermometers.												
Wet-				t -	-t', Diff	erence of	Wet ar	nd Dry Bu	ılb <b>T</b> he	rmometer	8.		
Bulb Thermo- meter t'	Mean Vertical Differ-	00.	.0	0°.	.2	0°.	4	<b>0</b> °.	6	00.	8	10.	.0
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid-ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim		Millim.		Millim.	
-35	0.003	0.22	100	0.12	53								1
-34	0.003	0.25	100	0.15	58	0.05	18						
-33	0.003	0.27	100	0.17	62	0.07	26						
-32	0.003	0.30	100	0.20	66	0.10	33	0.00					
-31	0.001	0.34	100	0.24	69	0.14	39	0.03	10				
-30	0.004	0.37	100	0.27	71	0.17	44	0.07	17				
-29	0.004	0.41	100	0.31	74	0.21	46	0.11	25				
-28	0.004	0.45	100	0.35	76	0.25	53	0.15	31	0.04	9		
-27	0.004	0.49	100	0.39	78	0.29	57	0.19	36	0.09	17		
-26	0.005	0.54	100	0.44	80	0.34	60	0.24	41	0.13	23	0.03	6
	0.005												
-25	0.000	0.59	100	0.49	81	0.39	63	0.29	46	0.18	29	0.08	12
-24	0.005	0.64	100	0.54	82	0.44	66	0.34	50	0.24	34	0.14	19
-23	0.006	0.70	100	0.60	84	0.50	69	0.40	53	0.30	39	0.19	25
-22	0.006	0.77	100	0.67	85	0.56	71	0.46	57	0.36	44	0.26	31
-21	0.007	0.84	100	0.74	86	0.63	73	0.53	60	0.43	48	0.33	36
	0.008												
-20	0.008	0.91	100	0.81	87	0.71	75	0.61	63	0.50	51	0.40	40
-19	0.003	0.99	100	0.89	88	0.79	77	0.69	66	0.58	55	0.48	45
-18	0.009	1.08	100	0.98	89	0.87	78	0.77	68	0.67	58	0.57	48
-17	0.003	1.17	100	1.07	90	0.97	80	0.87	70	0.76	61	0.66	52
-16		1.27	100	1.17	90	1.07	SI	1.97	72	0.86	63	0.76	55
	0.011												
-15	0.012	1.38	100	1.28	91	1.18	82	1.08	74	0.97	66	0.87	58
-14	0.013	1.50	100	1.40	92	1.30	83	1.19	76	1.09	68	0.99	61
-13	0.014	1.63	100	1.53	92	1.42	84	1.32	77	1.22	70	1.11	63
-12	0.015	1.77	100	1.66	93	1.56	85	1.46	78	1.35	71	1.25	65
-11		1.92	100	1.81	93	1.71	86	1.61	80	1.50	73	1.40	67
-10	0.016	2.08	100	1.97	94	107	0#	1 77	01	3 00	**	1 56	69
-10 - 9	0.019	2.26	100	2.16	94	1.87 2.05	87 88	1.77	81 82	1.66	75 76	1.56	71
- 8	0.021	2.46	100	2.16	94	2.25	89	2.14	83	2.04	78	1.74	73
- 7	0.023	2.67	100	2.56	94	2.46	89	2.14	84	2.25	79	2.15	74
- 6	0.024	2.89	100	2.79	95	2.68	90	2.58	85	2.47	80	2.15	76
Ť	0.025			2.10		2.00		2.50	00	211	0.0	2.51	. 0
- 5	01020	3.13	100	3.03	95	2.92	90	2.82	86	2.71	81	2.61	77
- 4	0.028	3.39	100	3.28	95	3.18	91	3.07	87	2.97	82	2.86	78
- 3	0.029	3.66	100	3.56	96	3.45	92	3.35	87	3.24	83	3.14	79
- 2	0.031	3.96	100	3.85	96	3.75	92	3.64	88	3.54	84	3.43	80
- 1	0.033	4.27	100	4.16	96	4.06	92	3.95	89	3.85	85	3.74	81
- 0	0.034	4.60	100	4.50	96	4.40	93	4.29	89	4.19	86	4.08	82

• Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.05$  mm.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

meter,	Mean Vertical			t -	- <b>t</b> ', Dif	Famonaa a	Below the Freezing-Point; the Bulb covered with a Film of Ice. $\mathbf{t}-\mathbf{t}', \text{ Difference of Wet and Dry Bulb Thermometers.}$												
Thermo- meter, t' Centi- grade	Vertical					ierence o.	f Wet a	nd Dry B	ulb The	ermomete	rs.								
grade	Differ-	10	.2	1°.	4	10	.6	10	.8	20	.0	2°	.2						
	ence for ach 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.						
-35 -34	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.							
-33 -32 -31				٠															
-30 -29 -28 -27 -26																			
-25 -24	,	0.04	5																
-23 -22	0.006 0.006 0.007	0.09 0.16 0.23	12 18 24	0.05 0.12	6 13														
-20 -19	0.007 0.008 0.008	0.30 0.38	30 34	0.20 0.28	18 25	0.09 0.17	9 15	0.07	6										
-18 -17 -16	0.009 0.010	0.46 0.56 0.66	39 43 47	0.36 0.46 0.56	30 35 39	0.26 0.35 0.45	21 26 31	0.16 0.25 0.35	13 18 24	0.05 0.15 0.25	4 11 16	0.04	3 9						
-15 -14	0.011 0.013 0.013	0.77 0.88 1.01	50 53	0.66	43 46 50	0.56 0.68 0.80	36 40 43	0.46 0.58 0.70	29 33 37	0.36 0.47 0.60	22 27 31	0.25 0.37 0.50	15 21 25						
-12 -11	0.015 0.017 0.018	1.01 1.15 1.30	56 59 61	0.91 1.04 1.19	53 55	0.80 0.94 1.09	47 50	0.70 0.84 0.99	41 44	0.73 0.88	35 39	0.63	30 34						
-10 - 9 - 8	0.019	1.46 1.64 1.83	63 66 68	1.35 1.53 1.73	58 61 63	1.25 1.43 1.62	52 56 58	1.15 1.33 1.52	47 51 54	1.04 1.22 1.42	42 46 49	0.94 1.12 1.31	38 41 45						
- 7 - 6	0.023 0.024 0.025	2.04 2.26	69 71	1.94 2.16	65 67	1.83 2.06	61 63	1.73 1.95	56 59	1.63 1.85	52 55	1.52 1.74	48 51						
- 5 - 4 - 3	0.028 0.029	2.50 2.76 3.03	73 74 75	2.40 2.65 2.93	69 70 72	2.30 2.55 2.82	65 67 68	2.19 2.45 2.72	61 63 65	2.09 2.34 2.61	57 59 61	1.98 2.24 2.51	53 55 58						
- 4	0.030	3.33 3.64	77 78	3.22 3.53	73 75	3.12 3.43	70 71	3.01 3.32	66 68	2.91 3.22	63 65	2.80 3.11	60 62						

Below the Freezing-Point; the Bulb covered with a Film of Ice.

				t —	- <b>t</b> ', Diff	erence of	Wet ar	nd Dry Bu	ılb The	rmometer	s.		
Wet- Bulb Thermo- meter	Mean Vertical Differ-	20.	4	20	.6	2°.	8	30.	.0	3°	.2	3°	.4 ,
t Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.	9	Millim.	3	Millim.		Millim.		Millim.	-	Millim.	
-15 -14	0.011	0.15	15	0.05	9	0.06	4						
-13	0.013	0.39	20	0.29	14	0.19	9	0.08	4				
-12	0.013	0.53	25	0.42	19	0.32	14	0.22	10	0.11	5		
-11		0.68	29	0.57	24	0.47	19	0.36	15	0.26	10	0.16	6
-10	0.016	0.83	33	0.73	28	0.63	24	0.52	20	0.42	16	0.32	12
<b>–</b> 10	0.018	1.02	37	0.91	33	0.81	28	0.70	24	0.60	20	0.50	17
- 8	0.019	1.21	40	1.10	36	1.00	32	0.90	28	6.79	25	0.69	21
- 7	0.021	1.42	44	1.31	40	1.21	36	1.11	32	1.00	29	0.90	26
- 6		1.64	47	1.54	43	1.43	40	1.33	36	1.22	33	1.12	30
- 5	0.024	1.88	50	1.77	46	1.67	43	1.57	40	1.46	36	1.36	33
4	0.025	2.13	52	2.03	49	1.92	46	1.82	43	1.71	40	1.61	37
- 3	0.027	2.40	55	2.30	52	2.19	48	2.09	45	1.99	43	1.88	40
- 2	0.029	2.70	57	2.59	54	2.49	51	2.38	48	2.28	46	2.17	43
- 1	0.031	3.01	59	2.90	56	2.80	54	2.69	51	2.59	48	2.48	46
		3∘.	.6	3°	8	40	.0	40	.2	40	.4	40	.6
		Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
-15													
-14													
-13 -12													
-12 -11		0.05	2										
	0.016												
-10	0.018	0.21	8	0.11	4								
- 9	0.019	0.39	13	0.29	9	0.19	6	0.08	8	0.17	5	0.06	2
- 8   - 7	0.021	0.58	18	0.48	14 19	0.38	11 16	0.27	13	0.17	10	0.00	7
- 6	0.022	1.01	26	0.09	23	0.33	20	0.70	17	0.60	15	0.49	12
	0.024												
- 5	0.025	1.25	30	1.15	27	1.04	24	0.94	22	0.83	19	0.73	16
- 4	0.027	1.50	34	1.40	31	1.30	28	1.19	26 29	1.09	23 27	0.98 $1.25$	20 24
- 3 - 2	0.029	$1.78 \\ 2.07$	37	1.67	34 37	1.57 1.86	32 35	1.46	33	1.36 1.65	30	1.54	28
- 1	0.031	2.38	43	2.27	40	2.17	38	2.06	36	1.96	34	1.85	31
	•		1		1 10	•				•			

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.05$  mm.

Wet-				t-1	', Diffe	erence of	Wet ar	nd Dry-Bu	ılb The	ermometer	3.		
Bulb Thermo- meter.	Mean Vertical Differ-	0	·.0	0°	.2	0°.	4	00	6	0°.	8	100	.0
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.	_	Millim	_	Millim.	-	Millim.		Millim.	
0	0.03	4.60	100	4.48	96	4.36	92	4.24	88	4.12	85	4.01	81
1 2	0.04	4.94 5.30	100 100	4.82 5.18	96	4.70	93	4.58 4.94	89 89	4.46	85 86	4.35	82
3	0.04	5.69	100	5.57	97	5.06	93	5.33	90	5.21	87	5.09	83
4	0.04	6.10	100	5.98	97	5.86	93	5.74	90	5.62	87	5.50	84
5	0.04	6.53	100	6.41	97	6.29	94	6.17	91	6.05	88	5.94	85
	0.05	0.00	100	0.11	"	0.20	04	0.11		0.00		0.01	
6	0.05	7.00	100	6.88	97	6.76	94	6.64	91	6.52	88	6.40	85
7	0.05 0.05	7.49	100	7.37	97	7.25	94	7.13	91	7.01	89	6.89	86
8	0.06	8.02	100	7.90	97	7.78	94	7.66	92	7.54	89	7.42	86
9	0.06	8.57	100	8.45	97	8.33	95	8.21	92	8.09	89	7.97	86
10		9.17	100	9.04	97	8.92	95	8.80	93	8.68	90	8.56	87
11	0.06	9.79	100	9.67	97	9.55	95	9.43	93	9.31	90	9.19	88
12	0.07	10.46	100	10.34	98	10.21	95	10.09	93	9.97	90	9.85	88
13	0.07	11.16	100	11.04	98	10.21	95	10.09	93	10.68	91	10.56	89
14	0.07	11.91	100	11.79	98	11.66	95	11.54	93	11.42	91	11.30	89
15	0.08	12.70	100	12.58	98	12.46	96	12.33	93	12.21	91	12.09	89
	0.08												
16	0.09	13.54	100	13.41	98	13.29	96	13.17	94	13.05	92	12.93	90
17	0.09	14.42	100	14.30	98	14.18	96	14.05	94	13.93	92	13.81	90
18	0.09	15.36	100	15.23	98	15.11	96	14.99	94	14.87	92	14.75	90
19	0.10	16.35	100	16.22	98	16.10	96	15.98	94	15.86	92	15.73	91
20		17.39	100	17.27	98	17.15	96	17.02	94	16.90	92	16.78	91
0.1	0.11	10.50	700	10.00	00	30.05		10.10		10.00	00	3 00	0.7
21 22	0.12	18.50 19.66	100	18.37	98 98	18.25	96 96	18.13	94 95	18.00 19.17	92 93	17.88	91
23	0.12	20.89	100	19.54 20.76	98	19.41 20.64	96	20.52	95	20.39	93	19.04 20.27	91 91
24	0.13	22.18	100	22.06	98	21.94	97	21.81	95	21.69	93	21.57	92
25	0.14	23.55	100	23.43	98	23.30	97	23.18	95	23.05	93	22.93	92
	0.14												
26	0.15	24.99	100	24.86	98	24.74	97	24.62	95	24.49	93	24.37	92
27	0.15	26.51	100	26.38	98	26.26	97	26.13	95	26.01	93	25.88	92
28	0.16	28.10	100	27.98	98	27.85	97	27.73	95	27.60	93	27.48	92
29	0.18	29.78	100	29.66	98	29.53	97	29.41	95	29.28	94	29.16	92
30		31.55	100	31.42	98	31.30	97	31.17	95	30.05	94	30.92	93
91	0.19	00.40	100	00.00	00	00.15	0.00	00.00	00	00.00	0.1	00 =	00
31 32	0.20	33.40	100	33.28	98	33.15	97	33.03	96	32.90	94	32.78	93
33	0.21	35.36	100	35.23 37.28	99	35.11 37.16	97   98	34.98 37.03	96	34.86	94 94	34.73	93
34	0.22	39.56	100	39.43	99	37.16 <b>3</b> 9.31	98	39.18	96	39.06	94	38.93	93
35	0.23	41.83	100	41.70	99	41.58	98	41.45	96	41.33	95	41.20	93
	1		100	110	00 1	11.00	30	110	00 1	11.00			
		Mean	Horizont	al Differe	ence of	Force of	Vapor	for each	0°.1 =	= 0.06 mi	n,		

Wet-				t – 1	t, Diffe	erence of	Wet a	nd Dry-Bu	ılb <b>T</b> he	rmometer	3.		
Bulb Thermo- meter.	Mean Vertical Differ-	10	.2	10.	.4	10.	6	10.	.8	20.	0	20	.2
Centi- grade Degrees	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	-
0	0.03	3.89	78	3.77	74	3.65	71	3.53	67	3.41	64	3.29	61
1	0.04	4.23	79	4.11	75	3.99	72	3.87	69	3.75	66	3.63	63
2 3	0.04	4.59	80	4.47	76	4.35	73	4.23	70	4.11	67	3.99	65
4	0.04	4.97	80	4.85	77	4.73	74	4.61	71	4.49	69	4.37	66
5	0.04	5.38	81	5.26	78	5.14	75	5.02	73	4.90	70	4.78	67
3	0.05	5.82	82	5.70	79	5.58	77	5.46	74	5.34	71	5.22	69
6		6.28	83	6.16	80	6.04	77	5.92	75	5.80	72	5.68	70
7	0.05	6.77	83	6.65	81	6.53	78	6.41	76	6.29	73	6.17	71
8	0.05	7.29	84	7.17	81	7.05	79	6.93	76	6.81	74	6.69	72
9	0.06	7.85	84	7.73	82	7.61	80	7.49	77	7.37	75	7.25	73
10	0.00	8.44	85	8.32	83	8.20	80	8.08	78	7.96	76	7.84	74
	0.06						İ						
11	0.07	9.07	86	8.95	83	8.82	81	8.70	79	8.58	77	8.46	75
12	0.07	9.73	86	9.61	84	9.49	82	9.37	80	9.25	78	9.12	76
13	0.08	10.43	86	10.31	84	10.19	82	10.07	80	9.95	78	9.83	76
14 15	0.08	11.18	87	11.06	85	10.94	83	10.81	81	10.69	79	10.57	77
1.9	0.08	11.97	87	11.85	85	11.73	83	11.60	81	11.48	80	11.36	78
16		12.80	88	12.68	86	12.56	84	12.44	82	12.32	80	12.19	mo.
17	0.09	13.69	88	13.57	86	13.44	84	13.32	83	13.20	81	13.08	78 79
18	0.09	14.62	88	14.50	87	14.38	85	14.26	83	14.13	81	14.01	80
19	0.10	15.61	89	15.49	87	15.37	85	15.24	83	15.12	82	15.00	80
20	0.11	16.65	89	16.53	87	16.41	86	16.29	84	16.16	82	16.04	81
	0.11			i				1	1				
21	0.12	17.76	89	17.63	88	17.51	86	17.39	84	17.27	83	17.14	81
22	0.12	18.92	90	18.80	ss	18.67	86	18.55	85	18.43	83	18.30	82
23	0.13	20.15	90	20.02	88	19.90	87	19.78	85	19.65	83	19.53	82
$\begin{bmatrix} 24 \\ 25 \end{bmatrix}$	0.14	21.44	90	21.32	SS	21 20	87	21.07	85	20.95	84	20.82	82
20	0.14	22.81	90	22.68	89	22.56	87	22.44	86	22.31	84	22.19	83
26		24.24	90	24.12	89	23.99	87	23.87	90	99 77	87	22.62	99
27	0.15	25.76	91	25.63	89	25.51	88	$\frac{23.87}{25.39}$	86	23.75	85 85	23.62	83
28	0.16	27.35	91	27.23	89	27.10	83	$\frac{25.39}{26.98}$	87	26.86	85	26.73	83 84
29	0.17	29.03	91	28.91	90	28.78	88	28.66	87	28.53	85	28.41	84
30	0.18	30.80	91	30.67	90	30.55	89	30.42	87	30.30	86	30.17	84
	0.19												-
31	0.20	32.65	91	32.53	90	32.40	89	32.23	87	32.15	86	32.03	85
32	0.21	34.61	91	34.48	90	31.36	89	34.23	88	34.11	86	33.98	85
33	0.22	36.66	92	36.53	90	36.41	89	36.28	88	36.16	86	36.03	85
34 35	0.23	38.81	92	38.68	90	38.56	89	38.43	88	38.31	87	38.18	85
- 33	1	41.07	92	40.91	91	40.82	89	40.69	88	40.57	87	40.44	86
		Maan I	Jorizontal	Differen	10 of E	area of W				0.0			

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.06 mm.

				t — t	', Diffe	rence of	Vet an	d Dry-Bu	lb The	rmometer	з.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ•	2°	.4	2°.	6	2°.	8	3°.	0	3°.	2	3°.	4
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim		Millim.		Millim.		Millim.	
0	0.03	3.17	58	3.06	55	2.94	52	2.82	50	2.70	47	2.58	44
1	0.04	3.51	60	3.39	57	3.27	54	3.16	52	3.04	49	2.92	47
2 3	0.04	3.87	62 63	3.75 4.13	59	3.63	56	3.51 3.90	54 56	3.39 3.78	51 53	3.28	49
4	0.04	4.25 4.66	65	4.54	61 62	4.02	58 60	4.30	57	4.18	55	3.66 4.06	51 53
5	0.04	5.10	66	4.98	64	4.42	61	4.74	59	$\frac{4.15}{4.62}$	57	4.50	55
0	0.05	5.10	00	4.00	0.4	4.00	01	4.14	59	4.02	07	4.50	99
6	0.05	5.56	67	5.44	65	5.32	63	5,20	61	5.08	58	4.96	56
7	0.05	6.05	69	5.93	66	5.81	64	5.69	62	5.57	60	5.45	58
8	0.05	6.57	70	6.45	68	6.33	65	6.21	63	6.09	61	5.97	59
9	0.06	7.13	71	7.01	69	6.89	67	6.77	65	6.64	63	6.52	61
10	0.06	7.72	72	7.59	70	7.47	68	7.35	66	7.23	64	7.11	62
	0.06												
11	0.07	8.34	73	8.22	71	8.10	69	7.98	67	7.86	65	7.74	63
12	0.07	9.00	74	8.88	72	8.76	70	8.64	68	8.52	66	8.40	64
13	0.07	9.71	75	9.58	73	9.46	71	9.34	69	9.22	67	9.10	66
14	0.08	10.45	75	10.33	73	10.21	72	10.08	70	9.96	68	9.84	67
15		11.24	76	11.12	74	10.99	72	10.87	71	10.75	69	10.63	67
10	0.08	70.0**		11.05						11.50		77.40	00
16	0.09	12.07	77	11.95	75 ~C	11.83	73	11.71	72 72	11.58	70	11.46	68
17 18	0.09	12.95 13.89	77 78	12.83 13.77	76	12.71	74 75	12.59	72	13.40	71 72	12.34 13.28	69 70
19	0.10	14.87	78	14.75	76 77	13.64 14.63	75 75	13.52 14.51	74	14.38	72	14.26	71
20	0.10	15.92	79	15.79	77	15.67	76	15.55	74	15.43	73	15.30	72
	0.11	10102		10.73	''	15.07	10	15.55	' 1	10.40	10	10.00	• ~
21		17.02	80	16.90	78	16.77	77	16.65	75	16.53	74	16.40	72
22	0.12	18.18	80	18.06	79	17.93	77	17.81	76	17.69	74	17.56	73
23	0.12	19.41	80	19.28	79	19.16	78	19.04	76	18.91	75	18.79	73
24	0.13	20.70	81	20.58	79	20.45	78	20.33	77	20.21	75	20.08	74
25	0.14	22.06	81	21.94	80	21.82	79	21.69	77	21.57	76	21.45	75
	0.14												
26	0.15	23.50	82	23.37	80	23.25	79	23.13	78	23.00	77	22.88	75
27	0.16	25.01	82	24.89	81	24.76	79	24.64	78	24.51	77	24.39	76
28	0.17	26.61	83	26.48	81	26.36	80	26.23	79	26.11	77	25.98	76
29	0.18	28.28	83	28.16	81	28.03	80	27.91	79	27.69	77	27.76	76
30	0.19	30.05	83	29.92	82	29.80	81	29.67	79	29.55	78	29.42	77
31	0.19	31.90	83	31.78	82	31.65	81	31.53	80	31.40	78	31.28	77
32	0.20	33.86	83	33.73	82	33.61	81	31.55 33.48	80	33.36	79	33.23	78
33	0.21	35.90	84	35.77	83	35.65	81	35.52	80	35.40	79	35.27	78
34	0.22	38.06	84	37.93	83	37.81	82	37.68	81	37.56	80	37.43	78
35	0.23	40.31	84	40.18	83	40.06	82	39.93	81	39.81	80	39.68	79
	1												

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.06$  mm.

Wet-				t t'	', Diffe	rence of \	Vet an	d Dry-Bu	lb Thei	mometer	3.		
Bulb Thermo- meter.	Mean Vertical Differ-	3°	.6	3°.	8	<b>4</b> °.	0	<b>4</b> °.	2	<b>4</b> °.	4	<b>4</b> °.	6
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor,	Rela- tive Hu- mid- ity.	Force of Vapor,	Rela- tive Hu- mid- ity.
0	Millim,	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
0	0.03	2.46	41	2.34	39	2.22	36	2.11	34	1.99	32	1.87	29
1	0.04	2.80	44	2.68	42	2.56	39	2.44	37	2.32	35	2.20	32
2	0.04	3.16	46	3.04	44	2.92	42	2.80	39	2.68	37	2.56	35
3	0.04	3.54	49	3.42	46	3.30	44	3.18	42	3.06	40	2.94	38
4	0.04	3.94	51	3.82	48	3.71	46	3.59	44	3.47	42	3.35 3.78	40 42
5	0.05	4.38	52	4.26	50	4.14	48	4.02	46	3.90	44	5.75	4.4
6	0.05	4.84	5.1	4.72	52	4.60	50	4.48	48	4.36	46	4.24	41
7	0.05	5.33	54 56	5.21	54	5.09	52	4.45	50	4.85	48	4.73	46
8	0.05	5.85	57	5.73	56	5.61	54	5.49	52	5.37	50	5.25	48
9	0.06	6.40	59	6.28	57	6.16	55	6.04	53	5.92	52	5.80	50
10	0.06	6.99	60	6.87	58	6.75	57	6.63	55	6.51	53	6.39	52
10	0.06	0.00	00	0.01	"	0.10		1 0.00		0.02			
11		7.61	61	7.49	60	7.37	58	7.25	56	7.13	55	7.01	53
12	0.07	8.28	62	8.15	61	8.03	59	7.91	58	7.79	56	7.67	55
13	0.07	8.98	64	8.85	63	8.73	61	8.61	59	8.49	57	8.37	56
14	0.07	9.72	65	9.60	63	9.48	62	9.35	60	9.23	59	9.11	57
15	0.08	10.51	66	10.38	64	10.26	63	10.14	61	10.02	60	9.90	58
	0.08												
16	0.00	11.34	67	11.22	65	11.10	64	10.97	62	10.85	61	10.73	59
17	0.09	12.22	68	12.10	67	11.98	65	11.85	63	11.73	62	11.61	61
18	0.10	13.15	69	13.03	67	12.91	66	12.79	64	12.66	63	12.54	62
19	0.10	14.14	69	14.02	68	13.89	66	13.77	65	13.65	64	13.53	62
20	0.71	15.18	70	15.06	69	14.94	67	14.81	66	14.69	65	14.57	63
	0.11								1	Í			
21	0.12	16.28	71	16.16	69	16.04	68	15.91	67	15.79	65	15.67	64
22	0.12	17.44	71	17.32	70	17.20	69	17.07	67	16.95	66	16.83	65
23	0.13	18.67	72	18.54	71	18.42	69	18.30	68	18.17	67	18.05 19.34	66 66
24	0.14	19.96	73	19.84	71	19.71	70	19.59	69	19.46	6S	20.70	67
25	0.14	21.32	73	21.20	72	21.07	71	20.95	70	20.83	68	20.70	01
26	0.14	22.75	74	22.63	73	22.50	71	22.38	70	22.26	69	22.13	68
27	0.15	24.27	74	24.14	73	24.02	71 72	23.89	71	23.77	70	23.64	68
28	0.16	25.86	75	25.73	74	25.61	72	25.48	71	25.36	70	25.24	69
29	0.17	27.44	75	27.31	74	27.29	73	27.16	72	27.04	71	26.91	70
30	0.18	29.30	76	29.17	75	29.05	73	28.92	72	28.80	71	28.67	70
	0.19	20.50		20	.		, ,						
31		31.15	76	31.03	75	30.90	74	30.78	73	30.65	72	30.53	71
32	0.20	33.10	77	32.97	76	32.85	75	32.72	73	32.60	72	32.47	71
33	0.21	35.15	77	35.02	76	34.90	75	34.77	74	34.65	73	34.52	72
34	0.22	37.30	77	37.17	76	37.05	75	36.92	74	36.80	73	36.67	72
35	0.23	39.56	78	39.43	77	39.31	76	39.18	74	39.06	73	38.93	72

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.06 mm.

Wet-Bulb Thermometer. t' Centigrade Degrees.	Mean Vertical Differ-										3,		
meter. t' Centi- grade	Differ-	40	.8	5°.	0	5°.	2	5°.	4	5°.		5°.	8
	ence for each 0°.1.	Force of	Relative Humid	Force of Vapor.	Rela- tive Hu-	Force of	Rela- tive Hu-	Force of Vapor.	Rela- tive Hu-	Force of Vapor.	Rela- tive Hu-	Force of	Rela- tive Hu-
		Vapor.	ity.		mid- ity.	Vapor.	mid- ity.		mid- ity.		mid- ity.	Vapor.	mid- ity.
0	Millim.	Millim.		Millim.		Millim.	20	Millim.	0.	Millim.		Millim.	
0	0.03	1.75	27	1.63	25	1.51	23	1.39	21	1.27	19	1.15	17
1	0.04	2.08	30	1.97	28	1.85	26	1.73	24	1.61	22	1.49	20
2	0.04	2.44	33	2.32	31	2.20	29	2.08	27	1.96	25	1.85	23
3	0.04	2.82	36	2.70	34	2.58	32	2.46	30	2.34 $2.75$	28 31	2.22	26 29
4	0.04	3.23	38	3.11	36	2.99	34	2.87	33	3.18	33	2.63 3.06	32
5	0.05	3.66	40	3.54	39	3.42	37	3.30	35	9.10	33	3.00	32
6	0.05	4.12	43	4.00	41	3.88	39	3.76	37	3.64	36	3.52	34
7	0.05	4.61	45	4.49	43	4.37	41	4.25	40	4.13	38	4.01	36
8	0.05	5.13	47	5.01	45	4.89	43	4.77	42	4.65	40	4.53	39
9	0.06	5.68	48	5.56	47	5.44	45	5.32	44	5.20	42	5.08	41
10	0.06	6.27	50	6.15	48	6.02	47	5.90	45	5.78	44	5.66	42
11	0.00	6.89	52	6.77	50	6.65	49	6.53	47	6.40	46	6.28	44
12	0.07	7.55	53	7.43	52	7.31	50	7.18	49	7.06	47	6.94	46
13.	0.07	8.25	55	8.13	53	8.01	52	7.88	50	7.76	49	7.64	47
14	0.07	8.99	56	8.87	54	8.75	53	8.62	51	8.50	50	8.38	49
15	0.08	9.78	57	9.65	55	9.53	54	9.41	53	9.29	51	9.17	50
	0.08	0.,0											
16	0.00	10.61	58	10.49	57	10.36	55	10.24	54	10.12	53	10.00	51
17	0.09	11.49	59	11.37	58	11.24	56	11.12	55	11.00	54	10.88	53
18	0.09	12.42	60	12.30	59	12.17	58	12.05	56	11.93	55	11.81	54
19	0.10	13.40	61	13.28	60	13.16	59	13.04	57	12.91	56	12.79	55
20		14.44	62	14.32	61	14.20	60	14.08	58	13.95	57	13.83	56
21	0.11	15.54	63	15.42	62	15.30	60	15.17	59	15.05	58	14.93	57
21 22	0.12	16.70	64	16.58	63	16.46	61	16.33	60	16.21	59	16.09	58
23	0.12	17.93	65	17.80	63	17.68	62	17.56	61	17.43	60	17.31	59
24	0.13	19.22	65	19.09	64	18.97	63	18.85	62	18.72	61	18.60	60
25	0.14	20.58	66	20.46	65	20.33	64	20.21	63	20.08	62	19.96	60
2.5	0.14	22.55	0.51	27.00	0~	01.77		07.00	00	01.51	00	07.00	67
26	0.15	22.01	67	21.88	65	21.76	64	21.63	63	21.51	62	21.39	61
27	0.16	23.52	67	23.40	66	23.27	65	23.15	64	23.02	63	22.90	62
28	0.17	25.11	68	24.99	67	24.86	66	24.74	65	24.61	64	24.49	63
29	0.18	26.79	68	26.66	67	26.54	66	26.41	65	26.29 28.05	64	26.16 27.92	63 64
30	0.19	28.55	69	28.42	68	28.30	67	28.17	66	28.05	65	27.92	04
31	0.20	30.40	70	30.28	69	30.15	68	30.03	67	29.90	66	29.78	65
32	0.20	32.35	70	32.22	69	32.10	68	31.97	67	31.85	66	31.72	65
33	0.21	34.40	71	34.27	70	34.15	69	34.02	68	33.90	67	33.77	66
34	0.22	36.55	71	36.42	70	36.30	69	36.17	68	36.05	67	35.92	66
35	0.00	38.80	71	38.68	70								

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.06 mm.

	$\mathbf{t}-\mathbf{t}'$ , Difference of Wet and Dry-Bulb Thermometers.												
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	60	.0	<b>6</b> °.	.2	6°.	4	60.	.6	6°.	.8	70	.0
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity,	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	_
0	0.03	1.04	15	0.92	13	0.80	11	0.68	9	0.56	8	0.44	6
1	0.04	1.37	18	1.25	16	1.13	15	1.01	13	0.89	11	0.78	10
2	0.04	1.73	22	1.61	20	1.49	18	1.37	16	1.25	15	1.13	13
3	0.04	2.11	25	1.99	23	1.87	21	1.75	19	1.63	18	1.51	16
4	0.04	2.51	28	2.39	26	2.27	24	2.15	23	2.03	21	1.91	19
5	0.05	2.94	30	2.82	28	2.70	27	2.58	25	2.46	24	2.34	22
6	0.05	2.40	00	9.00	0.7	9.10	00	2.04	90	0.00	90	0.00	
7	0.05	3.40 3.89	33	3.28 3.77	31	3.16	29	3.04	28	2.92	26	2.80	25
8	0.05		35 37	4.28	33 35	3.65	32	3.53	30 33	3.41	29	3.29	28
9	0.06	4.41 4.96	39	4.84	38	4.16 4.71	34	4.04		3.92 4.47	31	3.80	30
10	0.06	5.54	41	5.42	40	5.30	36 38	5.18	35 37	5.06	33 35	4.35	32
10	0.06	0.04	41	9.42	40	3.50	99	9.13	91	5.00	99	4.94	34
11		6.16	43	6.04	41	5.92	40	5.80	39	5.68	37	5.56	36
12	0.07	6.82	44	6.70	43	6.58	42	6.46	41	6.34	39	6.22	38
13	0.07	7.52	46	7.40	45	7.28	43	7.16	42	7.03	41	6.91	40
14	0.07	8.26	47	8.14	46	8.02	45	7.90	44	7.77	43	7.65	41
15	0.08	9.05	49	8.92	48	8.80	46	8.68	45	8.56	44	8.44	43
	0.08	0.05	10	0.02	10	0.00		0.00	10	0.50	^^	0.11	10
16		9.88	50	9.75	49	9.63	48	9.51	47	9.39	45	9.27	44
17	0.09	10.76	52	10.63	50	10.51	49	10.39	48	10.27	47	10.14	46
18	0.09	11.69	53	11.56	51	11.44	50	11.32	49	11.20	48	11.07	47
19	0.10	12.67	54	12.55	53	12.42	51	12.30	50	12.18	49	12.06	48
20	0.11	13.71	55	13.58	54	13.46	53	13.34	52	13.22	50	13.09	49
	0.11							{					
21	0.12	14.81	56	14.68	55	14.56	54	14.44	53	14.31	52	14.19	51
22	0.12	15.96	57	15.84	56	15.72	55	15.59	54	15.47	53	15.35	52
23	0.13	17.19	58	17.06	57	16.94	56	16.82	55	16.69	54	16.57	53
24	0.14	18.48	59	18.35	58	18.23	56	18.11	55	17.98	54	17.86	53
25	0.14	19.84	59	19.71	58	19.59	57	19.46	56	19.34	55	19.22	54
26	0.14	91.90	CO	01.14	50	91.07	-0	20.00		20.77	5.0	90.64	~ ~
26 27	0.15	21.26	60	21.14	59	21.01	58	20.89	57	20.77	56	20.64	55
28	0.16	22.77	61 62	22.65	60	22.52	59 60	22.40	58 59	22.28	57 58	22.15	56
29	0.17	26.04	62	25.91	61	25.79	60	25.66	59	25.54	58	25.41	57 57
30	0.18	27.80	63	27.67	62	27.55	61	27.42	60	27.30	59	27.17	58
• •	0.19	21.50	0.5	21.01	02	41.00	01	21.42	00	21.50	03	27.17	90
31		29.65	64	29.53	63	29.40	62	29.28	61	29.15	60	29.03	59
32	0.20	31.59	64	31.47	63	31.34	62	31.22	61	31.09	60	30.97	59
33	0.21	33.64	65	33.51	64	33.39	63	33.26	62	33.14	61	33.01	60
34													
35													
	\											- 1	

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.06$  mm.

	${f t}-{f t}'$ , Difference of Wet and Dry-Bulb Thermometers.												
Wet- Bulb Thermo- meter. t'	Mean Vertical Differ- ence for each 0°.1.	7°.2		7°.4		7°.6		7°.8		8°.0		8°.2	
Centi- grade Degrees.		Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim		Millim.		Millim.		Millim.	
0	0.03	0.32	4	0.20	3	0.09	1			0.00	_		
1	0.04	0.66	8	0.54	7	0.42	5	0.30	4	0.18	2	0.06	1
2	0.04	1.01	12	0.89	10	0.77	9	0.65	7	0.53	6	$0.41 \\ 0.79$	8
3	0.04	1.39	15	1.27	13	1.15	12	1.03	11	0.91 1.31	13	1.19	11
4	0.04	1.79 2.22	18 21	1.67 2.10	16 19	1.55	15 18	1.43 1.86	14 17	1.74	16	1.62	14
5	0.05	2.22	21	2.10	19	1.95	13	1.30	17	1.74	10	1.02	14
6	0.05	2.78	24	2.66	23	2.44	21	2.32	20	2.20	18	2.08	17
7	0.05	3.16	26	3.04	25	2.92	24	2.80	22	2.68	21	2.56	20
8	0.05	3.68	29	3.56	27	3.44	26	3.32	25	3.20	24	3.08	22
9	0.06	4.23	31	4.11	30	3.99	28	3.87	27	3.75	26	3.63	25
10	0.06	4.82	33	4.70	32	4.57	30	4.45	29	4.33	28	4.21	27
	0.06												
11	0.00	5.44	35	5.32	34	5.19	32	5.07	31	4.95	30	4.83	29
12	0.07	6.09	37	5.97	36	5.85	34	5.73	33	5.61	32	5.49	31
13	0.07	6.79	39	6.67	37	6.55	36	6.43	35	6.31	34	6.18	33
14	0.07	7.53	40	7.41	39	7.29	38	7.17	37	7.04	36	6.92	35
15		8.31	42	8.19	41	8.07	40	7.95	39	7.83	37	7.71	36
	0.08			0.00		0.00		0 = 0		0.00	00	0.50	90
16	0.09	9.14	43	9.02	42	8.90	41	8.78 9.66	40 42	8.66 9.53	39 40	8.53 9.41	38 39
17	0.09	10.02	45	9.90   10.83	44	9.78 10.71	43	10.58	42	10.46	40	10.34	41
18 19	0.10	10.95 11.93	46 47	11.81	45 46	11.69	44 45	11.56	44	11.44	43	11.32	42
20	0.10	12.97	48	12.85	40	12.72	46	12.60	45	12.48	44	12.36	43
20	0.11	12.57	40	12.00	*1	12.12	30	12.00	40	12.40	77	12.00	40
21		14.07	50	13.94	49	13.82	48	13.70	47	13.58	46	13.45	45
22	0.12	15.22	51	15 10	50	14.98	49	14.85	48	14.73	47	14.61	46
23	0.12	16.45	52	16.32	51	16.20	50	16.08	49	15.95	48	15.83	47
24	0.13	17.73	52	17.61	52	17.49	51	17.36	50	17.24	49	17.12	48
25	0.14	19.09	53	18.97	52	18.85	52	18.72	51	18.60	50	18.47	49
1	0.14								i				
26	0.15	20.52	54	20.39	53	20.27	52	20.14	51	20.02	51	19.90	50
27	0.16	22.03	55	21.90	54	21.78	53	21.65	52	21.53	51	21.41	51
28	0.17	23.61	55	23.49	54	23.36	53	23.24	53	23.11	52	22.99	51
29	0.18	25.29	56	25.16	55	25.04	54	24.91	54	24.79	53	24.66	52
30		27.05	57	26.92	56	26.80	55	26.67	55	26.55	54	26.42	53
31	0.19	28.90	58	28.78	57	28.65	56	28.53	55	28.40	55	28.27	54
31 32	0.20	30.85	58 59	30.72	58	30.60	57	30.47	56 56	30.35	56	20.21	94
33		90.09	59	30.72	00	30.00	91	90.41	50	,,0.00	00		
34													
35													
		·'						or each O					

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.06$  mm.

		$\mathbf{t}-\mathbf{t}'$ , Difference of Wet and Dry-Bulb Thermometers.											
Wet-				t-t'	, Differ	ence of V	Vet and	I Dry-Bul	b Ther	mometers	•		
Bulb Thermo- meter. t'	Mean Vertical Differ- ence for each 0°.1.	ertical 80.4		<b>8</b> °.	<b>8</b> °.6		8°.8		9°.0		9°.2		1
		Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.						
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
1													
2	0.04	0.30	3	0.18	2	0.06	1			0.10	2	0.08	1
3	0.04	0.67	7	0.55	5	0.43	4	0.31	3 6	0.19	5	0.08	4
4	0.04	1.07	10	0.95	9	0.83	8	0.72	10	1.02	8	0.90	7
5	0.05	1.50	13	1.38	12	1.26	11	1.14	10	1.02			
6	0.05	1.96	16	1.84	15	1.72	14	1.60	13	1.48	12	1.36	10
7	0.05	2.44	19	2.32	17	2.20	16	2.08	15	1.96	14	1.84	13
8	0.05	2.96	21	2.84	20	2.72	19	2.60	18	2.48	17	2.36	16
9	0.06	3.51	24	3.39	23	3.27	21	3.15	20	3.03	19	2.91	18
10	0.06	4.09	26	3.97	25	3.85	24	3.73	23	3.61	22	3.49	21
	0.06												99
11	0.07	4.71	28	4.59	27	4.47	26	4.35	25	4.23	24 26	4.11	23 25
12	0.07	5.37	30	5.25	29	5.12	28	5.00	27 29	4.88 5.58	28	5.46	27
13	0.07	6.06	32	5.94	31	5.82	30 32	5.70 6.44	31	6.31	30	6.19	29
14	0.08	6.80	34 35	6.68	33	6.56 7.34	33	7.22	33	7.10	32	6.97	31
15	0.08	7.58	55	1.40	0.4	1.04	30		00	"""			
16		8.41	37	8.29	36	8.17	35	8.05	34	7.92	33	7.80	32
17	0.09	9.29	39	9.17	38	9.04	37	8.92	36	8.80	35	8.68	34
18	0.09	10.22	40	10.09	39	9.97	38	9.85	37	9.73	36	9.60	35
19	0.10	11.20	41	11.07	40	10.95	39	10.83	39	10.71	38	10.58	37
20	0.11	12.23	43	12.11	42	11.99	41	11.87	40	11.74	39	11.62	38
	0.11	1		l		1							40
21	0.12	13.33	44	13.21	43	13.08	42	12.96	41	12.84	40	12.71	40
22	0.12	14.48	45	14.36	44	14.24	43	14.12	42	13.99 15.21	41 42	13.87 15.09	41
23	0.13	15.71	46	15.58 16.87	45	15.46 16.75	44 45	15.34 16.62	43	16.50	44	16.37	43
24 25	0.14	16.99	48	18.22	40	18.10	46	17.98	45	17.86	45	17.73	44
25	0.14	18.35	40	10.42	**	13.10	10	1	"		1		
26		19.77	49	19.65	48	19.52	47	19.40	46	19.27	46	19.15	45
27	0.15	21.28	50	21.16	49	21.03	48	20.91	47	20.78	47	20.66	46
28	0.16	22.86	51	22.74	50	22.61	49	22.49	48	22.36	47	22.24	47
29	0.17	24.54	51	24.41	51	24.29	50	24.16	49	24.04	48	23.91	47
30		26.30	52	26.17	51	26.05	51	25.92	50	25.80	49	25.67	48
	0.19			20.00		0	51	27.78	51				
31		28.16	53	28.03	52	27.91	91	21.15	31				
32													
33													
35								1					
	1		1			•		<u> </u>	-	-	-		-

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0 06 mm.

		$\mathbf{t}-\mathbf{t}'$ , Difference of Wet and Dry-Bulb Thermometers.											•
Wet- Bulb Thermo- meter. t'	Mean Vertical Differ-	9	.6	9°.	.8	100	.0	10°	.2	10°	.4	10°	.6
Centi- grade Degrees.	ence for each 0° 1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.								
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
1					:								
2 3													
4		0.36	3	0.24	2	0.12	1		,				
5	0.04	0.78	6	0.66	5	0.54	4	0.42	3	0.30	2	0.18	1
6	0.05	1.24	9	1.12	8	1.00	7	0.88	6	0.76	5	0.64	5
7	0.05	1.72	12	1 60	11	1.48	10	1.36	9	1.24	8	1.12	7
8	0.05	2.24	15	2.12	14	2.00	13	1.88	12	1.76	11	1.64	10
9	0.06	2.79	17	2.66	16	2.54	16	2.42	15	2.30	14	2.18	13
10	0.06	3.37	20	3.25	19	3.13	18	3.00	17	2.88	16	2.76	15
11		3.98	22	3.86	21	3.74	20	3.62	19	3.50	18	3.38	18
12	0.07	4.64	24	4.52	23	4.40	22	4.28	22	4.15	21	4.03	20
13	0.07	5.33	26	5.21	25	5.09	25	4.97	24	4.85	23	4.73	22
14 15	0.08	6.07 6.85	28 30	5.95 6.73	27 29	5.83 6.61	26 28	5.71 6.49	25 27	5.58 6.37	25 26	5.46 6.24	24 26
1.9	0.08	0.00	30	0.19	29	0.01	20	0.43	21	0.01	20	0.24	20
16	0.09	7.68	31	7.56	31	7.44	30	7.31	29	7.19	28	7.07	27
17	0.09	8.56	33	8.43	32	8.31	31	8.19	31	8.07	30	7.94	29
18 19	0.10	9.48 10.46	35 36	9.36 $10.34$	34 35	9.24	33 34	9.11 10.09	32 33	8.99 9.97	31 33	8.87 9.85	30 32
20	0.11	11.50	37	11.37	36	10.22 11.25	36	11.13	35	11.01	34	10.88	33
	0.11	11.00		11.01		11.20	00				•	20.00	00
21	0.12	12.59	39	12.47	38	12.35	37	12.22	36	12.10	35	11.98	35
22 23	0.12	13.75	40	13.62	39	13.50	38	13.38	37	13.25	37	13.13	36
23	0.13	14.96 16.25	41 42	14.84 16.13	40 41	14.72 16.00	39 40	14.59 15.88	39 40	14.47 15.76	38 39	14.35 15.63	37 38
25	0.14	17.61	43	17.48	42	17.36	42	17.24	41	17.12	400	16.99	39
	0.14												
26	0.15	19.02	44	18.90	43	18.78	42	18.65	42	18.53	41	18.40	40
27 28	0.16	20.54 22.12	45 46	20.41 $22.00$	44	20.29 $21.87$	43 44	20.16 21.75	43 44	20.04	42 43	19.91 21.50	41 42
29	0.17	23.79	47	23.66	46	23.54	45	23.41	45	23.29	44	23.16	43
30	0.18	25.55	48	25.42	47	25.30	46						
31												,	
32													
33													
34													
35													

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.06$  mm.

	1	1											
Wet-	Mean			t — t	t', Diffe	erence of	Wet a	nd Dry-Bu	ılb The	rmometer	S.		
Bulb Thermo- meter.	Vertical Differ- ence for	10	°.8	110	.0	110	.2	110	.4	110	.6	110	.8
Centi- grade Degrees.	each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.								
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
1 2													
3 4													
5		0											
6 7	0.05	0.52 1.00	4 7	0.40 0.88	3 6	0.28	2	0.16	1				
s	0.05	1.52	9	1.40	9	0.76 1.27	5 8	0.64 1.15	4 7	0.52 1.03	3 6	0.40 0.91	2
9	0.06 0.06	2.06	12	1.94	11	1.82	10	1.70	10	1.58	9	1.46	5 8
10	0.06	2.64	14	2.52	14	2.40	13	2.28	12	2.16	11	2.04	11
11	0.07	3.26,	17	3.14	16	3.02	15	2.90	14	2.77	14	2.65	13
12	0.07	3.91	19	3.79	18	3.67	17	3.55	17	3.43	16	3.31	15
13	0.07	4.61	21	4.49	20	4.36	19	4.24	19	4.12	18	4.00	17
14 15	0.08	5.34 6.12	23 25	5.22	22	5.10	21	4.98	21	4.86	20	4.73	19
	0.08			6.00	24	5.88	23	5.76	22	5.63	22	5.51	21
16 17	0.09	6.95 7.82	27 28	6.83	26	6.70	25	6.58	24	6.46	23	6.34	22
18	0.09	8.75	28	7.70 8.63	27 29	7.58 8.50	27 28	7.46 8.38	26 27	7.33 8.26	25 27	7.21 8.14	24
19	0.10	9.73	31	9.60	30	9.48	30	9.36	29	9.24	28	9.11	26 28
20	0.10	10.76	33	10.64	32	10.51	31	10.39	30	10.27	30	10.15	29
21	0.12	11.85	34	11.73	33	11.61	32	11.48	32	11.36	31	11.24	30
22	0.12	13.01	35	12.88	34	12.76	34	12.64	33	12.51	32	12.39	32
23	0.13	14.22	36	14.10	36	13.98	35	13.85	34	13.73	34	13.61	33
24 25	0.14	15.51	38	15.39	37	15.27	36	15.15	35	15.02	35	14.90	34
20	0.14	16.87	39	16.74	38	16.62	37	16.49	36	16.37	36	16.24	35
26	0.15	18.28	39	18.16	39	18.03	38	17.91	37	17.78	37	17.66	36
27	0.16	19.79	40	19.67	40	19.54	39	19.42	38	19.29	38	19.17	37
28 29	0.17	21.37	41	21.25	41	21.12	40	21.00	39	20.87	39	20.75	38
30		23.04	42	22.91	42		İ						
31													
32													
33				1			İ						
34 35													
99					1				1				

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.06 mm.

[													
Wet-				t-t	', Diffe	rence of	Wet an	d Dry-Bu	lb <b>T</b> he	rmometer	з.		
Bulb Thermo- meter.	Mean Vertical Differ-	12	e°.0	12°	.2	120	.4	129	.6	129	.8	13°	.0
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor,	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.	_	Millim.	_	Millim.		Millim.	
12	0.07	3.19	14	3.06	14	2.94	13	2.82	12	2.70	12	2.58	11
13	0.07	3.88	16	3.76	16	3.64	15	3.51	14	3.39	14	3.27	13
14	0.08	4.61	18	4.49	18	4.37	17	4.25	16	4.13	16	4.00	15
15	0.08	5.39	20	5.27	20	5.15	19	5.03	18	4.90	18	4.78	17
16		6.22	22	6.09	21	5.97	21	5.85	20	5.73	19	5.61	19
	0.09		Ī					l					
17	0.09	7.09	24	6.97	23	6.84	22	6.72	22	6.60	21	6.48	21
18	0.10	8.01	25	7.89	25	7.77	24	7.65	23	7.52	23	7.40	22
19	0.10	8.99	27	8.87	26	8.74	26	8.62	25	8.50	25	8.38	24
20	0.11	10.02	28	10.90	28	9.78	27	9.65	26	9.53	26	9.41	25
21	0.10	11.12	30	10.99	29	10.87	28	10.75	28	10.62	27	10.50	27
22	0.12	12.27	31	12.14	30	12.02	30	11.90	29	11.77	28	11.65	28
22	0.12	13.48	32	13.36	31	13.23	31	13.11	30	12.99	29	12.86	29
24	0.13	14.78	33.	14.65	33	14.53	32	14.40	31	14.28	31	14.16	30
25	0.14	16.11	35	15.99	34	15.87	33	15.74	33	15.62	32	15.50	31
26	0.14	17.54	36	17.42	35	17.29	34	17.17	34	17.04	33	16.92	33
20	0.15	11101	00	11.12	00	11.20	01	1	01	11101	00	10.02	00
27		19.04	37	18.92	36	18.80	35	18.67	35	18.55	34	18.42	34
28	0.16	20 63	38										
		-											
		13	.∘2	13°	4	13°.	.6	13°.	8	14°	0		
		Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
12	0.07	2.46	10	2.34	10	2.22	9	2.09	8	1.97	8		
13	0.07	3.15	12	3.03	12	2.91	11	2.79	11	2.66	10		
14	0.07	3.88	14	3.76	14	3.64	13	3.52	13	3.40	12		
15	0.08	4.66	16	4.54	16	4.42	15	4.29	15	4.17	14		
16		5.48	18	5.36	18	5.24	17	5.12	16	5.00	16		
	0.09		0.0	0.00	**	0.11	**						
17	0.09	6.36	20	6.23	19	6.11	19	5.99	18	5.87	17		
18	0.10	7.28	22	7.16	21	7.03	20	6.91	20	6.79	19		
19	0.10	8.25	23	8.13	22 24	8.01 9.04	22 23	7.89 8.92	21 23	7.76 8.80	21 22		
20	0.11	9.29	$\frac{25}{26}$	9.16 10.25	24 25	10.13	25	10.01	23	9.89	24		
21	0.12	10.55	20	10.20	20	10.19	20	10.01	2·t	3.03	24		
22		11.53	27	11.40	27	11.28	26	11.16	26	11.03	25		
23	0.12	12.74	28	12.62	28	12.49	27	12.37	27	12.25	26		
24	0.13	14.02	30	13.90	29	13.77	29	13.65	28	13.53	27		
25	0.14	15.37	31	15.25	30	15.12	30	15.00	29	14.88	29		
26	0.14	16.80	32	16.67	31	16.55	31	16.42	30	16.30	30		
								•					

## Correction for the Barometrical Height.

Baron	the netrical					I	Differer	ice of '	<b>F</b> herm	ometer	s <b>t</b> — <b>t</b> ′.					
Height	below.															
Add.	Subtr'ct.	10	2°	<b>3</b> °	<b>4</b> °	5°	60	70	80	9°	10°	110	12°	13°	14°	
			<u>'</u>		1	1	Vet-Bu	ilb abo	ve the	Freezi	ng Point		1	1	1	
						<u> </u>		i	1	1			Γ			
Millim.	Millim,	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	Milli.	
755	755	0.00		ł		0.00		0.00		ŀ	0.00	0.00	0.00	0.00	0.00	
750	760	0.00	0.01	0.01	0.02	0.02			}		0.04	0.04	0.05	0.05	0.06	
745	765	0.01	0.02	0.02	0.03	0.04	1				0.08	0.09	0.10	0.10	0.11	
740	770	0.01	0.02	$0.04 \\ 0.05$	0.05	$0.06 \\ 0.08$	0.07	0.08	0.10 0.13	0.11	0.12 0.16	0.13	0.14	0.16	0.17	
735	775	0.02	0.03	0.05	0.00	0.03	0.10	0.11	0.13	0.14	0.10	0.15	0.19	0.21	0.22	
730	780	0.02	0.04	0.06	0.08	0.10	0.12	0.14	0.16	0.18	0.20	0.22	0.24	0.26	0.28	
725	785	0.02		0.07	0.10	0.12			0.19		0.24	0.26	0.29	0.31	0.34	
720	790	0.03	0.06	0.08	0.11	0.14		0.20	0.22		0.28	0.31	0.34	0.36	0.39	
715	795	0.03	0.06	0.10	0.13	0.16	0.19	0.22	0.26	0.29	0.32	0.35	0.38	0.42	0.45	
710	800	0.04	0.07	0.11	0.14	0.18	0.22	0.25	0.29	0.32	0.36	0.40	0.43	0.47	0.50	
700	66	1	$06 \mid 0.12 \mid 0.18 \mid 0.24 \mid 0.30 \mid 0.36 \mid 0.42 \mid 0.48 \mid 0.54 \mid 0.60 \mid 0.66 \mid 0.72 \mid 0.78 \mid 0.84$													
690	66	0.05	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
680	66	0.06	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
670	66	0.07	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
660		0.08	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
650	66	0.08	08 0.15 0.23 0.30 0.38 0.46 0.53 0.61 0.68 0.76 0.84 0.91 0.99 1.06													
030		0.00	1.00													
			Wet-bi	alle bold	ow the		!			1			1			
				zing P												
								E	XAM:	PLE	OF C	ALCU	JLAT:	ION.		
755	755	0.00	0.00	0.00		0.00			Wet	-bulh a	bove the	Freezin	g Point			
750	760	0.00		0.01	0.01	0.02		, -					_			
745	765	0.01	0.01	0.02	0.03	0.04		'=1			-t' =			710mm	H	
740	770	0.01	0.02	0.03	0.04	0.05		The t ght 73		_	for me		rometr		nm.	
735	775	0.01	0.03	0.04	0.06	0.07		0			ce of v on for 7		ond so	$\cdot = 9$	0.30	
730	780	0.02	0.04	0.05	0.07	0.09		_uuiii					and o	= (		
725	785	0.02	0.04	0.06	0.08	0.11				Force	of var	or	•	. = 9	9.71	
720	790	1 1		0.07	0.10	0.12										
715	795	0.03	0.06	0.08	0.11	0.14	,	The r	nean	haroz	netrica	l press	mre a	ta mi	van	
710	800	0.03	0.06	0.09	0.13	0.16					, it is					
											ables fi					
700	66		0.08				det	ermin	ing, l	y me	ans of	this las	t table.	a cons	tant	
690	66		0.09				cor	rection	to b	e app	lied to	the n	umbers	s in the	ta-	
680	"		0.11			0.26	ble	s, giv	ing tl	he for	ce of	rapor.	This	correc	tion	
670	66		0.12			- 1	wil	l be f	ound	by tak	ing for	t-t'	or the	differe	nce	
660		0.07	0.13	0.20	0.27	0.33					mean					
650	"	0.07	0.15	0.22	0.29	0.36		ich wi the re			le influ	ence u	pon th	e accur	acy	

## III.

## TABLE

GIVING AT SIGHT THE RELATIVE HUMIDITY DEDUCED FROM THE INDICA-TIONS OF THE DEW POINT INSTRUMENTS.

By M. T. HAEGHENS.

This table, which has been published in the Annuaire Météorologique de France for 1850, page 86, and following, has been calculated by Mr. Haeghens, using Regnault's Tables of Elastic Forces of Vapor. It gives directly the relative humidity, when the hygrometrical observations have been made by means of dew point instruments like those of Daniell, Regnault, Bache, and others.

These hygrometers are destined to find out the temperature of the dew point, that is the temperature to which it would be necessary to lower the temperature of the air, in order that this air be completely saturated by the aqueous vapor which it contained at the time of the observation.

The force of vapor contained in the air, or its absolute humidity, is thus the maximum of force of vapor which corresponds to the temperature of the dew point; it is given directly in the Table I. of the Elastic Forces of Vapor, by Regnault.

The ratio of that maximum of force of vapor at the temperature of the dew point to the force of vapor which corresponds, in the same table, to the temperature of the surrounding air at the time of the observation, is the *relative humidity*. This ratio is given in hundredths in the following table, which relieves the observer of the trouble of calculating it.

Let t = temperature of the air surrounding the instrument.

t' = temperature of the dew point.

t-t'= the difference between these two temperatures.

The first column, on the left, contains the temperature of the air t, in centigrade degrees. The following ones, headed with the differences, t-t', between the temperatures of the air and of the dew point, give the relative humidity corresponding to the two elements.

•				
	Temp. of the Air $= t$ .	Dew point $= t'$ .	Difference $t-t'$ .	Relative Humidity.
Example:	10°.0	4°.4	5°.6	68

Should the temperature of the air t', or the difference t-t', fall between the numbers found in the columns, it is obvious, by glancing at the table, that an interpolation at sight will always be easy.

30

B

Femper-			t —	<b>t</b> ' = I	Differen	ce of T	empera	tures o	the D	ew Poi	nt and	of the	Air.		
the air.	0°.0	0°.2	0°.4	0°.6	0°.8	1°.0	1°.2	1°.4	1°.6	1°.8	2°.0	2°.2	2°.4	2°.6	2°.8
Centig.	100														~~
-8 -7	100	98 98	97 97	95 95	94 94	92 92	90	89 89	88 88	86 86	85 85	83 83	82 82	80 81	79 79
-7 -6	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
-5	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
													1		
-4	100	98	97	95	94	92	91	89	88	87	85	84	83	81	80
-3	100	98	97	95	94	92	91	90	88	87	85	84	83	81	80   80
-2 -1	100 100	98 98	97 97	95 95	94 94	93 93	91 91	90	88 89	87 87	86 86	84 85	83	82 82	81
			31	93	9-1									}	
0	100	98	97	96	94	93	91	90	89	87	86	85	83	82	81
+1	100	99	97	96	95	93	92	90	89	88	86	85	84	83	81
2	100	99	97	96	95	93	92	91	89	88	87	85	84	83	82
3	100	99	97	96	95	93	92	91	89	88	87	86	84	83	82
4	100	99	97	96	95	93	92	91	89	88	87	86	85	83	82 82
5	100	99	97	96	95	93	92	91	90	88	87	86	85	83	82
6	100	99	97	96	95	93	92	91	90	88	87	86	85	84	82
7	100	99	97	96	95	93	92	91	90	89	87	86	85	84	83
8	100	99	97	96	95	93	92	91	90	89	87	86	85	84	83
9	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
10	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
11	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
12	100	99	97	96	95	94	92	91	90	89	88	87	85	84	83
13	100	99	97	96	95	94	92	91	90	89	88	87	85	84	83
14	100	99	98	96	95	94	93	91	90	89	88	87	86	84	83
15	100	99	98	96	95	94	93	91	90	89	88	87	86	84	83
16	100	99	98	96	95	94	93	91	90	89	88	87	86	85	84
17	100	99	98	96	95	94	93	91	90	89	88	87	86	85	84
18	100	99	98	96	95	94	93	92	90	89	88	87	86	85	84
19	100	99	98	96	95	94	93	92	91	89	88	87	86	85	84
20	100	99	98	96	95	94	93	92	91	89	88	87	86	85	84
21	100	99	98	96	95	94	93	92	91	90	88	87	86	85	84
22	100	99	98	96	95	94	93	92	91	90	89	87	86	85	84
23	100	99	98	96	95	94	93	92	91	90	89	88	86	85	84
24	100	99	98	97	95	94	93	92	91	90	89	88	87	85	84
25	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
26	100	99	93	97	95	94	93	92	91	90	89	88	87	86	85
27	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
28	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85 85
29	100 100	99	93	97	96	94	93	92	91	90	89 89	88	87	86	85
30	i		98								1			1	
31	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
32	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
33	100	99	98	97	96	94	93	92	91	90	S9	88	87	86	85
34	100	99	98	97	96	95 95	93	92	91	90	89 89	88 88	87	86	85
35 R	100	99	98	97	90	95	93	92	91	90	09	00	1 01	30	00

Temper-			t –	$\mathbf{t}' = \mathbf{I}$	Differen	ce of T	'empera	tures of	the D	ew Poi	nt and	of the	Air.		
ature of tne air.	90 A	3°.2	9 0 4	3°.6	3°.8	4°.0	4°.2	4°.4	4°.6	4°.8	5°.0	5°.2	5°.4	50 G	5°.8
t =	3°.0	3 .2	3.°4	0.0	0 .0	4 .0	4 .3	4 •4	4 .0	4 .0	0.0	0 .2	0 .4	5°.6	0.0
Centig.	78	77	75	74	73	72	71	69	68	67	66	65	64	63	62
-7	78	77	75	74	73	72	71	69	68	67	66	65	64	63	62
-6	78	77	76	74	73	72	71	69	68	67	66	65	64	63	62
-5	79	77	76	75	73	72	71	70	68	67	66	65	64	63	62
-4	79	77	76	75	74	73	71	70	69	68	67	66	64	63	62
-3	79	77	76	75	74	73	72	70	69	68	67	66	65	64	63
-2	79	78	77	76	74	73	72	71	70	69	68	66	65	64	63
-1	79	78	77	76	75	73	72	71	70	69	68	67	66	65	64
0	80	78	77	76	75	74	73	71	70	69	68	67	66	65	64
+1	80	79	78	77	75	74	73	72	71	70	69	68	66	65	64
2	SI	79	78	77	76	75	74	72	71	70	69	68	67	66	65
3	81	80	78	77	76	75	74	73	72	71	70	69	68	66	65
4	81	80	79	78	77	75	74	73	72	71	70	69	68	67	66
5	81	80	79	78	77	76	75	73	72	71	70	69	68	67	66
6	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
7	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
8	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
8	82	80	79	78	77	76	75	74	73	72	71	70	69	68	67
10	82	81	80	78	77	76	75	74	73	72	71	70	69	68	67
11	82	81	80	79	78	76	75	74	73	72	71	70	70	69	68
12	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
13	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
14	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
15	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
16	82	81	80	79	78	77	76	75	74	73	72	71	71	70	69
17	83	81	80	79	78	77	76	75	74	73	73	72	71	70	69
18	83	82	81	80	79	78	77	76	75	74	73	72	71	70	69
19 20	83 83	82 82	81	80	79	78 78	77	76 76	75 75	74	73 73	72 72	71 71	70	69
	83	-	81	80	79	78	77	76	75	74	73	72	71	70	70
21 22	83	82 82	81	80	79	78	77	76	75	74	73	73	72	71	70
23	83	82	81	80	79	78	77	76	75	74	74	73	72	71	70
24	83	82	81	80	79	78	77	77	76	75	74	73	72	71	70
25	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
26	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
27	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
28	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
29	84	83	82	81	80	79	78	77	76	75	75	74	73	72	71
30	84	83	82	81	80	79	78	77	76	76	75	74	73	72	71
31	84	83	82	81	80	79	78	77	77	76	75	74	73	72	71
32	84	83	82	81	80	79	79	78	77	76	75	74	73	72	72
33	84	83	82 83	81 82	80	80	79 79	78 78	77	76	75 75	74	73 74	72 73	72
34	85	84	83	82	81	80	79	78	77	76	75	75	74	73	72
33	100	104		1 02	01	00	1 13	1	1 11		1 '	1.0	1	1 .0	

	Teniper- ature of			t	$-\mathbf{t}' =$	Differe	nce of	rempera	tures of	the De	w Poin	L and of	the Air			
	the air.	6°0	6°.2	6°.4	6°.6	6°.8	7°.0	7°.2	7°.4	7°.6	7°.8	8°.0	8°.2	8°.4	8°.6	8°.8
	Centig.															
	-7															
	-6	61	60	59	58	57	56	-0		<b>.</b>						
	<b>-</b> 5	61	60	59	58	58	57	56	55	54	53	52				
i	-4 -3	62 62	61 61	60 60	59 59	58 58	57 57	56 56	55 55	54 54	53 53	52 53	52	51	50	49
Ì	-2	62	61	60	60	59	58	57	56	55	54	53	52	51	50	49
1	-1	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49
	0	63	62	61	60	59	58	57	56	55	54	53	53	52	51	50
	+1	63	62	61	61	60	58	58	57	56	55	54	53	52	51	51
	2 3	64 64	63 63	62 62	61 62	60 60	59 60	58	57 58	56	55 56	55	54 54	53 53	52	51 52
	4	65	64	63	62	61	60	59 59	58	57 57	56	55 56	55 55	54	53 53	52
	5	65	64	63	62	62	61	60	59	58	57	56	55	54	54	53
	6	66	65	64	63	62	61	60	59	58	57	57	56	55	54	53
	7	66	65	64	63	62	61	60	60	59	58	57	56	55	55	54
	8 9	66 66	65 65	64 64	63 64	62 63	62 62	61 61	60 60	59 59	58 58	57 58	56 57	56 56	55 55	54 54
	10	67	66	65	64	63	62	61	60	59	59	58	57	56	55 55	55
	11	67	66	65	64	63	62	61	61	60	59	58	57	56	56	55
1	12	67	66	65	64	63	62	62	61	60	59	58	57	57	56	55
	13	67	66	65	64	64	63	62	61	60	59	59	58	57	56	55
	14 15	67 67	66 67	66 66	65 65	$\begin{array}{c} 64 \\ 64 \end{array}$	63 63	$\begin{bmatrix} 62 \\ 62 \end{bmatrix}$	61	60	60 60	59 59	58 58	57 57	56 57	56 56
																- 1
	16 17	68 68	67 67	66 66	65 65	64 64	63 64	63 63	62 62	61	60 60	59 59	58 59	58 58	57 57	56 56
	18	68	67	66	65	65	64	63	62	61	60	60	59	58	57	57
	19	68	67	67	66	65	64	63	62	62	61	60	59	58	58	57
	20	68	68	67	66	65	64	63	63	62	61	60	59	59	58	57
	21	69	68	67	66	65	64	64	63	62	61	60	60	59	58	57
	22 23	69 69	68 68	67 67	66	65 66	65 65	64 64	63	62 62	$\frac{61}{62}$	61	60	59 59	58 59	58 58
	24	69	68	68	67	66	65	64	63	63	62	61	60	60	59	58
	25	69	69	68	67	66	65	64	64	63	62	61	61	60	59	58
	26	70	69	68	67	66	65	65	64	63	62	61	61	60	59	58
	27 28	70 70	69	68 68	67	66	66	65	64	63	62	62	61	60	59 60	59 59
	29	70	69	69	68	67 67	66 66	65 65	$\begin{bmatrix} 64 \\ 64 \end{bmatrix}$	63 64	63 63	$\begin{array}{c c} 62 \\ 62 \end{array}$	$\begin{bmatrix} 61 \\ 61 \end{bmatrix}$	61	60	59
	30	70	69	69	68	67	66	65	65	64	63	62	62	61	60	59
	31	70	70	69	68	67	66	66	65	64	63	62	62	61	60	60
	32 33	71 71	70	69 69	68 68	67 68	67 67	66	65 65	$\begin{bmatrix} 64 \\ 64 \end{bmatrix}$	64 64	63	62 62	61 61	$\begin{bmatrix} 61 \\ 61 \end{bmatrix}$	60
	34	71	70	69	69	68	67	66	66	65	64	63	62	62	61	60
	35	71	70	70	69	68	67	66	66	65	64	63	63	62	61	60
L	B							- 96								

the air   g = 0   g	Temper-			t —	t'= [	differen	ce of T	empera	tures of	f the D	ew Poi	nt and	of the	Air.		
Centig		9°.0	9°.2	9°.4	9°.6	9°.8	10°.0	10°.2	10°.4	10°.6	10°.8	11°.0	11°.2	11°.4	11°.6	11°.8
-8					<u> </u>											
-6	-8															
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-4	}															
-3 -2 -1 -1 0 4-1 50 4-9 4-9 4-9 4-9 4-9 4-9 4-9 4-9 4-9 4-9																
-2	1															
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1	-1															
2         50         49         49         48         47         46         46         45         45         44         43         42         42         41         51         50         49         48         47         46         45         44         44         43         42         42         41         5         52         51         50         49         48         47         46         45         44         43         42         42         41           6         52         52         51         50         49         48         47         46         45         44         43         42         41           7         53         52         51         50         49         48         47         46         45         44         43         42         48         47         46         45         44         43         42         8         53         52         51         50         50         49         48         47         46         45         44         44         43         42         8         47         46         45         44         44         44         44         44	0															
2         50         49         49         48         47         46         46         45         45         44         43         42         42         41         51         50         49         48         47         46         45         44         44         43         42         42         41         5         52         51         50         49         48         47         46         45         44         43         42         42         41           6         52         52         51         50         49         48         47         46         45         44         43         42         41           7         53         52         51         50         49         48         47         46         45         44         43         42         48         47         46         45         44         43         42         8         53         52         51         50         50         49         48         47         46         45         44         44         43         42         8         47         46         45         44         44         44         44         44	4.1	50														
4         51         51         50         49         48         47         46         45         44         43         42         42         41           5         52         51         50         49         49         48         47         46         45         44         43         42         41           6         52         52         51         50         49         48         47         46         45         44         43         43         42         41           7         53         52         51         50         49         48         47         46         45         45         44         43         43         42           8         53         52         51         50         50         49         48         47         46         45         44         44         43         42           9         54         53         52         51         50         50         49         48         47         46         45         44         44         44         44         44         44         44         44         44         44         44         44		50	49	49	48	47	46									
5         52         51         50         49         49         48         47         46         46         45         44         43         43         42         41           6         52         52         51         50         49         48         47         46         45         45         44         43         43         42         21           8         53         52         51         50         49         48         47         46         45         45         44         43         42           8         53         52         51         50         50         49         48         47         46         46         45         44         44         43         40         48         47         46         46         45         44         44         43         42         41         43         42         48         47         46         45         44				1												
6 52 52 51 50 49 48 48 47 46 45 45 44 43 43 42 42 8 53 52 51 50 50 49 48 48 47 47 46 45 45 44 44 43 42 43 9 54 53 52 51 51 50 50 49 49 48 48 47 47 46 45 45 44 44 43 43 10 54 53 52 51 51 50 50 49 49 48 48 47 47 46 45 45 44 44 43 10 54 53 52 51 51 50 50 49 49 48 48 47 47 46 45 45 44 44 43 10 54 53 53 52 51 51 50 50 49 49 48 48 47 47 46 45 45 44 44 41 11 54 53 53 53 52 51 51 50 50 49 49 48 48 47 47 46 46 45 44 44 11 11 55 54 53 53 52 51 51 50 50 49 49 48 47 47 46 46 45 45 45 44 11 11 55 54 53 53 52 51 51 50 50 49 49 48 47 47 46 46 46 45 45 11 55 54 53 53 52 52 51 50 50 49 49 48 47 47 46 46 46 45 11 55 55 54 53 53 52 51 51 50 50 49 49 48 47 47 46 46 46 45 15 55 54 53 53 52 51 51 50 50 49 49 49 48 47 47 46 46 46 45 15 55 54 53 53 52 51 51 50 50 49 49 49 48 47 47 46 46 46 45 17 56 55 54 53 53 52 51 51 50 50 49 49 49 48 48 47 47 46 46 46 45 17 56 55 54 53 53 52 52 51 51 50 50 49 49 49 48 48 47 47 47 46 45 18 56 55 54 53 53 52 51 51 50 50 49 49 49 48 48 47 47 47 46 46 46 19 56 55 54 53 53 52 51 51 50 50 49 49 49 48 48 47 47 47 46 19 56 55 54 53 53 52 51 51 50 50 49 49 49 48 48 47 47 47 46 19 56 55 54 53 53 52 51 51 50 50 49 49 49 48 47 47 47 46 19 56 55 54 53 53 52 51 51 50 50 49 49 49 48 47 47 47 46 19 56 55 54 53 53 52 51 51 50 50 49 49 49 48 47 47 47 46 19 56 55 54 53 53 52 51 51 50 50 49 49 49 48 47 47 47 46 19 56 55 54 53 53 52 51 51 50 50 49 49 49 48 47 47 47 46 19 56 55 54 53 53 53 52 51 51 50 50 49 49 49 48 47 47 47 46 46 46 45 45 45 45 45 45 45 45 45 45 45 45 45		3														41
7         53         52         51         51         50         49         48         47         46         45         45         44         43         42           8         53         52         52         51         50         49         49         48         47         46         46         45         44         44         43           9         54         53         52         51         50         50         49         48         47         46         45         44         44         43           10         54         53         52         51         50         50         49         48         47         46         45         44         44           11         54         53         52         51         50         50         49         48         47         47         46         46         45         44         41           12         54         53         52         51         50         50         49         48         47         47         46         46         45         44           12         54         53         52         51																
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6	41	41	40	39	39	38	37	37	36	36	35	35	34	33	33
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8 9	42 43	42	41	40	40	39 40	38	38	37 38	37	36 37	35	35 35	34	34
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12	44	43	43	42	41	41	40	40	39	38	38	37	37	36	36
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17	45	45	44	44	43	43	42	41	41	40	40	39	39	38	38
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20	46	45	45	44	44	43	42	42	41	41	40	40	39	39	38
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$\begin{array}{c c} 23 \\ 24 \end{array}$	47	46	46	45	45	44	44	43	42	42	41	41	40	40	39
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#### TABLE IV.

Factor  $_{\mathbf{F}}^{100}$ , for computing the relative humidity, or the degree of moisture of the air from its absolute humidity, given in millimetres.

#### BY HAEGHENS.

The Relative Humidity, or the degree of moisture of the air, is the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $\frac{f \times 100}{F}$  = Relative Humidity in Hundredths.

But as  $\frac{f \times 100}{F} = f \times \frac{100}{F}$ , it is obvious that the operation indicated by the former expression, viz.  $\frac{f \times 100}{F}$ , would be reduced to a simple multiplication, if we had a table of the factors  $\frac{100}{F}$ . Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quotients to the tensions.

The following Table, taken from the Annuaire Météorologique de la France, for 1850, p. 79, gives the factor  $\frac{100}{F}$  for every tenth of a degree from -10 to  $+35^{\circ}$  Centigrade, corresponding to the Forces of Vapor in Table I.

#### USE OF THE TABLE.

The force of vapor contained in the air being given in millimetres, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the *Relative Humidity in Hundredths*.

## Examples.

- 1. Suppose the temperature of the air to be  $=24^{\circ}$  Centigrade.
  - " force of vapor in the air to be = 10.76 millimetres.

Opposite 24° is found in the table the factor 4.51.

Then  $10.76 \times 4.51 = 48.5$ , Relative Humidity in Hundredths.

- 2. Suppose the temperature of the air to be = 16.7.
  - " force of vapor in the air to be = 12.07.

Table gives for 16.7 the factor 7.07.

Then  $12.07 \times 7.07 = 85.3$ , Relative Humidity.

factor  $\frac{100}{\mathrm{F}}$ , to compute the relative humidity.

t =	1				Tenths of	Degrees.				
Temp.						I				4
of Air, Centig.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° -10	48.1	48.5	48.9	49.3	49.7	50.1	50.5	50.9	51.4	51.8
9	44.2	44.6	45.0	45.4	45.7	46.1	46.5	46.9	47.3	47.7
8	40.7	41.1	41.4	41.7	42.1	42.4	42.8	43.1	43.5	43.9
7	37.5	37.8	38.1	38.4	38.7	39.0	39.4	39.7	40.0	40.4
6	34.6	34.9	35.2	35.4	35.7	36.0	36.3	36.6	36.9	37.2
5	31.9	32.2	32.4	32.7	33.0	33.2	33.5	33.8	34.0	34.3
4	29.5	29.8	30.0	30.2	30.5	30.7	31.0	31.2	31.4	31.7
3	27.3	27.5	27.7	27.9	28.2	28.4	28.6	28.8	29.1	29.3
2	25.3	25.5	25.7	25.9	26.1	26.3	26.5	26.7	26.9	27.1
1	23.4	23.6	23.8	24.2	24.0	24.3	24.5	24.7	24.9	25.1
-0	21.7	21.9	22.1	22.2	22.4	22.6	22.8	22.9	23.1	23.3
+0	21.7	21.6	21.4	21.3	21.1	21.0	20.8	20.7	20.5	20.4
1	20.2	20.1	20.0	19.8	19.7	19.5	19.4	19.3	19.1	19.0
2	18.9	18.7	18.6	18.5	18.3	18.2	18.1	18.0	17.8	17.7
3	17.6	17.5	17.3	17.2	17.1	17.0	16.9	16.7	16.6	16.5
4	16.4	16.3	16.2	16.1	15.9	15.8	15.7	15.6	15.5	15.4
5	15.3	15.2	15.1	15.0	14.9	14.8	14.7	14.6	14.5	14.4
6	14.3	14.2	14.1	14.0	13.9	13.8	13.7	13.6	13.5	13.4
7	13.4	13.3	13.2	13.1	13.0	12.9	12.8	12.7	12.6	12.6
8	12.5	12.4	12.3	12.2	12.1	12.1	12.0	11.9	11.8	11.7
9	11.7	11.6	11.5	11.4	11.4	11.3	11.2	11.1	11.1	11.0
10	10.9	10.8	10.8	10.7	10.6	10.6	10.5	10.4	10.3	10.3
11	10.2	10.1	10.1	10.0	9.95	9.88	9.82	9.75	9.69	9.63
12	9.56	9.50	9.44	9.38	9.32	9.26	9.20	9.13	9.08	9.02
13	8.96	8.90	8.84	8.79	8.73	8.67	8.62	8.56	8.51	8.45
14	8.40	8.34	8.29	8.24	8.18	8.15	8.08	8.03	7.98	7.92
15	7.87	7.82	7.77	7.72	7.68	7.63	7.58	7.53	7.48	7.43
16	7.39	7.34	7.29	7.25	7.20	7.16	7.11	7.07	7.02	6.98
17	6.93	6.89	6.85	6.80	6.76	6.72	6.68	6.63	6.59	6.55
18	6.51	6.47	6.43	6.39	6.35	6.31	6.27	6.23	6.19	6.16
19 20	6.12 5.75	6.08 5.71	6.04 5.68	6.00 5.64	5.97 $5.61$	5.93 5.58	5.89 $5.54$	5.86 5.51	5.S2 5.47	5.79 5.44
21	5.41	5.37	5.34	5.31	5.27	5.24	5.21	5.18	5.15	5.12
22	5.09	5.06	5.02	4.99	4.96	4.93	4.90	4.87	4.85	4.82
23	4.79	4.76	4.73	4.70	4.67	4.65	4.62	4.59	4.56	4.53
24	4.51	4.48	4.45	4.43	4.40	4.37	4.35	4.32	4.30	4.27
25	4.25	4.22	4.20	4.17	4.15	4.12	4.10	4.07	4.05	4.03
26	4.00	3.98	3.95	3.93	3.91	3.89	3.86	3.84	3.82	3.79
27	3.77	3.75	3.73	3.71	3.69	3.66	3.64	3.62	3.60	3.58
28	3.56	3.54	3.52	3.50	3.48	3.46	3.44	3.42	3.40	3.38
29	3.36	3.34	3.32	3.30	3.28	3.26	3.24	3.22	3.21	3.19
30	3.17	3.15	3.13	3.12	3.10	3.08	3.06	3.05	3.03	3.01
31	2.99	2.98	2.96	2.94	2.93	2.91	2.89	2.88	2.86	2.84
32	2.83	2.81	2.80	2.78	2.77	2.75	2.73	2.72	2.70	2.69
33	2.67	2.66	2.64	2.63	2.61	2.60	2.58	2.57	2.56	2.54
34	2.53	2.51	2.50	2.49	2.47	2.46	2.44	2.43	2.42	2.40
35	2.39	2.38	2.36	2.35	2.34	2.33	2.31	2.30	2.29	2.28

#### TABLE V.

## WEIGHT OF VAPOR, IN GRAMMES,

contained in a cubic metre of saturated air under a barometric pressure of 760 millimetres, and at temperatures between  $-20^{\circ}$  and  $+40^{\circ}$  centigrade.

The theoretic density of aqueous vapor is very nearly 0.622, or  $\frac{5}{8}$ , of the density of the air at the same temperature and pressure. Regnault's experiments gave similar results. From this ratio the weight of the vapor contained in a given volume of air, the temperature and humidity of which are known, can be computed.

If we call

t = the temperature of the air;

f = the elastic force of the vapor contained in the air at the time of the observation;

F = the maximum elastic force of vapor due to the temperature t, as given in the table;

p = the weight of the vapor contained in a litre of air at the temperature t, and with a force of vapor f;

P = the weight of vapor in a litre of air at the temperature t, and at full saturation, or F.

Then,

$$p = 0.622 \, \frac{1.293223^{\text{gr.}}}{1 + 0.00367 \, t} \cdot \frac{f}{760^{\text{mins.}}}.$$

In which 1.293223 grammes is the weight of a litre of dry air, at the temperature of zero Centigrade, and under a barometric pressure of 760 millimetres, according to the determination of Regnault; 0.00367, the coefficient of the expansion of the air as found by the same; 760 millimetres, the assumed normal barometric pressure.

The weight of a litre of air given by Regnault in the Mémoires de l'Institut, Tom. XXI. p. 157, is 1.293187 grammes; but by correcting a slight error of computation (see E. Ritter, Mémoires de la Société Physique de Genève, Tom. XIII. p. 361), it becomes, as given above, 1.293223 grammes.

In order to obtain the weight of vapor in a cubic metre, or 1000 litres, of saturated air, the formula becomes,

$$P = 0.622 \, rac{1293.223 {
m gr.}}{1 + 0.00367 \, t} \cdot rac{F}{760 {
m mm.}} \, .$$

From this formula Table V, has been computed. The tensions due to the temperatures in the first column are placed opposite the weights of vapor; they are taken from Table I. It will be seen that, throughout the table, the number of grammes of vapor nearly corresponds to the number of millimetres of pressure expressing the tension.

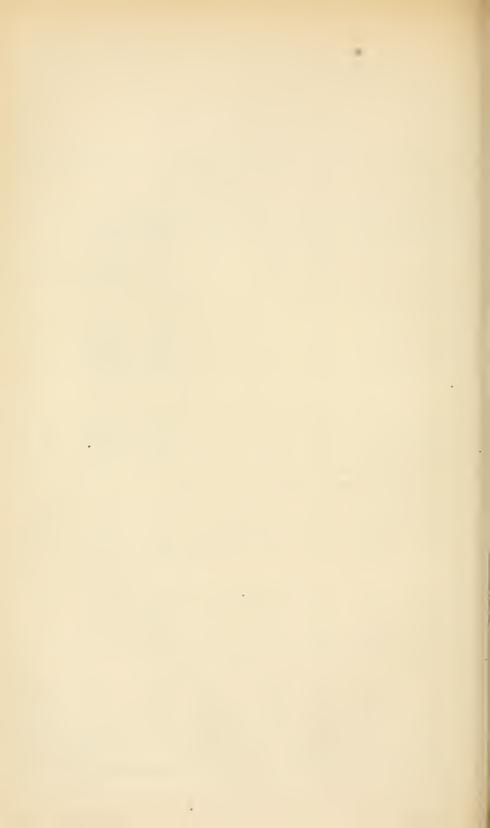
The table of the weights of vapor given in Pouillet's Eléments des Physique, Tom. II. p. 707, being based on older values, gives results somewhat different. In that published by Becquerel, Eléments de Physique Terrestre, p. 354, Regnault's tensions and coefficient of expansion of the air have been used, but the value of the weight of vapor in a litre of air formerly determined by Biot and Arago, viz. 1.29954 grammes, has been retained.

## V. WEIGHT OF VAPOR, IN GRAMMES,

## CONTAINED IN A CUBIC METRE OF SATURATED AIR,

At Temperatures between  $-20^{\circ}$  and  $+40^{\circ}$  Centigrade.

1:							
Temperature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Difference.	Temperature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Difference.
Centigrade.	Millimetres.	Grammes.	Grammes.	Centigrade.	Millimetres.	Grammes.	Grammes.
-20°	0.912	1.042		+10°	9.165	9.357	
-19	0.993	1.130	0.088	11	9.792	9.962	0.605
-18	1.080	1.224	0.094	12	10.457	10.601	0.639
-17	1.174	1.325	0.101	13	11.162	11.276	0.675
-16	1.275	1.434	0.109	14	11.908	11.988	0.712
-15	1.385	1.551	0.118	15	12.699	12.739	0.751
-14	1.503	1.678	0.127	16	13.536	13.532	0.793
-13	1.631	1.813	0.134	17	14.421	14.367	0.835
-12	1.768	1.957	0.145	18	15.357	15.247	0.880
-11	1.918	2.114	0.157	19	16.346	16.173	0.926
-10	2.078	2.283	0.169	20	17.391	17.148	0.975
- 9	2.261	2.475	0.192	21	18.495	18.174	1.026
- 8	2.456	2.678	0.203	22	19.659	19.253	1.078
- 7	2.666	2.896	0.218	23	20.888	20.387	1.134
- 6	2.890	3.128	0.232	24	22.184	21.579	1.192
					į		
					l		
- 5	3.131	3.376	0.248	25	23.550	22.831	1.252
- 4	3.387	3.638	0.262	26	24.988	24.144	1.313
- 3	3.662	3.919	0.281	27	26.505	25.524	1.380
- 2	3.955	4.217	0.298	28	28.101	26.971	1.447
- 1	4.267	4.534	0.317	29	29.782	28.489	1.519
							1
0	4.600	4.869	0.334	30	31.548	30.079	1.589
+ 1	4.940	5.209	0.341	31	33.405	31.744	1.666
2	5.302	5.571	0.361	32	35.359	33.491	1.747
3	5.687	5.953	0.383	33	37.410	35.317	1.827
4	6.097	6.360	0.406	34	39.565	37.230	1.913
			0.431				0.001
5	6.534	6.791	0.431	35	41.827	39.231	2.001
6	6.998	7.247	1	36	44.201	41.323	
7	7.492	7.731	0.484	37	46.691	43.510	2.187
8	8.017	8.243	0.512	38	49.302	45.795	2.285
9	8.574	8.785	0.541	39	52.039	48.182	2.387
+10	9.165	9.357	0.572	+40	54.906	50.674	2.492
					1	1	



# PRACTICAL TABLES,

IN

## ENGLISH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

## VI.

## TABLE OF THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT,
REDUCED FROM REGNAULT'S TABLE.

THE values of the elastic force of vapor furnished by V. Regnault, which are found in Table I. of this Hygrometrical set, are derived from a series of experiments conducted, during several years, with great care, consummate skill, and all the means of precision which are at the disposal of modern science. The methods of investigation, and all the steps in each experiment, were minutely described and submitted to the judgment of the scientific, successively in separate papers in several volumes of the Annales de Chimie et de Physique, and collectively in his final Report to the Minister of Public Works, (see above, p. 9,) which fills Volume XXI. of the Mémoires de l'Institut de France. The confidence which has been deservedly granted to these determinations by nearly all scientific men, is increased by the fact that one of the best physicists and experimenters in Germany, Professor Magnus, came, about the same time, to results so little different, that both tables, for most purposes, may be considered identical. (Compare below, Table XXII.) It seems, therefore, that these values ought to be used in our hygrometrical tables, as has been done in France, in preference to the older and less reliable determinations on which they are based.

Though Regnault's table of the elastic force of vapor is considered, even, it is believed, by a majority of scientific men in England, as the most reliable which science now possesses, the author is not aware that any extensive reduction of it to English measures, such as is wanted for meteorological purposes, has been as yet published; still less a series of tables based on these values. Such a set of hygrometrical tables in English measures, corresponding to the preceding one in French measures, is offered here, which, it is hoped, supplies a real want felt by a large number of meteorologists.

Table VI. is Regnault's Table of the Elastic Force of Vapor as given in Table I., reduced to English measures, in which the fourth decimal is given in order to secure the third, and otherwise to facilitate the computations. From these values Tables VII. to X. have been computed.

## VI. ELASTIC FORCE OF AQUEOUS VAPOR,

## EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

## REDUCED FROM REGNAULT'S TABLE.

	Force of	Vapor.		Force o	f Vapor			Fore	e of Vapor	\i		of Vapor.
Temper- ature Fahren- heit.	renths of	Degrees.	Temper- ature Fahren- heit.	Tenths of	f Degree	s. at	per- ure ren- eit.	Tenth	s of Degre	es. Temp	en-Tenths	of Degrees.
	0	0.5		0	0.5			0	0.6	. 11	0	0.5
	Eng. In.	Eng. In.		Eng. In.	Eng. I			Eng.			Eng. In	
-31	0.0087	0.0085	-19	0.0171	0.016	11	8	0.02	)	- 11	1	1
-30	0.0092	0.0090	-18	0.0181	0.017	- II	. 7	0.03		- 11	3 0.0498	
-29	0.0098	0.0095	-17	0.0190	0.018	- 11	6	0.03	1	11	4 0.0521	1
-28	0.0104	0.0101	-16	0.0200	0.019	- 11	5	0.03	- 1	- 11	5 0.0545	
-27	0.0110	0.0107	-15	0.0210	0.020		4	0.03		11	6 0.0570	1 1
-26	0.0117	0.0114	-14	0.0221	0.021	6   -	. 3	0.03	76 0.03	68	7 0.0597	0.0611
-25	0.0124	0.0120	-13	0.0232	0.022	27 -	2	0.03	95 0.03	86	8 0.0625	0.0639
-24	0.0131	0.0127	-12	0.0244	0.023	88 -	1	0.04	14 0.04	04	9 0.0654	0.0669
-23	0.0138	0.0135	-11	0.0257	0.025	60   -	0	0.04	34 0.04	24 1	0 0.0684	0.0700
· -22	0.0146	0.0142	-10	0.0270	0.026	63 +	0	0.04	34 0.04	14 1	1 0.0716	0.0732
-21	0.0154	0.0150	- 9	0.0283	0.027	6 +	1	0.04	54 0.04	65   1	2 0.0749	0.0766
-20	0.0163	0.0158	- 8	0.0297	0.029	+   00	2	0.04	76 0.04	87   +1	3 0.0783	0.0800
Temper- ature					Т	enths of	Deg	rees.				
Fahren-							_					
heit.	0.	1.	2.	3		4.		5.	6.	7.	8.	9.
0	Eng. In	Eng. In	Eng. I	n. Eng.	In. E	ing. In.	Eng	Jn.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
14	0.0818	1	1	26 0.08	530 0	0.0834	0.0	837	0.0841	0.0845	1	0.0853
15	0.0857	0.086	1 0.086	65 0.08	869   C	0.0873	0.0	877	0.0881	0.0885	0.0889	0.0893
16	0.0898	1	i	1		.0914		918	0.0923	0.0927	1	0.0936
17	0.0940	1			- 1	0.0958		962	0.0967	0.0971		0.0980
18	0.0984					0.1002		007	0.1012	0.1016	1 -	0.1025
19	0.1030	0.1033	5 0.104	0.10	044   0	.1049	0.1	054	0.1059	0.1064	0.1068	0.1073
20	0.1078	0.108	0.108	88 0.10	193 0	0.1098	0.1	103	0.1108	0.1113	0.1118	0.1123
21	0.1128			-		0.1148		153	0.1159	0.1164		0.1174
22	0.1179					).1200		206	0.1211	0.1217		0.1227
23	0.1233		1			.1255		260	0.1266	0.1272	1	0.1283
24	0.1289				- 1	.1312		318	0.1324	0.1329		0.1341
25	0.1347					.1371		377	0.1383	0.1389	1	0.1401
					- 1							
26	0.1407					.1432		438	0.1444	0.1450		0.1463
27	0.1469					.1495	1	501	0.1508	0.1514		0.1527
28	0.1534					.1560		567	0.1573	0.1580		0.1593
29	0.1600					.1627		634	0.1641	0.1647	1	0.1661
30	0.1668					.1696	1	703	0.1710	0.1717		0.1732
31	0.1739	0.174	6 0.175	0.13	760	).1767		775	0.1782	0.1789	0.1796	0.1804
	v.	1.	2.	3	•	4.		5.	6.	7.	8.	9.

Expressed in English Inches of Mercury for Temperatures of Fahrenheit.

Tempera-					Tenths o	f Degrees.				
ture of Fahren- heit.	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
32	0.1811	0.1818	0.1825	0.1833	0.1840	0.1847	0.1854	0.1861	0.1869	0.1876
33	0.1883	0.1891	0.1898	0.1906	0.1913	0.1921	0.1928	0.1936	0.1944	0.1951
34	0.1959	0.1967	0.1974	0.1982	0.1990	0.1998	0.2006	0.2013	0.2021	0.2029
35	0.2037	0.2045	0.2053	0.2061	0.2070	0.2077	0.2086	0.2094	0.2102	0.211
36	0.2119	0.2127	0.2135	0.2144	0.2152	0.2161	0.2169	0.2178	0.2186	0.219
37	0.2204	0.2212	0.2221	0.2230	0.2238	0.2247	0.2256	0.2265	0.2273	0.228
38	0.2291	0.2300	0.2309	0.2318	0.2327	0.2336	0.2345	0.2354	0.2364	0.2373
39	0.2382	0.2391	0.2400	0.2410	0.2419	0.2428	0.2438	0.2447	0.2457	0.246
40	0.2476	0.2485	0.2495	0.2504	0.2514	0.2524	0.2533	0.2543	0.2553	0.256
41	0.2572	0.2582	0.2592	0.2602	0.2612	0.2622	0.2632	0.2642	0.2652	0.2662
42	0.2672	0.2682	0.2692	0.2702	0.2713	0.2723	0.2733	0.2744	0.2754	0.276
43	0.2775	0.2785	0.2796	0.2807	0.2817	0.2828	0.2839	0.2850	0.2860	0.287
44	0.2882	0.2893	0.2904	0.2915	0.2926	0.2937	0.2948	0.2960	0.2971	0.298
45	0.2993	0.3005	0.3016	0.3028	0.3039	0.3050	0.3062	0.3074	0.3085	0.309
46	0.3108	0.3120	0.3132	0.3144	0.3156	0.3168	0.3179	0.3191	0.3203	0.321
47	0.3228	0.3240	0.3252	0.3264	0.3276	0.3289	0.3301	0.3313	0.3326	0.3338
48	0.3351	0.3363	0.3252	0.3388	0.3401	0.3414	0.3426	0.3439	0.3320	0.346
49	0.3477	0.3490	0.3503	0.3516	0.3529	0.3542	0.3556	0.3569	0.3582	0.359
50	0.3608	0.3622	0.3635	0.3648	0.3661	0.3675	0.3688	0.3702	0.3715	0.3729
51	0.3743	0.3756	0.3770	0.3784	0.3798	0.3812	0.3826	0.3840	0.3854	0.3868
52	0.3882	0.3896	0.3911	0.3925	0.3939	0.3954	0.3968	0.3983	0.3997	0.4015
53	0.4027	0.4041	0.4056	0.3923	0.4086	0.3954	0.4116	0.4131	0.3337	0.416
54	0.4176	0.4191	0.4207	0.4222	0.4237	0.4101	0.4268	0.4131	0.4299	0.431
55	0.4331	0.4346	0.4207	0.4222	0.4394	0.4233	0.4426	0.4442	0.4458	0.447
56	0.4490	0.4507	0.4523	0.4539	0.4556	0.4572	0.4589	0.4442	0.4622	0.463
57	0.4655	0.4672	0 1000	0 4505	0 (**00	0.4700	0.4750	0.4550	0.4701	0.4808
58	0.4825	0.4842	0.4689 0.4859	$0.4705 \\ 0.4876$	0.4722	0.4739	0.4756	0.4773	0.4791	0.498
59	0.4823	0.4842	0.4859		0.4894	0.4912		0.4947	0.4964	0.4987
60	0.5179	0.5198	0.5035	0.5053 $0.5234$	0.5253	$0.5089 \\ 0.5271$	0.5107	0.5125	0.5328	0.5340
61	0.5365	0.5384	0.5210	0.5422	0.5441	0.5461	0.5480	0.5499	0.5519	0.553
63	0.5550	0 ====	0.5505	0.5035	0.500.0	0.500	0.5000	0 5000	0.5510	0.573
62					1	0.5656				
63	0.5756	0.5777	0.5797	0.5817	0.5838	0.5858	0.5879	0.5899	0.5920	0.594
64	0.5962	0.5983	0.6004	0.6025	0.6046	0.6067	0.6088	0.6109	0.6131	0.6152
65	0.6173	0.6195	0.6217	0.6238	0.6260	0.6282	0.6304	0.6325	0.6347	0.6369
66 67	0.6392 0.6616	0.6414	0.6436 0.6662	0.6458 0.6685	0.6481 0.6708	0.6503 0.6731	$0.6525 \\ 0.6754$	0.6548 0.6777	0.6571 0.6800	0.659 $0.682$
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Expressed in English Inches of Mercury for Temperatures of Fahrenheit.

Tempera-					Tenths of	Degrees.				
ture of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In. 0.7036	Eng. In. 0.7060							
68	0.6847	0.6870	0.6894	0.6917	0.6941	0.6965	0.6989	0.7012 $0.7255$	0.7030	0.7305
69 70	0.7084	0.7108 $0.7354$	0.7133 0.7379	0.7157 $0.7405$	0.7181 0.7430	0.7206 $0.7455$	0.7230 $0.7480$	0.7506	0.7531	0.7557
71	0.7583	0.7609	0.7634	0.7403	0.7686	0.7433	0.7739	0.7765	0.7791	0.7818
72	0.7844	0.7871	0.7897	0.7924	0.7951	0.7978	0.8005	0.8032	0.8059	0.8086
73	0.8113	0.8141	0.8168	0.8196	0.8223	0.8251	0.8279	0.8307	0.8335	0.8363
74	0.8391	0.8419	0.8447	0.8476	0.8504	0.8533	0.8561	0.8590	0.8619	0.8648
75	0.8676	0.8705	0.8735	0.8764	0.8793	0.8822	0.8852	0.8881	0.8911	0.8940
76	0.8970	0.9000	0.9030	0.9060	0.9090	0.9120	0.9150	0.9180	0.9211	0.9241 $0.9550$
77	0.9272	0.9302	0.9333	0.9364	0.9395	0.9426	0.9457	0.9488	0.9519	
78	0.9582	0.9613	0.9645	0.9677	0.9709	0.9740	0.9773	0.9805	0.9837	0.9869
79	0.9902	0.9934	0.9967	1.0000	1.0033	1.0065	1.0099	1.0132	1.0165	1.0198
80	1.0232	1.0265	1.0299	1.0332	1.0366	1.0400	1.0434	1.0468	1.0503	1.0537
81	1.0572	1.0606	1.0641	1.0675	1.0710	1.0745	1.0780	1.0815	1.0851	1.0886
82	1.0922	1.0957	1.0993	1.1028	1.1064	1.1100	1.1136	1.1172	1.1209	1.1245
83	1.1281	1.1318	1.1354	1.1391	1.1428	1.1465	1.1502	1.1539	1.1576	1.1614
84	1.1651	1.1689	1.1726	1.1764	1.1802	1.1840	1.1878	1.1916	1.1954	1.1993
85	1.2031	1.2070	1.2108	1.2147	1.2186	1.2225	1.2264	1.2303	1.2342	1.2381
86	1.2421	1.2460	1.2500	1.2540	1.2580	1.2620	1.2660	1.2700	1.2740	1.2781
87	1.2821	1.2862	1.2903	1.2944	1.2985	1.3026	1.3068	1.3109	1.3151	1.3192
88	1.3234	1.3276	1.3318	1.3361	1.3403	1.3445	1.3488	1.3531	1.3573	1.3616
89	1.3659	1.3703	1.3746	1.3789	1.3833	1.3877	1.3920	1.3964	1.4008	1.4053
90	1.4097	1.4141	1.4186	1.4230	1.4275	1.4320	1.4365	1.4410	1.4456	1.4501
91	1.4546	1.4592	1.4638	1.4684	1.4730	1.4776	1.4822	1.4869	1.4915	1.4962
92	1.5008	1.5055	1.5102	1.5149	1.5197	1.5244	1.5291	1.5339	1.5387	1.5435
93	1.5482	1.5531	1.5579	1.5627	1.5676	1.5724	1.5773	1.5822	1.5871	1.5920
94	1.5969	1.6018	1.6068	1.6117	1.6167	1.6217	1.6267	1.6317	1.6367	1.6417
95	1.6468	1.6518	1.6569	1.6620	1.6671	1.6722	1.6773	1.6825	1.6876	1.6928
96	1.6980	1.7032	1.7084	1.7137	1.7189	1.7242	1.7295	1.7348	1.7401	1.7454 1.7995
97	1.7508 1.8050	1.7561	1.7615	1.7669	1.7723	1.7777	1.7831	1.7886 1.8438	1.7940 1.8494	1.7555
98	1.5050	1.8105	1.8160	1.8215	1.8271	1.8327	1.8382	1,0400	1.0434	1.0001
99	1.8607	1.8664	1.8720	1.8777	1	1.8891	1.8949	1.9006	1.9064	1.9121
100	1.9179	1.9237	1.9295	1.9354	1.9412	1.9471	1.9530	1.9589	1.9648	1.9707
101	1.9766	1.9826	1.9885	1.9945	2.0005	2.0065	2.0126	2.0186	2.0247	2.0307
102	2.0368	2.0429	2.0490	2.0552	2.0613	2.0675	2.0737	2.0798 2.1426	2.0861 2.1489	2.0923
103	2.0985	2.1048 2.1681	2.1110 2.1745	2.1173 2.1810	2.1236 2.1874	2.1299 2.1939	2.1362 2.2004	2.1420	2.1405	2.2200
104					·				·	9.
	0.	1.	2.	3.	4.	5.	6.	7.	8.	3.

## VII.

## PSYCHROMETRICAL TABLES,

GIVING, IN ENGLISH INCHES OF MERCURY, THE ELASTIC FORCE OF VAPOR CONTAINED

IN THE AIR, AND ITS RELATIVE HUMIDITY IN HUNDREDTHS;

DERIVED FROM THE INDICATIONS OF THE WET AND DRY BULB THERMOMETERS,

IN DEGREES OF FAHRENHEIT.

### By A. Guyor.\*

M. V. Regnault, in his Etudes sur l'Hygrométrie Annales de Chimie et de Physique, 3<sup>me</sup> série, Tom. XV. p. 129, after having discussed the theoretical bases of the psychrometric formula given by August, and modified the numerical values of some of its coefficients, adopts the formula

$$x = f - \frac{0.480 (t - t')}{610 - t'} h$$

for temperatures above the freezing-point; and when the temperature of the wet thermometer is below the freezing-point, the bulb being covered with a film of ice,

$$x = f - \frac{0.480 (t - t')}{689 - t'} h,$$

<sup>\*</sup> While this table was going through the press, a similar one, prepared by Prof. T. H. Coffin for his private use, was published by the Smithsonian Institution, in order to meet an urgent demand from many quarters. Being based on the same formula, it gives the same results, except, perhaps, in degrees below 14° Fahrenheit, where the tables show slight discrepancies. These unimportant differences arise from the fact that Prof. Coffin's table was computed from Regnault's tensions, as given in the first edition of this collection, while the author's table is based on the table of tensions as given in this second edition, in which the values below 14° Fahrenheit have been somewhat modified, for reasons given above. The following table gives also the relative humidity with one more decimal, which makes the interpolations more easy; and a column of differences for finding the values for fractions of t'. A table for reducing the results to another barometric height is added at the end of the table.

in which

x represents the force of vapor in the air at the time of the observation;

t, the temperature of the air in Centigrade degrees, indicated by the dry thermometer;

t', the temperature of evaporation given by the wet thermometer;

f, the force of vapor in a saturated air at the temperature t';

h, the height of the barometer.

Substituting the Fahrenheit scale for the Centigrade, the formula, for temperatures above the freezing-point, reads

$$x = f - \frac{0.480 \times \frac{5}{9} (t - t')}{610 - \frac{5}{9} (t' - 32^{\circ})} \ h = f - \frac{0.480 \ (t - t')}{1130 - t'} \ h \,;$$

and below the freezing-point,

$$x = f - \frac{0.480 \times \frac{5}{9} (t - t')}{689 - \frac{5}{9} (t' - 32^{\circ})} h = f - \frac{0.480 (t - t')}{1240.2 - t'} h.$$

Making, further, h=29.7 English inches, these formulæ become

$$x = f - \frac{0.480 (t - t')}{1130 - t'} 29.7 = f - \frac{14.256 (t - t')}{1130 - t'}$$

and

$$x = f - \frac{0.480 (t - t')}{1240.2 - t'} 29.7 = f - \frac{14.256 (t - t')}{1240.2 - t'}.$$

The mean barometric pressure for which the table has been computed, viz. 29.7 inches, is, within a small fraction, the same as that adopted in Haeghens's Tables, No. II., which is 755 millimetres = 29.725 Eng. inches. As that slight difference in the barometric pressure cannot cause, in the most extreme cases, a difference exceeding two thousandths of an inch in the elastic forces, the results in the two tables may be considered identical.

That barometric pressure, corresponding, in our latitudes, to a mean altitude of 250 to 300 feet above the sea, is likely to suit, without correction, the largest number of meteorological stations. Should the mean height of the barometer, in consequence of the elevation of the station, much differ from that adopted in the table, a constant correction can be determined, to be applied to the numbers in the table. At the end, page 72, will be found a table which furnishes that correction for barometric heights between 20 and 31 inches, and for values of t - t' between 2° and 26° Fahrenheit.

The effect of the irregular variations of the barometer at the same station can, in most cases, be neglected; for the error due to that cause will scarcely ever exceed those which may arise from the uncertainty of the very elements on which the tables are based.

#### ARRANGEMENT OF THE TABLES.

The same arrangement as is found in the Psychrometrical for the Centigrade scale has been adopted.

The first column at the left contains the indications of the wet-bulb thermometer, from -31° to 105° Fahrenheit.

The second column gives the differences of the force of vapor for each tenth of a degree, between each two consecutive full degrees in the first column. It enables the observer easily to find the values for the fractions of degrees of the wet thermometer.

The following double columns furnish the forces of vapor and the relative humidity corresponding to each full degree of the wet-bulb thermometer given in the first column in the same horizontal line, and to the difference of the two thermometers, or t-t', found at the head of each column, for every half-degree from 0° to 26°.5. The relative humidity, or the fraction of saturation, is given in hundredths, which is near enough for meteorological purposes; but one decimal more has been added, though separated by a point, in order to facilitate the interpolations.

At the bottom of each page is found the mean difference, for each tenth of a degree, between the forces of vapor on the same line. It gives the means of finding the values for the intermediate differences of t - t', not found in the tables.

## Use of the Tables.

Enter the tables with the difference of the two thermometers, or t-t', and the temperature of the wet-bulb thermometer, given by observation.

In the column headed by the observed difference of the thermometer, t-t', and on the horizontal line headed by the observed temperature of the wet thermometer, t', are found the force of vapor, and the relative humidity corresponding to these temperatures.

For the fractions of degrees of the wet thermometer, multiply the decimal fraction by the number placed in the second column between the full degree and the next, and add the product if the temperature is above, and subtract it if it is below zero Fahrenheit.

The intermediate values of t - t' not given in the table are found by *subtracting* the number in the line at the bottom of the page, multiplied by the number of additional tenths, from the value given in the table. This correction, being always very small, can usually be neglected.

For the relative humidity, interpolations at sight will generally suffice.

## Examples.

Dry thermometer,  $t=50^{\circ}$  F. Wet thermometer,  $t'=43^{\circ}$  F. Difference, or  $t-t'=7^{\circ}$  F.

Page 58, we find for  $t - t' = 7^{\circ}$  in the third double column, and for  $t' = 43^{\circ}$  in the first column

Force of vapor in the air = 0.186 inch. Relative humidity in hundredths = 51

#### PSYCHROMETRICAL TABLES.

2. Dry thermometer,  $t = 88^{\circ}.5$  F. Wet thermometer,  $t' = 76^{\circ}.3$  F.

Difference,  $t - t' = 12^{\circ}.2$  F.

Page 63, Table gives for t - t' = 12 and  $t' = 76^{\circ}$  = 0.735 inch.

Add for fraction of t' = 0.3,  $0.003 \times 3 = 0.009$ 

Subtract for fraction of  $t - t' = 0^{\circ}.2$ ,  $.0013 \times 2 = -0.003$ 

Force of vapor in the air = 0.741

Relative humidity = 55

3. Dry thermometer,  $t = -4^{\circ}.5 \text{ F.}$ 

Wet thermometer,  $t' = 6^{\circ}.0 \text{ F}.$ 

Difference,  $t - t' = 1^{\circ}.5$  F.

Page 50, Table gives for  $t-t'=1^{\circ}.5$  and  $t'=-6^{\circ}=0.016$  inch.

Subtract for fraction of t' = 0.5,  $0.0002 \times 5 = -0.001$ Force of vapor in the air = 0.015

Relative humidity = 45

 $\textbf{T}emperature, Fahrenheit. \textbf{--} Force of Vapor in English Inches. \textbf{--} Relative Humidity in Hundredths.}$ 

								t and Dry se Bulb co				e.	
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	1	.0	00	.5	10	.0	10	.5	20	.0	20	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative IIu- mid- ity.	Force of Vapor	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu-mid-ity.	Force o Vapor.	
-31		Eng. In. 0.009	100	Eng. In. 0.003	36.0	Eng. In.		Eng. In.		Eng. In		Eng. In	
-30	.00005	0.009	100	0.004	39.6								
-29	.00006	0.010	100	0.004	42.9								
-28	.00006	0.010	100	0.005	46.1							l .	
-27	.00000	0.011	100	0.006	49.0							1	
	.00006										1		
-26	00007	0.012	100	0.006	51.8								
-25	.00007	0.012	100	0.007	54.4			i i		l			
-24	.00008	0.013	100	0.008	56.8					1			
-23	.00008	0.014	100	0.008	59.0								
-22		0.015	100	0.009	61.0			1					
	.00008												
-21		0.015	100	0.010	62.6	0.004	26.9						
-20	.00008	0.016	100	0.011	64.2	0.005	30.3						
-19	.00009	0.017	100	0.012	65.9	0.006	33.5	ĺ				l	
-18	.00003	0.018	100	0.012	67.5	0.007	36.6						
-17		0.019	100	0.013	69.0	0.008	39.5						
	.0001												
-16	0001	0.020	100	0.014	70.4	0.009	42.3						
-15	.0001	0.021	100	0.015	71.8	0.010	44.9	0.004	19.4				
-14	.0001	0.022	100	0.017	73.0	0.011	47.4	0.005	23.0				
-13	.0001	0.023	100	0.018	74.3	0.012	49.8	0.007	26.4				
-12		0.024	100	0.019	75.4	0.013	51.9	0.008	29.5				
	.0001					1							
-11	0001	0.026	100	0.020	76.5	0.014	53.9	0.009	32.5				
-10	.0001	0.027	100	0.021	77.5	0.016	55.7	0.010	35.3	0.005	15.6		
- 9	1000.	0.028	100	0.023	78.5	0.017	57.7	0.012	38.3	0.006	19.1		
- 8	.0001	0.030	100	0.024	79.4	0.018	59.4	0.013	40.6	0.007	22.5		
- 7 - 6	•0001	0.031	100	0.026	80.3	0.020	61.1	0.014	43.0	0.009	25.7	0.00=	70.0
- 0		0.000	100	0.027	81.1	0.021	62.7	0.016	45.4	0.010	28.4	0.005	12.9
	•0002												
- 5	.0002	0.034					64.5	0.017	47.6	0.012	31.7		16.4
- 4	.0002	0.036	100	0.030	82.5	0.025	65.8	0.019	49.8	0.014	34.5	0.008	19.8
- 3	.0002	0.038	100	0.032	83.2	0.026	67.1	0.021	51.7	0.015	36.9	0.010	22.8
- 2 - 1	.0002	0.039	100	0.034	83.9	0.028	68.3	0.023	53.5	0.017	39.3	0.011	25.8
- 0	.0002	0.041	100	0.038	84.5 85.0	$0.030 \\ 0.032$	69.5 71.0	$0.024 \\ 0.026$	55.3 57.0	$0.019 \\ 0.021$	41.6 43.8	0.013	28.6 31.3
				3.000	30.0	J.00	, 110	31020	31.0	0.021	10.0	31010	91.0
'	·	Mea	n Horiz	ontal Diff	crence o	of Force	of Vapo	r for each	0°.1=	0.0012.			

## PSYCHROMETRICAL TABLES.

Temperature, Fahrenheit. -- Force of Vapor in English Inches. -- Relative Humidity in Hundredths.

	Temperati	ire, rann	enner.										
			1	t', below				and Dry					
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	<b>0</b> °.	0	0°.	5	<b>1</b> °.	0	1°.	5	2°.	0	2°.	5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity
0		Eng. In.	100	Eng. In.	05.0	Eng. In.	70.7	Eng. In. 0.026	5 <b>7</b> 0	Eng. In. 0.021	43.8	Eng. In 0.015	31.3
0	0.0002	0.043	100	0.038 $0.040$	85.0 85.6	$0.032 \\ 0.034$	70.7	0.028	57.0 58.6	0.021	46.0	0.017	33.9
1	.0002		100	0.040	86.2	0.034	73.0	0.023	60.2	0.025	48.0	0.019	36.4
2	.0002	$0.047 \\ 0.050$	100	0.042	86.7	0.038	74.0	0.033	61.8	0.027	50.0	0.022	38.8
3	.0002	0.050	100	0.046	87.2	0.041	75.0	0.035	63.3	0.030	52.0	0.024	41.2
4		0.002	100	0.040	02	0.011							
	.0002	0.0==	100	0.010	87.7	0.043	76.0	0.038	64.7	0.032	53.8	0.026	43.4
5	.0002	$0.055 \\ 0.057$	100	0.049	88.2	0.043	76.9	0.040	66.0	0.032	55.3	0.029	45.2
6	.0003	0.057	100	0.054	88.6	0.048	77.7	0.043	67.1	0.037	56.8	0.031	47.0
7 8	.0003	0.062	100	0.057	89.0	0.051	78.4	0.045	68.2	0.040	58.2	0.034	48.8
9	.0003	0.065	100	0.059	89.4	0.054	79.1	0.048	69.2	0.043	59.6	0.037	50.5
3		0.000	100	0.000									
	.0003	0.000	100	0.062	89.8	0.057	79.7	0.051	70.1	0.046	61.0	0.040	52.2
10	.0003	0.068	100	0.062	90.1	0.061	80.4	0.054	71.1	0.049	62.3	0.043	53.8
11 12	•0003	0.075	100	0.069	90.4	0.063	81.0	0.058	72.1	0.052	63.5	0.046	55.3
13	.0003	0.078	100	0.072	90.7	0.067	81.6	0.061	73.0	0.056	64.8	0.050	56.8
14	.0004	0.082	100	0.076	91.0	0.071	82.3	0.065	73.9	0.059	65.9	0.054	58.2
	.0004												
15		0.086	100	0.080	91.3	0.074	82.9	0.069	74.8	0.063	67.1	0.057	59.7
16	•0004	0.090	100	0.084	91.6	0.078	83.4	0.073	75.7	0.067	68.2	0.061	61.0
17	.0004	0.094	100	0.088	91.9	0.083	84.0	0.077	76.5	0.071	69.2	0.066	62.3
18	•0004	0.098	100	0.093	92.1	0.087	84.5	0.081	77.2	0.076	70.2	0.070	63.5
19	.0005	0.103	100	0.097	92.4	0.092	85.0	0.086	78.0	0.080	71.2	0.075	64.7
-	.0005												
20	1	0.108	100	0.102	92.6	0.096	85.5	0.091	78.7	0.085	72.1	0.079	65.8
21	.0005	0.113	100	0.107	92.9	0.101	86.0	0.096	79.4	0.090	73.0	0.084	66.9
22	.0005	0.118	100	0.112	93.1	0.107	86.4	0.101	80.0	0.095	73.8	0.089	68.0
23	.0005	0.123	100	0.118	93.3	0.112	86.8	0.106	80.7	0.100	74.6	0.095	68.9
24	.0006	0.129	100	0.123	93.6	0.117	87.2	0.112	81.2	0.106	75.4	0.100	69.9
25	.000	0.135	100	0.129	93.8	0.123	87.6	0.118	81.8	0.112	76.1	0.106	70.7
	.0006												
26		0.141	100	0.135	94.0	0.129	88.0	0.123	82.4	0.117	76.8	0.112	71.6
27	.0006	0.147			94.1		88.3	0.130	82.9	0.124	77.5	0.118	72.5
28	.0006	0.153		0.148	94.3	0.142	88.7	1	83.4		78.2	0.125	73.3
29	.0007	0.160	100	0.154			89.0		83.9		78.8	0.131	74.0
30	.0007	0.167	1				89.3	1	84.3		79.4	0.138	74.8
31	.0007	0.174	100	0.168	94.8	0.162	89.6	0.157	84.8	0.151	80.0	0.145	75.6
		1		1	1		1	1	1	1	1	1	1
		Me	ean Hor	izontal D	ifference	of Force	of Var	or for cac	h 0°.1	= 0.0012.			

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

					-			and Dry I e Bulb co				е.	
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	3°.	0	3°.	.5	40	.0	40	.5	50	.0	5°	.5
fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
0	0.0002	0.010	19.3	0.004	7.9			1					
1	.0002	0.012	22.3	0.006	11.3								
2	.0002	0.014	25.3	0.008	14.7								
3	-0002	0.016	28.1	0.010	17.8								
4		0.018	30.8	0.013	20.9	0.007	11.4						}
	.0002												
5	.0002	0.021	33.4	0.015	23.8	0.010	14.6						
6	.0002	0.023	35.6	0.018	26.3	0.012	17.5	0.006	9.0				
7	.0003	0.026	37.7	0.020	28.8	0.014	20.2	0.009	12.0				
8	.0003	0.028	39.8	0.023	31.2	0.017	22.9	0.011	15.0				
9	.0003	0.031	41.8	0.026	33.5	0.020	25.5	0.014	17.9	0.009	10.6		
	.0003												
10		0.034	43.8	0.029	35.7	0.023	28.0	0.017	20.6	0.012	13.6		
11	.0003	0.037	45.7	0.032	37.9	0.026	30.4	0.020	23.3	0.014	16.4	0.009	9.9
12	.0003	0.041	47.5	0.035	40.0	0.029	32.7	0.024	25.8	0.018	19.2	0.012	12.9
13	.0003	0.044	49.2	0.039	42.0	0.033	35.0	0.027	28.3	0.022	21.9	0.016	15.8
14	.0004	0.048	50.9	0.042	43.9	0.037	37.1	0.031	30.7	0.025	24.5	0.020	18.5
	.0004												
15		0.052	52.5	0.046	45.7	0.040	39.2	0.035	32.9	0.029	26.9	0.023	21.2
16	.0004	0.056	54.1	0.050	47.5	0.044	41.2	0.039	35.1	0.023	29.3	0.027	23.7
17	•0004	0.060	55.6	0.054	49.2	0.049	43.1	0.043	37.2	0.037	31.6	0.032	26.2
18	•0004	0.065	57.0	0.059	50.9	0.053	44.9	0.047	39.2	0.042	33.7	0.036	28.5
19	.0004	0.069	58.4	0.063	52.5	0.058	46.7	0.052	41.2	0.046	35.8	0.040	30.7
	.0005												
20	10000	0.074	59.8	0.068	54.0	0.062	48.3	0.057	43.0	0.050	37.8	0.045	32.9
21	.0005	0.079	61.0	0.073	55.4	0.067	50.0	0.062	44.7	0.056	39.7	0.050	34.9
22	.0005	0.081	62.2	0.078	56.8	0.072	51.5	0.067	46.4	0.061	41.5	0.055	36.8
23	.0005	0.089	63.4	0.083	58.1	0.078	52.9	0.072	48.0	0.066	43.3	0.061	38.6
24	.0006	0.095	64.4	0.089	59.3	0.083	54.3	0.077	49.6	0.072	44.9	0.066	40.5
25	.0006	0.100	65.5	0.095	60.5	0.089	55.6	0.083	51.0	0.078	46.5	0.072	42.2
	.0006												
26		0.106	66.5	0.101	61.7	0.095	56.9	0.089	52.4	0.083	48.0	0.078	43.9
27	.0006	0.106	67.5	0.101	62.8	0.095	58.2	0.089	53.8	0.083	49.6	0.078	45.5
28	•0006	0.113	68.5	0.107	63.9	0.101	59.4	0.102	55.2	0.096	51.0	0.090	47.0
29	.0007	0.119	69.4	0.113	64.9	0.108	60.6	0.102	56.4	0.090	52.4	0.097	48.5
30	<b>-</b> 0007	0.120	70.3	0.120	65.9	0.114	61.7	0.105	57.7	0.103	53.7	0.104	49.9
31	.0007	0.132	71.2	0.127	66.9	0.121	62.8	0.113	58.8	0.109	55.0	0.104	51.2
.,.		31103		0.10.1	00.0	0.120	02.0	0.122	00.0	31110	30.0		01.2

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

												dredths.	
										ermomete ith a Filn			
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	6°.	0	6°.	.5	70.	.0	70.	5	80.	0	80	5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor,	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng In.	
12 13	0.0003	0.007	6.8 9.9										
14	.0004	0.014	12.8	0.008	7.5								
15	.0004	0.018	15.7	0.012	10.4	0.006	5.4						
16	.0004	0.022	18.4	0.016	13.3	0.010	8.4						
	.0004												
17	.0004	0.026	21.0	0.020	16.0	0.015	11.3	0.009	6.7	0.000			
18 19	.0005	$0.030 \\ 0.035$	23.5 25.8	0.025	18.6 21.2	0.019	14.0 16.6	0.013	9.6	0.00S 0.012	5.3 8.2	0.006	4.2
20	.0005	0.035	28.1	0.029	23.5	0.028	19.0	0.015	15.0	0.012	11.0	0.000	7.1
21	.0005	0.040	30.3	0.039	25.8	0.023	21.5	0.022	17.5	0.017	13.5	0.011	9.8
	.0005	0.011	1	0,000		0.000		0.02.	11.0	0.022	10.0	0.010	0.0
22	.0005	0.050	32.3	0.044	28.0	0.038	23.8	0.032	19.8	0.027	16.0	0.021	12.3
23	.0005	0.055	34.2	0.049	30.1	0.043	26.0	0.038	22.1	0.032	18.4	0.026	14.8
24	.0006	0.060	36.1	0.055	32.1	0.049	28.1	0.043	24.4	0.038	20.7	0.032	17.2
25	.0006	0.066	38.0	0.060	34.0	0.055	30.2	0.049	26.5	0.043	23.0	0.038	19.5
26	.0006	0.072	39.8	0.066	35.9	0.061	32.2	0.055	28.6	0.049	25.1	0.043	21.8
27		0.078	41.5	0.073	37.8	0.067	34.0	0.061	30.6	0.055	27.2	0.050	23.9
28	•0006	0.085	43.2	0.079	39.5	0.073	35.9	0.067	32.5	0.062	29.1	0.056	25.9
29	.0007	0.091	44.8	0.085	41.1	0.080	37.6	0.074	34.2	0.068	31.0	0.063	27.9
30	.0007	0.098	46.2	0.092	42.7	0.086	39.2	0.081	35.9	0.075	32.8	0.069	29.7
31	.0007	0.105	47.6	0.099	44.2	0.093	40.8	0.088	37.5	0.082	34.4	0.076	31.4
		90	.0	90	.5	100	0.0	100	.5	110	.0	110	.5
		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
20		0.005	3.4										
21	0.0005	0.010	6.1	0.005	2.7								
22	.0005	0.015	8.8	0.010	5.4	0.004	2.2						
23	.0005	0.021	11.4	0.015	8.0	0.009	4.9						
21	.0006	0.026	13.9	0.020	10.6	0.015	7.5	0.009	4.5				
25		0.032	16.2	0.026	13.1	0.020	10.0	0.015	7.1	0.009	4.2		
26	.0006	0.038	18.5	0.032	15.4	0.026	12.4	0.021	9.5	0.015	6.8	0.009	4.1
27	.0006	0.014	20.7	0.038	17.7	0.032	14.7	0.027	11.9	0.021	9.2	0.015	6.5
28	.0006	0.050	22.8	0.045	19.9	0.039	16.9	0.033	14.2	0.027	11.5	0.022	8.9
29	.0007	0.057	24.9	0.051	21.9	0.045	19.0	0.040	16.3	0.031	13.7	0.028	11.1
30	.0007	0.064	26.7	0.058	23.8	0.052	21.0	0.046	18.4	0.041	15.8	0.035	13.3
31	.0007	0.071	28.5	0.065	25.7	0.059	22.9	0.053	20.3	0.048	17.8	0.042	15.3
		Mea	n Horiz	zontal Di	ference	of Force	of Vap	or for eac	h 0°.1	= 0.0012.			

 ${\bf Temperature, Fahrenheit. -- Force\ of\ Vapor\ in\ English\ Inches. -- Relative\ Humidity\ in\ Hundredths.}$ 

				t - t	t', or Di	fference o	of Wet a	and Dry I	Bulb Th	ermomet	ers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	0°.	0	0°.	5	10	.0	10	.5	20	.0	20	.5
t Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32	0.0007	0.181	100	0.175	91.5	0.168	89.3	0.162	84.1	0.155	79.2	0.149	74.
33	.0008	0.188	100	0.182	94.7	0.175	89.5	0.169	84.5	0.162	79.7	0.156	75.
34	•0008	0.196	100	0.189	94.8	0.183	89.8	0.176	84.9	0.170	80.2	0.163	75.
35	•0008	0.204	100	0.197	94.9	0.191	90.0	0.184	85.3	0.178	80.7	0.171	76.
36	.0009	0.212	100	0.205	95.0	0.199	90.3	0.192	85.6	0.186	81.1	0.179	76.
37		0.220	100	0.214	95.2	0.207	90.5	0.201	86.0	0.194	81.6	0.188	77.
38	•0009	0.229	100	0.223	95.3	0.216	90.7	0.210	86.3	0.203	82.0	0.196	77.
39	.0009	0.238	100	0.232	95.4	0.225	91.0	0.219	86.6	0.212	82.4	0.206	78.
40	.0009	0.248	100	0.241	95.5	0.235	91.2	0.228	86.9	0.221	82.9	0.215	78.
41	•0010	0.257	100	0.251	95.6	0.244	91.4	0.238	87.3	0.231	83.3	0.224	79.
	•0010												
42	.0010	0.267	100	0.260	95.7	0.254	91.6	0.247	87.5	0.241	83.6	0.234	79.
43	.0010	0.278	100	0.271	95.8	0.264	91.8	0.258	87.8	0.251	84.0	0.245	80.
44	.0011	0.288	100	0.282	95.9	0.275	92.0	0.268	88.1	0.262	84.3	0.255	80.
45	.0011	0.299	100	0.293	96.0	0.286	92.1	0.280	88.3	0.273	84.7	0.266	81.
46		0.311	100	0.304	96.1	0.297	92.3	0.291	88.6	0.284	85.0	0.278	81.
	.0012	0.000											
47	.0012	0.323	100	0.316	96.2	0.310	92.5	0.303	88.8	0.297	85.3	0.290	81.9
48	.0013	0.335	100	0.329	96.2	0.322	92.6	0.315	89.0	0.309	85.6	0.302	82.2
49	.0013	0.348	100	0.341	96.3	0.335	92.7	0.328	89.3	0.321	85.9	0.315	82.0
50	.0013		100	0.354	96.4	0.348	92.9	0.341	89.5	0.334	86.1	0.328	82.9
51	.0014	0.374	100	0.368	96.5	0.361	93.0	0.354	89.7	0.348	86.4	0.341	83.5
52	•0014	0.388	100	0.332	96.5	0.375	93.2	0.369	89.9	0.362	86.7	0.355	83.6
53	•0014	0.403	100	0.396	96.6	0.389	93.3	0.383	90.1	0.376	86.9	0.370	83.9
54	•0015	0.418	100	0.411	96.7	0.404	93.4	0.398	90.2	0.391	87.2	0.385	84.2
55	.0015	0.433	100	0.426	96.7	0.420	93.5	0.413	90.4	0.407	87.4	0.400	84.4
56	•0016	0.449	160	0.442	96.8	0.436	93.6	0.429	90.6	0.422	87.6	0.416	84.7
	.0016												
57	0017	0.466	100	0.459	96.8	0.452	93.7	0.446	90.7	0.439	87.8	0.432	85.0
<b>5</b> 8	.0017	0.482	100	0.476	96.9	0.469	93.9	0.463	90.9	0.456	88.0	0.449	85.2
59	.0017	0.500	100	0.493	96.9	0.487	94.0	0.480	91.0	0.473	88.2	0.467	85.5
60	•0018	0.518	100	0.511	97.0	0.505	94.1	0.498	91.2	0.491	88.4	0.485	85.7
61	•10019	0.537	100	0.530	97.0	0.523	94.2	0.517	91.3	0.510	88.6	0.503	85.9
CO	.0019	0.550	100	0.510	0.00	0 5 10	0.4.0	0.500	01.5	0 #20	00.0	0.500	0.0
62	.0020	0.556	100	0.549	97.1	0.542	94.2	0.536	91.5	0.529	88.8	0.522	86.2
63	.0020	0.576	100	0.569	97.1	0.562	94.3	0.556	91.6	0.549	89.0	0.542	86.4
64	.0021	0.596	100	0.589	97.2	0.583	94.4	0.576	91.7	0.569	89.1	0.563	86.6
65 66	•0022	0.639	100 100	0.611	97.2	0.604	94.5	0.597	91.9	0.591	89.3	0.584	86-8
66 67	•0023	0.662	100	0.633	97.3	0.626	94.6	0.619	92.0	0.612	89.5	$0.606 \\ 0.628$	87.0
01		0.002	100	0.000	97.3	0.648	94.7	0.642	92.1	0.635	89.6	0.023	87.2

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

				t - t					Bulb Th	nermomet	ers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	<b>0</b> °.	0	0°.	5	10	0	10	5	2°.	0	2°.	5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Ilumid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.	-00	Eng. In.		Eng. In.		Eng. In.	00.0	Eng. In.	00.0	Eng In.	0~ 0
68	0.0023	0.685	100	0.678	97.3	0.671	94.7	0.665	92.2	0.658	89.8	0.651	87.3
69	.0024	0.708	100	0.702	97.4	0.695	94.8	0.688	92.3	0.682	89.9	0.675	87.5
70	.0025	0.733	100	0.726	97.4	0.720	94.9	0.713	92.4	0.706	90.0	0.699	87.7
71	.0026	0.758	100	0.752	97.5	0.745	95.0	0.738	92.5	0.731	90.2	0.725	87.9 88.0
72	.0027	0.784	100	0.778	97.5	0.771	95.0	0.764	92.7	0.757	90.3	0.751	30.0
73		0.811	100	0.805	97.5	0.798	95.1	0.791	92.7	0.784	90.4	0.778	88.2
74	.0028	0.839	100	0.832	97.6	0.826	95.2	0.819	92.8	0.812	90.6	0.805	88.3
75	.0028	0.868	100	0.861	97.6	0.854	95.2	0.847	92.9	0.841	90.7	0.834	88.5
76	.0029	0.897	100	0.890	97.6	0.883	95.3	0.877	93.0	0.870	90.8	0.863	88.6
77	.0030	0.927	100	0.920	97.7	0.914	95.4	0.907	93.1	0.900	90.9	0.893	88.8
	.0031		100	0.020		0.011							
78	0000	0.958	100	0.951	97.7	0.945	95.4	0.938	93.2	0.931	91.0	0.924	88.9
79	.0032	0.990	100	0.983	97.7	0.977	95.5	0.970	93.3	0.963	91.1	0.956	89.0
80	.0033	1.023	100	1.016	97.7	1.010	95.5	1.003	93.4	0.996	91.2	0.989	89.2
81	.0034	1.057	100	1.050	97.8	1.044	95.6	1.037	93.4	1.030	91.3	1.023	89.3
82	.0035	1.092	100	1.085	97.8	1.079	95.6	1.072	93.5	1.065	91.4	1.058	89.4
	.0036							ł					
83	.0037	1.128	100	1.121	97.8	1.115	95.7	1.108	93.6	1.101	91.5	1.094	89.5
84	.0038	1.165	100	1.158	97.8	1.152	95.7	1.145	93.6	1.138	91.6	1.131	89.6
85	ı	1.203	100	1.196	97.9	1.189	95.8	1.183	93.7	1.176	91.7	1.169	89.7
86	.0039	1.242	100	1.235	97.9	1.228	95.8	1.222	93.8	1.215	91.8	1.208	89.8
87	•0040	1.282	100	1.275	97.9	1.268	95.9	1.263	93.8	1.256	91.9	1.249	90.0
	.0041												
88	.0042	1.323	100	1.317	97.9	1.310	95.9	1.303	93.9	1.296	92.0	1.289	90.1
89	.0044	1.366	100	1.359	97.9	1.352	95.9	1.345	94.0	1.339	92.0	1.332	90.2
90	.0045	1.410	100	1.403	98,0	1.396	96.0	1.389	94.0	1.382	92.1	1.375	90.3
91	.0046	1.455	100	h.448	98.0	1.441	96.0	1.434	94.1	1.427	92.2	1.420	90.3
92	.0040	1.501	100	1.494	98.0	1.487	96.1	1.480	94.1	1.473	92.3	1.466	90.4
00	•0048	1 740	100	1, 7,1	00.0	1 505	96.1	1.528	94.2	1.521	92.4	1.514	90.5
93	.0049	1.548	100	1.541	98.0	1.535	96.1	1.576	94.3	1.569	92.4	1.562	90.6
94	.0050	1.597	100	1.590	98.1	1.583 1.633	96.2	1.626	94.3	1.619	92.5	1.612	90.7
95 96	.0051	1.647 1.698	100	1.640 1.691	98.1	1.684	96.2	1.677	94.4	1.670	92.6	1.664	90.8
[[	.0053	1.751	100	1.744	98.1	1.739	96.2	1.730	94.4	1.723	92.6	1.716	90.9
97 98	.0054	1.805	100	1.798	98.1	1.791	96.3	1.784	94.5	1.777	92.7	1.770	90.9
90	.0056	1.605	100	1.730	30.1	151	00.0	1	0 1.0				
99	*0000	1.861	100	1.854	98.1	1.847	96.3	1.840	94.5	1.833	92.8	1.826	91.0
100	.0057	1.918	100	1.911	98.2	1.904	96.3	1.897	94.6	1.890	92.8	1.883	91.1
101	.0059	1.977	100	1.970	98.2	1.963	96.4	1.956	94.6	1.949	92.9	1.942	91.2
102	.0060	2.037	100	2.030	98.2	2.023	96.4	2.016	94.7	2.009	92.9	2.002	91.2
103	.0062	2.098	100	2.092	98.2	2.085	96.4	2.078	94.7	2.071	93.0	2.064	91.3
104	.0063	2.162	100	2.155	98.2	2.148	96.5	2.141	94.7	2.134	93.1	2.127	91.4
	•		1	<u> </u>	erence	of Force	of Vap	or for eac	h 00.1	= 0.0013.			

 ${\bf Temperature, Fahrenheit. -- Force\ of\ Vapor\ in\ English\ Inches. -- Relative\ Humidity\ in\ Hundredths.}$ 

				t-	t', or D	ifference	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	3°.	.0	3 °.	.5	40.	0	40.	.5	5∘.	.0	50	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Relative Hu-mid-ity.	Force of Vapor.	Relative Hu- mid- ity.						
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32	0.0007	0.142	69.S	0.136	65.3	0.129	61.0	0.123	56.8	0.116	52.7	0.110	48.8
33	.0007	0.149	70.5	0.143	66.1	0.136	61.9	0.130	57.7	0.123	53.7	0.117	50.
34	.0008	0.157	71.2	0.150	66.9	0.144	62.8	0.137	58.6	0.131	54.7	0.124	51.
35	.0008	0.165	71.9	0.158	67.7	0.152	63.6	0.145	59.5	0.139	55.7	0.132	52.
36		0.173	72.6	0.166	68.5	0.160	64.5	0.153	60.5	0.147	56.7	0.140	53.
	.0008												
37	.0009	0.181	73.2	0.175	69.2	0.168	65.3	0.162	61.4	0.155	57.7	0.149	54.
38	.0009	0.190	73.8	0.183	69.9	0.177	66.1	0.170	62.3	0.164	58.7	0.157	55.
39	•0010	0.199	74.4	0.192	70.6	0.186	66.9	0.179	63.2	0.173	59.7	0.166	56.
40	.0010	0.208	75.0	0.202	71.3	0.195	67.7	0.189	64.1	0.182	60.7	0.176	57.
41		0.218	75.6	0.211	72.0	0.205	68.4	0.198	65.0	0.192	61.7	0.185	5S.
	.0010												
42	.0010	0.228	76.2	0.221	72.6	0.215	69.1	0.208	65.7	0.202	62.4	0.195	59.
43	.0011	0.238	76.7	0.232	73.2	0.225	69.8	0.219	66.3	0.212	63.1	0.205	60.
44	.0011	0.249	77.2	0.242	73.7	0.236	70.4	0.229	67.0	0.223	63.S	0.216	61.
45	.0011	0.260	77.7	0.253	74.3	0.247	71.0	0.240	67.6	0.234	64.6	0.227	61.
46	.0011	0.271	78.1	0.265	74.8	0.258	71.6	0.252	68.3	0.245	65.3	0.238	62.
	.0012												
47	.0012	0.283	78.6	0.277	75.3	0.270	72.2	0.264	68.9	0.257	66.0	0.250	63.
48	.0013	0.296	79.0	0.289	75.8	0.282	72.7	0.276	69.6	0.269	66.7	0.263	64.0
49	•0013	0.308	79.4	0.302	76.3	0.295	73.3	0.288	70.2	0.282	67.4	0.275	64.
50	.0013	0.321	79.8	0.315	76.7	0.308	73.8	0.301	70.9	0.295	68.1	0.288	65.
51	.0013	0.335	80.2	0.328	77.2	0.321	74.3	0.315	71.4	0.308	68.7	0.302	66.0
ı	-0014												
52	.0014	0.349	80.5	0.342	77.6	0.335	74.7	0.329	71.9	0.322	69.2	0.315	66.6
53	.0014	0.363	80.9	0.356	78.0	0.350	75.2	0.343	72.5	0.336	69.8	0.330	67.2
54	.0015	0.378	81.2	0.371	78.4	0.365	75.6	0.358	72.9	0.351	70.3	0.345	67.8
55		0.393	81.6	0.387	78.8	0.380	76.1	0.373	73.4	0.367	70.8	0.360	68.3
56	.0016	0.409	81.9	0.403	79.1	0.396	76.5	0.389	73.9	0.383	71.3	0.376	68.9
į	.0016												
57	.0017	0.426	S2.2	0.419	79.5	0.412	76.9	0.406	74.3	0.399	71.8	0.392	69.
58	.0017	0.443	82.5	0.436	79.8	0.429	77.2	0.423	74.8	0.416	72.3	0.409	69.9
59	.0017	0.460	82.8	0.453	80.2	0.447	77.6	0.440	75.1	0.433	72.7	0.427	70.
60	.0019	0.478	83.1	0.471	80.5	0.465	78.0	0.458	75.5	0.451	73.1	0.445	70.8
61	•0019	0.497	83.3	0.490	80.8	0.483	78.3	0.477	75.9	0.470	73.5	0.463	71.3
00	-0019	0										0 (00	
62	.0020	0.516	83.6	0.509	81.1	0.502	78.6	0.496	76.3	0.489	74.0	0.482	71.
63	.0020	0.536	83.8	0.529	81.4	0.522	79.0	0.516	76.6	0.509	74.3	0.502	72.
64	.0021	0.556	84.1	0.549	81.7	0.543	79.3	0.536	77.0	0.529	74.7	0.523	72.
65		0.577	84.3	0.570	81.9	0.564	79.6	0.557	77.3	0.550	75.1	0.544	72.
66	.0022	0.599	84.6	0.592	82.2	0.586	79.9	0.579	77.6	0.572	75.4	0.566	73.3
67	.0023	0.622	84.8	0.615	82.4	0.608	80.2	0.601	78.0	0.595	75.8	0.588	73.
							,						

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-t	', or Di	fference o	of Wet	and Dry	Bulb Tt	ermomet	ers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	30,	.0	3 °	.5	40.	0	40.	5	<b>5</b> °.	0	50	.5
Fahren- heit	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0		Eng. In.	27.0	Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
68	0.0024	0.644	85.0	0.638	82.7	0.631	80.4	0.624	78.3	0.618	76.1	0.611	74.0
69	.0024	0.668	85.2	0.661	82.9	0.655	80.7	$0.648 \\ 0.672$	78.6	0.641	76.4	0.635	74.
70 71	.0025	0.693	85.4 85.6	0.686 $0.711$	83.2 83.4	$0.679 \\ 0.704$	81.0 81.2	0.672	78.8 79.1	$0.666 \\ 0.691$	76.8 77.1	0.659 0.684	74.3
72	.0026	0.718 $0.744$	85.8	0.711	83.6	0.704	81.5	0.038	79.4	0.718	77.4	0.034	75.4
12	.0027	0.744	00.0	0.757	00.0	0.791	01.0	0.724	13.4	0.715	44.2	0.710	10.4
73		0.771	86.0	0.764	83.8	0.757	81.7	0.751	79.7	0.744	77.6	0.737	75.7
71	.0028	0.799	86.2	0.792	84.0	0.785	81.9	0.778	79.9	0.772	77.9	0.765	76.0
75	.0028	0.827	86.3	0.820	84.2	0.814	82.2	0.807	80.2	0.800	78.2	0.793	76.3
76	.0029	0.856	86.5	0.850	84.4	0.843	82.4	0.836	80.4	0.829	78.4	0.823	76.6
77	•0030	0.887	86.7	0.880	84.6	0.873	82.6	0.866	80.6	0.860	78.7	0.853	76.8
	.0031												
78	.0032	0.918	86.8	0.911	84.8	0.904	82.8	0.897	80.8	0.890	78.9	0.884	77.
79	.0033	0.949	87.0	0.943	85.0	0.936	83.0	0.929	81.1	0.922	79.2	0.916	77.
80	.0034	0.982	87.1	0.976	85.1	0.969	83.2	0.962	81.3	0.955	79.4	0.949	77.0
81	•0035	1.016	87.3	1.010	85.3	1.003	83.4	0.996	81.5	0.989	79.7	0.982	77.9
82		1.051	87.4	1.045	85.5	1.038	83.6	1.031	81.7	1.024	79.9	1.017	78.1
83	•0036	1.087	87.5	1.080	85.6	1.074	83.7	1.067	81.9	1.060	80.1	1.053	78.3
84	.0037	1.124	87.7	1.117	85.8	1.111	83.9	1.104	82.1	1.096	80.3	1.090	78.5
85	•0038	1.162	87.8	1.155	85.9	1.148	84.1	1.142	82.3	1.135	80.5	1.128	78.8
86	.0039	1.201	87.9	1.194	86.1	1.187	84.2	1.181	82.4	1.174	80.7	1.167	79.0
87	•0010	1.242	88.1	1.235	86.2	1.228	84.4	1.222	82.6	1.215	80.9	1.208	79.2
	.0041	1.512	00.1	11200	00,2	11220			02.0	1.210	00.0	11200	
88		1.282	88.2	1.276	86.3	1.269	84.6	1.262	82.8	1.255	81.1	1.248	79
89	-0042	1.325	88.3	1.318	86.5	1.311	84.7	1.304	83.0	1.297	81.3	1.291	79.6
90	.0044	1.369	88.4	1.362	86.6	1.355	84.9	1.348	83.1	1.341	81.4	1.334	79.8
91	.0045	1.413	88.5	1.407	86.7	1.400	85.0	1.393	83.3	1.386	81.6	1.379	80.0
92	.0046	1.460	88.6	1.453	86.9	1.446	85.1	1.439	83.4	1.432	81.8	1.425	80.2
	.0047		00 -	1 -00	2~ 0	1 400	05.0	1 400	00.0	100	00.0		00.6
93	.0049	1.507	88.7	1.500	87.0	1.493	85.3	1.486	83.6	1.480	82.0	1.473	80.
94	.0050	1.556	88.8	1.549	87.1	$1.542 \\ 1.592$	85.4	1.535	83.8	1.528	82.1		80.
95	.0051	1.606	88.9	1.599	87.2	1.643	85.5 85.7	1.585 1.636	83.9	1.578 1.629	82.3 82.4	$1.571 \\ 1.622$	80.9
96	.0052	1.657	89.0	1.650 $1.702$	87.3	1.696	85.S	1.688	84.0	1.682	82.6	1.675	81.0
97 98	.0054	1.709	89.2	1.757	87.5 87.6	1.750	85.9	1.743	84.2 84.3	1.736	S2.7	1.729	81.2
33	.0055	1.104	00.2	11101	01.0	11.00	00.0	11,40	04.0	1.100	- w.1	11.20	01.2
99		1.819	89.3	1.812	87.7	1.805	86.0	1.798	84.4	1.792	82.9	1.785	81.8
100	.0057	1.876	89.4	1.869	87.8	1.863	86.2	1.856	84.6	1.849	83.0	1.842	81.8
101	.0058	1.935	89.5	1.928	87.9	1.921	86.3	1.914	84.7	1.907	83.2	1.900	81.6
102	.0060	1.995	89.6	1.988	88.0	1.981	86.4	1.974	84.8	1.967	83.3	1.961	81.8
103	.0062	2.057	89.7	2.050	88.1	2.043	86.5	2.036	84.9	2.029	83.4	2.022	81.9
104	.0063	2.120	89.8	2.113	88.2	2.106	86.6	2.099	85.1	2.092	83.5	2.085	82.

Mean Horizontal Difference of Force of Vapor for each  $0^{\circ}.1 = 0.0013$ .

Temperature, Fahrenheit — Force of Vapor in English Inches. — Relative Humidity in Hundredths

W	V			t-1	t', or Di	ifference (	of Wet	and Dry	Bulb Tl	ermome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	<b>6</b> °.	0	6°.	5	70	.0	70	.5	80	.0	80	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- nid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32	0.0007	0.103	45.0	0.097	41.4	0.090	37.9	0.084	34.5	0.077	31.2	0.071	28.0
33	.0007	0.110	46.3	0.104	42.7	0.097	39.3	0.091	36.0	0.084	32.8	0.078	29.6
34 35	•0008	0.118	47.6	0.111	44.1	0.105	40.7	0.098	37.4	0.092	34.3	0.085	31.2
36	.0008	$0.126 \\ 0.134$	48.8	0.119	45.3	0.113	42.0	0.106	38.8	0.100	35.7	0.093	32.8
	.0009	0.154	50.0	0.127	46.6	0.121	43.3	0.114	40.2	0.108	37.2	0.101	34.3
37		0.142	51.1	0.136	47.8	0.129	44.6	0.123	41.6	0.116	38.6	0.109	35.7
38	.0009 .0009	0.151	52.2	0.144	49.0	0.138	45.9	0.131	42.9	0.125	40.0	0.118	37.2
39	.0009	0.160	53.3	0.153	50.1	0.147	47.1	0.140	44.1	0.134	41.3	0.127	38.5
40	.0009	0.169	54.3	0.163	51.3	0.156	48.3	0.149	45.4	0.143	42.6	0.136	39.9
41		0.179	55.4	0.172	52.3	0.166	49.4	0.159	46.6	0.153	43.9	0.146	41.2
42	.0010	0.189	56.3	0.182	53.4	0.175	50.5	0.169	47.7	0.162	45.0	0.156	42.4
43	.0010	0.199	57.2	0.192	54.3	0.175	51.5	0.179	48.8	0.102	46.1	0.166	43.6
44	.0011	0.209	58.1	0.203	55.3	0.196	52.5	0.190	49.8	0.183	47.2	0.177	44.7
45	.0011	0.220	59.0	0.214	56.2	0.207	53.5	0.201	50.8	0.194	48.3	0.188	45.8
46	•0011	0.232	59.8	0.225	57.0	0.219	54.4	0.212	51.8	0.206	49.3	0.198	46.9
	.0012												
47	.0012	0.244	60.6	0.237	57.9	0.231	55.2	0.224	52.7	0.217	50.2	0.211	47.9
48	.0013	0.256	61.3	0.249	58.7	0.243	56.1	0.236	53.6	0.230	51.2	0.223	48.8
49	.0013	0.269	62.0	0.262	59.4	0.255	56.9	0.249	54.5	0.242	52.1	0.236	49.7
50 51	.0013	0.282	62.7	0.275	60.2	0.268	57.7	0.262	55.3	0.255	52.9	0.249	50.6
91		0.295	63.4	0.288	60.9	0.282	58.4	0.275	56.1	0.269	53.7	0.262	51.5
52	.0014	0.309	64.1	0.302	61.6	0.296	59.2	0.289	56.8	0.282	54.6	0.276	52.3
53	.0014	0.323	64.7	0.317	62.3	0.310	59.9	0.303	57.6	0.297	55.3	0.290	53.2
54	•0015	0.338	65.3	0.332	62.9	0.325	60.6	0.318	58.3	0.312	56.1	0.305	53.9
55	.0015	0.354	65.9	0.347	63.5	0.340	61.2	0.334	59.0	0.327	56.8	0.320	54.9
56	.0016	0.369	66.5	0.363	64.1	0.356	61.9	0.349	59.7	0.343	57.5	0.336	55.4
5 74	-0017	0.000	0= 0	0.0~0	0.1-	0.000	60.5	0.200	00.0	0.050	50.0	0.950	EC 1
57 58	.0017	0.386	67.0	0.379 0.396	64.7	0.373	62.5 63.1	0.366	60.3	0.359	58.2	0.353	56.1 56.8
59	•0017	0.420	67.5 68.0	0.396	65.3 65.8	0.389	63.6	0.383	60.9 61.5	0.376	58.8 59.5	0.369 0.387	57.5
60	.0018	0.420	68.5	0.431	66.3	0.425	64.2	0.418	62.1	0.333	60.1	0.405	58.1
61	.0018	0.457	69.0	0.450	66.9	0.443	64.7	0.436	62.7	0.430	60.7	0.423	58.7
	.0019		30.0		30.0	.,,,,	,		J		,,,,		
62		0.476	69.5	0.469	67.4	0.462	65.3	0.456	63.2	0.449	61.3	0.442	59.3
63	.0020	0.495	70.0	0.489	67.8	0.482	65.8	0.475	63.8	0.469	61.8	0.462	59.9
64	.0021	0.516	70.4	0.509	68.3	0.503	66.3	0.496	64.3	0.489	62.4	0.483	60.5
65	.0021 .0022	0.537	70.8	0.530	68.8	0.524	66.8	0.517	64.8	0.510	62.9	0.504	61.0
66 67	.0022	0.559	71.2	0.552	69.2	0.545	67.2	0.539	65.3	0.532	63.4	0.525	61.6
07		0.581	71.6	0.575	69.6	0.568	67.7	0.561	65.7	0.554	63.9	0.549	62.1
		Me	an Hor	izontal Di	fference	of Force	of Vap	or for eac	h 0°.1 =	= 0.0013.			

Temperature, Fahrenheit. - Force of Vapor in English Inches - Relative Humidity in Hundredths.

Wet-	Mean			t-t	, or Di	ference o	f Wet a	nd Dry I	Bulb Th	ermomet	ers.		
Bulb	Vertical Difference of Force of Vapor	6°.	.0	60	.5	70.	.0	70	.5	80	.0	80	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative IIu- mid- ity.
0		Eng. In.	~~ ^	Eng. In.	-0.0	Eng. In.	20.1	Eng. In.	00.0	Eng. In.	CAA	Eng In.	CD C
68	0.0024	0.604	72.0	0.597	70.0	0.591	68.1 68.5	0.584	66.2	0.577	64.4 64.8	0.571	62.6
69 70	.0024	$0.628 \\ 0.652$	72.4 72.7	0.621	70.4	$0.614 \\ 0.639$	68.9	$0.608 \\ 0.632$	66.6 67.1	$0.601 \\ 0.625$	65.3	$0.594 \\ 0.619$	63.5
71	.0025	0.678	73.1	0.646	71.2	0.664	69.3	0.657	67.5	0.651	65.7	0.644	64.0
72	.0026	0.704	73.4	0.697	71.5	0.690	69.7	0.683	67.9	0.677	66.1	0.670	64.4
14	.0027	0.104	10.4	0.057	11.0	0.050	00.1	0.000	01.0	0.0	00.1	0.0.0	0 21 1
73	.0028	0.730	73.8	0.724	71.9	0.717	70.1	0.710	68.3	0.703	66.5	0.697	64.8
74	.0025	0.758	74.1	0.751	72.2	0.745	70.4	0.738	68.7	0.731	66.9	0.724	65.3
75	.0029	0.787	74.4	0.780	72.6	0.773	70.8	0.766	69.0	0.760	67.3	0.753	65.7
76	.0030	0.816	74.7	0.809	72.9	0.802	71.1	0.796	69.4	0.789	67.7	0.782	66.1
77		0.846	75.0	0.839	73.2	0.832	71.4	0.826	69.7	0.819	68.1	0.812	66.4
	.0031												
78	.0032	0.877	75.3	0.870	73.5	0.863	71.8	0.857	70.1	0.850	68.4	0.843	66.8
79	.0033	0.909	75.6	0.902	73.8	0.895	72.1	0.888	70.4	0.882	68.8	0.875	67.2
80	.0034	0.942	75.8	0.935	74.1	0.928	72.4	0.921	70.7	0.915	69.1	0.908	67.5
81	.0035	0.976	76.1	0.969	74.4	0.962	72.7	0.955	71.0	0.948	69.4	0.942	67.9
82	.0036	1.011	76.4	1.004	74.6	0.997	73.0	0.990	71.3	0.983	69.8	0.977	68.2
83		1.046	76.6	1.040	74.9	1.033	73.3	1.026	71.6	1.019	70.1	1.012	68.5
84	.0037	1.083	76.8	1.077	75.2	1.070	73.5	1.063	71.9	1.056	70.4	1.049	68.8
85	.0038	1.121	77.1	1.114	75.4	1.108	73.8	1.101	72.2	1.094	70.7	1.087	69.1
86	.0038	1.160	77.3	1.153	75.7	1.147	74.1	1.140	72.5	1.133	70.9	1.126	69.4
87	.0639	1.201	77.5	1.194	75.9	1.187	74.3	1.181	72.7	1.174	71.2	1.167	69.7
	.0040												
88	.0042	1.241	77.7	1.235	76.1	1.228	74.6	1.221	73.0	1.214	71.5	1.207	70.0
89	.0042	1.284	78.0	1.277	76.4	1.270	74.8	1.263	73.3	1.256	71.8	1.250	70.3
90	.0044	1.327	78.2	1.321	76.6	1.314	75.0	1.307	73.5	1.300	72.0	1.293	70.6
91	.0046	1.372	78.4	1.365	76.8	1.359	75.3	1.352	73.7	1.345	72.3	1.338	70.8
92	- 1	1.418	78.6	1.412	77.0	1.405	75.5	1.398	74.0	1.391	72.5	1.384	71.1
0.0	.0047	1 400	~0.0	7 450	0	, ,,,			~	1 490	#0 C	7 407	*1.0
93	.0049	1.466	78.8	1.459	77.2	1.452	75.7	1.445	74.2	1.438	72.8	1.431	71.3
94 95	.0050	1.514 1.564	79.0	1.507	77.4	1.501 1.550	75.9	1.494 1.544	74.4	1.487 1.537	73.0 73.2	1.480 1.530	71.6 71.8
96	.0051	1.615	79.1	1.557	77.6	1.602	76.1 76.3	1.595	74.7 74.9	1.588	73.4	1.581	72.1
97	.0052	1.668	79.3 79.5	1.608	77.8 78.0	1.654	76.5	1.647	75.1	1.640	73.7	1.633	72.1
98	.0054	1.722	79.7	1.715	78.2	1.708	76.7	1.701	75.3	1.694	73.9	1.688	72.5
00	.0056	1.722	13.1	1.719	10.2	1.,05	10.1	1.701	10.0	1.054	,0,0	1.000	
99		1.778	79.8	1.771	78.4	1.764	76.9	1.757	75.5	1.750	74.1	1.743	72.7
100	.0057	1.835	80.0	1.828	78.5	1.821	77.1	1.814	75.7	1.807	74.3	1.800	72.9
101	.0059	1.893	80.2	1.887	78.7	1.880	77.3	1.873	75.9	1.866	74.5	1.859	73.2
102	•0060	1.954	80.3	1.947	78.9	1.940	77.4	1.933	76.1	1.926	74.7	1.919	73.4
103	•0061	2.015	80.5	2.008	79.0	2.001	77.6	1.994	76.2	1.987	74.9	1.980	73.6
104	•0063	2.078	80.6	2.071	79.2	2.064	77.8	2.057	76.4	2.051	75.1	2.044	73.8

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

meter t	Mean Vertical Difference of Force of Vapor for each 0°.1.	9°.	0					$\mathbf{t-t'},$ or Difference of Wet and Dry Bulb Thermometers.												
Fahren- heit.	for each			90	9°.5		100.0		10°.5		110.0		11°.5							
32		Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity,	Force of Vapor.	Relative Hu- mid- ity.							
		Eng. In.		Eng. In		Eng. In.		Eng. In.		Eng. In.		Eng. In								
29	0 0007	0.064	25.0	0.058	22.0	0.051	19.2	0.045	16.4	0.038	13.8	0.032	11.5							
	.0007	0.071	26.7	0.065	23.8	0.058	21.0	0.052	18.3	0.045	15.7	0.039	13.5							
34	•0008	0.079	28.3	0.072	25.5	0.066	22.7	0.059	20.1	0.053	17.5	0.046	15.							
35	.0008	0.087	29.9	0.080	27.1	0.074	24.4	0.067	21.8	0.061	19.3	$0.054 \\ 0.062$	16.							
36	.0008	0.095	31.4	0.088	40.1	0.082	26.0	0.075	23.5	0.069	21.1	0.002	18.							
37		0.103	33.0	0.096	30.3	0.090	27.6	0.083	25.2	0.077	22.8	0.070	20.							
38	.0009	0.112	34.4	0.105	31.8	0.099	29.2	0.092	26.8	0.086	24.4	0.079	22.							
39	.0009	0.121	35.9	0.114	33.3	0.108	30.7	0.101	28.4	0.094	26.1	0.088	23.8							
40	.0009	0.130	37.3	0.123	34.8	0.117	32.2	0.110	29.9	0.104	27.6	0.097	25.4							
41	.0010	0.139	38.6	0.133	36.2	0.126	33.7	0.120	31.4	0.113	29.2	0.107	27.0							
	.0010																			
42	.0010	0.149	39.9	0.143	37.5	0.136	35.0	0.130	32.8	0.123	30.6	0.116	28.4							
43	•0010	0.160	41.1	0.153	38.7	0.146	36.3	0.140	34.1	0.133	32.0	0.127	29.8							
44	.0011	0.170	42.3	0.163	39.9	0.157	37.6	0.150	35.4	0.144	33.3	0.137	31.5							
45	.0011	0.181	43.4	0.175	41.1	0.168	38.8	0.161	36.7	0.155	34.6	0.148	32.							
46		0.192	44.5	0.186	42.2	0.179	39.9	0.173	37.9	0.166	35.8	0.160	33.8							
47	.0012	0.204	45.5	0.198	43.3	0.191	41.1	0.185	39.0	0.178	37.0	0.171	35.0							
48	.0012	0.217	46.5	0.133	44.3	0.191	42.1	0.197	40.1	0.190	38.1	0.184	36.							
49	.0012	0.217	47.5	0.222	45.3	0.203	43.2	0.209	41.2	0.203	39.2	0.196	37.5							
50	.0013	0.242	48.4	0.235	46.3	0.210	44.2	0.222	42.2	0.216	40.2	0.209	38.3							
51	.0013	0.255	49.3	0.249	47.2	0.242	45.2	0.236	43.2	0.229	41.2	0.222	39.							
"	.0014	0.200	10.0	0.240	41.2	0.242	40.4	0.200	10.2	0.220	11.2									
52		0.269	50.2	0.263	48.1	0.256	46.1	0.249	44.1	0.243	42.2	0.236	40.5							
53	.0015	0.284	51.1	0.277	49.0	0.270	47.0	0.264	45.1	0.257	43.2	0.250	41.3							
54	.0015	0.298	51.9	0.292	49.8	0.285	47.9	0.279	46.0	0.272	44.1	0.265	42.3							
55	.0015	0.314	52.7	0.307	50.7	0.300	48.7	0.294	46.8	0.287	45.0	0.281	43.2							
56	.0016	0.330	53.5	0.323	51.4	0.316	49.5	0.310	47.7	0.303	45.9	0.296	44.							
	.0016			0.000				0.000	40 =	0.010		0.010								
57	.0017	0.346	54.3	0.339	52.2	0.333	50.3	0.326	48.5	0.319	46.7	0.313	44.9							
58	.0017	0.363	55.0	0.356	52.9	0.350	51.1	0.343	49.2	0.336	47.5	0.330	45.7							
59	.0018	0.380	55.7	0.373	53.6	0.367	51.8	0.360	50.0	0.354	48.2	0.347	46.5							
60	.0018	0.398	56.4	0.391	54.3	0.385	52.5	0.378	50.7 51.4	0.371	49.0	0.365 0.383	47.8							
61	.0019	0.416	57.0	0.410	55.0	0.403	53.2	0.396	31.4	0.390	49.7	0.000	48.1							
62		0.436	57.6	0.429	55.6	0.422	53.9	0.416	52.1	0.409	50.4	0.402	48.8							
63	•0020	0.455	58.2	0.449	56.3	0.442	54.5	0.435	52.8	0.429	51.1	0.422	49.3							
64	.0021	0.476	58.8	0.469	56.9	0.462	55.1	0.456	53.4	0.449	51.8	0.442	50.2							
65	.0021	0.497	59.3	0.490	57.5	0.483	55.8	0.477	54.1	0.470	52.4	0.463	50.8							
66	.0022	0.519	59.9	0.512	58.0	0.505	56.3	0.498	54.7	0.492	53.1	0.485	51.							
67	.0023	0.542	60.3	0.534	58.6	0.527	56.9	0.521	55.3	0.514	53.7	0.507	52.1							

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

		${f t-t'},$ or Difference of Wet and Dry Bulb Thermometers.												
Wet-Bulb Vertical Thermo-Difference meter of Force  tf of Vapor		9°.0		9°.5		100.0		10°.5		11°.0		11°.5		
Fahren- for each heit. 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Rela- tive IIu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.		
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		
68	0.0024	0.564	60.8	0.557	59.1	0.550	57.4	0.544	55.8	0.537	54.2	0.530	52.7	
69	.0025	0.588	61.3	0.581	59.6	0.574	58.0	0.567	56.4	0.561	54.8	0.554	53.3	
70	.0025	0.612	61.8	0.605	60.1	0.598	58.5	0.592	56.9	0.585	55.4	0.578	53.8	
71	.0026	0.637	62.3	0.630	60.6	0.624	59.0	0.617	57.4	0.610	55.9	0.603	54.4	
72	00.35	0.663	62.7	0.656	61.1	0.650	59.5	0.643	58.0	0.636	56.4	0.629	54.9	
73	.0027	0.390	63.2	0.683	61.6	0.677	60.0	0.670	58.4	0.663	56.9	0.656	55.5	
74	.0027	0.390	63.6	0.003	62.0	0.701	60.5	0.697	58.9	0.691	57.4	0.684	56.0	
75	.0028	0.716	64.0	0.711	62.5	0.733	60.9	0.037	59.4	0.031	57.9	0.712	56.5	
76	.0029	0.740	64.4	0.769	62.9	0.762	61.3	0.755	59.8	0.748	58.4	0.741	56.9	
77	•0030	0.805	64.8	0.799	63.3	0.792	61.8	0.785	60.3	0.778	58.8	0.772	57.4	
" "	.0031	0.000	0410	0.755	00.0	0.152	01.0	0.100	0010	0.770	00.0	0.7.2	0	
78		0.836	65.2	0.829	63.7	0.823	62.2	0.816	60.7	0.809	59.2	0.802	57.8	
79	.0032	0.868	65.6	0.861	64.1	0.855	62.6	0.848	61.1	0.841	59.7	0.834	58.3	
80	•0033	0.901	66.0	0.894	64.5	0.897	63.0	0.881	61.5	0.874	60.1	0.867	58.7	
81	.0034	0.935	66.3	0.928	64.8	0.921	63.4	0.914	61.9	0.908	60.5	0.901	59.1	
82	•0035	0.970	66.7	0.963	65.2	0.956	63.7	0.949	62.3	0.943	60.9	0.936	59.5	
	.0036													
83		1.006	67.0	0.999	65.5	0.992	64.1	0.985	62.7	0.978	61.3	0.972	59.9	
84	.0037	1.042	67.3	1.036	65.9	1.029	64.4	1.022	63.0	1.015	61.7	1.008	60.3	
85	.0038	1.080	67.7	1.073	66.2	1.067	64.8	1.060	63.4	1.053	62.0	1.046	60.7	
86	.0039	1.119	68.0	1.112	66.5	1.106	65.1	1.099	63.7	1.092	62.4	1.085	61.0	
87	•0040	1.160	68.3	1.153	66.8	1.146	65.4	1.140	64.1	1.133	62.7	1.126	61.4	
	.0041													
88	.0042	1.200	68.6	1.194	67.1	1.187	65.8	1.180	64.4	1.173	63.1	1.166	61.7	
89	.0042	1.243	68.9	1.236	67.4	1.229	66.1	1.222	64.7	1.215	63.4	1.208	62.1	
90	.0045	1.286	69.1	1.279	67.7	1.273	66.4	1.266	65.0	1.259	63.7	1.252	62.4	
91	.0046	1.331	69.4	1.324	68.0	1.317	66.7	1.311	65.3	1.304	64.0	1.297	62.7	
92	*0040	1.377	69.7	1.370	68.3	1.363	67.0	1.357	65.6	1.350	64.3	1.343	63.1	
00	.0047	0.	CO 0		20.0		0=0		2= 0		0,0		CO. 4	
93	.0048	1.425	69.9	1.418	68.6	1.411	67.2	1.404	65.9	1.397	64.6	1.390	63.4	
94	.0050	1.473	70.2	1.466	68.8	1.459	67.5	1.452	66.2	1.446	64.9	1.439	63.7	
95	.0051	1.523	70.4	1.516	69.1	1.509	67.8	1.502	66.5	1.495	65.2	1.488	64.0	
96	.0053	1.574	70.7	1.567	69.4	1.560	68.0	1.553	66.7	1.546	65.5	1.539	64.2	
97	.0054	1.627	70.9	1.620	69.6	1.613	68.3	1.606	67.0	1.599	65.8	1.592	64.5	
98		1.681	71.2	1.674	69.8	1.667	68.5	1.660	67.3	1.653	66.0	1.646	64.8	
99	.0056	1.736	71.4	1.729	70.1	1.722	68.8	1.716	67.5	1.709	66.3	1.702	65.1	
100	.0057	1.793	71.6	1.786	70.3	1.780	69.0	1.773	67.8	1.766	66.5	1.759	65.3	
101	.0058	1.852	71.8	1.845	70.5	1.838	69.3	1.831	68.0	1.824	66.8	1.817	65.6	
102	.0060	1.912	72.0	1.905	70.8	1.898	69.5	1.891	68.2	1.884	67.0	1.877	65.8	
102	.0062	1.974	72.3	1.967	71.0	1.960	69.7	1.953	68.5	1.946	67.3	1.939	66.1	
103	.0063	2.037	1	2.030	71.0	2.023	69.9	2.016	68.7	2.009	67.5	2.002	66.3	
104		2.007	12.0	12.050	11.2	12.025	00.0	12.010	1 00.7	2.009	07.0	2.002	00.0	

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

meter t	Mean Vertical Difference of Force of Vapor for each 0°.1.	12 Force of Vapor.	Rela-	12	°.5	Ī .		1		1		1	
o 32 33 34 35	of Vapor for each 0°.1.				·.5   13·.0			13°.5		140.0		14°.5	
32 33 34 35		rupoti	tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
33 34 35		Eng. In.		Eng. ln.		Eng. ln.		Eng. In.		Eng. In.		Eng. 1n.	
34 35	0.0007	0.025	8.8	0.019	6.4	0.012	4.1	0.010		1		1	
35	.0007	0.032	10.8	0.026	8.4	0.019	6.2	0.013	4.0	0.014	4.		
- 1	.0007	0.040	12.7 14.6	0.033	10.4	0.027 $0.034$	8.2	0.020	6.0 8.0	0.014	6.1	0.015	4.
	.0008	0.056	16.4	0.041	14.2	0.034	12.0	0.028	10.0	0.021	8.1	0.013	6.
	.0008	0.000	10.4	0.043	14.2	0.042	12.0	0.0.0	10.0	0.029	0.1	0.025	0.
37		0.064	18.2	0.057	16.0	0.051	13.9	0.044	11.9	0.038	10.0	0.031	8.
38	•0009	0.072	19.9	0.066	17.8	0.059	15.7	0.053	13.7	0.046	11.9	0.040	10.
39	.0009	0.081	21.6	0.075	19.5	0.068	17.5	0.062	15.5	0.055	13.7	0.049	11.
40		0.091	23.3	0.084	21.2	0.078	19.2	0.071	17.2	0.064	15.4	0.058	13.
41	•0010	0.100	24.9	0.094	22.8	0.087	20.8	0.081	18.9	0.074	17.1	0.067	15.
	•0010				2.5								
42	.0010	0.110	26.4	0.103	24.3	0.097	22.4	0.090	20.5	0.084	18.6	0.077	16.
43	•0011	0.120	27.8	0.114	25.8	0.107	23.9	0.100	22.0	0.095	20.1	0.087	18.
44	.0011	0.131	29.2	0.124	27.2	0.118	25.3	0.111	23.5	0.104	21.5	0.098	19.
45	.0011	0.142	30.5	0.135	28.6	0.129	26.7	0.122	24.9	0.115	22.9	0.109	21.
46	0010	0.153	31.8	0.146	30.0	0.140	28.1	0.133	26.3	0.127	24.3	0.119	22.
47	.0012	0.165	33.0	0.158	31.2	0.152	29.3	0.145	27.6	0.138	25 7	0.132	24.0
48	.0012	0.177	34.2	0.170	32.4	0.164	30.6	0.157	28.8	0.151	27.0	0.144	25.
49	.0013	0.190	35.3	0.183	33.5	0.176	31.7	0.170	30.0	0.163	28.3	0.157	26.
50	.0013	0.202	36.4	0.196	34.6	0.189	32.9	0.183	31.2	0.176	29.5	0.169	27.9
51	•0014	0.216	37.5	0.209	35.7	0.202	34.0	0.196	32.3	0.189	30.7	0.183	29.
1	.0014												
52		0.229	38.5	0.223	36.8	0.216	35.1	0.210	33.4	0.203	31.8	0.196	30.5
53	.0014	0.244	39.5	0.237	37.8	0.231	36.1	0.224	34.5	0.217	32.9	0.211	31.
54	.0015	0.259	40.5	0.252	38.8	0.245	37.1	0.239	35.5	0.232	34.0	0.226	32.
55	.0015	0.274	41.5	0.267	39.8	0.261	38.1	0.254	36.5	0.247	35.0	0.241	33.
56	- 1	0.290	42.4	0.283	40.7	0.276	39.1	0.270	37.5	0.263	35.9	0.257	34.
57	.0016	0.306	43.2	0.299	41.6	0.293	40.0	0.286	38.4	0.280	36.9	0.273	35.4
58	.0017	0.323	44.1	0.299	42.4	0.293	40.8	0.303	39.3	0.296	37.8	0.273	36.3
59	.0017	0.340	44.9	0.334	43.3	0.310	41.7	0.320	40.1	0.290	38.7	0.307	37.2
60	•0018	0.358	45.7	0.351	44.1	0.345	42.5	0.338	41.0	0.331	39.5	0.325	38.
61	.0018	0.376	46.4	0.370	14.9	0.363	43.3	0.356	41.8	0.350	40.3	0.343	38.9
	.0019			,,,,,		,,,,,,				,,,,,,			
62		0.396	47.2	0.389	45.6	0.382	44.1	0.376	42.6	0.369	41.2	0.362	39.8
63	.0020	0.415	47.9	0.409	46.4	0.402	44.8	0.395	43.4	0.389	41.9	0.382	40.6
64	.0021	0.436	48.6	0.429	47.1	0.422	45.6	0.416	44.1	0.409	42.7	0.402	41.8
65	.0021	0.457	49.3	0.450	47.8	0.443	46.3	0.437	44.8	0.431	43.4	0.423	42.1
66	.0022	0.478	49.9	0.472	48.4	0.465	47.0	0.458	45.5	0.452	44.1	0.445	42.8
67	.0023	0.501	50.6	0.494	49.1	0.487	47.6	0.481	46.2	0.474	44.8	0.467	43.5

 ${\bf Temperature, Fahrenheit. -- Force of \ Vapor \ in \ English \ Inches. -- Relative \ Humidity \ in \ Hundredths.}$ 

Wet- Bulb				t-1	t', or D	ifference (	of West	and Day	D., 13, 701		A		
Bulb	Mean						or wer	and Dry	Buib II	nermome	ters.		
Thermo-l	Vertical Difference of Force	12°	apor. mid- ity. V ag. In524 51.2 0 .547 51.8 0 .572 52.4 0 .597 52.9 0 .623 53.5 0 .663 54.0 0 .6677 54.5 0 .705 55.0 0		.5	130	.0	130	.5	149	0.0	14	.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	tive Hu- mid-	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng In.	
68	0.0024	0.524	51.2	0.517	49.7	0.510	48.3	0.503	46.9	0.497	45.5	0.490	44.1
69	.0024	0.547		0.541	50.3	0.534	48.9	0.527	47.5	0.520	46.1	0.514	44.8
70	.0025	0.572		0.565	50.9	0.558	49.5	0.551	48.1	0.545	46.8	0.538	45.8
71	.0026	0.597		0.590	51.5	0.583	50.1	0.577	48.7	0.570	47.4	0.563	46.1
72	00.10	0.623	53.5	0.616	52.1	0.609	50.7	0.603	49.3	0.596	48.0	0.589	46.7
~0	.0026	0.050	5 4 A	0.049	52.6	0.636	51.3	0.629	49.9	0.623	48.6	0.616	47.8
73	.0027			0.643	53.2		51.8	0.657	50.5	0.650	49.2	0.643	47.9
74	.0028			0.670	53.7	0.664	52.3	0.685	51.0	0.678	49.7	0.672	48.4
75	.0029	1		0.699		0.692			51.5	0.708	50.3	0.701	48.9
76	•0630	0.735	56.0	0.728	54.2	0.721	52.9	0.714	52.1	0.739	50.8	0.731	49.5
77	.0031	0.765	36.0	0.759	54.7	0.752	53.4	0.745	92.1	0.709	90.0	0.751	40.0
78		0.796	56.5	0.782	55.2	0.782	53.8	0.775	52.5	0.768	51.3	0.762	50.0
79	.0032	0.527	56.9	0.821	55.6	0.814	54.3	0.807	53.0	0.800	51.8	0.794	50.5
80	.0033	0.860	57.3	0.853	56.1	0.847	54.8	0.840	53.5	0.833	52.2	0.826	51.0
81	.0034	0.894	57.8	0.887	56.5	0.880	55.2	0.874	53.9	0.867	52.7	0.860	51.4
82	.0035	0.929	58.2	0.922	56.9	0.915	55.6	0.909	54.4	0.902	53.2	0.895	51.9
04	.0036	0.929	90.2	0.922	30.5	0.915	55.0	0.303	94.4	0.502	00.2	0.000	01.0
83		0.965	58.6	0.958	57.3	0.951	56.1	0.944	54.8	0.937	53.6	0.931	52.4
84	.0037	1.002	59.0	0.995	57.7	0.988	56.5	0.981	55.2	0.974	54.0	0.968	52.8
85	.0038	1.039	59.4	1.033	58.1	1.026	56.8	1.019	55.6	1.012	54.4	1.005	53.2
86	•0039	1.078	59.7	1.071	58.5	1.065	57.2	1.058	56.0	1.051	54.8	1.044	53.6
87	.0040	1.119	60.1	1.112	58.8	1.105	57.6	1.099	56.4	1.092	55.2	1.085	54.0
0.	.0041		00.1	*****	00.0		0	21000					
88		1.159	60.5	1.152	59.2	1.146	58.0	1.139	56.8	1.132	55.6	1.125	54.4
89	.0042	1.202	60.9	1.195	59.6	1.188	58.3	1.181	57.1	1.174	56.0	1.167	54.8
90	.0044	1.245	61.3	1.238	59.9	1.231	58.7	1.225	57.5	1.218	56.3	1.211	55.2
91	.0045	1.290	61.6	1.283	60.2	1.276	59.0	1.269	57.9	1.263	66.7	1.256	55.6
92	•0046	1.336	61.9	1.329	60.6	1.322	59.4	1.315	58.2	1.309	57.0	1.302	55.9
	.0047												
93	.0049	1.383	62.2	1.376	60.9	1.370	59.7	1.363	58.5	1.356	57.4	1.349	56.3
94		1.432	62.5	1.425	61.2	1.418	60.0	1.411	58.9	1.404	57.7	1.397	56.6
95	.0050	1.482	62.7	1.475	61.5	1.468	60.4	1.461	59.2	1.454	58.1	1.447	57.0
96	.0051	1.533	63.0	1.526	61.8	1.519	60.7	1.512	59.5	1.505	58.4	1.498	57.8
97	.0052	1.585	63.3	1.578	62.1	1.571	61.0	1.564	59.8	1.558	58.7	1.551	57.6
98	10094	1.639	63.6	1.632	62.4	1.625	61.3	1.618	60.1	1.612	59.0	1.605	57.9
0.7	.0056		25.5		0.0		av c		00.	1 000	<b>70.0</b>	1 600	ED 6
99	.0057	1.695	63.9	1.688	62.7	1.681	61.6	1.674	60.4	1.667	59.3	1.660	58.2
100	.0059	1.752	64.2	1.745	63.0	1.738	62.0	1.731	60.7	1.721	59.6	1.717	58.5
101	•0060	1.810	64.4	1.803	63.2	1.797	62.3	1.790	61.0	1.783	59.9	1.776	58.8
102	.0062	1.870	64.7	1.863	63.5	1.857	62.6	1.850	61.3	1.843	60.2	1.836	59.1
103		1.932	64.9	1.925	63.8	1.918	62.9	1.911	61.5	1.904	60.4	1.897	59.4
104	•0063	1.995	65.2	1.988	64.0	1.981	63.2	1.974		1.967	60.7	1.960	59.6

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t	t', or D	ifference o	of Wet a	and Dry	Bulb Tl	aermomet	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	150	0.0	15	∘.5	169	•.0	16	.5	179	.0	17	∘.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Ilunid- ity.	Force of Vapor.	Rela- tive Hu- nid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0		Eng. In.		Eng. In		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32						i							
33									1				
34													
35 36		0.016	4.4										
30	0.0009	0.010	4.4								}		
37	2000	0.025	6.4	0.018	4.6								
38	.0009	0.033	8.3	0.027	6.5	0.020	4.8	0.014	3.2				
39	.0009	0.042	10.1	0.036	8.4	0.029	6.7	0.023	5.1	0.016	3.6	0.010	2.
40	.0009	0.051	11.9	0.045	10.1	0.038	8.5	0.032	6.9	0.025	5.4	0.019	3.9
41	.0010	0.061	13 6	0.054	11.8	0.048	10.3	0.041	8.7	0.035	7.2	0.028	5.1
42	•0010	0.071	15.1	0.064	13.4	0.058	11.9	0.051	10.3	0.044	8.8	0.038	7.
43	.0010	0.081	16.6	0.074	15.0	0.068	13.4	0.061	11.9	0.055	10.4	0.048	9.0
44	•0011	0.091	18.1	0.085	16.5	0.078	15.0	0.072	13.5	0.065	12.0	0.058	10.6
45	.0011	0.102	19.6	0.096	18.0	0.089	16.5	0.083	15.0	0.076	13.5	0.069	12.
46	.0011	0.114	21.0	0.107	19.4	0.100	17.9	0.094	16.4	0.087	15.0	0.081	13.6
	.0012												
47	.0012	0.125	22.4	0.119	20.8	0.112	19.3	0.106	17.9	0.099	16.5	0.092	15.1
48	.0013	0.137	23.8	0.131	22.2	0.124	20.7	0.118	19.3	0.111	17.9	0.104	16.5
49	.0013	0.150	25.1	0.143	23.6	0.137	22.1	0.130	20.7	0.124	19.3	0.117	17.9
50	.0013	0.163	26.4	0.156	24.9	0.150	23.4	0.143	22.0	0.136	20.6	0.130	19.3
51	.0014	0.176	27.6	0.169	26.1	0.163	24.6	0.156	23.2	0.150	21.9	0.143	20.6
52		0.190	28.7	0.183	27.3	0.177	25.8	0.170	24.4	0.163	23.1	0.157	21.8
53	.0014	0.204	29.9	0.197	28.4	0.191	27.0	0.184	25.6	0.178	24.3	0.171	23.0
54	.0015	0.219	30.9	0.212	29.5	0.206	28.1	0.199	26.7	0.192	25.4	0.186	24.1
55	.0015	0.234	32.0	0.228	30.6	0.221	29.2	0.214	27.8	0.208	26.5	0.201	25.2
56	.0016	0.250	33.0	0.243	31.6	0.237	30.2	0.230	28.9	0.223	27.6	0.217	26.3
	•0016											0.000	
5 <b>7</b>	.0017	0.266	34.0	0.260	32.6	0.253	31.2	0.246	29.9	0.240	28.6	0.233	27.8
58	.0017	0.283	34.9	0.276	33.5	0.270	32.2	0.268	30.8	0.256	29.6	0.249	28.3
59 60	.0018	0.300	35.8	0.294	34.4	0.287	33.1	0.280	31.8	0.274	30.5	0.267	29.3
60 61	.0019	0.318	36.7 37.5	$0.311 \\ 0.330$	35.3	$0.305 \\ 0.323$	$34.0 \\ 34.9$	$0.298 \\ 0.316$	32.7 33.6	0.291 0.310	31.4	$0.285 \\ 0.303$	31.2
01	.0019	0.000	91.9	0.000	36.2	0.020	34.3	0.010	00.0	0.010	04.4	0.000	01.2
62		0.356	38.4	0.349	37.0	0.342	35.7	0.336	34.5	0.329	33.2	0.322	32.0
63	•0020	0.375	39.2	0.369	37.9	0.362	36.6	0.355	35.3	0.349	34.1	0.342	32.9
64	•0020	0.396	40.0	0.389	38.7	0.382	37.4	0.376	36.1	0.369	31.9	0.362	33.7
65	•0021	0.417	40.7	0.410	39.4	0.403	38.2	0.396	36.9	0.390	35.7	0.383	34.5
66	.0022	0.438	41.5	0.431	40.2	0.425	38.9	0.418	37.7	0.411	36.5	0.405	35.8
67	.0023	0.460	42.2	0.454	40.9	0.447	39.6	0.440	38.4	0.434	37.2	0.427	36.1
						I							

 $\textbf{Temperature, Fahrenheit.} \ - \textbf{Force of Vapor in English Inches.} \ - \textbf{Relative Humidity in Hundredths}.$ 

***				t — t	', or Di	fference o	of Wet	and Dry 1	Bulb Ti	nermomet	ers.		
Wet- Bulb Chermo- meter	Mean Vertical Difference of Force of Vapor	15°	ree of Humidity. Force of Vapor. Humidity.  g. In. 483 42.8 0.477 41.4 507 43.5 0.500 42.5 531 44.2 0.524 42.5 556 44.8 0.550 43.4 582 45.4 0.576 44.5			16°	.0	16°	.5	170	.0	170	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	tive Hu- mid-		Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0		Eng. In.		-		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
68	0.0024	0.483			41.6	0.470	40.3	0.463	39.1	0.456	37.9	0.450	36.8
69	.0024	0.507			42.3	0.594	41.0	0.487	39.8	0.480	38.7	0.473	37.
70	.0025	0.531			42.9	0.518	41.7	0.511	40.5	0.504	39.3	0.498	38.
71	.0026	0.556	44.8	0.550	43.6	0.543	42.4	0.536	41.2	0.529	40.0	0.523	38.
72		0.582	45.4	0.576	44.2	0.569	43.0	0.562	41.8	0.555	40.7	0.549	39.
	.0027					0 700		0 700	10.4	0 700	41.0	0	40
73	.0028	0.609				0.596	43.6	0.589	42.4	0.582	41.3	0.575	40.
74	.0028	0.637	46.6	0.630	45.4	0.623	44.2	0.616	43.0	0.610	41.9	0.603	40.
75	.0029	0.665	47.2	0.658	46.0	0.651	44.8	0.645	43.6	0.638	42.5	0.631	41.
76	.0030	0.694	47.7	0.687	46.5	0.681	45.4	0.674	44.2	0.667	43.1	0.660	42.
77		0.721	48.2	0.717	47.1	0.711	45.9	0.704	44.8	0.697	43.6	0.690	42.
***	.0031		40.0	0 = 40		0.741	10.4	0 795	45.0	0.728	44.2	0.721	43.
78	.0032	0.755	48.8	0.748	47.6	0.741	46.4	0.735	45.3				
79	.0033	0.787	49.3	0.780	48.1	0.773	47.0	0.766	45.8	0.760	44.7	0.753	43.
80	.0034	0.820	49.8	0.813	48.6	0.806	47.5	0.799	46.4	0.792	45.3	0.786	44.
81	.0035	0.853	50.3	0.847	49.1	0.840	48.0	0.833	46.9	0.826	45.8	0.819	44.
82		0.888	50.7	0.881	49.6	0.875	48.5	0.868	47.4	0.861	46.3	0.854	45.
00	.0036		-10			0.010	40.0	0.000	400	0.00-	46.8	0.890	45.
83	.0037	0.924	51.2	0.917	50.0	0.910	48.9	0.903	47.8	0.897		1	
84	.0038	0.961	51.6	0.954	50.5	0.947	49.4	0.940	48.3	0.933	47.2	0.927	46.
85	.0039	0.998	52.1	0.992	50.9	0.985	49.8	0.978	48.7	0.971	47.7	0.964	46.
86	.0040	1.037	52.5	1.030	51.3	1.024	50.3	1.017	49.2	1.010	48.1	1.003	47.
87		1.078	52.9	1.071	51.8	1.064	50.7	1.058	49.6	1.051	48.6	1.044	47.
88	.0041	1 110	53.3		52.2	1.105	51.1	1.098	50.0	1.091	49.0	1.084	48.
89	.0042	1.118		1.111		1.147	51.5	1.140	50.4	1.133	49.4	1.126	48.
	.0044	1.161	53.7	1.154	52.6			1.183	50.4	1.177	49.8	1.170	48.
90	.0045	1.204	54.1	1.197	53.0	1.190	51.9			,	50.2	1.215	49.
91	.0046	1.249	54.5	1.242	53.4	1.235	52.3	1.228	51.2	1.221	50.2	1.213	49.
92		1.295	54.8	1.288	53.7	1.281	52.7	1.274	51.6	1.267	30.0	1.200	49.
93	.0048	1.342	55.2	1.335	54.1	1.328	53.0	1.321	52.0	1.315	51.0	1.308	50.
94	.0019	1.390	55.5	1.384	54.4	1.377	53.4	1.370	52.4	1.363	51.4	1.356	50.
95	.0050	1.440	55.9	1.433	54.8	1.426	53.7	1.420	52.7	1.413	51.7	1.406	50.
96	.0051	1.491	56.2	9		1.477	54.1	1.471	53.1	1.464	52.1	1.457	51.
97	•0053	1.544	56.5	1.484	55.1 55.5	1.530	54.4	1.523	53.4	1.516	52.4	1.509	51.
98	.0054	1.598	56.8	1.591	55.8	1.584	54.4	1.525	53.8	1.570	52.8	1.563	51.
30	.0056	1.059	50.3	1.591	99.3	1.004	0.1.0	1.577	99.0	1.570	02.0	1.505	01.
99	•0000	1.653	57.2	1.646	56.1	1.639	55.1	1.633	54.1	1.626	53.1	1.619	52.
100	.0057	1.710	57.5	1.703	56.4	1.696	55.4	1.690	54.4	1.683	53.4	1.676	52.
101	.0059	1.769	57.8	1.762	56.7	1.755	55.7	1.748	54.7	1.741	53.7	1.734	52.
102	.0060	1.829	58.0	1.822	57.0	1.815	56.0	1.809	55.0	1.802	54.0	1.794	53.
102	.0062	1.890	58.3	1.883	57.3	1.876	56.3	1.869	55.3	1.863	54.3	1.856	53.
103	.0063	1.953	58.6	1.946	57.6	1.939	56.6	1.932	55.6	1.925	54.6	1.919	53.
104	l	1.333	00.0	1.340	01.0	1.0.00	20.0	1.502	00.0	1.320	0.4.0	1.010	000

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-t	, or Di	fference o	of Wet	and Dry I	Bulb Ti	hermome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	18	°.0	18	°.5	19	°.0	199	.5	20	° <b>.0</b>	20	°.5
t' Fabren- heit	of Vapor for each 0°.1.	Force of Vapor.	Relative Ilumid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Ilu- mid- ity	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu-mid-ity.	Force of Vapor.	Relative Hu mid ity
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32												1	
33										1		l	
34													
35													-
36					}								
37													
38	٠									1			
39										İ		i	
40	0.0010	0.012	2.5										
41		0.022	4.3	0.015	3.0	0.009	1.6						
42	•0010	0.031	6.0	0.025	4.6	0.018	3.3	0.012	2.1				
43	.0010	0.041	7.6	0.035	6.3	0.028	5.0	0.022	3.7	0.015	2.6		
44	•0011	0.052	9.2	0.045	7.9	0.039	6.6	0.032	5.4	0.026	4.3	0.019	3.
45	.0011	0.063	10.8	0.056	9.5	0.050	8.2	0.043	7.0	0.037	5.9	0.030	4.
46	•0011	0.074	12.3	0.068	11.0	0.061	9.7	0.054	8.5	0.048	7.5	0.041	6.
	.0012												
47	.0012	0.086	13.8	0.079	12.5	0.073	11.2	0.066	10.0	0.059	9.0	0.053	7.
48	.0013	0.098	15.2	0.091	13.9	0.085	12.7	0.078	11.5	0.072	10.4	0.065	9.
49	.0013	0.110	16.6	0.104	15.4	0.097	14.1	0.091	12.9	0.084	11.9	0.077	10.
50	•0013	0.123	18.0	0.117	16.7	0.110	15.5	0.103	14.4	0.097	13.2	0.090	12. 13.
51	0014	0.136	19.3	0.130	18.0	0.123	16.8	0.117	15.7	0.110	14.5	0.103	10.
52	•0014	0.150	20.5	0.144	19.3	0.137	18.1	0.130	16.9	0.124	15.7	0.117	14.
53	.0014	0.164	21.7	0.158	20.5	0.151	19.3	0.145	18.2	0.138	16.9	0.131	15.
54	•0015	0.179	22.9	0.173	21.7	0.166	20.5	0.159	19.3	0.152	18.1	0.146	17.
55	.0015	0.194	24.0	0.188	22.8	0.181	21.6	0.174	20.5	0.168	19.2	0.161	18.
56	.0016	0.210	25.1	0.203	23.9	0.197	22.7	0.190	21.6	0.184	20.4	0.177	19.
57	.0016	0.226	26.1	0.220	24.9	0.213	23.8	0.206	22.7	0.200	21.5	0.193	20.
58	.0017	0.243	27.1	0.236	25.9	0.213	24.8	0.223	23.7	0.200	22.6	0.133	21.
59	.0017	0.260	28.1	0.254	26.9	0.247	25.8	0.240	24.7	0.234	23.6	0.227	22.
60	•0018	0.278	29.0	0.271	27.9	0.265	26.8	0.258	25.7	0.251	24.6	0.245	23.
61	•0019	0.296	30.0	0.290	28.8	0.283	27.7	0.276	26.6	0.270	25.5	0.263	24.
	.0019												
62	.0020	0.316	30.9	0.309	29.7	0.302	28.6	0.295	27.5	0.289	26.5	0.282	25.
63	.0020	0.335	31.7	0.328	30.6	0.322	29.5	0.315	28.4	0.308	27.4	0.302	26.
64	.0020	0.355	32.6	0.349	31.5	0.342	30.4	0.335	29.3	0.329	28.2	0.322	27.
65 66	.0021	0.376   0.398	33.4	0.370	32.3	0.363	31.2	0.356	30.1	0.350	29.1 29.9	0.343	28. 28.
67	.0023	0.420	34.2 34.9	0.391	33.1 33.8	$0.385 \\ 0.407$	32.0 32.8	0.378	30.9	0.371 0.393	30.7	0.387	29.
01		0.420	94.0	0.414	00.0	0.407	0.40	0.400	91.7	0.000	90.1	3.007	20.

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.0013.

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

				t-t	, or Di	fference o	f Wet a	nd Dry I	Bulb <b>T</b> h	ermome	ters.		
meter	Mean Vertical Difference of Force	180	.0	180	.5	19	•.0	19	.5	200	•.0	20	·.5
fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng In.	
68	0.0024	0.443	35.7	0.436	34.6	0.430	33.5	0.423	32.5	0.416	31.4	0.409	30.4
69	.0025	0.467	36.4	0.460	35.3	0.453	34.2	0.446	33.2 33.9	$0.440 \\ 0.464$	32.2 32.9	0.433 $0.457$	31.9
70 71	.0025	$0.491 \\ 0.516$	37.1 37.8	0.484	36.0 36.7	$0.477 \\ 0.502$	35.0 35.7	0.471	34.6	0.489	33.6	0.482	32.7
72	.0026	0.510	38.5	0.535	37.4	0.528	36.3	0.522	35.3	0.515	34.3	0.508	33.
	.0026	0.542	30.0	0.353	01.4	0.520	00.0	0.022	0010	0.010	0 1.0	0.500	00.
73	.0027	0.569	39.1	0.562	38.0	0.555	37.0	0.548	36.0	0.542	35.0	0.535	34.0
74	.0028	0.596	39.7	0.589	38.7	0.583	37.7	0.576	36.6	0.569	35.7	0.562	34.7
75	.0029	0.624	40.3	0.618	39.3	0.611	38.3	0.604	37.3	0.597	36.3	0.591	35.3
76	.0030	0.654	40.9	0.647	39.9	0.640	38.9	0.633	37.9	0.627	36.9	0.620	35.9
77		0.683	41.5	0.677	40.5	0.670	39.5	0.663	38.5	0.656	37.5	0.650	36.3
78	.0031	0.714	42.1	0.707	41.0	0.701	40.0	0.694	39.0	0.687	38.1	0.680	37.
79	.0032	0.714	42.6	0.739	41.6	0.732	40.6	0.726	39.6	0.719	38.6	0.712	37.
80	.0033	0.779	43.2	0.772	42.1	0.765	41.1	0.758	40.2	0.752	39.2	0.745	38.3
81	.0034	0.813	43.7	0.806	42.7	0.799	41.7	0.792	40.7	0.785	39.7	0.779	38.8
82	.0035	0.847	44.2	0.840	43.2	0.834	42.2	0.827	41.2	0.820	40.2	0.813	39
	.0036												
83	.0036	0.883	44.7	0.876	43.7	0.869	42.7	0.863	41.7	0.856	40.7	0.849	39.9
84	.0038	0.920	45.2	0.913	44.2	0.906	43.2	0.899	42.2	0.893	41.3	0.886	40
85	.0039	0.958	45.6	0.951	44.6	0.944	43.7	0.937	42.7	0.930	41.8	0.923	40.9
86	.0040	0.996	46.1	0.989	45.1	0.983	44.1	0.976	43.2	0.969	42.3	0.962	41.3
87		1.037	46.5	1.030	45.6	1.023	44.6	1.017	43.6	1.010	42.7	1.003	41.8
88	•0041	1.077	47.0	1.070	46.0	1.064	45.0	1.057	44.1	1.050	43.2	1.043	42.
89	.0042	1.119	47.4	1.113	46.4	1.106	45.5	1.099	44.5	1.092	43.6	1.085	42.
90	.0043	1.163	47.8	1.156	46.9	1.149	45.9	1.142	45.0	1.136	44.1	1.129	43.5
91	.0045	1.208	48.2	1.201	47.3	1.194	46.3	1.187	45.4	1.180	44.5	1.173	43.6
92	.0047	1.254	48.6	1.247	47.7	1.240	46.7	1.233	45.8	1.226	44.9	1.219	44.0
	.0048												
93	.0049	1.301	49.0	1.294	48.1	1.287	47.1	1.280	46.2	1.273	45.3	1.266	44
94	.0049	1.349	49.4	1.342	48.4	1.335	47.5	1.329	46.6	1.322	45.7	1.315	44.8
95	.0051	1.399	49.8	1.392	48.8	1.385	47.9	1.378	47.0	1.371	46.1	1.364	45.2
96	.0053	1.450	50.1	1.443	49.2	1.436	48.3	1.429	47.3	1.422	46.5	1.415	45.6
97	.0054	1.502	50.5	1.495	49.5	1.489	48.6	1.482	47.7	1.475	46.8	1.468	46.0
98		1.556	50.8	1.549	49.9	1.543	49.0	1.536	48.1	1.529	47.2	1.522	46.5
99	.0055	1.612	51.2	1.605	50.2	1.598	49.3	1.591	48.4	1.584	47.5	1.577	46.7
100	.0057	1.669	51.5	1.662	50.6	1.655	49.7	1.648	48.8	1.641	47.9	1.634	47.0
101	•0058	1.727	51.8	1.720	50.9	1.713	50.0	1.706	49.1	1.700	45.2	1.693	47
102	•0060	1.787	52.2	1.780	51.2	1.773	50.3	1.766	49.4	1.759	48.6	1.753	47.7
103	.0062	1.849	52.5	1.842	51.5	1.835	50.7	1.828	49.8	1.821	48.9	1.814	48.0
104	•0063	1.912	52.8	1.905	51.9	1.898	51.0	1.891	50.1	1.884	49.2	1.877	48.4

 $\textbf{Temperature, Fahrenheit.} \leftarrow \textbf{Force of Vapor in English Inches.} \leftarrow \textbf{Relative Humidity in Hundredths.}$ 

				t-	t', or D	ifference	of Wet	and Dry	Bulb T	hermome	eters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	21	° <b>.</b> 0	21	°.5	22	°.0	22	∘.5	23	°.0	23	∘.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity	Force of Vapor.	Relative Hu-mid-ity.	Force of Vapor.	Relative Hu-mid-ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In		Eng. In	
32													
33 34													
35													
36											İ		
0.4													
37 38											ì		
39													
40													
41													
42													
43													
44		0.013	2.0										
45	0.0011	0.023	3.7	0.017	2.6	0.010	1.6						
46	1100.	0.035	5.2	0.028	4.2	0.022	3.1	0.015	2.1				
47	.0012	0.046	6.8	0.040		0.000		0.00=	۰.~	0.000	0 =	0.010	3.0
48	.0012	0.058	8.2	0.052	5.7 7.2	0.033	6.2	0.027 $0.039$	$\frac{3.7}{5.2}$	$0.020 \\ 0.032$	2.7 4.2	0.013 $0.025$	1.8 3.3
49	•0013	0.071	9.7	0.064	8.6	0.043	7.6	0.051	6.6	0.044	5.7	0.023	4.7
50	•0013	0.084	11.0	0.077	10.0	0.070	9.0	0.064	8.0	0.057	7.1	0.051	6.1
51	•0013	0.097	12.3	0.090	11.3	0.084	10.3	0.077	9.3	0.070	8.3	0.064	7.4
52	•0014	0.110	13.5	0.104	10.5	0.00=	11.5	0.001	10.0	0.004	0.0	0.000	0 =
53	.0014	0.110	14.8	0.118	12.5 13.7	0.097	11.5 12.8	0.091	10.6	0.084	9.6	$0.077 \\ 0.092$	S.7 9.9
54	<b>-</b> 0015	0.139	16.0	0.113	14.9	0.111	14.0	0.120	13.0	0.033	12.1	0.032	11.2
55	.0015	0.155	17.1	0.148	16.1	0.141	15.1	0.135	14.2	0.128	13.3	0.121	12.4
56	.0016	0.170	18.2	0.164	17.2	0.157	16.3	0.150	15.3	0.144	14.4	0.137	13.5
57	-0016	0.186	19.4	0.180	18.4	0.179	17 (	0.16*	16.5	0.160	15.6	0.159	14.7
58	.0017	0.203	20.5	0.197	19.5	0.173	17.4 18.5	0.167	17.6	0.160	15.6 16.7	0.153	15.8
59	.0017	0.220	21.5	0.214	20.6	0.207	19.6	0.200	18.7	0.194	17.7	0.187	16.9
60	•0018	0.238	22.5	0.231	21.6	0.225	20.6	0.218	19.6	0.211	18.7	0.205	17.8
61	•0019	0.256	23.4	0.250	22.5	0.243	21.5	0.236	20.6	0.230	19.7	0.223	18.8
62	•0019	0.275	24.4	0.269	23.5	0.262	22.4	0.255	21.5	0.249	20.6	0.242	19.7
63	.0020	0.295	25.3	0.288	24.4	0.282	23.3	0.235	22.4	0.249	21.5	0.242	20.7
64	•0020	0.315	26.1	0.309	25.3	0.302	24.2	0.295	23.3	0.289	22.4	0.282	21.6
65	.0021	0.336	27.0	0.330	26.1	0.323	25.1	0.316	24.2	0.309	23.3	0.303	22.4
66	.0022	0.358	27.9	0.351	27.0	0.344	26.0	0.338	25.1	0.331	24.2	0.324	23.3
67	.0023	0.380	28.7	0.373	27.8	0.367	26.8	0.360	25.9	0.353	25.0	0.346	24.2

 $\textbf{Temperature, Fahrenheit.} \\ \textbf{—Force of Vapor in English Inches.} \\ \textbf{—Relative Humidity in Hundredths.}$ 

1		•				ference o		nd Dry I					
Wet-	Mean												
	Vertical Difference of Force	210	.0	21°	.5	220	.0	22°	.5	230	.0	23°	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	2-0	Eng. In.	0" 0
68	0.0024	0.403	29.5	0.396	28.5	0.389	27.6	0.383	26.7	0.376	25.8	0.369	25.0 25.8
69	.0024	0.426	30.2	0.420	29.3	0.413	28.4	0.406	27.5	0.399	26.6	0.393	26.5
70	.0025	0.451	31.0	0.444	30.1	0.437	29.1	0.430	28.2	0.424	27.4 28.1	0.417	27.3
71	.0026	0.476	31.7	0.469	30.8	0.462	29.9	0.455	29.0	0.449	28.8	0.442	28.0
72		0.501	32.4	0.495	31.5	0.488	30.6	0.481	29.7	0.475	40.0	0.400	20.0
**0	.0027	0.500	33.1	0.521	32.2	0.515	31.3	0.508	30.4	0.501	29.5	0.494	28.7
73	.0028	0.528	33.8	0.549	32.8	0.542	31.9	0.535	31.1	0.529	30.2	0.522	29.4
74	.0028	$0.556 \\ 0.584$	34.4	0.577	33.5	0.570	32.6	0.564	31.7	0.557	30.9	0.550	30.0
75	.0029	0.613	35.0	0.606	34.1	0.599	33.2	0.593	32.3	0.586	31.5	0.579	30.7
76	•0030	0.613	35.6	0.636	34.7	0.629	33.S	0.623	33.0	0.616	32.1	0.609	31.3
77	.0031	0.043	99.0	0.000	04.1	0.020	55.0	0.020	5.5.0				
78		0.674	36.2	0.667	35.3	0.660	34.4	0.653	33.6	0.647	32.7	0.640	31.9
79	.0032	0.705	36.8	0.699	35.9	0.692	35.0	0.685	34.2	0.678	33.3	0.671	32.5
80	•0033	0.738	37.4	0.731	36.5	0.724	35.6	0.718	34.7	0.711	33.9	0.704	33.1
81	.0034	0.772	37.9	0.765	37.0	0.758	36.1	0.751	35.3	0.745	34.5	0.738	33.5
82	.0035	0.806	38.4	0.800	37.6	0.793	36.7	0.786	35.8	0.779	35.0	0.772	34.2
0.3	.0036	0.000	00.1										
83		0.842	39.0	0.835	38.1	0.829	37.2	0.822	36.4	0.815	35.5	0.808	34.7
84	.0037	0.879	39.5	0.872	38.6	0.865	37.7	0.858	36.9	0.852	36.1	0.845	35.2
. 85	•0038	0.917	40.0	0.910	39.1	0.903	38.2	0.896	37.4	0.889	36.6	0.882	35.8
86	.0039	0.955	40.4	0.948	39.6	0.942	38.7	0.935	37.9	0.928	37.1	0.921	36.3
87	•0040	0.995	40.9	0.988	40.1	0.981	39.2	0.975	38.4	0.968	37.5	0.961	36.7
	.0041			1							90.0		07 0
88	0043	1.036	41.4	1.029	40.5	1.022	39.7	1.016	38.8	1.009	38.0	1.002	37.2
89	.0042	1.078	41.8	1.071	41.0	1.065	40.1	1.058	39.3	1.051	38.5	1.044	37.7
90	.0044	1.122	42.3	1.115	41.4	1.108	40.6	1.101	39.7	1.094	38.9	1.088	38.1
91	.0045	1.166	42.7	1.160	41.9	1.153	41.0	1.146	40.2	1.139	39.4	1.132	38.6
92	.0046	1.212	43.1	1.206	42.3	1.199	41.4	1.192	40.6	1.185	39.8	1.178	39.0
	•004S	1.000	10-	1 050	10 ~	1.246	41.9	1.239	41.0	1.232	40.2	1.225	39.4
93	.0049	1.260	43.5	1.253	42.7	1.246	42.3	1.287	41.4	1.280	40.6	1.274	39.9
94	.0050	1.308	43.9	1.301	43.1	1.344	42.7	1.337	41.8	1.330	41.0	1.323	40.3
95	.0051	1.358	44.3		43.5		43.0	1	42.2	1	41.4	1.374	40.7
96	.0053	1.408	44.7	1.402	43.9	1.395	43.4		42.6		41.8	1.426	41.1
97	.0054	1.461	45.1	1.454	44.3	1.447	43.8	1	43.0	1	42.2	1.480	41.4
98		1.515	45.5	1.508	44.6	1.501	49.0	1.434	30.0	1.131			
99	.0056	1.570	45.8	1.563	45.0	1.556	44.2	1.550	43.4	1.543	42.6	1.536	41.8
100	.0057	1.627	46.2				44.5	4	43.7		43.0	1.593	42.2
101	.0059	1.686			1	1	44.9	1	44.1	1	43.3	1.651	42.5
102	.0060	1.746	1		46.0		45.2	1	41.4			1.711	42.9
103	.0062	1.807	1				45.6		1		44.0	1.772	43.2
103	.0063	1.870		1.863						1	44.3	1.835	43.6
101		u .		·		ce of Fore	<u> </u>		·	<u>'</u>			

 ${\bf Temperature, Fahrenheit. - Force\ of\ Vapor\ in\ English\ Inches. -- Relative\ Humidity\ in\ Hundredths.}$ 

				t –	- <b>t</b> ', or l	Difference	of Wet	and Dry	Bulb 7	lhermom	eters.		
Wet- Bulb Thermo meter	Mean Vertical Difference of Force of Vapor	1 4	<b>10.0</b>	24	<b>1</b> °.5	26	5°.0	25	5°.5	20	6°.0	20	3°.5
Fahren- heit.		Force o		Force ( Vapor	Relative Hu- mid- ity.	Force of		Force of		Force of		Force o	
0		Eng. In	1.	Eng. Ir	1.	Eng. In	a.	Eng. Ir	1.	Eng. Ir	n.	Eng. In	
32 33													
34	1			1									
35				1								1	
36	ł											1	
												1	1
37												1	
38												-	
39 40				İ									
41											1		
42													
43													
44													
45 46				1									
40													
47													1
48	0.0013	0.019	2.4	0.012	1.5			1				1	
49	.0013	0.031	3.9	0.025	3.0	0.018	2.2	0.011	1.3				
50	•0013	0.044	5.2	0.037	4.4	0.031	3.6	0.024	2.7	0.018	2.0	0.011	1.2
51	•0014	0.057	6.5	0.051	5.7	0.044	4.9	0.037	4.1	0.031	3.3	0.024	2.5
52		0.071	7.8	0.064	7.0	0.058	6.1	0.051	5.3	0.044	4.6	0.038	3.8
53	.0014	0.085	9.1	0.078	8.2	0.072	7.4	0.065	6.6	0.058	5.8	0.052	5.1
54	•0015	0.100	10.3	0.093	9.4	0.086	8.6	0.080	7.8	0.073	7.0	0.067	6.3
55	.0015 .0016	0.115	11.5	0.108	10.6	0.102	9.8	0.095	9.0	0.088	8.2	0.082	7.5
56		0.130	12.7	0.124	11.8	0.117	11.0	0.111	10.2	0.104	9.4	0.097	8.7
57	•10016	0.1.17	19.0	0.140	100	A 100	10.1	0.10**	11.0	0 100	700	0.110	
58	.0017	$0.147 \\ 0.163$	13.8 14.9	0.140 0.157	13.0 14.1	0.133	12.1 13.2	0.127 $0.143$	11.3 12.5	$0.120 \\ 0.137$	10.6	0.113	9.8
59	.0017	0.180	16.0	0.174	15.2	0.150	14.3	0.143	13.6	0.154	12.8	0.130	12.0
60	.0018	0.198	17.0	0.191	16.1	0.185	15.3	0.178	14.6	0.172	13.8	0.147	13.0
61	•0019	0.216	17.9	0.210	17.1	0.203	16.3	0.196	15.5	0.190	14.7	0.183	14.0
00	-0019												
62 63	.0020	0.235	18.9	0.229	18.1	0.222	17.2	0.215	16.5	0.209	15.7	0.202	15.0
64	•0020	$0.255 \ 0.275$	19.8 20.7	$0.248 \\ 0.269$	19.0	0.242	18.2	0.235	17.4	0.228	16.6	0.222	15.9
65	.0021	0.275	21.6	0.269	19.9 20.8	$0.262 \\ 0.283$	19.1 20.0	$0.255 \\ 0.276$	18.3 19.2	$0.248 \\ 0.269$	17.5 18.4	$0.242 \\ 0.263$	16.8 17.7
66	.0022	0.318	22.5	0.259	21.7	0.283	20.0	0.276	20.1	0.269	19.3	0.284	18.6
67	*0053 F	0.340	23.3	0.333	22.5	0.326	21.7	0.320	20.1	0.231	20.2	0.306	19.4
			1										

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

					l o P'	or	C TE +	- d D	Daille Mi		0.50		
Wet-	Mean			t — t	or Di	Herence o	or Wet a	ind Dry I	sulb Tk	ermomet	ers.		
meter	Vertical Difference of Force	24°	.0	24	.5	25	.0	25	.5	26°	.0	26	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.	22.5	Eng. In.		Eng. In.	21.0	Eng In.	20.0
68	0.0024	0.363	24.2	0.356	23.3	0.349	22.5	0.342	21.8	0.336	21.8	0.329	20.3
69	.0024	0.386	24.9	0.379	24.1	0.373	23.3	0.366	22.6	0.359	$\frac{21.8}{22.6}$	0.352	21.
70	.0025	0.410	25.7	0.403	24.9	0.397	$24.1 \\ 24.9$	0.390	23.3	0.383	23.3	$0.377 \\ 0.402$	22.6
71	.0026	$0.435 \\ 0.461$	26.4	0.428	25.6	0.422	25.6	0.415	$24.1 \\ 24.8$	0.434	24.1	0.402	23.
72	.0027	0.401	27.2	0.454	26.4	0.448	49.0	0.441	24.0	0.494	44.1	0.427	£0.6
73		0.488	27.9	0.481	27.1	0.474	26.3	0.467	25.5	0.461	24.8	0.454	24.0
74	.0028	0.515	28.5	0.508	27.7	0.502	27.0	0.495	26.2	0.488	25.5	0.481	24.3
75	.0028	0.543	29.2	0.537	28.4	0.530	27.6	0.523	26.8	0.516	26.1	0.510	25.
76	.0029	0.572	29.8	0.566	29.1	0.559	28.3	0.552	27.4	0.545	26.8	0.539	26.
77	.0030	0.602	30.5	0.595	29.7	0.589	28.9	0.582	28.0	0.575	27.4	0.568	26.3
	1800.												
78	.0032	0.633	31.1	0.626	30.3	0.619	29.5	0.613	28.7	0.606	28.0	0.599	27.
79	.0033	0.665	31.7	0.658	30.9	0.651	30.1	0.644	29.3	0.638	28.6	0.631	27.9
80	.0034	0.697	32.3	0.691	31.5	0.684	30.7	0.677	29.9	0.670	29.2	0.663	28.
81	.0035	0.731	32.8	0.724	32.1	0.717	31.3	0.711	30.5	0.704	29.8	0.697	29.
82		0.766	33.4	0.759	32.6	0.752	31.8	0.745	31.0	0.738	30.4	0.732	29.
	.0036			1							00.0	0 -0-	
83	.0037	0.801	33.9	0.795	33.2	0.788	32.4	0.781	31.6	0.774	30.9	0.767	30.5
84	.0038	0.838	34.5	0.831	33.7	0.824	32.9	0.818	32.1	0.811	31.5	0.804	30.
85	.0039	0.876	35.0	0.869	34.2	0.862	33.4	0.855	32.7	0.848	32.0	0.842	31.
86	.0040	0.914	35.5	0.908	34.7	0.901	33.9	0.894	33.2	0.887	32.5	0.880	31.8
87		0.954	36.0	0.947	35.2	0.940	34.4	0.934	33.7	0.927	33.0	0.920	32.
88	.0041	0.995	36.4	0.988	35.7	0.981	34.9	0.975	34.2	0.968	33.5	0.961	32.8
89	.0042	1.037	36.9	1.030	36.1	1.024	35.4	1.017	34.7	1.010	33.9	1.003	33.5
90	.0044	1.081	37.4	1.074	36.6	1.067	35.8	1.060	35.1	1.053	34.4	1.046	33.
91	.0045	1.125	37.8	1.118	37.1	1.112	36.3	1.105	35.6	1.098	34.9	1.091	34.5
92	•0046	1.171	38.2	1.164	37.5	1.157	36.7	1.151	36.0	1.144	35.3	1.137	34.0
34	.0048	1.171	30.2	1.104	37.5	1.101	30.7	1.151	30.0	1.144	00.0	1.10.	01
93		1.218	38.7	1.211	37.9	1.205	37.1	1.198	36.5	1.191	35.7	1.184	35.0
94	.0049	1.267	39.1	1.260	38.3	1.253	37.5	1.246	36.9	1.239	36.2	1.232	35.
95	•0050	1.316	39.5	1.309	38.7	1.302	37.9	1.296	37.3	1.289	36.6	1.282	35.9
96	.0051	1.367	39.9	1.360	39.1	1.353	38.3	1.346	37.7	1.340	37.0	1.333	36.3
97	•0053	1.420	40.3	1.413	39.5	1.406	38.7	1.399	38.1	1.392	37.4	1.385	36.3
98	.0054	1.473	40.7	1.467	39.9	1.460	39.1	1.453	38.5	1.446	37.8	1.439	37.
	.0056												
99	.0057	1.529	41.1	1.522	1	1.515	1	1.508	38.9	1.501	38.2	1.494	37.
100	.0059	1.586	41.4	1.579	10.7	1.572	39.9	1.565	39.2	1.558	38.5	1.551	37.9
101	.0059	1.644	41.8	1.637	41.0	1.630	40.3	1.623	39.6	1.616	38.9	1.609	38.
102	.0062	1.704	42.2	1.697	41.4	1.690	40.7	1.683	40.0	1.676	39.3	1.669	38.0
103 104	.0063	1.765	42.5	1.758	41.8	1.751	41.0	1.745	40.3	1.738	39.6	1.731	38.
	***************************************	1.828	42.8	1.821	42.1	1.814	41.4	1.807	40.7	1.800	40.0	1.793	39.3

Correction for Barometrical Height above or below the Normal Height of 29.7 inches.

For				Diffe	rence of	Thermo	meters,	or t-t	Fahrer	nheit.			
Baromet- rical Height.	20	4°	6°	80	10°	12°	14°	16°	180	20°	220	24°	26°
					Wet I	Bulb abo	ve the F	reezing-l	Point.		,	·	,
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
31.0	001	002	003	005	006	007	008	009	010	012	013	014	015
30.5	.001	.001	.002	.003	.004	.004	.005	.006	.006	.007	.008	.009	.009
30.0	000	000	001	001	001	002	002	002	002	003	003	003	004
29.5	+.000	+.000	+.001	+.001	+.001	+.001	+.001	+.001	+.002	+.002	+.002	+.002	+.002
29.0	100.	.001	.002	.003	.003	.004	.004	.005	.006	.006	.007	.008	.008
28.5	.001	.002	.003	.004	.005	.006	.007	.009	.010	.011	.012	.013	.014
28.0	.001	.003	.005	.006	.008	.009	.011	.012	.014	.015	.017	.018	.020
27.5	.002	.004	.006	.007	.010	.012	.014	.016	.018	.020	.022	.024	.026
27.0	.002	.005	.007	.009	012	.014	.017	.019	.022	.024	.027	.029	.031
26.5	.003	.006	.008	.011	.014	.017	.020	.023	.026	.029	.031	.034	.037
26.0	.003	.006	.010	.013	.016	.020	.023	.026	.030	.033	.036	.040	.043
25.5	.004	.007	.011	.014	.019	.022	.025	.030	.034	.037	.041	.045	.049
25.0	.004	.008	.012	.016	.021	.025	.028	.033	.038	.042	.046	.050	.055
24.0	.005	.010	.015	.020	.025	.030	.034	.040	.046	.051	.056	.061	.066
23.0	.006	.012	.018	.023	.030	.035	.041	.047	.054	.060	.066	.072	.078
22.0	.007	.013	.020	.027	.034	.041	.047	.054	.062	.069	.076	.083	.090
21.0	.008	.015	.023	.030	.038	.046	.053	.062	.070	.077	.085	.093	.101
20.0	+.008	+.017	+.026	+.034	+.043	+.051	+.059	+.069	+.078	+.086	+.095	+.104	+.113
		Wet B	ulb belo	w the	<u> </u>		TP 37 /	MDI	e or	CATO	TITE A.	EXON.	<u> </u>
			1	1							CULAT		
31.0	001	002	003	004	006						zing-Poi		
30.5	.001	.001	.002	.003	.003	1						. = 26.	5 in.
30.0	000	000	001	001	001	1	~		0		ean bar		
29.5	+.000	+.000	+.000	+.001	+.001			ight of	27.9 m	iches.	Force		Inch.
29.0	.001	.001	.002	.002	.003	Vap		• • •	tion in	· · this ·	table, f		0.403
28.5	.001	.002	.003	.004	.005			nches,			anore, I		0.014
28.0	.001	.003	.004	.005	.007			ĺ			•		
27.5	.002	.003	.005	.007	.009		Co	orrected	Force	of Va	por	• =	0.417
27.0	.002	.004	.006	.008	.011		1	1		1			
26.5	.002	.005	.007	.010	.013							ı given	
26.0	.003	.006	.009	.012	.014							ove Psy at plac	
25.5	.003	.007	.010	.013	.016							constan	
												n the ta	
25.0	.003	.007	.011	.015	.018							rrection	
24.0	.004	.009	.013	.018	.022							differen	
23.0	.005	.010	.016	.021	.026							ng the	
22.0	.006	.012	.018	.024	.030							ing from	
21.0	.006	.014	.020	.027	.034	1				ean wil	ll little	impai	r the
20.0	+.007	+.015	+.023	+.030	+.038	acet	racy o	f the re	sults.				
			1	i									

### TABLE VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR FROM THE INDICATIONS, IN ENGLISH MEASURES, OF THE DEW-POINT INSTRUMENTS.

The object of every Dew-Point instrument is to ascertain, by causing a part of the apparatus to cool, the temperature at which the vapor contained in the air begins to condense, in the shape of light dew, on the cooled portion of the instrument. It is obvious that this is the temperature at which the atmosphere itself, if cooled likewise, would be fully saturated by the amount of vapor present in the air at the time of the observation.

The temperature of the dew-point being known, all the hygrometrical conditions of the air can be easily deduced from it.

The Absolute Humidity, or the total amount of vapor in the atmosphere, is expressed by the number, in the Tables of Elastic Forces of Vapor, due to that temperature.

The Relative Humidity, or the degree of moisture, being the ratio of the quantity of vapor actually contained in the air to the quantity it could contain if fully saturated, is expressed by the proportion

Relative Humidity: 1:: Force of Vapor at Dew-Point: Maximum Force of Vapor.

Calling the

Force of Vapor at the Temperature of the Dew-Point, f; Force of Vapor at the Temperature of the Air, F;

then

Relative Humidity =  $\frac{f}{F}$ .

It is thus found by dividing the force of vapor due, in the Table of Elastic Forces, to the temperature of the dew-point, by the maximum of the force of vapor due, in the same table, to the temperature of the air at the time of the observation. F being always greater than f, when the air is not saturated, the Relative Humidity is expressed by a fraction, which is termed the *fraction of saturation*. Making the point of saturation = 100, in order to obtain this fraction in hundredths, we have

Relative Humidity =  $\frac{f \times 100}{F}$ .

## Example.

# Suppose the

Temperature of the Air, or t, to be  $= 43^{\circ} \text{ F.}$ Temperature of the Dew-Point, or t', to be  $= 35^{\circ} \text{ F.}$ Difference between the two, or t - t', to be  $= 8^{\circ} \text{ F.}$ 

Taking in Table VI. the Elastic Forces due to t and t', we have

Force of Vapor at  $t' = \frac{.2037 \times 100}{.2775} = 73.4$ , Relative Humidity in Hundredths.

The following Table VIII. gives, in hundredths, the fraction of saturation, or Relative Humidity, corresponding to each degree of t', or of the temperature of the air, from 0° to 104°; and for every half degree of t—t', or of the difference between the temperature of the air and of the dew-point, from 0.°5 to 24.°5. Regnault's Table of Elastic Forces of Vapor, reduced to English measures, has been used in the computation.

Though the fraction of saturation expressed in hundredths indicates the Relative Humidity with sufficient accuracy, the thousandths have been added to facilitate, as remarked above in the preface to the Psychrometrical Tables, the interpolations for any number falling between those given in the table.

# USE OF THE TABLE.

# Example.

Temperature of Air, or t, being  $= 62^{\circ}$  F. Temperature of the Dew-Point, or t',  $= 53^{\circ}$  F. Difference, or t-t',  $= 9^{\circ}$  F.

Find out the Relative Humidity.

In the column of temperatures, the first on the left, find 62°; on the same horizontal line, in the column headed 9°, is found 72.4, which is the Relative Humidity required.

Should it seem desirable to compute the Relative Humidity for values of  $t-t^\prime$  not contained in the table, the factors given below in Table IX. may be used. It may be seen, however, that an interpolation at sight will always suffice for meteorological purposes.

# VIII.

# FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR,

FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS.

Relative Humidity expressed in Hundredths, full Saturation being = 100.

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Oifference o	f Temperat	tures of the	Air and o	f the Dew-	Point. — Fa	hrenheit.	
- Fahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
	100.	97.7	95.4	93.2	91.0	88.9	86.8	84.8	82.8	80.9
1	100.	97.7	95.5	93.3	91.1	89.0	86.9	84.9	82.9	81.0
2	100.	97.7	95.5	93.3	91.2	89.1	87.0	85.0	83.0	81.1
3	100.	97.8	95.5	93.4	91.2	89.2	87.1	85.1	83.1	81.2
4	100.	97.8	95.6	93.4	91.3	89.2	87.2	85.2	83.2	81.3
5	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.3	81.4
6	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.3	81.5
7	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.4	81.5
8	100.	97.8	95.6	93.5	91.3	89.3	87.3	85.3	83.4	81.5
9	100.	97.8	95.6	93.5	91.3	89.3	87.3	85.3	83.4	81.5
10	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.4	81.5
11	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.4	81.6
12	100.	97.8	95.5	93.4	91.3	89.3	87.3	85.4	83.4	81.6
13	100.	97.8	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.6
14	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.7
15	100.	97.7	95.5	93.4	91.3	89.4	87.4	85.5	83.5	81.7
16	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.6
17	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.3	83.4	81.6
18	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.3	83.4	81.5
19	100.	97.8	95.5	93.4	91.3	89.3	87.2	85.2	83.3	81.4
	0.0	0.5	1.0	1.5	2.0	2.5	3.0.	3.5	4.0	4.5

В

ature for Air, Fahren-heit.         5.0         5.5         6.0         6.5         7.0         7.5         8.0         8.5         9.0           0°         79.0         77.2         75.4         73.6         71.9         70.1         68.5         66.9         65.3           1         79.1         77.3         75.5         73.7         72.0         70.2         68.6         67.0         65.5           2         79.2         77.4         75.6         73.8         72.1         70.3         68.7         67.1         65.5           3         79.3         77.5         75.7         73.9         72.2         70.5         68.8         67.2         65.6           4         79.4         77.6         75.8         74.0         72.3         70.6         68.9         67.3         65.7           5         79.5         77.7         75.9         74.1         72.4         70.7         69.1         67.4         65.8           6         79.6         77.8         76.0         74.2         72.5         70.8         69.2         67.6         66.0           7         79.6         77.9         76.1         74.4         72.7	63.7 63.8 64.0 64.1 64.2 64.4 64.5 64.6 64.7 64.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	63.8 64.0 64.1 64.2 64.4 64.5 64.6 64.7 64.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	64.0 64.1 64.2 64.4 64.5 64.6 64.7 64.8
3         79.3         77.5         75.7         73.9         72.2         70.5         68.8         67.2         65.6           4         79.4         77.6         75.8         74.0         72.3         70.6         68.9         67.3         65.7           5         79.5         77.7         75.9         74.1         72.4         70.7         69.1         67.4         65.8           6         79.6         77.8         76.0         74.2         72.5         70.8         69.2         67.6         66.0           7         79.6         77.8         76.0         74.3         72.6         70.9         69.3         67.7         66.1           8         79.6         77.9         76.1         74.4         72.7         71.1         69.5         67.9         66.1           9         79.7         77.9         76.2         74.5         72.8         71.2         69.6         68.0         66.4           11         79.7         78.0         76.2         74.5         72.8         71.2         69.6         68.0         66.5           12         79.8         78.0         76.2         74.5         72.9         71.3	64.1 64.2 64.4 64.5 64.6 64.7 64.8
3     79.3     77.5     75.7     73.9     72.2     70.5     68.8     67.2     65.6       4     79.4     77.6     75.8     74.0     72.3     70.6     68.9     67.3     65.7       5     79.5     77.7     75.9     74.1     72.4     70.7     69.1     67.4     65.8       6     79.6     77.8     76.0     74.2     72.5     70.8     69.2     67.6     66.0       7     79.6     77.8     76.0     74.3     72.6     70.9     69.3     67.7     66.1       8     79.6     77.9     76.1     74.4     72.7     71.1     69.4     67.8     66.2       9     79.7     77.9     76.1     74.4     72.7     71.1     69.5     67.9     66.3       10     79.7     77.9     76.2     74.5     72.8     71.2     69.6     68.0     66.4       11     79.7     78.0     76.2     74.5     72.8     71.2     69.6     68.0     66.5       12     79.8     78.0     76.2     74.5     72.9     71.3     69.6     68.1     66.5       13     79.8     78.0     76.3     74.6     72.9	64.1 64.2 64.4 64.5 64.6 64.7 64.8
4       79.4       77.6       75.8       74.0       72.3       70.6       68.9       67.3       65.7         5       79.5       77.7       75.9       74.1       72.4       70.7       69.1       67.4       65.8         6       79.6       77.8       76.0       74.2       72.5       70.8       69.2       67.6       66.0         7       79.6       77.8       76.0       74.3       72.6       70.9       69.3       67.7       66.1         8       79.6       77.9       76.1       74.4       72.7       71.0       69.4       67.8       66.2         9       79.7       77.9       76.1       74.4       72.7       71.1       69.5       67.9       66.3         10       79.7       77.9       76.2       74.5       72.8       71.2       69.6       68.0       66.4         11       79.7       78.0       76.2       74.5       72.8       71.2       69.6       68.0       66.5         12       79.8       78.0       76.2       74.5       72.9       71.3       69.6       68.1       66.5         13       79.8       78.1       76.3	64.2 64.4 64.5 64.6 64.7 64.8 64.9
6       79.6       77.8       76.0       74.2       72.5       70.8       69.2       67.6       66.0         7       79.6       77.8       76.0       74.3       72.6       70.9       69.3       67.7       66.1         8       79.6       77.9       76.1       74.4       72.7       71.0       69.4       67.8       66.2         9       79.7       77.9       76.1       74.4       72.7       71.1       69.5       67.9       66.3         10       79.7       77.9       76.2       74.5       72.8       71.2       69.6       68.0       66.4         11       79.7       78.0       76.2       74.5       72.8       71.2       69.6       68.0       66.5         12       79.8       78.0       76.2       74.5       72.9       71.2       69.6       68.0       66.5         13       79.8       78.0       76.3       74.6       72.9       71.3       69.6       68.1       66.5         14       79.8       78.1       76.3       74.6       72.9       71.3       69.6       68.1       66.5         15       79.8       78.0       76.2 <td>64.5 64.6 64.7 64.8 64.9</td>	64.5 64.6 64.7 64.8 64.9
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19         79.6         77.8         76.0         74.3         72.7         71.1         69.5         68.0         66.4           10.0         10.5         11.0         11.5         12.0         12.5         13.0         13.5         14.0           0°         62.1         60.7         59.2         57.7         56.3         54.9         53.6         52.3         51.0           1         62.3         60.8         59.3         57.9         56.5         55.1         53.7         52.5         51.2           2         62.4         61.0         59.5         58.1         56.6         55.3         53.9         52.7         51.4           3         62.6         61.1         59.6         58.2         56.8         55.5         54.1         52.8         51.5	65.0
10.0         10.5         11.0         11.5         12.0         12.5         13.0         13.5         14.0           0°         62.1         60.7         59.2         57.7         56.3         54.9         53.6         52.3         51.0           1         62.3         60.8         59.3         57.9         56.5         55.1         53.7         52.5         51.2           2         62.4         61.0         59.5         58.1         56.6         55.3         53.9         52.7         51.4           3         62.6         61.1         59.6         58.2         56.8         55.5         54.1         52.8         51.5	65.0
0°   62.1   60.7   59.2   57.7   56.3   54.9   53.6   52.3   51.0   1   62.3   60.8   59.3   57.9   56.5   55.1   53.7   52.5   51.2   2   62.4   61.0   59.5   58.1   56.6   55.3   53.9   52.7   51.4   3   62.6   61.1   59.6   58.2   56.8   55.5   54.1   52.8   51.5	65.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	49.8
2     62.4     61.0     59.5     58.1     56.6     55.3     53.9     52.7     51.4       3     62.6     61.1     59.6     58.2     56.8     55.5     54.1     52.8     51.5	50.0
3   62.6   61.1   59.6   58.2   56.8   55.5   54.1   52.8   51.5	50.1
	50.3
	50.5
5 62.9 61.4 60.0 58.6 57.2 55.8 54.5 53.2 51.9	50.7
6 63.0 61.5 60.1 58.7 57.3 55.9 54.6 53.3 52.0	50.8
7 63.1 61.7 60.2 58.8 57.4 56.0 54.7 53.4 52.1	50.9
8   63.2   61.8   60.3   58.9   57.5   56.2   54.8   53.5   52.3	51.0
9 63.3 61.9 60.4 59.0 57.6 56.3 54.9 53.6 52.4	51.2
10 63.4 62.1 60.5 59.1 57.7 56.4 55.0 53.8 52.5	51.3
11 63.5 62.1 60.6 59.2 57.8 56.5 55.1 53.9 52.6	51.4
12   63.5   62.1   60.6   59.3   57.9   56.6   55.2   54.0   52.7	
13   63.5   62 2   60.7   59.3   58.0   56.6   55.3   54.1   52.8	51.5
14     63.6     62.3     60.8     59.4     58.1     56.7     55.4     54.2     52.9	51.5 51.6
15 63.6 62.3 60.8 59.5 58.1 56.8 55.5 54.3 53.0	
16     63.6     62.3     60.8     59.5     58.1     56.8     55.5     54.3     53.0	51.6
17   63.6   62.2   60.8   59.4   58.1   56.7   55.5   54.2   53.0	51.6 51.7
18   63.5   62.2   60.7   59.4   58.0   56.7   55.4   54.2   53.0	51.6 51.7 51.8
19   63.5   62.1   60.7   59.3   58.0   56.6   55.4   54.2   52.9	51.6 51.7 51.8 51.8

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	tures of the	Air and o	f the Dew-	Point. — Fa	ahrenheit.	
Fahren- heit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5
0°	48.5	47.3	46.1	45.0	43.9	42.8	41.6	40.6	39.5	38.5
1	48.7	47.5	46.3	45.2	44.0	42.9	41.8	40.8	39.7	38.7
2	48.9	47.7	46.5	45.4	44.2	43.1	42.0	41.0	39.9	38.9
3	49.1	47.9	46.7	45.5	44.4	43.3	42.2	41.2	40.2	39.2
4	49.3	48.1	46.9	45.7	44.6	43.5	42.4	41.4	40.4	39.4
5	49.4	48.2	47.1	45.9	44.8	43.7	42.6	41.6	40.6	39.6
6	49.6	48.4	47.2	46.1	44.9	43.9	42.8	41.8	40.7	39.S
7	49.7	48.5	47.3	46.2	45.1	44.0	42.9	41.9	40.9	39.9
8	49.8	48.7	47.5	46.4	45.3	44.2	43.1	42.1	41.1	40.1
9	50.0	48.8	47.6	46.5	45.4	44.3	43.3	42.2	41.2	40.2
10	50.1	48.9	47.8	46.7	45.6	44.5	43.4	42.4	41.4	40.4
11	50.2	49.0	47.9	46.8	45.7	44.6	43.5	42.5	41.5	40.5
12	50.3	49.1	48.0	46.9	45.8	44.7	43.6	42.6	41.6	40.6
13	50.4	49.2	48.1	47.0	45.9	44.8	43.7	42.7	41.7	40.7
14	50.5	49.3	48.2	47.1	46.0	44.9	43.8	42.8	41.8	40.8
15	50.6	49.4	48.3	47.2	46.1	45.0	43.9	42.9	41.9	40.9
16	50.6	49.5	48.3	47.2	46.1	45.0	44.0	43.0	41.9	41.0
17	50.6	49.5	48.3	47.2	46.1	45.0	44.0	43.0	42.0	41.0
18	50.6	49.5	48.3	47.2	46.2	45.0	44.1	43.1	42.0	41.1
19	50.6	49.5	48.3	47.3	46.2	45.1	44.1	43.1	42.1	41.1
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5
0°	37.5	36.5	35.5	34.6	33.7	32.8	31.9	31.0	30.2	29.3
1	37.7	36.8	35.8	34.8	33.9	33.0	32.1	31.3	30.4	29.6
2	37.9	37.0	36.0	35.1	34.2	33.3	32.4	31.5	30.7	29.9
3	38.2	37.2	36.2	35.3	34.4	33.5	32.6	31.8	30.9	30.1
-1	38.4	37.4	36.5	35.6	34.6	33.8	32.9	32.0	31.2	30.4
5	38.6	37.7	36.7	35.8	34.9	34.0	33.1	32.3	31.4	30.6
6	38.8	37.8	36.9	36.0	35.0	34.2	33.3	32.5	31.6	30.8
7	38.9	38.0	37.0	36.1	35.2	34.3	33.5	32.6	31.8	31.0
8	39.1	38.1	37.2	36.3	35.4	34.5	33.6	32.8	32.1	31.2
9	39.2	38.3	37.3	36.4	35.5	34.7	33.8	33.0	32.3	31.4
10	39.4	38.4	37.5	36.6	35.7	34.8	34.0	33.1	32.5	31.6
11	39.5	38.6	37.6	36.7	35.8	35.0	34.1	33.3	32.6	31.7
12	39.6	38.7	37.8	36.9	36.0	35.1	34.2	33.4	32.7	31.8
13 14	39.8 39.9	38.8 39.0	37.9 38.0	37.0 37.1	36.1 36.2	35.2 35.4	34.4 34.5	33.6 33.7	32.8 32.9	32.0 32.1
					20.4	05.5	34.7	33.9	99.0	22.0
15	40.0	39.1	38.9	37.3	36.1					
15 16	40.0	39.1 39.1	38.2 38.2	37.3	36.4	35.5 35.6		1	33.0 33.1	32.2
16	40.0	39.1	38.2	37.3	36.4	35.6	34.7	33.9	33.1	32.3
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Temper-		$\mathbf{t} - \mathbf{t}' = 1$	Difference	of Tempera	tures of th	e Air and	of the Dew-	-Point. — F	ahrenheit.	
of Air, Fahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
20°	100.	97.8	95.6	93.4	91.3	89.2	87.2	85.2	83.2	81.5
21	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.3	81.5
22	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.4	83.4	81.6
23	100.	97.8	95.6	93.5	91.4	89.4	87.4	85.5	83.5	81.
24	100.	97.8	95.7	93.5	91.5	89.5	87.5	85.5	83.6	81.8
25	100.	97.8	95.7	93.6	91.5	89.5	87.6	85.6	83.7	81.9
26	100.	97.8	95.7	93.6	91.6	89.6	87.7	85.7	83.8	82.0
27	100.	97.9	95.8	93.7	91.7	89.7	87.8	85.9	84.0	82.
28	100.	97.9	95.8	93.8	91.8	89.8	87.9	86.0	84.1	82.
29	100.	97.9	95.9	93.8	91.8	89.9	88.0	86.1	84.2	82.
30	100.	97.9	95.9	93.9	91.9	90.0	88.1	86.2	84.3	82.5
31	100.	98.0	96.0	94.0	92.0	90.1	88.2	86.4	84.5	82.
32	100.	98.0	96.0	94.0	92.1	90.2	88.4	86.6	84.7	83.0
33	100.	98.0-	96.1	94.1	92.2	90.4	88.6	86.7	84.9	83.2
34	100.	98.0	96.1	94.2	92.3	90.5	88.7	86.9	85.1	83.
35	100.	98.0	96.1	94.3	92.4	90.6	88.9	87.1	85.3	83.6
36	100.	98.1	96.2	94.3	92.5	90.7	88.9	87.1	85.4	83.7
37	100.	98.1	96.2	94.3	92.5	90.7	88.9	87.2	85.4	83.7
38	100.	98.1	96.2	94.3	92.5	90.7	89.0	87.2	85.5	83.8
39	100.	98.1	96.2	94.3	92.5	90.7	89.0	87.2	85.5	83.9
40	100.	98.1	96.2	94.4	92.5	90.8	89.0	87.3	85.6	83.9
41	100.	98.1	96.2	94.4	92.6	90.8	89.1	87.3	85.7	84.0
42	100.	98.1	96.2	94.4	92.6	90.8	89.1	87.4	85.7	84.1
43	100.	98.1	96.3	94.4	92.6	90.9	89.2	87.5	85.8	84.2
44	100.	98.1	96.3	94.5	92.7	90.9	89.2	87.5	85.9	84.2
45	100.	98.1	96.3	94.5	92.7	91.0	89.3	87.6	85.9	84.3
46	100.	98.1	96.3	94.5	92.7	91.0	89.3	87.6	86.0	84
47	100.	98.1	96.3	94.5	92.8	91.0	89.3	87.7	86.0	84.4
48	100.	98.2	96.3	94.6	92.8	91.1	89.4	87.7	86.1	84.4
49	100.	98.2	96.4	94.6	92.8	91.1	89.4	87.7	86.1	84.5
50	100.	98.2	96.4	94.6	92.9	91.1	89.4	87.8	86.2	84.5
51	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.8	86.2	84.6
52	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.9	86.3	84.7
53	100.	98.2	96.4	94.7	92.9	91.2	89.6	87.9	86.3	84.7
54	100.	98.2	96.4	94.7	93.0	91.3	89.6	88.0	86.4	84.8
55	100.	98.2	96.5	94.7	93.0	91.3	89.7	88.0	86.4	84.8
56	100.	98.2	96.5	94.7	93.0	91.4	89.7	88.1	86.5	84.9
57	100.	98.2	96.5	94.8	93.1	91.4	89.7	88.1	86.5	85.0
58	100.	98.2	96.5	94.8	93.1	91.4	89.8	88.2	86.6	85.0
59	100.	98.2	96.5	94.8	93.1	91.5	89.8	88.2	86.6	85.1
60	100.	98.2	96.5	94.8	93.2	91.5	89.9	88.3	86.7	85.1
61	100.	98.3	96.5	94.9	93.2	91.5	89.9	88.3	86.7	85.2
62	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.3
	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5

Temper-		$\mathbf{t} - \mathbf{t}' = 1$	Difference o	of Tempera	tures of th	e Air and	of the Dew-	Point. — F	ahrenheit.	
of Air,		1	1	1	1		1 4	1	1	
Fahreu- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
62°	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.3
63	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.3
64	100.	98.3	96.6	94.9	93.3	91.6	90.0	88.5	86.9	85.3
65	100.	98.3	96.6	94.9	93.3	91.7	90.1	88.5	86.9	85.4
66	100.	98.3	96.6	94.9	93.3	91.7	90.1	88.5	87.0	85.4
67	100.	98.3	96.6	95.0	93.3	91.7	90.1	88.6	87.0	85.5
68	100.	98.3	96.6	95.0	93.4	91.8	90.2	88.6	87.1	85.5
69	100.	98.3	96.6	95.0	93.4	91.8	90.2	88.7	87.2	85.6
70	100.	98.3	96.7	95.0	93.4	91.8	90.3	88.7	87.2	85.7
71	100.	98.3	96.7	95.0	93.4	91.9	90.3	88.8	87.2	85.S
72	100.	98.3	96.7	95.1	93.5	91.9	90.3	88.8	87.3	85.8
<b>7</b> 3	100.	98.3	96.7	95.1	93.5	91.9	90.4	88.8	87.3	85.9
74	100.	98.3	96.7	95.1	93.5	91.9	90.4	88.9	87.4	85.9
75	100.	98.3	96.7	95.1	93.5	92.0	90.4	88.9	87.4	86.0
76	100.	98.3	96.7	95.1	93.6	92.0	90.5	89.0	87.5	86.0
77	100.	98.4	96.7	95.2	93.6	92.0	90.5	89.0	87.5	86.1
78	100.	98.4	96.7	95.2	93.6	92.1	90.5	89.1	87.6	86.1
79	100.	93.4	96.8	95.2	93.6	92.1	90.6	89.1	87.6	86.2
80	100.	98.4	96.8	95.2	93.6	92.1	90.6	89.1	87.7	86 2
81	100.	98.4	96.8	95.2	93.7	92.1	90.6	89.2	87.7	86.3
82	100.	98.4	96.8	95.2	93.7	92.2	90.7	89.2	87.8	86.3
83	100.	98.4	96.8	95.3	93.7	92.2	90.7	89.3	87.8	86.4
84	100.	98.4	96.8	95.3	93.7	92.2	90.8	89.3	87.8	86.4
85	100.	98.4	96.8	95.3	93.8	92.3	90.8	89.3	87.9	86.5
86	100.	98.4	96.8	95.3	93.8	92.3	90.8	89.4	87.9	86.5
87	100.	98.4	96.9	95.3	93.8	92.3	90.9	89.4	88.0	86.6
88	100.	98.4	96.9	95.3	93.8	92.3	90.9	89.4	88.0	86.6
89	100.	98.4	96.9	95.4	93.9	92.4	90.9	89.5	88.1	86.7
90	100.	98.4	96.9	95.4	93.9	92.4	91.0	89.5	88.1	86.7
91	100.	98.4	96.9	95.4	93.9	92.4	91.0	89.6	88.2	86.8
92	100.	98.5	96.9	95.4	93.9	92.5	91.0	89.6	88.2	86.8
93	100.	98.5	96.9	95.4	93.9	92.5	91.1	89.6	88.2	86.9
94	100.	98.5	96.9	95.4	94.0	92.5	91.1	89.7	88.3	86.9
95	100.	98.5	97.0	95.5	94.0	92.5	91.1	89.7	88.3	87.0
96	100.	98.5	97.0	95.5	94.0	92.6	91.2	89.7	88.4	87.0
97	100.	98.5	97.0	95.5	94.0	92.6	91.2	89.8	88.4	87.0
98	100.	98.5	97.0	95.5	94.1	92.6	91.2	89.8	88.4	87.1
99	100.	98.5	97.0	95.5	94.1	92.7	91.3	89.9	88.5	87.1
100	100.	98.5	97.0	95.6	94.1	92.7	91.3	89.9	88.5	87.2
101	100.	98.5	97.0	95.6	94.1	92.7	91.3	89.9	\$8.6	87.2
102	100.	98.5	97.0	95.6	94.2	92.7	91.4	90.0	88.6	87.3
103	100.	98.5	97.0	95.6	94.2	92.8	91.4	90.0	88.7	87.3
104	100.	98.5	97.0	95.6	94.2	92.8	91.4	90.0	88.7	87.4
	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5

Temper-		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	ifference o	f Temperat	cures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
20°	79.5	77.7	75.9	74.2	72.6	71.0	69.4	67.9	66.4	64.9
21	79.6	77.8	76.0	74.3	72.7	71.1	69.5	68.0	66.4	65.0
22	79.7	77.9	76.1	74.4	72.8	71.2	69.6	68.0	66.5	65.0
23	79.8	78.0	76.2	74.6	72.9	71.3	69.6	68.1	66.5	65.0
24	79.9	78.1	76.4	74.7	73.0	71.4	69.7	68.1	66.6	65.1
25	80.0	78.2	76.5	74.8	73.1	71.5	69.8	68.2	66.6	65.1
26	80.2	78.4	76.6	74.9	73.2	71.7	70.0	68.4	66.8	65.3
27	80.3	78.5	76.8	75.1	73.4	71.8	70.1	68.6	67.0	65.5
28	80.5	78.7	76.9	75.2	73.6	72.0	70.3	68.8	67.2	65.7
29	80.6	78.8	77.1	75.4	73.7	72.1	70.5	68.9	67.4	65.9
30	80.7	78.9	77.2	75.6	73.9	72.3	70.7	69.1	67.6	66.1
31	81.0	79.2	77.5	75.8	74.2	72.6	71.0	69.4	67.9	66.4
32	81.2	79.4	77.7	76.1	74.4	72.8	71.3	69.7	68.2	66.7
33	81.4	79.7	78.0	76.4	74.7	73.1	71.5	70.0	68.5	67.0
34	81.7	79.9	78.3	76.6	75.0	73.4	71.8	70.3	68.8	67.3
35	81.9	80.2	78.5	76.9	75.3	73.7	72.1	70.6	69.1	67.6
36	82.0	80.3	78.6	77.0	75.4	73.9	72.3	70.8	69.3	67.8
37	82.0	80.4	78.8	77.2	75.6	74.0	72.5	71.0	69.5	68.1
38	82.1	80.5	78.9	77.3	75.8	74.2	72.7	71.2	69.8	68.3
39	82.2	80.6	79.0	77.4	75.9	74.4	72.9	71.5	70.0	68.6
40	82.3	80.7	79.1	77.6	76.1	74.6	73.2	71.7	70.2	68.8
41	82.4	80.8	79.2	77.7	76.2	74.7	73.2	71.8	70.3	68.9
42	82.5	80.9	79.3	77.8	76.3	74.8	73.3	71.9	70.5	69.0
43	82.5	80.9	79.4	77.9	76.4	74.9	73.4	72.0	70.6	69.2
44	82.6	81.0	79.5	78.0	76.5	75.0	73.5	72.1	70.7	69.3
45	82.7	81.1	79.6	78.0	76.5	75.1	73.6	72.2	70.8	69.4
46	82.8	81.2	79.6	78.1	76.6	75.1	73.7	72.3	70.9	69.5
47	82.8	81.2	79.7	78.2	76.7	75.2	73.8	72.4	71.0	69.6
48	82.9	81.3	79.8	78.2	76.8	75.3	73.9	72.5	71.1	69.7
49	82.9	81.3	79.8	78.3	76.8	75.4	74.0	72.6	71.2	69.8
50	83.0	81.4	79.9	78.4	76.9	75.5	74.0	72.7	71.3	69.9
51	83.0	81.5	80.0	78.5	77.0	75.5	74.1	72.8	71.4	70.0
52	83.1	81.5	80.0	78.5	77.1	75.6	74.2	72.8	71.5	70.1
53	83.2	81.6	80.1	78.6	77.2	75.7	74.3	72.9	71.6	70.2
54	83.2	81.7	80.2	78.7	77.2	75.8	74.4	73.0	71.7	70.3
55	83.3	81.8	80.3	78.8	77.3	75.9	74.5	73.1	71.8	70.4
56	83.4	81.8	80.3	78.9	77.4	76.0	74.6	73.2	71.9	70.5
57	83.4	81.9	80.4	78.9	77.5	76.1	74.7	73.3	72.0	70.6
58	83.5	82.0	80.5	79.0	77.6	76.2	74.8	73.4	72.1	70.7
59	83.6	82.0	80.6	79.1	77.7	76.2	74.9	73.5	72.2	70.9
60	83.6	82.1	80.6	79.2	77.7	76.3	75.0	73.6	72.3	71.0
61 62	S3.7 S3.7	82.2 82.2	80.7 80.8	79.2 79.3	77.8	76.4 76.5	75.0 75.1	73.7 73.8	72.4 72.4	71.0

Temper-		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Tempera	tures of th	e Air and o	of the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
62°	83.7	82.2	80.8	79.3	77.9	76.5	75.1	73.8	72.4	71.1
63	83.8	82.3	80.8	79.4	78.0	76.6	75.2	73.9	72.5	71.2
64	83.9	82.4	80.9	79.5	78.1	76.7	75.3	74.0	72.6	71.3
65	83.9	82.4	81.0	79.6	78.1	76.8	75.4	74.0	72.7	71.4
66	84.0	82.5	81.1	79.6	78.2	76.8	75.5	74.1	72.8	71.5
67	84.0	82.6	81.1	79.7	78.3	76.9	75.6	74.2	72.9	71.6
68	84.1	82.6	81.2	79.8	78.4	77.0	75.7	74.3	73.0	71.7
69	84.2	82.7	81.3	79.9	78.5	77.1	75.7	74.4	73.1	71.8
70	84.2	82.8	81.3	79.9	78.5	77.2	75.8	74.5	73.2	71.9
71	84.3	82.8	81.4	80.0	78.6	77.3	75.9	74.6	73.3	72.0
72	84.3	82.9	81.5	80.1	78.7	77.3	76.0	74.7	73.4	72.1
73	84.4	83.0	81.5	80.1	78.7	77.4	76.1	74.8	73.5	72.2
74	84.5	83.0	81.6	80.2	78.8	77.5	76.2	74.9	73.6	72.3
75	84.5	83.1	81.7	80.3	78.9	77.6	76.2	74.9	73.7	72.4
76	84.6	83.1	81.7	80.4	78.9	77.7	76.3	75.0	73.7	72.5
77	84.6	83.2	81.8	80.4	79.0	77.7	76.4	75.1	73.8	72.6
78	84.7	83.3	81.9	80.5	79.1	77.8	76.5	75.2	73.9	72.7
79	84.7	83.3	81.9	80.6	79.1	77.9	76.6	75.3	74.0	72.8
80	84.8	83.4	82.0	80.6	79.2	78.0	76.7	75.4	74.1	72.9
81	84.9	83.5	82.1	80.7	79.3	78.0	76.7	75.5	74.2	73.0
82	84.9	83.5	82.1	80.8	79.4	78.1	76.8	75.5	74.3	73.0
83	85.0	83.6	82.2	80.8	79.4	78.2	76.9	75.6	74.4	73.1
84	85.0	83.6	82.3	80.9	79.5	78.3	77.0	75.7	74.5	73.2
85	85.1	83.7	82.3	81.0	79.6	78.4	77.1	75.8	74.6	73.3
86	85.1	83.7	82.4	81.1	79.7	78.4	77.1	75.9	74.6	73.4
87	85.2	83.8	82.5	81.1	79.8	78.5	77.2	76.0	74.7	73.5
88	85.2	83.9	82.5	81.2	79.9	78.6	77.3	76.1	74.8	73.6
89	85.3	83.9	82.6	81.3	79.9	78.7	77.4	76.1	74.9	73.7
90	85.3	84.0	82.6	81.3	80.0	78.7	77.5	76.2	75.0	73.8
91	85.4	84.0	82.7	81.4	80.1	78.8	77.5	76.3	75.1	73.9
92	85.4	84.1	82.8	81.5	80.2	78.9	77.6	76.4	75.2	74.0
93	85.5	84.2	82.8	81.5	80.2	79.0	77.7	76.5	75.2	74.0
94	85.6	84.2	82.9	81.6	80.3	79.0	77.8	76.6	75.3	74.1
95	85.6	84.3	83.0	81.7	80.4	79.1	77.9	76.6	75.4	74.2
96	85.7	84.3	83.0	81.7	80.4	79.2	77.9	76.7	75.5	74.3
97	85.7	84.4	83.1	81.8	80.5	79.3	78.0	76.8	75.6	74.4
93	85.8	84.4	83.1	81.9	80.6	79.3	78.1	76.9	75.7	74.5
99	85.8	84.5	83.2	81.9	80.7	79.4	78.2	77.0	75.8	74.6
100	85.9	84.6	83.3	82.0	80.7	79.5	78.3	77.0	75.8	74.7
101	85.9	84.6	83.3	82.0	80.8	79.6	78.3	77.1	75.9	74.8
102	86.0	84.7	83.4	82.1	80.9	79.6	78.4	77.2	76.0	74.9
103	86.0	84.7	83.4	82.2	80.9	79.7	78.5	77.3	76.1	74.9
104	86.1	84.8	83.5	82.2	81.0	79.8	78.6	77.4	76.2	75.0
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5

Temper-		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	ures of the	e Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.6
20°	63.5	62.1	60.6	59.3	58.0	56.6	55.4	54.1	52.9	51.7
21	63.5	62.1	60.7	59.3	58.0	56.6	55.4	54.2	53.0	51.8
22	63.5	62.1	60.7	59.4	58.0	56.7	55.5	54.2	53.0	51.8
23	63.6	62.1	60.7	59.4	58.0	56.7	55.5	54.3	53.0	51.9
24	63.6	62.1	60.7	59.4	58.1	56.8	55.5	54.3	53.1	51.9
25	63.6	62.1	60.7	59.4	58.1	56.8	55.6	54.4	53.1	52.0
26	63.8	62.3	60.9	59.6	58.3	57.0	55.7	54.5	53.3	52.1
27	64.0	62.5	61.1	59.8	58.5	57.2	55.9	54.6	53.4	52.2
28	64.2	62.7	61.3	60.0	58.6	57.3	56.0	54.8	53.5	52.3
29	64.4	63.0	61.5	60.2	58.8	57.5	56.2	54.9	53.7	52.4
30	64.6	63.2	61.8	60.4	59.0	57.7	56.3	55.1	53.8	52.6
31	64.9	63.5	62.1	60.7	59.3	58.0	56.6	55.4	54.1	52.9
32	65.2	63.8	62.4	61.0	59.6	58.3	57.0	55.7	54.4	53.2
33	65.5	64.1	62.7	61.3	59.9	58.6	57.3	56.0	54.7	53.5
34	65.8	64.4	63.0	61.6	60.2	58.9	57.6	56.3	55.0	53.8
35	66.1	64.7	63.3	61.9	60.5	59.2	57.9	56.6	55.4	54.1
36	66.4	64.9	63.5	62.1	60.8	59.5	58.2	56.9	55.6	54.4
37	66.6	65.2	63.8	62.4	61.1	59.8	58.5	57.2	55.9	54.7
	66.9	65.5	64.1	62.7	61.4	60.1	58.8	57.5	56.2	55.0
38 39	67.1	65.7	64.4	63.0	61.7	60.3	59.1	57.8	56.5	55.3
40	67.4	66.0	64.6	63.3	62.0	60.6	59.4	58.1	56.8	55.6
41	67.5	66.1	64.8	63.5	62.1	60.9	59.6	58.3	57.1	55.9
	67.7	66.3	65.0	63.6	62.3	61.1	59.8	58.6	57.3	56.1
42	67.8	66.4	65.1	63.8	62.5	61.3	60.0	58.8	57.6	56.1
43 44	67.9	66.6	65.3	64.0	62.7	61.5	60.3	59.0	57.8	56.6
	68.1	66.7	65.4	64.2	62.9	61.7	60.5	59.3	58.1	56.9
45	63.2	66 9	65.6	64.3	63.0	61.8	60.6	59.4	58.2	57.0
46	1				63.2	61.9	60.7	59.5	58.3	57.2
47	68.3	67.0	65.7	64.4		62.0	60.8		58.5	
48	68.4	67.1	65.S	64.5	63.3			59.6		57.3
49 50	68.5 68.6	$67.2 \\ 67.3$	65.9 66.0	61.6 64.7	$63.4 \\ 63.5$	$\begin{array}{c} 62.1 \\ 62.2 \end{array}$	61.0 61.1	59.8 59.9	58.6 58.7	57.4 57.6
	68.7	67.4	66.1	64.9	63.6	62.4	61.2	60.0	58.9	57.7
51	63.8	67.5	66.2	65.0	63.7	62.5	61.3	60.1	59.0	57.8
52	68.9	67.6	66.4	65.1	63.9	62.6	61.4	60.3	59.1	58.0
53			1	65.2	64.0	62.7	61.6	60.4	59.1	58.1
54	69.0	67.7	66.5	65.3					59.4	58.2
55 56	69.1 69.2	67.8 67.9	66.6 66.7	65.4	64.1 64.2	62.9 63.0	61.7 61.8	60.5 60.6	59.4	58.4
1										58.5
57	69.3	68.1	66.8	65.6	64.3	63.1	61.9 62.1	60.8 60.9	59.6 59.8	58.6
58	69.5	68.2	66.9	65.7	61.4	63.2				58 8
59	69.6	68.3	67.0	65.8	64.6	63.4	62.2	61.0	59.9	
60	69.7	68.4	67.1	65.9	64.7	63.5	62.3	61.2 61.3	60.0	58.9 59.0
61 62	69.8 69.9	68.5 68.6	67.2 67.4	66.0 66.1	64.8 64.9	63.6 63.7	62.4 62.6	61.4	60.1 60.3	59.0
	10.0		11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}^{\dagger} = \mathbf{I}$	Difference o	f Temperat	ures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5
62°	69.9	68.6	67.4	66.1	64.9	63.7	62.6	61.4	60.3	59.1
63	70.0	68.7	67.5	66.2	65.0	63.8	62.7	61.5	60.4	59.3
64	70.1	68.8	67.6	66.3	65.1	64.0	62.8	61.6	60.5	59.4
65	70.2	68.9	67.7	66.5	65.3	64.1	62.9	61.8	60.6	59.5
66	70.3	69.0	67.8	66.6	65.4	64.2	63.0	61.9	60.8	59.7
67	70.4	69.1	67.9	66.7	65.5	64.3	63.2	62.0	60.9	59.8
68	70.5	69.2	68.0	66.8	65.6	64.4	63.3	62.1	61.0	59.9
69	70.6	69.3	68.1	66.9	65.7	64.5	63.4	62.3	61.1	60.0
70	70.7	69.4	68.2	67.0	65.8	64.7	63.5	62.4	61.3	60.2
71	70.8	69.5	68.3	67.1	65.9	64.8	63.6	62.5	61.4	60.3
72	70.9	69.6	68.4	67.2	66.0	64.9	63.7	62.6	61.5	60.4
73	71.0	69.7	68.5	67.3	66.2	65.0	63.9	62.7	61.6	60.5
74	71.1	69.8	68.6	67.4	66.3	65.1	64.0	62.8	61.7	60.7
75	71.1	69.9	68.7	67.5	66.4	65.2	64.1	63.0	61.9	60.8
76	71.2	70.0	68.8	67.6	66.5	65.3	64.2	63.1	62.0	60.9
77	71.3	70.1	68.9	67.8	66.6	65.5	64.3	63.2	62.1	61.0
78	71.4	70.2	69.0	67.9	66.7	65.6	64.4	63.3	62.2	61.1
79	71.5	70.3	69.1	68.0	66.8	65.7	64.5	63.4	62.3	61.3
80	71.6	70.4	69.2	68.1	66.9	65.8	64.7	63.6	62.5	61.4
81	71.7	70.5	69.3	68.2	67.0	65.9	64.8	63.7	62.6	61.5
82	71.8	70.6	69.4	68.3	67.1	66.0	64.9	63.8	62.7	61.6
83	71.9	70.7	69.5	68.4	67.2	66.1	65.0	63.9	62.8	61.8
84	72.0	70.8	69.6	68.5	67.3	66.2	65.1	64.0	62.9	61.9
85	72.1	70.9	69.7	68.6	67.4	66.3	65.2	64.1	63.0	62.0
86	72.2	71.0	69.8	68.7	67.5	66.4	65.3	64.2	63.2	62.1
-87	72.3	71.1	69.9	68.8	67.7	66.5	65.4	64.4	63.3	62.2
88	72.4	71.2	70.0	68.9	67.8	66.6	65.5	64.5	63.4	62.3
89	72.5	71.3	70.1	69.0	67.9	66.8	65.7	64.6	63.5	62.5
90	72.6	71.4	70.2	69.1	68.0	66.9	65.8	64.7	63.6	62.6
91	72.7	71.4	70.3	69.2	68.1	67.0	65.9	64.8	63.7	62.7
92	72.8	71.5	70.4	69.3	68.2	67.1	66.0	64.9	63.9	62.8
93	72.9	71.6	70.5	69.4	68.3	67.2	66.1	65.0	64.0	62.9
94	72.9	71.7	70.6	69.5	68.4	67.3	66.2	65.1	64.1	63.0
95	73.0	71.8	70.7	69.6	68.5	67.4	66.3	65.2	64.2	63.2
96	73.1	71.9	70.8	69.7	68.6	67.5	66.4	65.4	64.3	63.3
97	73.2	72.0	70.9	69.8	68.7	67.6	66.5	65.5	64.4	63.4
98	73.3	72.1	71.0	69.9	68.8	67.7	66.6	65.6	64.5	63.5
99	73.4	72.3	71.1	70.0	68.9	67.8	66.7	65.7	64.6	63.6
100	73.5	72.4	71.2	70.1	69.0	67.9	66.8	65.8	64.8	63 <b>.7</b>
101	73.6	72.5	71.3	70.2	69.1	68.0	67.0	65.9	64.9	63.9
102	73.7	72.6	71.4	70.3	69.2	68.1	67.1	66.0	65.0	64.0
103 104	73.8 73.9	72.7 72.8	71.5 71.6	70.4 70.5	69.3 69.4	68.2 68.3	67.2 67.3	66.1 66.2	65.1 65.2	$64.1 \\ 64.2$
	10.0	10.5	11.0	11.5	12.0		13.0	13.5	14.0	14.5
R	20.0	1010	11.0	11.0	02	12.5	10.0	20.0	22.0	R-R-O

20°         50.6         49.5         48.4         47.3         46.2         45.1         44.1         43.1         42.1         41.2           21         50.6         49.5         48.4         47.3         46.2         45.1         44.2         43.2         42.2         41.2           22         50.7         49.6         48.5         47.4         46.3         45.2         44.2         43.3         42.3         41.2           24         50.7         49.6         48.5         47.4         46.3         45.2         44.2         43.3         42.3         41.3           25         50.8         49.7         48.5         47.5         46.4         45.4         44.3         43.3         42.4         41.2           26         50.9         49.9         48.6         47.6         46.5         45.5         44.4         43.3         42.4         41.2           27         51.0         50.1         48.8         47.7         46.6         45.5         44.6         43.6         42.6         41.4           29         51.2         50.1         48.9         47.8         46.8         45.8         44.7         43.7         42.7	Temper-		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	ures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
21         50.6         49.5         48.4         47.3         46.2         45.1         44.2         43.2         42.2         41.2           23         50.7         49.6         48.5         47.4         46.3         45.2         44.2         43.2         42.2         41.2           24         50.7         49.6         48.5         47.4         46.4         45.3         44.2         43.3         42.3         41.2           25         50.8         49.7         48.6         47.5         46.4         45.4         44.3         43.3         42.3         41.2           26         50.9         49.5         48.6         47.6         46.5         45.4         44.4         43.4         42.4         44.1           27         51.0         49.9         48.8         47.7         46.6         45.5         44.6         43.6         42.6         41.4           29         51.2         50.1         48.9         47.8         46.8         45.7         44.7         43.7         42.7         41.5           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.2         47.1	Fahren-	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.3
22         50.7         49.5         48.4         47.4         46.3         45.2         44.2         43.2         42.2         41.2           24         50.7         49.6         48.5         47.4         46.3         45.2         44.2         43.3         42.3         41.2           25         50.8         49.7         48.6         47.6         46.5         45.4         44.3         43.3         42.3         41.2           26         50.9         49.9         48.7         47.7         46.6         45.5         44.5         43.4         42.4         41.4           27         51.0         49.9         48.7         47.7         46.6         45.5         44.5         43.6         42.6         41.4           29         51.2         50.1         48.9         47.8         46.8         45.7         44.6         43.6         42.6         41.6           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.8           31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.3	20°	50.6	49.5	48.4	47.3	46.2	45.1	44.1	43.1	42.1	41.2
23         50.7         49.6         48.5         47.4         46.3         45.2         44.2         43.3         42.3         41.2           24         50.7         49.6         48.5         47.4         46.4         45.3         44.3         43.3         42.3         41.           25         50.8         49.7         48.6         47.6         46.5         45.4         44.4         43.4         42.4         41.4           26         50.9         49.8         48.6         47.6         46.5         45.4         44.4         43.4         42.4         41.4           27         51.0         49.9         48.8         47.7         46.6         45.5         44.6         43.6         42.6         41.4           29         51.2         50.1         48.9         47.8         46.8         45.7         44.7         43.7         42.7         41.3           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.3           31         51.7         50.6         49.1         48.0         46.9         45.9         44.8         43.8         42.2     <	21	50.6	49.5	48.4	47.3	46.2	45.1	44.2	43.2	42.2	41.2
24         50.7         49.6         48.5         47.4         46.4         45.3         44.3         43.3         42.3         41.           26         50.9         49.8         48.6         47.6         46.5         45.4         44.1         43.4         42.4         41.4           27         51.0         49.9         48.7         47.7         46.6         45.5         44.5         43.5         42.5         41.4           29         51.2         50.1         48.9         47.8         46.8         45.7         44.7         43.6         42.6         41.4           29         51.2         50.1         48.9         47.8         46.8         45.7         44.7         43.7         42.7         41.5           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.8           31         51.7         50.5         49.4         48.5         47.1         46.1         45.0         44.0         43.3         42.2           31         52.6         51.4         50.3         49.1         48.0         46.9         45.9         44.8         43.3	22	50.7	49.5	48.4	47.4	46.3	45.2	44.2	43.2	42.2	41.3
25         50.8         49.7         48.5         47.5         46.4         45.4         44.3         43.3         42.4         41.2           26         50.9         49.9         48.6         47.6         46.5         45.4         44.4         43.4         42.4         41.4           27         51.0         49.9         48.7         47.7         46.6         45.5         44.5         43.6         42.6         41.4           29         51.2         50.1         48.8         47.7         46.7         45.6         44.6         43.6         42.6         41.4           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.3           31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.0         42.7         41.3           32         52.0         50.8         49.7         48.5         47.4         46.4         45.3         44.3         43.3         42.8           33         52.6         51.7         50.6         49.4         48.3         47.2         46.1         45.1	23	50.7	49.6	48.5	47.4	46.3	45.2	44.2	43.3	42.3	41.3
26         50.9         49.8         48.6         47.6         46.5         45.4         44.4         43.4         42.4         41.1           27         51.0         49.9         48.7         47.7         46.6         45.5         44.5         43.5         42.5         41.4           29         51.2         50.1         48.8         47.7         46.7         45.6         44.6         43.6         42.6         41.4           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.3           31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.0         42.0           32         52.0         50.8         49.7         48.5         47.4         46.4         45.3         44.3         43.3         42.5           33         52.3         51.1         50.0         48.8         47.7         46.6         45.6         44.5         43.5         42.5           34         52.6         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1	24	50.7	49.6	48.5	47.4	46.4	45.3	44.3	43.3	42.3	41.4
27         51.0         49.9         48.7         47.7         46.6         45.5         44.5         43.5         42.5         41.6           29         51.2         50.1         48.9         47.8         46.8         45.7         44.7         43.7         42.7         41.3           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.3           31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.0         42.2           32         52.0         50.8         49.7         48.5         47.4         46.4         45.3         44.3         43.3         42.3           33         52.3         51.1         50.0         48.8         47.7         46.6         45.6         44.5         43.5         42.5           34         52.6         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.6           35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1	25	50.8	49.7	48.5	47.5	46.4	45.4	44.3	43.3	42.4	41.4
28         51.1         50.0         48.8         47.7         46.7         45.6         44.6         43.6         42.6         41.6           29         51.2         50.1         48.9         47.8         46.8         45.7         44.7         43.7         42.7         41.7           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.8           31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.0         42.0           32         52.0         50.8         49.7         48.5         47.7         46.6         45.6         44.3         43.3         42.2           34         52.6         51.1         50.0         48.8         47.7         46.6         45.6         44.5         44.3         43.5         42.2           35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.6           36         53.2         52.0         50.9         49.7         48.6         47.5         46.1         45.1	26	50.9	49.8	48.6	47.6	46.5	45.4	44.4 •	43.4	42.4	41.5
29         51.2         50.1         48.9         47.8         46.8         45.7         44.7         43.7         42.7         41.7           30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.8           31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.0         42.6           32         52.0         50.8         49.7         48.5         47.7         46.6         45.6         44.5         43.3         42.6           34         52.6         51.4         50.0         48.8         47.7         46.6         45.6         44.5         43.5         42.6           35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.5           36         53.2         52.0         50.9         49.7         48.6         47.5         46.4         45.4         44.4         43.3           37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.1	27	51.0	49.9	48.7	47.7	46.6	45.5	44.5	43.5	42.5	41.6
30         51.4         50.2         49.0         47.9         46.8         45.8         44.7         43.7         42.7         41.8           31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.0         42.0           32         52.0         50.8         49.7         48.5         47.4         46.4         45.3         44.3         43.3         42.3           33         52.3         51.1         50.0         48.8         47.7         46.6         45.6         44.5         43.5         42.8           34         52.6         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.8           35         52.9         51.7         50.6         49.7         48.6         47.5         46.1         45.1         44.1         43.3           36         53.2         52.0         50.9         49.7         48.6         47.5         46.1         45.1         44.1         43.5           37         53.5         52.3         51.2         50.0         48.9         47.8         46.1         45.1         44.7	28	51.1	50.0	48.8	47.7	46.7	45.6	44.6	43.6	42.6	41.6
31         51.7         50.5         49.4         48.2         47.1         46.1         45.0         44.0         43.0         42.1           32         52.0         50.8         49.7         48.5         47.4         46.4         45.3         44.3         43.3         42.3           34         52.6         51.4         50.3         49.1         48.0         46.9         45.9         44.8         43.8         42.8           35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.6           36         53.2         52.0         50.9         49.7         48.6         47.5         46.4         45.1         44.1         43.6           37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.6         45.7         44.7         48.6           38         53.8         52.6         51.5         50.3         49.2         48.1         47.0         46.0         45.7         44.6           40         54.1         52.9         51.8         50.6         49.5         48.4         47.3	29	51.2	50.1	48.9	47.8	46.8	45.7	44.7	43.7	42.7	41.7
32         52.0         50.8         49.7         48.5         47.4         46.4         45.3         44.3         43.3         42.3           33         52.3         51.1         50.0         48.8         47.7         46.6         45.6         44.5         43.5         42.8           34         52.6         51.4         50.3         49.1         48.0         46.9         45.9         44.8         43.8         42.8           35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.6           36         53.2         52.0         50.9         49.7         48.6         47.5         46.7         45.7         44.7         48.6           37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.7         48.6           39         54.1         52.9         51.8         50.6         49.5         48.4         47.0         46.0         45.7         44.6           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6	30	51.4	50.2	49.0	47.9	46.8	45.8	44.7	43.7	42.7	41.8
33         52.3         51.1         50.0         48.8         47.7         46.6         45.6         44.5         43.5         42.8           34         52.6         51.4         50.3         49.1         48.0         46.9         45.9         44.8         43.8         42.8           35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.6           36         53.2         52.0         50.9         49.7         48.6         47.5         46.4         45.4         44.4         43.3           37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.4         43.3           39         54.1         52.9         51.8         50.6         49.5         48.4         47.3         46.3         45.3         44.2           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.5           41         54.7         53.8         52.6         51.5         50.1         49.0         47.9         46.1         45.1	31	51.7	50.5	49.4	48.2	47.1	46.1	45.0	44.0	43.0	42.0
34         52.6         51.4         50.3         49.1         48.0         46.9         45.9         44.8         43.8         42.8           35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.6           36         53.2         52.0         50.9         49.7         48.6         47.5         46.4         45.4         44.4         43.3           37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.7         43.6           38         53.8         52.6         51.5         50.3         49.2         48.1         47.0         46.0         45.0         43.8           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.5           41         54.7         53.5         52.3         51.2         50.1         49.0         47.9         46.9         45.8         44.8           41         54.7         53.8         52.6         51.5         50.4         49.3         48.2         47.2         46.1	32	52.0	50.8	49.7	48.5	47.4	46.4	45.3	44.3	43.3	42.3
35         52.9         51.7         50.6         49.4         48.3         47.2         46.1         45.1         44.1         43.3           36         53.2         52.0         50.9         49.7         48.6         47.5         46.4         45.4         44.4         43.3           37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.7         43.6           38         53.8         52.6         51.5         50.3         49.2         48.1         47.0         46.0         45.0         43.5           39         54.1         52.9         51.8         50.6         49.5         48.4         47.3         46.3         45.3         44.2           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.5           41         54.7         53.5         52.3         51.2         50.1         49.0         47.9         46.9         45.8         44.5           41         54.7         53.8         52.6         51.5         50.4         49.3         48.2         47.2         46.1	33	52.3	51.1	50.0	48.8	47.7	46.6	45.6	44.5	43.5	42.5
36         53.2         52.0         50.9         49.7         48.6         47.5         46.4         45.4         44.4         43.3           37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.7         43.6           38         53.8         52.6         51.5         50.3         49.2         48.1         47.0         46.0         45.0         43.5           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.5           41         54.7         53.5         52.3         51.2         50.1         49.0         47.9         46.9         45.8         44.8           42         54.9         53.8         52.6         51.5         50.4         49.3         48.2         47.2         46.1         45.8           44         55.5         54.3         53.2         52.1         50.9         49.6         48.5         47.5         46.4         45.4           44         55.5         54.3         53.2         52.1         50.9         49.9         48.8         47.7         46.7	34	52.6	51.4	50.3	49.1	48.0	46.9	45.9	44.8	43.8	42.8
37         53.5         52.3         51.2         50.0         48.9         47.8         46.7         45.7         44.7         43.6           38         53.8         52.6         51.5         50.3         49.2         48.1         47.0         46.0         45.0         43.8           39         54.1         52.9         51.8         50.6         49.5         48.4         47.3         46.3         45.3         44.2           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.5           41         54.7         53.5         52.3         51.2         50.1         49.0         47.9         46.9         45.8         44.5           42         54.9         53.8         52.6         51.5         50.4         49.3         48.2         47.2         46.1         45.4           43         55.2         54.0         52.9         51.8         50.7         49.6         48.5         47.5         46.4         45.4           44         55.5         54.3         53.2         52.1         50.9         49.9         48.8         47.7         46.7	35	52.9	51.7	50.6	49.4	48.3	47.2	46.1	45.1	44.1	43.0
33         53.8         52.6         51.5         50.3         49.2         48.1         47.0         46.0         45.0         43.6           39         54.1         52.9         51.8         50.6         49.5         48.4         47.3         46.3         45.3         44.2           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.5           41         54.7         53.5         52.3         51.2         50.1         49.0         47.9         46.9         45.8         44.5           42         54.9         53.8         52.6         51.5         50.4         49.3         48.2         47.2         46.1         45.1           43         55.2         54.0         52.9         51.8         50.7         49.6         48.5         47.5         46.4         45.4           44         55.5         54.6         53.4         52.3         51.2         50.2         49.1         48.0         47.0         46.2           45         55.7         54.6         53.4         52.3         51.2         50.2         49.1         48.0         47.0	36	53.2	52.0	50.9	49.7	48.6	47.5	46.4	45.4	44.4	43.3
39         54.1         52.9         51.8         50.6         49.5         48.4         47.3         46.3         45.3         44.2           40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.5           41         54.7         53.5         52.3         51.2         50.1         49.0         47.9         46.9         45.8         44.8           42         54.9         53.8         52.6         51.5         50.1         49.0         47.9         46.9         45.8         44.8           42         54.9         53.8         52.6         51.5         50.4         49.3         48.2         47.2         46.1         45.4           44         55.5         54.0         52.9         51.8         50.7         49.6         48.5         47.7         46.7         45.7           44         55.5         54.0         52.9         51.8         50.2         49.1         48.0         47.0         46.6           45         55.7         54.6         53.4         52.3         51.2         50.2         49.1         48.0         47.0         46.2	37	53.5	52.3	51.2	50.0	48.9	47.8	46.7	45.7	44.7	43.6
40         54.4         53.2         52.1         50.9         49.8         48.7         47.6         46.6         45.6         44.8           41         54.7         53.5         52.3         51.2         50.1         49.0         47.9         46.9         45.8         44.8           42         54.9         53.8         52.6         51.5         50.4         49.3         48.2         47.2         46.1         45.4           43         55.2         54.0         52.9         51.8         50.7         49.6         48.5         47.5         46.4         45.4           44         55.5         54.3         53.2         52.1         50.9         49.9         48.8         47.7         46.7         45.7           45         55.7         54.6         53.4         52.3         51.2         50.2         49.1         48.0         47.0         46.2           46         55.9         54.7         53.6         52.5         51.4         50.4         49.3         48.3         47.2         46.2           47         56.0         54.9         53.8         52.7         51.6         50.6         49.5         48.5         47.5	33	53.8	52.6	51.5	50.3	49.2	48.1	47.0	46.0	45.0	43.9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	39	54.1	52.9	51.8	50.6	49.5	48.4	47.3	46.3	45.3	44.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	40	54.4	53.2	52.1	50.9	49.8	48.7	47.6	46.6	45.6	44.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	41	54.7	53.5	52.3	51.2	50.1	49.0	47.9	46.9	45.8	44.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	42	54.9	53.8	52.6	51.5	50.4	49.3	48.2	47.2	46.1	45.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	43	55.2	54.0	52.9	51.8	50.7	49.6	48.5	47.5	46.4	45.4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	44	55.5	54.3	53.2	52.1	50.9	49.9	48.8	47.7	46.7	45.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	45	55.7	54.6	53.4	52.3	51.2	50.2	49.1	48.0	47.0	46.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	46	55.9	54.7	53.6	52.5	51.4	50.4	49.3	48.3	47.2	46.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	47	56.0	54.9	53.8	52.7	51.6	50.6	49.5	48.5	47.5	46.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	48		55.0	54.0	52.9	51.8	50.8	49.8		47.7	46.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			1				51.0			47.9	47.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	50	56.5	55.4	54.3	53.2	52.2	51.2	50.2	49.2	48.2	47.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	51						51.3			48.3	47.4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			i	54.6	1		51.5			48.5	47.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					i						47.7
56         57.3         56.2         55.1         54.1         53.0         52.0         51.0         50.0         49.1         48.1           57         57.4         56.3         55.2         54.2         53.2         52.2         51.2         50.2         49.2         48.3           58         57.5         56.4         55.4         54.3         53.3         52.3         51.3         50.3         49.4         48.4           59         57.7         56.6         55.5         54.5         53.4         52.4         51.4         50.5         49.5         48.6           60         57.8         59.7         55.6         54.6         53.6         52.6         51.6         50.6         49.7         48.7           61         57.9         56.8         55.8         54.7         53.7         52.7         51.7         50.8         49.8         48.9           62         58.0         57.0         55.9         54.9         53.8         52.8         51.9         50.9         49.9         49.0					1						47.8
57         57.4         56.3         55.2         54.2         53.2         52.2         51.2         50.2         49.2         48.3           58         57.5         56.4         55.4         54.3         53.3         52.3         51.3         50.3         49.4         48.4           59         57.7         56.6         55.5         54.5         53.4         52.4         51.4         50.5         49.5         48.6           60         57.8         59.7         55.6         54.6         53.6         52.6         51.6         50.6         49.7         48.7           61         57.9         56.8         55.8         54.7         53.7         52.7         51.7         50.8         49.8         48.9           62         58.0         57.0         55.9         54.9         53.8         52.8         51.9         50.9         49.9         49.0											48.0
58     57.5     56.4     55.4     54.3     53.3     52.3     51.3     50.3     49.4     48.4       59     57.7     56.6     55.5     54.5     53.4     52.4     51.4     50.5     49.5     48.6       60     57.8     59.7     55.6     54.6     53.6     52.6     51.6     50.6     49.7     48.7       61     57.9     56.8     55.8     54.7     53.7     52.7     51.7     50.8     49.8     48.9       62     58.0     57.0     55.9     54.9     53.8     52.8     51.9     50.9     49.9     49.0	56	57.3	56.2	55.1	54.1	53.0	52.0	51.0	50.0	49.1	48.1
59         57.7         56.6         55.5         54.5         53.4         52.4         51.4         50.5         49.5         48.6           60         57.8         56.7         55.6         54.6         53.6         52.6         51.6         50.6         49.7         48.7           61         57.9         56.8         55.8         54.7         53.7         52.7         51.7         50.8         49.8         48.9           62         58.0         57.0         55.9         54.9         53.8         52.8         51.9         50.9         49.9         49.0				1	1						48.3
60         57.8         56.7         55.6         54.6         53.6         52.6         51.6         50.6         49.7         48.7           61         57.9         56.8         55.8         54.7         53.7         52.7         51.7         50.8         49.8         48.9           62         58.0         57.0         55.9         54.9         53.8         52.8         51.9         50.9         49.9         49.0				1							48.4
61 57.9 56.8 55.8 54.7 53.7 52.7 51.7 50.8 49.8 48.9 62 58.0 57.0 55.9 54.9 53.8 52.8 51.9 50.9 49.9 49.0				- 1	- 1		- 1				48.6
62         58.0         57.0         55.9         54.9         53.8         52.8         51.9         50.9         49.9         49.0			- 1	i							48.7
		1		- 1	1			- 1			48.9
		15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Tempera	tures of the	e Air and o	of the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5
62°	58.0	57.0	55.9	54.9	53.8	52.8	51.9	50.9	49.9	49.0
63	58.2	57.1	56.0	55.0	54.0	53.0	52.0	51.0	50.1	49.1
64	58.3	57.2	56.2	55.1	54.1	53.1	52.1	51.2	50.2	49.3
65	58.4	57.4	56.3	55.3	54.3	53.3	52.3	51.3	50.4	49.4
66	58.6	57.5	56.4	55.4	54.4	53.4	52.4	51.5	50.5	49.6
67	58.7	57.6	56.6	55.5	54.5	53.5	52.6	51.6	50.6	49.7
68	58.8	57.8	56.7	55.7	54.7	53.7	52.7	51.7	50.8	49.9
69	59.0	57.9	<b>56.</b> S	55.8	54.8	53.8	52.8	51.9	50.9	50.0
70	59.1	58.0	57.0	55.9	54.9	53.9	53.0	52.0	51.1	50.1
71	59.2	58.2	57.1	56.1	55.1	54.1	53.1	52.1	51.2	50.3
72	59.3	58.3	57.2	56.2	55.2	54.2	53.2	52.3	51.3	50.4
73	59.5	58.4	57.4	56.3	55.3	54.3	53.4	52.4	51.5	50.6
74	59.6	58.5	57.5	56.5	55.5	54.5	53.5	52.6	51.6	50.7
75	59.7	58.7	57.6	56.6	55.6	54.6	53.6	52.7	51.7	50.8
76	59.8	58.8	57.8	56.7	55.7	54.7	53.8	52.8	51.9	51.0
77	60.0	58.9	57.9	56.9	55.9	54.9	53.9	53.0	52.0	51.1
78	60.1	59.1	58.0	57.0	56.0	55.0	54.0	53.1	52.2	51.2
79	60.2	59.2	58.1	57.1	56.1	55.1	54.2	53.2	52.3	51.4
80	60.3	59.3	58.3	57.3	56.3	55.3	54.3	53.4	52.4	51.5
81	60.5	59.4	58.4	57.4	56.4	55.4	54.5	53.5	52.6	51.7
82	60.6	59.6	58.5	57.5	56.5	55.5	54.6	53.6	52.7	51.8
83	60.7	59.7	58.6	57.6	56.6	55.7	54.7	53.8	<b>52.</b> 8	51.9
84	60.8	59.8	58.8	57.8	56.8	55.8	54.8	53.9	53.0	52.1
85	60.9	59.9	58.9	57.9	56.9	55.9 .	55.0	54.0	53.1	52.2
86	61.1	60.0	59.0	58.0	57.0	56.1	55.1	54.2	53.2	52.3
87	61.2	60.2	59.1	58.1	57.2	56.2	55.2	54.3	53.4	52.5
88	61.3	60.3	59.3	58.3	57.3	56.3	55.4	54.4	53.5	52.6
89	61.4	60.4	59.4	58.4	57.4	56.5	55.5	54.6	53.7	52.7
90	61.6	60.5	59.5	58.5	57.6	56.6	55.6	54.7	53.8	52.9
91	61.7	60.7	59.6	58.7	57.7	56.7	55.8	54.8	53.9	53.0
92	61.8	60.8	59.8	58.8	57.8	56.9	55.9	55.0	54.1	53.2
93	61.9	60.9	59.9	58.9	57.9	57.0	56.0	55.1	54.2	53.3
94	62.0	61.0	60.0	59.0	58.1	57.1	56.2	55.2	54.3	53.4
95	62.1	61.1	60.1	59.2	58.2	57.2	56.3	55.4	54.5	53.6
96	62.3	61.3	60.3	59.3	58.3	57.4	56.4	55.5	54.6	53.7
97	62.4	61.4	60.4	59.4	58.4	57.5	56.5	55.6	54.7	53.8
98	.62.5	61.5	60.5	59.5	58.6	57.6	56.7	55.8	54.9	54.0
99	62.6	61.6	60.6	59.6	58.7	57.7	56.8	55.9	55.0	54.1
100	62.7	61.7	60.7	59.8	58.8	57.9	56.9	56.0	55.1	54.2
101	62.8	61.9	60.9	59.9	58.9	58.0	57.1	56.2	55.3	54.4
102	63.0	62.0	61.0	60.0	59.1	58.1	57.2	56.3	55.4	54.5
103	63.1	62.1	61.1	60.1	59.2	58.3	57.3	56.4	55.5	54.6
104	63.2	62.2	61.2	60.3	59.3	58.4	57.5	56.6	55.7	54.8
	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	tures of the	e Air and o	f the Dew-	Point.—F	ahrenheit.	
Fahren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5
20°	40.2	39.3	38.4	37.5	36.6	35.8	34.9	34.1	33.3	32.5
21	40.3	39.4	38.4	37.6	36.7	35.8	35.0	34.2	33.4	32.6
22	40.3	39.4	38.5	37.6	36.8	35.9	35.1	34.3	33.5	32.7
23	40.4	39.5	38.6	37.7	36.8	36.0	35.2	34.4	33.6	32.8
24	40.4	39.6	38.6	37.8	36.9	36.1	35.2	34.4	33.6	32.9
25	40.5	39.6	38.7	37.8	37.0	36.2	35.3	34.5	33.7	33.0
26	40.5	39.7	38.8	37.9	37.0	36.2	35.4	34.6	33.8	33.1
27	40.6	39.7	38.8	38.0	37.1	36.3	35.5	34.7	33.9	33.1
28	40.7	39.8	38.9	38.0	37.2	36.3	35.5	34.7	34.0	33.2
29	40.8	39.9	38.9	38.1	37.2	36.4	35.6	34.8	34.0	33.3
30	40.8	39.9	39.0	38.1	37.3	36.5	35.7	34.9	34.1	33.4
31	41.1	40.2	39.2	38.4	37.5	36.7	35.9	35.1	34.3	33.6
32	41.3	40.4	39.5	38.6	37.7	37.0	36.1	35.3	34.5	33.8
33	41.6	40.6	39.7	38.8	38.0	37.2	36.3	35.5	34.7	34.0
34	41.8	40.9	39.9	39.1	38.2	37.4	36.5	35.7	34.9	34.2
35	42.1	41.1	40.2	39.3	38.4	37.7	36.7	35.9	35.1	34.4
36	42.3	41.4	40.4	39.6	38.7	37.9	37.0	36.2	35.4	34.6
37	42.6	41.7	40.7	39.8	38.9	38.2	37.2	36.4	35.6	34.8
38	42.8	42.0	41.0	40.1	39.2	38.4	37.5	36.6	35.8	35.0
39	43.1	42.3	41.3	40.4	39.5	38.6	37.7	36.9	36.0	35.2
40	43.3	42.6	41.6	40.7	39.8	38.9	38.0	37.1	36.3	35.4
41	43.7	42.9	41.9	41.0	40.0	39.1	38.3	37.4	36.5	35.7
42	44.0	43.2	42.2	41.2	40.3	39.4	38.5	37.7	36.8	36.0
43	44.3	43.4	42.5	41.5	40.6	39.7	38.8	38.0	37.1	36.3
44	44.7	43.7	42.8	41.8	40.9	40.0	39.1	38.2	37.4	36.6
45	45.0	44 0	43.1	42.1	41.2	40.3	39.4	38.5	37.7	36.8
46	45.2	44.3	43.3	42.4	41.4	40.5	39.7	38.8	37.9	37.1
47	45.5	44.5	43.6	42.6	41.7	40.8	39.9	39.1	38.2	37.4
43	45.7	44.8	43.8	42.9	42.0	41.1	40.2	39.3	38.5	37.6
49	46.0	45.0	44.1	43.2	42.2	41.3	40.5	39.6	38.7	37.9
50	46.2	45.3	44.3	43.4	42.5	41.6	40.7	39.9	39.0	37.2
51	46.4	45.4	44.5	43.6	42.7	41.8	40.9	40.1	39.2	38.4
52	46.6	45.5	44.7	43.8	42.9	42.0	41.2	40.3	39.5	38.6
53	46.7	45.8	44.9	44.0	43.1	42.2	41.4	40.5	39.7	38.9
51	46.9	46.0	45.1	44.2	43.3	42.4	41.6	40.8	39.9	39.1
55	47.0	46.1	45.2	44.4	43.5	42.6	41.8	41.0	40.1	39.3
56	47.2	46.3	45.4	44.5	43.6	42.8	42.0	41.1	40.3	39.5
57	47.3	46.4	45.5	44.7	43.8	42.9	42.1	41.3	40.5	39.6
58	47.5	46.6	45.7	44.8	43.9	43.1	42.3	41.4	40.6	39.8
59	47.6	46.7	45.8	45.0	44.1	43.2	42.4	41.6	40.8	40.0
60	47.8	46.9	46.0	45.1	44.2	43.4	42.5	41.7	40.9	40.1
61	47.9	47.0	46.1	45.3	44.4	43.5	42.7	41.9	41.1	40.3
62	48.1	47.2	46.3	45.4	44.5	43.7	42.8	42.0	41.2	40.4
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	ifference o	f Temperat	ures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5
62°	48.1	47.2	46.3	45.4	44.5	43.7	42.8	42.0	41.2	40.4
63	48.2	47.3	46.4	45.5	44.7	43.8	43.0	42.2	41.4	40.6
64	48.4	47.5	46.6	45.7	44.8	44.0	43.1	42.3	41.5	40.7
65	48.6	47.6	46.7	45.8	45.0	44.1	43.3	42.5	41.7	40.9
66	48.7	47.8	46.9	46.0	45.1	44.3	43.4	42.6	41.8	41.0
67	48.8	47.9	47.0	46.1	45.3	44.4	43.6	42.8	42.0	41.2
68	48.9	48.0	47.2	46.3	45.4	44.6	43.7	42.9	42.1	41.3
69	49.1	48.2	47.3	46.4	45.6	44.7	43.9	43.1	42.3	41.5
70	49.2	48.3	47.4	46.6	45.7	44.9	44.0	43.2	42.4	41.6
71	49.4	48.5	47.6	46.7	45.9	45.0	44.2	43.4	42.6	41.8
72	49.5	48.6	47.7	46.9	46.0	45.2	44.3	43.5	42.7	41.9
73	49.6	48.8	47.9	47.0	46.1	45.3	44.5	43.7	42.9	42.1
74	49.8	48.9	48.0	47.1	46.3	45.4	44.6	43.8	43.0	42.2
<b>7</b> 5	49.9	49.0	48.2	47.3	46.4	45.6	44.8	44.0	43.1	42.4
76	50.1	49.2	48.3	47.4	46.6	45.7	44.9	44.1	43.3	42.5
77	50.2	49.3	48.5	47.6	46.7	45.9	45.1	44.2	43.4	42.6
78	50.3	49.5	48.6	47.7	46.9	46.0	45.2	44.4	43.6	42.8
79	50.5	49.6	48.7	47.8	47.0	46.2	45.3	44.5	43.7	43.0
80	50.6	49.7	48.9	48.0	47.2	46.3	45.5	44.7	43.9	43.1
81	50.8	49.9	49.0	48.1	47.3	46.5	45.6	44.8	44.0	43.2
82	50.9	50.0	49.2	48.3	47.4	46.6	45.8	45.0	44.2	43.4
83	51.0	50.1	49.3	48.4	47.6	46.8	45.9	45.1	44.3	43.5
84	51.2	50.3	49.4	48.6	47.7	46.9	46.1	45.3	44.5	43.7
85	51.3	50.4	49.6	48.7	47.9	47.0	46.2	45.4	44.6	43.S
86	51.4	50.6	49.7	48.8	48.0	47.2	46.4	45.6	44.8	44.0
87	51.6	50.7	49.8	49.0	48.1	47.3	46.5	45.7	44.9	44.1
88	51.7	50.8	50.0	49.1	48.3	47.5	46.6	45.8	45.0	44.3
89	51.9	51.0	50.1	49.3	48.4	47.6	46.8	46.0	45.2	44.4
90	52.0	51.1	50.3	49.4	48.6	47.7	46.9	46.1	45.3	44.6
91	52.1	51.3	50.4	49.5	48.7	47.9	47.1	46.3	45.5	44.7
92	52.3	51.4	50.5	49.7	48.8	48.0	47.2	46.4	45.6	44.8
93	52.4	51.5	50.7	49.8	49.0	48.2	47.4	46.6	45.8	45.0
94	52.5	51.7	50.8	50.0	49.1	48.3	47.5	46.7	45.9	45.1
95	52.7	51.8	50.9	50.1	49.3	48.4	47.6	46.8	46.1	45.3
96	52.8	51.9	51.1	50.2	49.4	48.6	47.8	47.0	46.2	45.4
97 98	52.9 $53.1$	$52.1 \\ 52.2$	51.2 51.4	50.4 50.5	49.5	48.7 48.9	47.9 48.1	47.1 47.3	46.3 46.5	45.6 45.7
99	53.2	52.3 52.5	51.5	50.6	49.8	49.0	48.2	47.4	46.6	45.9
100	53.4	52.5 52.6	51.6	50.8	50.0	49.1	48.3	47.5	46.8	46.0
101	53.5 53.6	$52.6 \\ 52.8$	51.8 51.9	50.9 51.1	50.1 50.2	49.3 49.4	48.5	47.7	46.9	46.2
102 103	53.8	52.9	52.0	51.2	50.2	49.4	48.6 48.8	47.8 48.0	47.1 47.2	46.3
103	53.9	53.0	52.2	51.3	50.4	49.7	48.9	48.1	47.3	46.6
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5
	20.0	20.0	21.0	~1.0	22.0	~~.0	20.0	20.0	24.0	24.0

### TABLE IX.

FACTOR  $\frac{100}{F}$ , FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR, EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE

HUMIDITY GIVEN IN ENGLISH MEASURES.

The Relative Humidity, or the degree of moisture of the air, is, as explained above, the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $f_{\rm F}^{100}$  = Relative Humidity in Hundredths.

But as  $\frac{f \times 100}{F} = f \times \frac{100}{F}$ , it is obvious that the operation indicated by the former expression, viz.  $\frac{f \times 100}{F}$ , would be reduced to a simple multiplication, if we had a table of the factors  $\frac{100}{F}$ . Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quotients for the tensions, or forces of vapor.

The following Table gives the factor  $\frac{100}{F}$  for every tenth of a degree from 0° to 104° Fahrenheit, corresponding to the Forces of Vapor in Table VI., or Regnault's table reduced to English measures.

#### USE OF THE TABLE.

The force of vapor contained in the air, or its absolute humidity, being given in English measures, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the *Relative Humidity in Hundredths*.

# Examples.

- 1. Suppose the temperature of the air to be = 60° Fahrenheit.
  - " force of vapor in the air to be = .388 English inch.

Opposite 60° is found in the table the factor 193.1.

Then  $0.388 \times 193.1 = 74.9$ , Relative Humidity in Hundredths.

Suppose the temperature of the air to be = 74°.5 Fahrenheit." force of vapor in the air to be = .650 English inch.

Table gives for 74°.5 the factor 117.2.

Then  $0.650 \times 117.2 = 76.2$ , Relative Humidity required.

# IX. FACTOR $\frac{100}{F}$ , FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR,

# EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE HUMIDITY GIVEN IN ENGLISH INCHES.

Temper-					Tenths of	f Degrees.				
of Air, Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0°	2306	2295	2285	2275	2264	2254	2243	2233	2222	2211
1	2201	2191	2181	2171	2162	2152	2142	2132	2122	2111
2	2101	2092	2083	2074	2064	2055	2045	2036	2026	2017
3	2007	1998	1990	1981	1972	1963	1954	1945	1936	1927
4	1918	1910	1901	1893	1885	1876	1868	1859	1851	1842
5	1834	1826	1818	1810	1802	1794	1786	1777	1769	1761
6	1753	1745	1738	1730	1722	1714	1707	1699	1691	1683
7	1675	1668	1660	1653	1646	1638	1631	1623	1616	1608
8	1600	1594	1587	1580	1572	1565	1558	1551	1544	1537
9	1529	1523	1516	1509	1503	1496	1489	1482	1475	1469
10	1462	1455	1449	1443	1436	1430	1423	1417	1410	1404
11	1397	1391	1385	1379	1373	1367	1361	1355	1348	1342
12	1336	1330	1324	1319	1313	1307	1301	1295	1289	1284
13	1278	1272	1267	1261	1255	1250	1244	1239	1233	1228
14	1222	1217	1211	1206	1200	1195	1189	1184	1178	1173
15	1167	1162	1157	1151	1146	1141	1136	1130	1125	1120
16	1114	1109	1104	1099	1094	1089	1084	1079	1074	1069
17	1064	1059	1055	1050	1045	1040	1035	1031	1026	1021
18	1016	1012	1007	1003	998.2	993.6	989.1	984.5	979.9	975.3
19	970.6	966.4	962.2	957.9	953.7	949.4	945.0	940.7	936.3	931.9
20	927.5	923.5	919.5	915.5	911.4	907.4	903.3	899.1	895.0	890.8
21	886.7	882.9	879.1	875.3	871.4	867.6	863.7	859.8	855.8	851.9
22	847.9	844.3	840.7	837.1	833.4	829.8	826.1	822.4	818.7	815.0
23	811.2	807.8	804.3	800.8	797.3	793.8	790.2	786.7	783.1	779.5
24	775.9	772.6	769.3	766.0	762.7	759.3	756.0	752.6	749.2	745.8
25	742.4	739.3	736.2	733.0	729.9	726.7	723.5	720.3	717.1	713.9
26	710.6	707.7	704.7	701.8	698.8	695.8	692.8	689.7	686.7	683.6
27	680.5	677.8	675.0	672.1	669.3	666.5	663.6	660.7	657.8	654.9
28	652.0	649.4	646.7	644.1	641.4	638.7	636.0	633.3	630.5	627.8
29	625.0	622.5	620.0	617.5	614.9	612.4	609.8	607.2	604.6	602.0
30	599.4	597.1	594.7	592.3	589.9	587.4	585.0	582.6	580.1	577.6
31	575.1	572.9	570.7	568.4	566.2	563.9	561.6	559.2	556.9	554.5
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Temper- ature											
of Air, Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
32°	552.2	550.0	547.8	545.7	543.6	541.4	539.3	537.2	535.1	533.0	
33	530.9	528.8	526.8	524.7	522.7	520.6	518.6	516.5	514.5	512.	
34	510.5	508.5	506.5	504.5	502.5	500.5	498.6	496.6	494.7	492.	
35	490.8	488.9	487.0	485.1	483.2	481.3	479.4	477.5	475.6	473.8	
36	471.9	470.1	468.2	466.4	464.6	462.8	461.0	459.2	457.4	455.	
37	453.8	452.0	450.3	448.5	446.8	445.0	443.3	441.6	439.9	438.	
38	436.4	434.7	433.1	431.4	429.7	428.0	426.4	424.7	423.1	421.	
39	419.8	418.2	416.6	415.0	413.4	411.8	410.2	408.6	407.0	405.	
40	403.9	402.4	400.8	399.3	397.8	396.2	394.7	393.2	391.7	290.	
41	388.7	387.2	385.8	384.3	382.9	381.4	380.0	378.5	377.1	375.	
42	374.3	372.9	371.5	370.0	368.6	367.3	365.9	364.5	363.1	361.	
43	360.4	359.0	357.6	356.3	354.9	353.6	352.3	350.9	349.6	348.	
44	347.0	345.6	344.3	343.0	341.7	340.4	339.2	337.9	336.6	335.	
45	334.1	332.8	331.6	330.3	328.1	327.8	326.6	325.4	324.1	322.	
46	321.7	320.5	319.3	318.1	316.9	315.7	314.5	313.3	312.2	311.	
47	309.8	308.7	307.5	306.4	305.2	304.1	302.9	301.8	300.7	299.	
49	298.5	297.3	296.2	295.1	294.0	292.9	291.9	290.8	289.7	288.	
49	287.6	286.5	285.4	284.4	283.3	282.3	281.3	280.2	279.2	278.	
50	277.1	276.1	275.1	274.1	273.1	272.1	271.1	270.1	269.1	268.	
51	267.2	266.2	265.2	264.3	263.3	262.3	261.4	260.4	259.5	258.	
52	257.6	256.6	255.7	254.8	253.8	252.9	252.0	251.1	250.2	249.	
53	248.3	247.4	246.5	245.6	244.7	243.9	243.0	242.1	241.2	240.	
54	239.5	238.6	237.7	236.9	236.0	235.1	234.3	233.4	232.6	231.	
55	230.9	230.1	229.2	228.4	227.6	226.8	225.9	225.1	224.3	223.	
.56	222.7	221.9	221.1	220.3	219.5	218.7	217.9	217.1	216.4	215.	
57	214.8	214.0	213.3	212.5	211.8	211.0	210.2	209.5	208.7	208.	
58	207.3	206.5	205.8	205.0	204.3	203.6	202.9	202.2	201.4	200.	
59	200.0	199.3	198.6	197.9	197.2	196.5	195.8	195.1	194.4	193.	
60	193.1	192.4	191.7	191.0	190.4	189.7	189.0	188.4	187.7	187.	
61	186.4	185.7	185.1	184.4	183.8	183.1	182.5	181.8	181.2	180.	
62	179.9	179.3	178.7	178.0	177.4	176.8	176.2	175.6	174.9	174.	
63	173.7	173.1	172.5	171.9	171.3	170.7	170.1	169.5	168.9	168.	
64	167.7	167.1	166.6	166.0	165.4	164.8	164.3	163.7	163.1	162.	
65	162.0 156.5	161.4	160.9	160.3	159.7	159.2	158.6	158.1	157.5	157.0	
66 67	151.1	155.9 150.6	155.4 150.1	154.8 149.6	154.3 149.1	153.8 148.6	153.2 148.1	152.7 147.6	152.2 147.1	151. <sup>7</sup>	
07											
	0.	1.	2.	3.	4.	5.	6.	7.	₿.	9.	

	1									
Temper- ature	Tenths of Degrees.									
of Air,		1	1	1	1	1	}	I	1	1
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
6s°	146.0	145.6	145.1	144.6	144.1	143.6	143.1	142.6	142.1	141.6
69	141.2	140.7	140.2	139.7	139.2	138.8	138.3	137.8	137.4	136.9
70	136.4	136.0	135.5	135.1	134.6	134.1	133.7	133.2	132.8	132.3
71	131.9	131.4	131.0	130.5	130.1	129.7	129.2	128.8	128.3	127.9
72	127.5	127.1	126.6	126.2	125.8	125.3	124.9	124.5	124.1	123.7
73	123.3	122.8	122.4	122.0	121.6	121.2	120.8	120.4	120.0	119.6
74	119.2	118.8	118.4	118.0	117.6	117.2	116.8	116.4	116.0	115.6
75	115.3	114.9	114.5	114.1	113.7	113.3	113.0	112.6	112.2	111.9
76	111.5	111.1	110.7	110.4	110.0	109.6	109.3	108.9	108.6	108.2
77	107.9	107.5	107.1	106.8	106.4	106.1	105.7	105.4	105.1	104.7
78	104.4	104.0	103.7	103.3	103.0	102.7	102.3	102.0	101.7	101.3
79	101.4	100.7	100.3	100.0	99.68	99.35	99.02	98.70	98.38	98.06
80	97.73	97.42	97.10	96.78	96.47	96.15	95.84	95.52	95.21	94.90
81	94.59	94.29	93.98	93.67	93.37	93.06	92.76	92.46	92.16	91.86
82	91.56	91.26	90.97	90.67	90.38	90.09	89.80	89.51	89.22	88.93
٥ <b>ء</b>						,	00.00		55.22	00.00
83	88.64	88.36	88.07	87.79	87.50	87.22	86.94	86.66	86.38	86.10
84	85.83	85.55	85.27	85.00	84.73	84.46	84.19	83.92	83.65	83.38
85	83.12	82.85	82.59	82.32	82.06	81.80	81.54	81.28	81.02	80.77
86	80.51	80.25	80.00	79.74	79.49	79.24	78.99	78.74	78.49	78.24
87	77.99	77.75	77.50	77.26	77.01	76.77	76.52	76.28	76.04	75.80
00	** *0	#F 99	## 00	#4.0×	W4 C7	m 4 0 m		*0.01	#0 0#	
88	75.56	75.32	75.08	74.85	74.61	74.37	74.14	73.91	73.67	73.44
89 90	73.21 70.94	72.98 70.72	72.75 70.49	72.52 70.27	72.29 70.05	72.06 69.83	71.84 69.61	71.61	71.39	71.16
90	68.74	68.53	68.32	68.10	67.89	67.68	67.47	69.39 67.26	69.18	68.96
91	66.63	66.42	66.22	66.01	65.81	65.60	65.40	65.19	67.05 64.99	66.84
92	00.05	00.42	00.22	00.01	09.51	09.00	09,40	09.19	04.59	64.79
93	64.59	64.39	64.19	63.99	63.79	63.59	63.40	63.20	63.01	62.81
94	62.62	62.43	62.24	62.04	61.85	61.66	61.47	61.29	61.10	60.91
95	60.72	60.54	60.35	60.17	59.98	59.80	59.62	59.43	59.25	59.07
96	58.89	58.71	58.53	58.35	58.17	58.00	57.82	57.64	57.47	57.29
97	57.12	56.94	56.77	56.60	56.42	56.25	56.08	55.91	55.74	55.57
98	55.40	55.23	55.06	54.90	54.73	54.56	54.40	54.23	54.07	53.91
99	53.74	53.58	53.42	53.26	53.09	52.93	52.77	52.61	52.45	52.30
100	52.14	51.98	51.82	51.67	51.51	51.36	51.20	51.05	50.90	50.74
101	50.59	50.44	50.29	50.14	49.99	49.84	49.69	49.54	49.39	49.24
102	49.10	48.95	48.80	48.66	48.51	48.37	48.22	48.08	47.94	47.79
103	47.65	47.51	47.37	47.23	47.09	46.95	46.81	46.67	46.53	46.40
104	46.26	46.12	45.99	45.85	45.72	45.58	45.45	45.31	45.18	45.04
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

#### TABLE X.

# WEIGHT OF VAPOR, IN GRAINS TROY,

contained in a cubic foot of saturated air, under a barometric pressure of 30 english inches, at temperatures between  $0^\circ$  and  $105^\circ$  fahrenheit.

The weight of a litre of dry air at the temperature of zero Centigrade, or 32° Fahrenheit, and under a barometric pressure of 760 millimetres, as determined by the experiments of Regnault (Mémoires de l'Institut, Tom. XXI. p. 157), and corrected for a slight error of computation (see above, p. 38), is 1.293223 grammes. The coefficient of expansion of the air, according to the same physicist, is 0.00367 for 1° Centigrade; and the theoretic density of vapor is nearly 0.622, or  $\frac{5}{8}$ , of that of the air at the same temperature and pressure. From these elements the weight of the vapor contained in a determined volume of air, the temperature and humidity of which are known, can be deduced.

Reducing these values to English measures, 1 litre being = 61.02705 cubic inches, and 1 gramme = 15.43208 grains Troy, we have

1.293223 grammes = 19.9571208 grains,

and

61.027051 cubic inches: 19.9571208 grains:: 1 cubic inch: 0.32702 grain.

Therefore, the weight of a cubic foot of dry air, at 32° Fahrenheit, under a pressure of 760 millimetres, or 29.922 English inches, is = 0.32702 grain  $\times$  1728 = 565.0923 grains Troy. Under a barometric pressure of 30 inches, it becomes

$$\frac{30}{29.922} \times 565.0923 = 566.5654$$
 grains.

The coefficient for the expansion of the air becomes 0.0020361 of its bulk for 1° Fahrenheit.

Now, if we call

t = the temperature of the air;

W = the weight of vapor in a saturated air at the temperature t;

F = the maximum of the force of vapor due to the temperature t, as given in the tables;

then the weight of the vapor contained in a cubic foot of saturated air is given by the formula

$$W = 0.622 \frac{566.5654 \text{ grains}}{1 + 0.002036 \times (t - 32^{\circ})} \cdot \frac{F}{30};$$

from which the values in Table X. have been computed. The forces of vapor due to the temperatures in the first column are those of Regnault, as given in Table VI.

It is evident, that, in order to find the weight of the vapor contained in the air at any state of humidity and pressure, it suffices to substitute for the normal values of  $\frac{\mathbf{F}}{30}$  the force of vapor and the barometric pressure given by the observation.

В

# X. WEIGHT OF VAPOR, IN GRAINS TROY,

# contained in a cubic foot of saturated air, at temperatures between $0^{\circ}$ and $105^{\circ}$ fahrenheit.

O												
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ature of Air,	of Vapor in Eng.	of Vapor in		of Air,	of Vapor in Eng.	of Vapor in		ature of Air,	of Vapor in Eng.	of Vapor in	Differ- ence.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0°	0.013	0.545		35°	0.201	2.379		70°	0.733	7.999	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				0.024		1		0.090				0.261
3				0.025	1			0.093		1	i	0.268
4         0.052         0.649         0.029         39         0.238         2.759         0.100         74         0.839         9.081         0           5         0.055         0.678         0.030         40         0.248         2.862         0.106         75         0.868         9.372         0           7         0.060         0.739         0.031         42         0.267         3.076         0.113         77         0.927         9.977         0           8         0.062         0.772         0.034         43         0.277         3.189         0.116         78         0.958         10.292           9         0.065         0.806         0.034         44         0.288         3.306         0.116         79         0.990         10.616         0           10         0.068         0.841         0.037         45         0.299         3.426         0.124         80         1.023         10.949           11         0.072         0.878         0.033         46         0.311         3.550         0.124         81         1.057         11.291         0           12         0.075         0.916         0.042 <td< td=""><td></td><td></td><td></td><td>0.027</td><td>1 1</td><td></td><td></td><td>0.097</td><td></td><td></td><td>1</td><td>0.276</td></td<>				0.027	1 1			0.097			1	0.276
5         0.055         0.678         0.030         40         0.248         2.862         0.106         75         0.868         9.372         0           7         0.060         0.739         0.031         42         0.267         3.076         0.109         77         0.927         9.977         0           8         0.062         0.772         0.034         43         0.277         3.189         0.116         78         0.958         10.292         0           9         0.065         0.806         0.841         0.034         44         0.288         3.306         0.116         79         0.990         10.616         0           10         0.068         0.841         0.037         45         0.299         3.426         0.124         80         1.023         10.949           11         0.072         0.878         0.038         47         0.323         3.679         0.124         80         1.023         10.949           12         0.075         0.916         0.040         48         0.335         3.811         0.133         83         1.128         12.005         0           14         0.082         0.999         <				0.028				0.100		1	1	0.284
6         0.057         0.708         0.031         41         0.257         2.967         0.106         76         0.897         9.670         0           7         0.060         0.739         0.033         42         0.267         3.076         0.109         77         0.927         9.977         0           8         0.062         0.772         0.034         44         0.288         3.306         0.116         78         0.958         10.292         0           10         0.068         0.841         0.035         45         0.299         3.426         0.116         79         0.990         10.616         0           11         0.072         0.878         0.037         46         0.311         3.550         0.124         80         1.023         10.949           12         0.075         0.916         0.038         47         0.323         3.679         0.129         82         1.092         11.643         0           13         0.078         0.957         0.040         48         0.335         3.811         0.133         83         1.128         12.005         0           14         0.082         0.999		0.002	0.010	0.029		0.200		0.103		0.000	0.501	0.291
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	0.055	0.678		40	0.248	2.862		75	0.868	9.372	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.057	0.708		41	0.257	2.967		76	0.897		0.298
8         0.062         0.772         0.034         43         0.277         3.189         0.116         78         0.958         10.292         0.990         10.616         0           10         0.068         0.841         0.037         45         0.299         3.426         0.124         80         1.023         10.949         0           11         0.072         0.878         0.038         47         0.323         3.679         0.124         81         1.057         11.291         0           12         0.075         0.916         0.040         48         0.335         3.811         0.133         82         1.092         11.643         0           13         0.078         0.999         0.042         49         0.348         3.948         0.137         84         1.165         12.376         0           14         0.082         0.999         0.044         49         0.348         3.948         0.141         84         1.165         12.376         0           15         0.086         1.043         0.046         50         0.361         4.089         0.145         86         1.242         13.146         0	7	0.060	0.739		42	0.267	3.076		77	0.927	9.977	0.307
10	8	0.062	0.772		43	0.277	3.189		78	0.958	10.292	0.315
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.065	0.806		44	0.288	3.306		79	0.990	10.616	0.324
11         0.072         0.878         0.037         46         0.311         3.550         0.124         81         1.057         11.291         0           12         0.075         0.916         0.040         47         0.323         3.679         0.129         82         1.092         11.643         0           13         0.078         0.957         0.042         48         0.335         3.811         0.133         83         1.128         12.005         0           14         0.082         0.999         0.042         49         0.348         3.948         0.137         84         1.165         12.376         0           15         0.086         1.043         0.046         50         0.361         4.089         0.145         86         1.242         13.146         0           16         0.090         1.090         0.049         52         0.388         4.383         0.149         87         1.282         13.546         0           17         0.094         1.133         0.051         53         0.403         4.537         0.154         88         1.323         13.957         0           18         0.098 <td< td=""><td></td><td></td><td></td><td>0.035</td><td></td><td></td><td></td><td>0.120</td><td></td><td>ĺ</td><td></td><td>0.332</td></td<>				0.035				0.120		ĺ		0.332
11         0.072         0.878         0.038         46         0.311         3.550         0.129         81         1.057         11.291         0.129         82         1.092         11.643         0         0         0         0.333         3.679         0.133         82         1.092         11.643         0         0         0         0         0.335         3.811         0.137         84         1.165         12.376         0           14         0.082         0.999         0.044         49         0.348         3.948         0.137         84         1.165         12.376         0           15         0.086         1.043         0.046         50         0.361         4.089         0.141         84         1.165         12.376         0           16         0.090         1.090         0.046         51         0.374         4.234         0.145         86         1.242         13.146         0           17         0.094         1.138         0.051         53         0.433         4.537         0.154         88         1.323         13.957         0           18         0.098         1.190         0.053         54         0.41	10	0.068	0.841	0.00#	45	0.299	3.426	0.104	80	1.023	10.949	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	0.072	0.878		46	0.311	3.550		81	1.057	11.291	0.342
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	0.075	0.916		47	0.323	3.679		82	1.092	11.643	0.352
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	0.078	0.957		48	0.335	3.811		83	1.128	12.005	0.361
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	0.082	0.999		49	0.348	3.948		84	1.165	12.376	0.371
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				0.044				0.141				0.350
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	0.086	1.043	0.046	50	0.361	4.089	0.145	85	1.203	12.756	0.390
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			1.090						86	1.242	13.146	0.400
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$											13.546	0.411
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$											13.957	0.421
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	0.103	1.243		54	0.418	4.696		89	1.366	14.378	0.432
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												00.00
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 1			0.057				0.168				0.443
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				0.059				0.174				0.455
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				0.062				0.179	1			0.467
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				0.064				0.185				0.479
26 0.141 1.674 0.068 61 0.537 5.952 0.196 96 1.698 17.648 0	24	0.129	1.940	0.066	99	0.500	9.500	0.190	94	1.597	10.054	0.491
26 0.141 1.674 0.068 61 0.537 5.952 0.196 96 1.698 17.648 0	25	0.135	1 606		60	0.518	5 756		95	1.647	17 145	
0.070				0.068	1			0.196				0.503
	27	0.147	1.745	0.070	62	0.556	6.154	0.202	97	1.751	18.164	0.516
28   0.153   1.817   0.073   63   0.576   6.361   0.208   98   1.805   18.693   0												0.529
$oxed{29} egin{array}{ c c c c c c c c c c c c c c c c c c c$									1	i	1	0.542
				0.077	1			0.220		1.501	10.200	0.555
30   0.167   1.969	30	0.167	1.969		65	0.617	6.795		100	1.918	19.790	
$egin{array}{ c c c c c c c c c c c c c c c c c c c$												0.567
$\parallel 32 \mid 0.181 \mid 2.126 \mid 0.080 \mid 67 \mid 0.662 \mid 7.253 \mid 0.232 \mid 102 \mid 2.037 \mid 20.938 \mid 0$	32	0.181	2.126		67	0.662	7.253		102	2.037	1	0.582
33   0.188   2.208     08   0.685   7.493     103   2.099   21.535	33	0.188	2.208		68	0.685	7.493		103	2.099	21.535	0.596
$oxed{\parallel 34 \mid 0.196 \mid 2.292 \mid 0.084 \mid 69 \mid 0.708 \mid 7.739 \mid 0.246 \mid 104 \mid 2.162 \mid 22.146 \mid 0}$	34	0.196	2.292		69	0.708	7.739		104	2.162		0.611
35 0.204 2.379 0.087 70 0.733 7.992 0.253 105 2.227 22.771 0	35	0.204	2.379	0.087	70	0.733	7.992	0.253	105	2.227	22.771	0.625

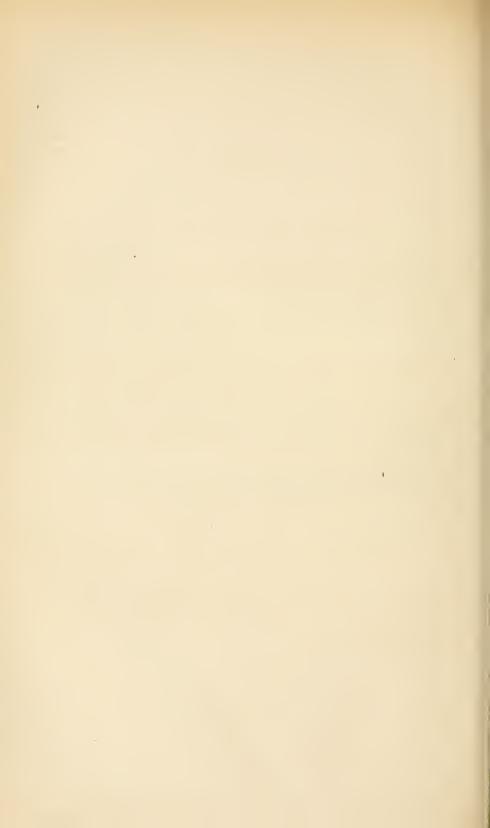


# PRACTICAL TABLES,

IN

# ENGLISH MEASURES,

BASED ON THE HYGROMETRICAL CONSTANTS ADOPTED IN THE GREENWICH OBSERVATIONS.



### TABLE

OF

### THE ELASTIC FORCES OF AQUEOUS VAPOR,

UNDER A PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT, ADOPTED IN THE GREENWICH OBSERVATIONS.

This table contains the values of the elastic force of vapor for temperatures from 0° to 90° Fahrenheit, derived from Dalton's experiments by Biot's formula, by Anderson, and published in Edinburgh Encyclopædia, Art. Hygrometry. It is republished, without the last decimal, in the volumes of the Greenwich Magnetic and Meteorological Observations, and on it are based the various hygrometrical tables published by Mr. Glaisher, either in the Greenwich volumes, or separately, most of which will be found below, Tables XII. to XVII.

Since Dalton published his experiments, numerous attempts have been made by various skilful physicists to determine with greater accuracy the elastic force of vapor. Dr. Ure in England, Regnault in France, and Magnus in Germany, deserve in this respect a special notice.

The last two experimenters having arrived simultaneously at results nearly identical, and their experiments having been conducted with all the care that modern science requires, and the means that it can secure, their determinations seem to command an especial confidence, and to deserve the preference over all others. It is, therefore, much to be regretted that the usefulness of the following otherwise so valuable tables, the formation of which involved so much labor, is in a measure impaired by the fact that they were computed from elements which cannot be regarded as the most reliable we now possess.



# XI.

# TABLE

OF THE

# ELASTIC FORCE OF AQUEOUS VAPOR,

UNDER A BAROMETRIC PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

#### From the Greenwich Observations.

Temper-					Tenths of	Degrees.				
ature Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
0	0.061	0.061	0.062	0.062	0.062	0.062	0.063	0.063	0.063	0.063
1	0.064	0.064	0.064	0.064	0.065	0.065	0.065	0.065	0.066	0.066
2	0.066	0.066	0.067	0.067	0.067	0.067	0.068	0.068	0.068	0.068
3	0.069	0.069	0.069	0.069	0.070	0.070	0.070	0.071	0.071	0.071
4	0.071	0.072	0.072	0.072	0.072	0.073	0.073	0.073	0.073	0.074
5	0.074	0.074	0.075	0.075	0.075	0.075	0.076	0.076	0.076	0.077
6	0.077	0.077	0.077	0.078	0.078	0.078	0.079	0.079	0.079	0.080
7	0.080	0.080	0.080	0.081	0.081	0.081	0.082	0.082	0.082	0.083
8	0.083	0.083	0.083	0.084	0.084	0.084	0.085	0.085	0.085	0.086
9	0.086	0.086	0.087	0.087	0.087	0.088	0.088	0.088	0.089	0.089
10	0.089	0.090	0.090	0.090	0.091	0.091	0.091	0.092	0.092	0.092
11	0.093	0.093	0.093	0.094	0.094	0.094	0.095	0.095	0.096	0.096
12	0.096	0.097	0.097	0.097	0.098	0.098	0.098	0.099	0.099	0.099
13	0.100	0.100	0.101	0.101	0.101	0.102	0.102	0.102	0.103	0.103
14	0.104	0.104	0.104	0.105	0.105	0.106	0.106	0.106	0.107	0.107
15	0.108	0.108	0.108	0.109	0.109	0.110	0.110	0.110	0.111	0.111
16	0.112	0.112	0.112	0.113	0.113	0.114	0.114	0.115	0.115	0.115
17	0.116	0.116	0.117	0.117	0.118	0.118	0.118	0.119	0.119	0.120
18	0.120	0.121	0.121	0.121	0.122	0.122	0.123	0.123	0.124	0.124
19	0.125	0.125	0.126	0.126	0.126	0.127	0.127	0.128	0.128	0.129
20	0.129	0.130	0.130	0.131	0.131	0.132	0.132	0.133	0.133	0.134
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

## ELASTIC FORCE OF AQUEOUS VAPOR.

From the Greenwich Observations.

Temper-					Teaths of	Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.									
21	0.134	0.135	0.135	0.136	0.136	0.137	0.137	0.138	0.138	0.139
22	0.139	0.140	0.140	0.141	0.141	0.142	0.142	0.143	0.143	0.144
23	0.144	0.145	0.145	0.146	0.146	0.147	0.147	0.148	0.148	0.149
24	0.150	0.150	0.151	0.152	0.152	0.152	0.153	0.153	0.154	0.155
25	0.155	0.156	0.156	0.157	0.157	0.158	0.158	0.159	0.160	0.160
26	0.161	0.161	0.162	0.163	0.163	0.164	0.164	0.165	0.165	0.166
27	0.167	0.167	0.168	0.168	0.169	0.170	0.170	0.171	0.172	0.172
28	0.173	0.173	0.174	0.175	0.175	0.176	0.177	0.177	0.178	0.178
29	0.179	0.180	0.180	0.181	0.182	0.182	0.183	0.184	0.184	0.185
30	0.186	0.186	0.187	0.188	0.188	0.189	0.190	0.190	0.191	0.192
31	0.192	0.193	0.194	0.194	0.195	0.196	0.197	0.197	0.198	0.198
32	0.192	0.200	0.201	0.201	0.202	0.203	0.204	0.204	0.205	0.206
33	0.133	0.207	0.201	0.201	0.202	0.210	0.211	0.212	0.203	0.200
34	0.207	0.207	0.203	0.203	0.217	0.218	0.211	0.212	0.213	0.213
35	0.214	0.213	0.210	0.210	0.225	0.226	0.227	0.213	0.228	0.229
99	0.222	0.220	0.220	0.224	0.220	0.220	0.227	0.221	0.220	0.225
36	0.230	0.231	0.231	0.232	0.233	0.234	0.235	0.235	0.236	0.237
37	0.238	0.239	0.240	0.240	0.241	0.242	0.243	0.244	0.245	0.246
38	0.246	0.247	0.248	0.249	0.250	0.251	0.252	0.253	0.253	0.254
39	0.255	0.256	0.257	0.258	0.259	0.260	0.261	0.262	0.263	0.263
40	0.264	0.265	0.266	0.267	0.268	0.269	0.270	0.271	0.272	0.273
41	0.274	0.275	0.276	0.277	0.278	0.279	0.280	0.281	0.282	0.282
42	0.283	0.284	0.285	0.286	0.287	0.288	0.289	0.290	0.291	0.292
43	0.293	0.295	0.296	0.297	0.298	0.299	0.300	0.301	0.302	0.303
44	0.304	0.305	0.306	0.307	0.308	0.309	0.310	0.311	0.312	0.313
45	0.315	0.316	0.317	0.318.	0.319	0.320	0.321	0.322	0.323	0.324
46	0.326	0.327	0.328	0.329	0.330	0.331	0.332	0.333	0.335	0.336
47	0.320	0.327	0.339	0.340	0.342	0.343	0.344	0.345	0.333	0.348
48	0.349	0.350	0.351	0.352	0.354	0.355	0.356	0.357	0.358	0.360
49	0.349	0.362	0.363	0.365	0.366	0.367	0.368	0.370	0.333	0.372
50	0.373	0.302	0.376	0.377	0.379	0.380	0.381	0.382	0.383	0.385
30	0.010	0.010	0.070	0.011	0.015	0.000	0.501	0.002	0.000	0.000
51	0.386	0.388	0.389	0.390	0.392	0.393	0.394	0.396	0.397	0.398
52	0.400	0.401	0.402	0.404	0.405	0.407	0.408	0.409	0.411	0.412
53	0.414	0.415	0.416	0.418	0.419	0.421	0.422	0.423	0.425	0.426
5 i 55	0.428 0.442	0.429 0.444	0.431 0.445	0.432 0.447	0.434 0.449	0.435 0.450	0.437 0.452	0.438 0.453	0.440 0.455	0.441 $0.456$
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

### ELASTIC FORCE OF AQUEOUS VAPOR.

From the Greenwich Observations.

			,	Tom the G	1eenwich C	bservation				
Temper-					Tenths of	f Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eug. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
56	0.458	0.459	0.461	0.462	0.464	0.465	0.467	0.469	0.470	0.472
57	0.473	0.475	0.476	0.478	0.480	0.481	0.483	0.485	0.486	0.488
58	0.489	0.491	0.493	0.494	0.496	0.498	0.499	0.501	0.503	0.504
59	0.506	0.508	0.509	0.511	0.513	0.515	0.516	0.518	0.520	0.521
60	0.523	0.525	0.527	0.528	0.530	0.532	0.534	0.536	0.537	0.539
61	0.541	0.543	0.544	0.546	0.548	0.550	0.552	0.554	0.555	0.557
62	0.559	0.561	0.563	0.565	0.567	0.568	0.570	0.572	0.574	0.576
63	0.578	0.580	0.582	0.584	0.586	0.588	0.590	0.591	0.593	0.595
64	0.597	0.599	0.601	0.603	0.605	0.607	0.609	0.611	0.613	0.615
65	0.617	0.619	0.621	0.623	0.626	0.628	0.630	0.632	0.634	0.636
66	0.638	0.640	0.642	0.644	0.646	0.648	0.651	0.653	0.655	0.657
67	0.659	0.661	0.664	0.666	0.668	0.670	0.672	0.674	0.677	0.679
68	0.681	0.684	0.686	0.688	0.690	0.692	0.695	0.697	0.699	0.701
69	0.704	0.706	0.708	0.711	0.713	0.715	0.717	0.720	0.722	0.725
70	0.727	0.729	0.732	0.734	0.736	0.739	0.741	0.744	0.746	0.748
		0.000	0 === 0	0 ===0	0 =07	0 = 40	0.200	0 = 20	0 ====	0 ==0
71	0.751	0.753	0.756	0.758	0.761	0.763	0.766	0.768	0.771	0.773
72	0.776	0.778	0.781	0.783	0.785	0.787	0.790	0.792	0.795	0.797
73	0.801	0.803	0.806	0.809	0.811	0.814	0.817	0.819	0.822	0.824
74	0.827	0.830	0.832	0.835	0.838	0.840	0.843	0.846	0.849	0.851
75	0.854	0.857	0.860	0.862	0.865	0.868	0.871	0.873	0.876	0.879
76	0.882	0.885	0.887	0.890	0.893	0.896	0.899	0.902	0.905	0.908
77	0.852	0.913	0.916	0.919	0.933	0.925	0.928	0.902	0.934	0.937
78	0.910	0.943	0.916	0.919	0.952	0.955	0.928	0.961	0.964	0.967
79	0.940	0.943	0.976	0.979	0.983	0.986	0.989	0.992	0.995	0.998
80	1.001	1.005	1.008	1.011	1.014	1.017	1.021	1.024	1.027	1.030
	1.001	21000	11000	1.011	1.011	1.01.	1.021	1.021	11021	1.000
81	1.034	1.037	1.040	1.043	1.047	1.050	1.053	1.057	1.060	1.063
82	1.067	1.069	1.073	1.077	1.080	1.083	1.087	1.090	1.094	1.097
83	1.101	1.104	1.108	1.111	1.114	1.118	1.121	1.125	1.129	1.132
84	1.136	1.139	1.143	1.146	1.150	1.153	1.157	1.160	1.164	1.167
85	1.171	1.175	1.178	1.182	1.186	1.190	1.193	1.197	1.201	1.205
86	1.209	1.212	1.216	1.220	1.224	1.228	1.232	1.235	1.239	1.243
87	1.247	1.251	1.255	1.258	1.262	1.266	1.270	1.274	1.278	1.282
88	1.286	1.290	1.294	1.298	1.302	1.306	1.310	1.314	1.318	1.322
89	1.326	1.330	1.335	1.339	1.343	1.347	1.351	1.355	1.359	1.364
90	1.368	1.372	1.376	1.381	1.385	1.389	1.393	1.397	1.402	1.406
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	•					•	•		•	•

## XII.

## PSYCHROMETRICAL TABLE,

GIVING THE TEMPERATURE OF THE DEW-POINT, THE FORCE AND THE WEIGHT OF VAPOR IN THE ATMOSPHERE, AND ITS RELATIVE HUMIDITY, DEDUCED FROM THE INDICATIONS OF THE PSYCHROMETER, OR DRY AND WET BULB THERMOMETERS.

#### By James Glaisher.

This elaborate table, first published in London, in 1847, in pamphlet form, by J. Glaisher, of the Royal Observatory at Greenwich, is based on the tables of elastic forces of vapor deduced from Dalton's experiments, and given above, Table XI.

The weight of a cubic foot of dry air at 32° Fahrenheit, and under the barometric pressure of 30 inches, which has been adopted by Glaisher, and from which the weight of vapor in a cubic foot of air is derived, is the mean of the determinations obtained by Shuckburgh and by Biot and Arago, which is 563.2154 grains Troy; 563 being the number actually used in the calculations. See Preface to the Table, p. 13, and also the *Greenwich Meteorological Observations* for 1842, p. xlvi.

The coefficient of the expansion of air which has been employed is that determined by the experiments of Gay-Lussac, according to which the air expands 0.00375 of its bulk for 1° Centigrade, or  $\frac{1}{1200}$  for 1° Fahrenheit.

All these values, as may be seen by comparing Tables VI. and XI. of the elastic forces, and also page 92, materially differ from those more recently determined with great care by Regnault, and on which are based the Psychrometrical Tables given above, page 50 et seq. This will account for the no inconsiderable differences often found between the results in the two tables derived from the same data. A few examples, taken from various parts of the tables, may be given here, in order to enable the meteorologist to judge of the amount of the discrepancies which may occur in the results when computed from different hygrometrical constants.

1. Suppose the temperature of the air indicated by the dry thermometer ter to be  $= 10^{\circ} \text{ F.}$ The temperature of evaporation indicated by the wet thermometer  $= 9^{\circ} \text{ F.}$ Difference  $1^{\circ} \text{ F.}$ 

Then, Glaisher's table gives,

The Force of Vapor = 0.065 inch. The Relative Humidity = 0.730

Guyot's table gives,

The Force of Vapor = 0.054 inch. The Relative Humidity = 0.791

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2. By observation we have,

Dry Thermometer  $= 50^{\circ}$  F.

Wet Thermometer  $= 40^{\circ}$  F.

Difference =  $10^{\circ}$  F.

Then, by Glaisher's table, we find,

Force of Vapor = 0.186 inch.

Relative Humidity = 0.495

And by Guyot's table, we find,

Force of Vapor = 0.117 inch.

Relative Humidity = 0.322

3. The reading of the

Dry Thermometer is  $= 90^{\circ}$  F.

Wet Thermometer is  $= 70^{\circ}$  F.

Difference =  $20^{\circ}$  F.

By Glaisher's table we have,

Force of Vapor = 0.523 inch.

Relative Humidity = 0.381

And by Guyot's table,

Force of Vapor = 0.464 inch.

Relative Humidity = 0.329

The temperatures of the Dew-Point, given in Glaisher's tables, have been computed by means of the empirical factors given below, page 140, and in the manner there described. See Preface to the Table, page 11.

#### ARRANGEMENT OF THE TABLE.

In the first two columns, at the left, are found the indications, in degrees of Fahrenheit, of the dry and wet bulb thermometers. In the following columns, in their order, and opposite to each of the temperatures of the wet thermometer, are given the temperature of the dew-point; the force of vapor, in English inches; the weight of vapor, in grains, contained in a cubic foot of air; the amount of the same required for saturation; and the relative humidity in thousandths, corresponding to the difference of temperature between the two thermometers. The second half of the page, at the right, furnishes, in seven columns, the weight, in grains, of a cubic foot of air, under various barometric pressures from 28 to 31 inches, and in the different hygrometric conditions indicated by the differences of the two thermometers. These numbers have been computed in the manner described below, page 142.

The range of the table extends from 10° to 90° of the dry thermometer, or of the temperature of the air. From 10° to 34° Fahrenheit the results are calculated for every second, third, and fifth of a degree of the wet thermometer, and for extreme differences of the temperature of evaporation ranging from 2° to 5° below the temperature of the air. From 34° to 90° the results are given only for every full degree of the wet thermometer, and for extreme differences gradually increasing

В

#### PSYCHROMETRICAL TABLE.

from 5° to 27°. This range falls short of the wants of the extreme climate of North America, where temperatures above 90° and far below 10° are of usual occurrence over a great portion of the continent. The same may be said of the range of the differences between the two thermometers in the first part of the table. The double interpolation for the fractions of degrees of both thermometers being rather too large to be neglected, its application becomes inconvenient.

### USE OF THE TABLE.

Enter the table with the observed temperatures of the dry and wet bulb thermometers. On the same line as the last, and in their appropriate columns, the results deduced from these data will be found.

## Example.

The observation has given,

Temperature of the air by the dry thermometer  $= 62^{\circ}$  F.

Temperature of evaporation by the wet-bulb thermometer  $=53^{\circ}$  F.

Page 129, find in the first column, headed Reading of the Dry Thermometer, the temperature of 62°, and in the second, that of the wet, 53°. On the line beginning with 53° are found, in their respective columns, the results deduced from these data, viz.:—

The temperature of the Dew-point  $= 46^{\circ}.7$  F.

The force of vapor in the air = 0.333 inch.

The weight of vapor in a cubic foot of air = 3.72 grains.

The amount of vapor required for saturation = 2.53 grains.

The relative humidity in thousandths = 0.595

	ading Ther-	Temp.	Force	Wei of V		Hu-		Weigh	t in Grain	ns of a Cu	bic Foot	of Air.	
moi	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0 10	10.0	10.0	in. 0.089	gr. 1.11	gr. 0.00	1.000	gr. 550.1	gr. 560.0	gr. 569.8	gr. 579.6	gr. 589.4	gr. 599.2	gr. 609.0
	9.8	8.3	0.084	1.05	0.06	0.946	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.6	6.6	0.079	0.98	0.13	0.883	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.4	4.9	0.074	0.92	0.19	0.829	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.2	3.2	0.069	0.86	0.25	0.775	550.3	560.2	570.0	579.8	589.6	599.4	609.2
	9.0	1.5	0.065	0.81	0.30	0.730	550.3	560.3	570.0	579.8	589.6	599.4	609.3
11	11.0	11.0	0.093	1.15	0.00	1.000	548.9	558.7	568.5	578.3	588.1	597.9	607.7
	10.8	9.3	0.087	1.08	0.07	0.939	548.9	558.7	568.5	578.3	588.1	597.9	607.7
	10.6	7.6	0.082	1.02	0.13	0.887	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.4	5.9	0.077	0.96	0.19	0.835	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.2	4.2	0.072	0.90	0.25	0.783	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.0	2.5	0.067	0.84	0.31	0.731	549.1	558.9	568.7	578.6	588.3	598.1	607.9
	9.8	0.8	0.063	0.78	0.37	0.679	549.1	558.9	568.7	578.6	588.3	598.1	607.9
12	12.0	12.0	0.096	1.19	0.00	1.000	547.7	557.5	567.2	577.0	586.8	596.6	606.4
	11.8	10.3	0.090	1.12	0.07	0.942	547.7	557.5	567.2	577.0	586.8	596.6	606.4
	11.6	8.6	0.085	1.05	0.14	0.883	547.8	557.6	567.3	577.1	586.9	596.7	606.5
	11.4	6.9	0.080	0.99	0.20	0.832	547.8	557.6	567.3	577.1	586.9	596.7	606.5
	11.2	5.2	0.075	0.93	0.26	0.782	547.8	557.6	567.3	577.1	586.9	596.7	606.5
	11.0	3.5	0.070	0.87	0.32	0.731	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.8	1.8	0.066	0.81	0.38	0.681	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.6	0.1	0.061	0.76	0.43	0.639	547.9	557.7	567.4	577.2	587.0	596.8	606.6
13	13.0	13.0	0.100	1.24	0.00	1.000	546.5	556.3	566.0	575.8	585.5	595.3	605.0
	12.8	11.3	0.094	1.16	0.08	0.936	546.5	556.3	566.0	575.8	585.5	595.3	605.0
	12.6	9.6	0.088	1.08	0.16	0.871	546.6	556.4	566.1	575.9	585.6	595.4	605.1
	12.4	7.9	0.083	1.02	0.22	0.823	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	12.2	6.2	0.077	0.97	0.27	0.783	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	12.0	4.5	0.073	0.91	0.33	0.734	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	11.8	2.8	0.068	0.84	0.40	0.678	546.8	556.6	566.3	576.1	585.8	595.6	605.3
	11.6	1.1	0.064	0.79	0.45	0.637	546.8	556.6	566.3	576.1	585.8	595.6	605.3
14	14.0	14.0	0.104	1.28	0.00	1.000	545.3	555.0	564.7	574.4	584.2	594.0	603.7
	13.8	12.3	0.097	1.20	0.08	0.938	545.3	555.0	564.7	574.4	584.2	594.0	603.7
	13.6	10.6	0.091	1.12	0.16	0.875	545.4	555.1	564.8	574.5	584.3	594.1	603.8
	13.4	8.9	0.086	1.06	0.22	0.828	545.4	555.1	564.8	574.5	584.3	594.1	603.8
	13.2	7.2	0.080	1.00	0.28	0.782	545.4	555.1	564.8	574.5	584.3	594.1	603.8
- Anna Communication	13.0 12.8	3.8	0.075	0.93	0.35	0.727	545.5	555.2	564.9	574.6 574.6	584.4 584.4	594.2	603.9
	12.6	2.1	0.066	0.82	0.41	0.680	545.5 545.6	555.2 555.3	564.9 565.0	574.7	584.5	594.2	603.9
15	15.0	15.0	0.108	1.32	0.00	1.000	544.0	553.8	563.5	573.2	582.9	592.6	602.3
	14.8	13.3	0.101	1.24	0.08	0.940	544.0	553.8	563.5	573.2	582.9	592.6	602.3
	14.6	11.6	0.095	1.16	0.16	0.879	544.1	553.9	563.6	573.3	583.0	592.7	602.4
	14.4	9.9	0.089	1.10	0.22	0.833	544.1	553.9	1	573.3	583.0	592.7	602.4
	14.2	8.2	0.083	1.04	0.28	0.788	544.2	554.0	563.7	573.4	583.1	592.8	602.5
	14.0	6.5	0.078	0.97	0.35	0.735	544.2	554.0	563.7	573.4	583.1	592.8	602.5
	13.8	4.8	0.073	0.90	1	0.682	544.2	1	1	573.4	583.1	592.8	602.5
	13.6	3.1	0.069	0.85	0.47	0.644	544.3	554.1	563.8	573.5	583.2	592.9	602.6

		ding	Temp.	Force		ight apor	Hu-		Weigh	t in Grai	ns of a Cu	ıbic Foot	of Air.	
		neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
I	ry.	Wet.	Fahr.	English Inches.	Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	in. 29.5	30.0	30.5	31.0
	. 0	100	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
1	16	16.0 15.8	16.0 14.3	0.112	1.37 1.29	0.00	0.942	542.8 542.9	552.5 552.6	562.2 562.3	571.9 572.0	581.6 581.7	591.3 591.4	601.0
		15.6	12.6	0.098	1.21	0.16	0.883	542.9	552.6	562.3	572.0	581.7	591.4	601.1
		15.4	10.9	0.092	1.14	0.23	0.832	543.0	552.7	562.4	572.1	581.8	591.5	601.2
		15.2	9.2	0.087	1.07	0.30	0.781	543.0	552.7	562.4	572.1	581.8	591.5	601.2
		15.0	7.5	0.081	1.00	0.37	0.730	543.0	552.7	562.4	572.1	581.8	591.5	601.2
	- 1	14.8	5.8	0.076	0.94	0.43	0.686	543.1	552.8	562.5	572.1	581.9	591.6	601.3
		14.6	4.1	0.072	0.88	0.49	0.643	543.1	552.8	562.5	572.1	581.9	591.6	601.3
	17	17.0	17.0	0.116	1.41	0.00	1.000	541.3	551.0	560.8	570.5	580.1	589.8	599.4
		16.8	15.3	0.109	1.33	0.08	0.943	541.3	551.0	560.8	570.5	580.1	589.8	599.4
-		16.6	13.6	0.102	1.25	0.16	0.887	541.4	551.1	560.9	570.6	580.2	589.9	599.5
		16.4	11.9	0.096	1.17	0.24	0.830	541.4	551.1	560.9	570.6	580.2	589.9	599.5
		16.2	10.2	0.090	1.10	0.31	0.780	541.5	551.2	561.0	570.7	580.3	590.0	599.6
		16.0	8.5	0.084	1.03	0.38	0.730	541.5	551.2	561.0	570.7	580.3	590.0	599.6
	ĺ	15.8	6.8	0.079	0.97	0.44	0.688	541.5	551.2	561.0	570.7	580.3	590.0	599.6
		15.6	5.1	0.074	0.91	0.50	0.646	541.6	551.3	561.1	570.8	580.4	590.1	599.7
	18	18.0	18.0	0.120	1.47	0.00	1.000	540.5	550.2	559.8	569.5	579.1	588.8	598.4
		17.8	16.3	0.113	1.38	0.09	0.939	540.5	550.2	559.8	569.5	579.1	588.8	598.4
i		17.6	14.6	0.106	1.29	0.18	0.878	540.6	550.3	559.9	569.6	579.2	588.9	598.5
		17.4	12.9	0.099	1.21	0.26	0.824	540.6	550.3	559.9	569.6	579.2	588.9	598.5
		17.2	11.2	0.093	1.14	0.33	0.776	540.7	550.4	560.0	569.7	579.3	589.0	598.6
		17.0	9.5	0.088	1.07	0.40	0.728	540.7	550.4	560.0	569.7	579.3	589.0	598.6
		16.8	7.8	0.082	1.01	0.46	0.688	540.7	550.5	560.1	569.8	579.3	589.0	598.6
		16.6	6.1	0.077	0.95	0.52	0.647	540.8	550.6	560.2	569.9	579.4	589.1	598.7
	19	19.0	19.0	0.125	1.52	0.00	1.000	539.3	548.9	558.5	568.2	577.8	587.5	597.1
		18.8	17.3	0.117	1.43	0.09	0.941	539.3	548.9	558.5	568.2	577.8	587.5	597.1
		18.6	15.6	0.110	1.34	0.18	0.882	539.4	549.0	558.6	568.3	577.9	587.6	597.2
		18.4	13.9	0.103	1.26	0.26	0.829	539.4	549.0	558.6	568.3	577.9	587.6	597.2
		18.2	12.2	0.097	1.18	0.34	0.776	539.5	549.1	558.7	568.4	578.0	587.7	597.3
		18.0	10.5	0.091	1.11	0.41	0.730	539.5	549.1	558.7	568.4	578.0	587.7	597.3
		17.8	8.8	0.085	1.04 0.98	0.48	0.684	539.6	549.2	558.8	568.5	578.1	587.8 587.8	597.4
		17.6	7.1	0.050	0.98	0.54	0.645	539.6	549.2	558.8	568.5	578.1	957.8	597.4
	20	20.0	20.0	0.129	1.58	0.00	1.000	538.1	547.7	557.3	566.9	576.5	586.1	595.7
		19.8	18.3	0.121	1.48	0.10	0.937	538.2	547.8	557.4	567.0	576.6	586.2	595.8
		19.6	16.6	0.114	1.38	0.20	0.874	538.3	547.9	557.5	567.1	576.7	586.3	595.9
		19.4	14.9	0.107	1.30	0.28	0.823	538.3	547.9	557.5		576.7	586.3	595.9
		19.2	13.2	0.101	1.23	0.35	0.779	538.3	547.9	557.5	567.1	576.7	586.3	595.9
		19.0	11.5	0.094	1.15	0.43	0.728	538.4	548.0	557.6	567.2	576.8	586.4	596.0
		18.8	9.8	0.089	1.08	0.50	0.684	538.4	548.0	557.6	1	576.8	586.4	596.0
		18.6	8.1	0.083	1.01	0.57	0.639	538.5	548.1	557.7	567.3	576.9	586.5	596.1
		18.4	6.4	0.078	0.95	0.63	0.601	538.5	548.1	557.7	567.3	576.9	586.5	596.1
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Rea of '	ding	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cu	bic Foot	of Air.	
	neter,	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
21	21.0	21.0	in. 0.134	gr. 1.63	gr. 0.00	1.000	gr. 537.0	gr. 546.6	gr. 556.1	gr. 565.7	gr. 575.3	gr. 584.9	gr. 594.5
	20.8	19.3	0.126	1.53	0.10	0.939	537.0	546.6	556.1	565.7	575.3	584.9	594.5
	20.6	17.6	0.118	1.44	0.19	0.884	537.1	546.7	556.2	565.8	575.4	555.0	594.6
	20.4	15.9	0.111	1.36	0.27	0.835	537.1	546.7	556.2	565.8	575.4	585.0	594.6
	20.2	14.2	0.104	1.28	0.35	0.785	537.2	546.8	556.3	565.9	575.5	585.1	594.7
	20.0	12.5	0.098	1.20	0.43	0.736	537.2	546.8	556.3	565.9	575.5	585.1	594.7
	19.8	10.8	0.092	1.12	0.51	0.687	537.3	546.9	556.4	566.0	575.6	585.2	594.8
	19.6	9.1	0.086	1.05	0.58	0.644	537.3	546.9	556.4	566.0	575.6	585.2	594.8
	19.4	7.4	0.081	0.99	0.64	0.607	537.3	546.9	556.4	566.0	575.6	585.2	594.8
22	22.0	22.0	0.139	1.69	0.00	1.000	535.7	545.3	554.9	564.5	574.0	583.6	593.1
24	21.8	20.3	0.131	1.59	0.10	0.941	535.8	545.4	555.0	564.6	574.1	583.7	593.2
	21.6	18.6	0.123	1.49	0.20	0.882	535.8	545.4	555.0	564.6	574.1	583.7	593.2
	21.4	16.9	0.115	1.40	0.29	0.828	535.9	545.5	555.1	564.7	574.2	583.8	593.3
	21.2	15.2	0.108	1.31	0.38	0.775	535.9	545.5	555.1	564.7	574.2	583.8	593.3
	21.0	13.5	0.102	1.23	0.46	0.728	536.0	545.6	555.2	564.8	574.3	583.9	593.4
	20.8	11.8	0.096	1.16	0.53	0.686	536.0	545.6	555.2	564.8	574.3	583.9	593.4
	20.6	10.1	0.090	1.09	0.60	0.645	536.1	545.7	555.3	564.9	574.4	584.0	593.5
	20.4	8.4	0.084	1.02	0.67	0.604	536.1	545.7	555.3	564.9	574.4	584.0	593.5
	20.2	6.7	0.079	0.96	0.73	0.568	536.1	545.7	555.3	564.9	574.4	584.0	593.5
23	23.0	23.0	0.144	1.75	0.00	1.000	534.6	544.2	553.7	563.3	572.8	582.4	591.9
	22.8	21.3	0.136	1.65	0.10	0.943	534.6	544.2	553.7	563.3	572.8	582.4	591.9
	22.6	19.6	0.127	1.55	0.20	0.886	534.7	544.3	553.8	563.4	572.9	582.5	592.0
	22.4	17.9	0.120	1.45	0.30	0.829	534.7	544.3	553.8	563.4	572.9	582.5	592.0
	22.2	16.2	0.112	1.36	0.39	0.777	534.8	544.4	553.9	563.5	573.0	582.6	592.1
	22.0	14.5	0.106	1.28	0.47	0.731	534.8	544.4	553.9	563.5	573.0	582.6	592.1
	21.8	12.8	0.099	1.21	0.54	0.691	534.9	544.5	554.0	563.6	573.1	582.7	592.2
	21.6	11.1	0.093	1.13	0.62	0.646	534.9	544.5	554.0	563.6	573.1	582.7	592.2
	21.4	9.4	0.087	1.06	0.69	0.606	535.0	544.6	554.1	563.7	573.2	582.8	592.3 592.3
	21.2	7.7	0.082	1.00	0.75	0.571	535.0	544.6	554.1	563.7	573.2	582.8	392.3
24	24.0	24.0	0.150	1.81	0.00	1.000	533.4	542.9	552.4	562.0	571.5	581.1	590.6
	23.8	22.5	0.142	1.72	0.09	0.951	533.5	543.0	552.5	562.1	571.6	581.2	590.7
	23.6	21.1	0.135	1.63	0.18	0.901	533.5	543.1	552.5	562.1	571.6	581.2	590.7
	23.4	13	0.127	1.55	0.26	0.856	533.6	543.2	552.6	562.2	571.7	581.3	590.8
	23.2	18.2	0.121	1.46	0.35	0.807	533.6	543.2	552.6	562.2	571.7	581.3	590.8
	23.0	16.7	0.115	1.38	0.43	0.762	533.7	543.3	552.7	562.3	571.8	581.4	
	22.8	15.2	0.108		0.50			543.3			571.8	581.4	
	22.6	il .	0.103	1		0.685	533.7	1	1	1	571.8	581.4	
	22.4	III .		1	1		533.8		1	562.4	571.9	581.5	591.0
1	22.2	10.8	0.091	1.12	0.69	0.634	533.8	543.4	552.8	562.4	571.9	581.5	591.0

Re	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	ns of a Cu	abic Foot	of Air.	
	meter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.		of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	in. 31.0
0	0	0	in.	gr.	gr.	7 000	gr.						
25	$25.0 \\ 24.8$	25.0 23.7	0.155 0.148	1.87	0.00	1.000	532.3 532.3	541.8 541.8	551.3 551.3	560.8 560.8	570.3 570.3	579.8 579.8	589.3 589.3
	24.6	22.4	0.141	1.70	0.03	0.909	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.4	21.2	0.135	1.62	0.25	0.867	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.2	19.9	0.129	1.55	0.32	0.829	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.0	18.6	0.123	1.48	0.49	0.791	532.5	542.0	551.5	561.0	570.5	580.0	589.5
	23.8	17.3	0.117	1.41	0.46	0.754	532.5	542.0	551.5	561.0	570.5	580.0	589.5
	23.6	16.0	0.112	1.34	0.53	0.717	532.6	542.1	551.6	561.1	570.6	580.1	589.6
	23.4	14.8	0.107	1.28	0.59	0.685	532.6	542.1	551.6	561.1	570.6	580.1	589.6
	23.2	13.5	0.102	1.22	0.65	0.653	532.6	542.1	551.6	561.1	570.6	580.1	589.6
26	26.0	26.0	0.161	1.93	0.00	1.000	531.1	540.6	550.0	559.5	569.0	578.5	588.0
20	25.8	24.8	0.154	1.85	0.08	0.959	531.1	540.7	550.1	559.6	569.1	578.6	588.1
	25.6	23.6	0.147	1.78	0.15	0.923	531.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.4	22.3	0.141	1.70	0.23	0.881	531.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.2	21.2	0.135	1.62	0.31	0.839	531.3	540.8	550.2	559.7	569.2	578.7	588.2
	25.0	19.9	0.129	1.55	0.38	0.804	531.3	540.8	550.2	559 <b>.7</b>	569.2	578.7	588.2
	24.8	18.7	0.123	1.48	0.45	0.767	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.6	17.5	0.118	1.41	0.52	0.731	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.4	16.2	0.112	1.35	0.58	0.700	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.2	15.0	0.108	1.29	0.64	0.668	531.5	541.0	550.4	559.9	569.4	578.9	588.4
27	27.0	27.0	0.167	2.00	0.00	1.000	529.9	539.4	548.9	558.4	567.8	577.3	586.7
-	26.7	25.2	0.156	1.88	0.12	0.940	529.9	539.4	548.9	558.4	567.8	577.4	586.8
	26.4	23.3	0.146	1.76	0.24	0.880	530.0	539.5	549.0	558.5	567.9	577.5	586.9
	26.1	21.5	0.137	1.64	0.36	0.820	530.1	539.6	549.1	558.6	568.0	577.6	587.0
	25.8	19.7	0.128	1.53	0.47	0.765	530.1	539.6	549.1	558.6	568.0	577.6	587.0
	25.5	17.8	0.119	1.43	0.57	0.715	530.2	539.7	549.2	558.7	568.1	577.7	587.1
	25.2	16.0	0.112	1.34	0.66	0.670	530.3	539.8	549.3	558.8	568.2	577.8	587.5
	24.9	14.2	0.104	1.26	0.74	0.630	530.3	539.8	549.3	558.8	568.2	577.8	587.2
	24.6	12.4	0.098	1.17	0.83	0.585	530.4	539.9	549.4	558.9	568.3	577.9	587.3
	24.3	10.5	0.091	1.09	0.91	0.545	530.5	540.0	549.5	559.0	568.3	577.9	587.3
28	28.0	28.0	0.173	2.07	0.00	1.000	528.7	538.1	547.6	557.0	566.5	575.9	585.4
	27.7	26.3	1	i	0.12	0.942	528.8	1	547.7		566.6	576.0	585.
	27.4	24.6	0.153	1.84	0.23	0.889	528.9	538.3	547.8	557.2	566.7	576.1	585.6
	27.1	22.9	0.144	1.73	0.34	0.836	528.9	538.3	547.8	557.2	566.7	576.1	585.0
	26.8	21.2	0.135	1.62	0.45	0.783	529.0	538.4	547.9	557.3	566.8	576.2	585.
	26.5	19.4	0.126	1.52	0.55	0.734	529.1	538.5	548.0	557.4	566.9	576.3	585.8
	26.2	17.7	0.119	1.42	0.65	0.686	529.1	538.5	548.0	557.4	566.9	576.3	585.8
	25.9	16.0	0.112	1.34	0.73	0.648	529.2	538.6	548.1	557.5	567.0	576.4	585.9
	25.6	14.3 12.6	0.105	1.26	0.82	0.604	529.2	538.6	548.1	557.5	567.0 567.0	576.4 576.4	585.9 585.9
1	20.3	12.0	0.098	1.18	0.89	0.571	529.2	538.6	548.1	997.0	307.0	970.4	1 999.5

	ading	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	in. 28.0	28.5	29.0	29.5	30.0	30.5	31.0
29	29.0	29.0	in. 0.179	gr. 2.14	gr. 0.00	1.000	gr. 527.6	gr. 537.0	gr. 546.5	gr. 555.9	gr. 565.3	gr. 574.7	gr. 584.1
20	28.7	27.5	0.170	2.03	0.11	0.949	527.7	537.1	546.6	556.0	565.4	574.8	584.2
	28.4	26.0	0.161	1.92	0.22	0.898	527.7	537.1	546.6	556.0	565.4	574.8	584.2
	28.1	24.5	0.152	1.82	0.32	0.851	527.8	537.2	546.7	556.1	565.5	574.9	584.3
	27.8	23.0	0.144	1.73	0.41	0.809	527.8	537.2	546.7	556.1	565.5	574.9	584.3
	27.5	21.5	0.137	1.64	0.50	0.766	527.9	537.3	546.7	556.2	565.6	575.0	584.5
	27.2	20.0	0.129	1.55	0.59	0.725	528.0	537.4	546.8	556.2	565.7	575.1	584.6
	26.9	18.5	0.122	1.47	0.67	0.687	528.0	537.4	546.8	556.3	565.7	575.2	584.6
	26.6	17.0	0.116	1.38	0.76	0.645	528.1	537.5	546.9	556.4	565.8	575.3	584.7
	26.3	15.5	0.110	1.30	0.84	0.617	528.1	537.5	546.9	556.4	565.8	575.3	584.7
30	30.0	30.0	0.186	2.21	0.00	1.000	526.5	535.9	545.3	554.7	564.1	573.5	582.9
30	29.7	28.6	0.130	2.10	0.00	0.951	526.5	535.9	545.3	554.7	564.1	573.5	582.9
	29.4	27.2	0.168	2.00	0.21	0.905	526.6	536.0	545.4	554.8	564.2	573.6	583.0
	29.1	25.9	0.160	1.91	0.30	0.864	526.7	536.1	545.5	554.9	564.3	573.7	583.1
	28.8	24.5	0.152	1.82	0.39	0.824	526.7	536.1	545.5	554.9	564.3	573.7	583.1
	28.5	23.1	0.145	1.73	0.48	0.783	526.8	536.2	545.6	555.0	564.4	573.8	583.2
	28.2	21.7	0.138	1.64	0.57	0.742	526.8	536.2	545.6	555.0	564.4	573.8	583.2
	27.9	20.3	0.131	1.56	0.65	0.706	526.9	536.3	545.7	555.1	564.5	573.9	583.3
	27.6	19.0	0.125	1.49	0.72	0.674	526.9	536.3	545.7	555.1	564.5	573.9	583.3
	27.3	17.6	0.118	1.42	0.79	0.643	527.0	536.4	545.8	555.2	564.6	574.0	583.4
					}								
31	31.0	31.0	0.192	2.29	0.00	1.000	525.4	534.7	544.1	553.5	562.9	572.3	581.7
	30.7	29.9	0.185	2.20	0.09	0.961	525.4	534.7	544.1	553.5	562.9 563.0	572.3 572.4	581.7 581.8
	30.4	28.8 27.7	0.178	$\begin{vmatrix} 2.12 \\ 2.04 \end{vmatrix}$	$\begin{vmatrix} 0.17 \\ 0.25 \end{vmatrix}$	0.926	525.5	534.8 534.8	544.2 544.2	553.6 553.6	563.0	572.4	581.8
	30.1	26.6	0.171	1.95	0.23	0.852	525.6	534.9	544.3	553.7	563.1	572.5	581.9
	29.5	25.5	0.158	1.87	0.42	0.817	525.6	534.9	544.3	553.7	563.1	572.5	581.9
	29.2	24.4	0.152	1.80	0.49	0.786	525.6	534.9	544.3	553.7	563.1	572.5	581.9
	28.9	23.4	0.146	1.73	0.56	0.756	525.7	535.0	544.4	553.8	563.2	572.6	582.0
	28.6	22.3	0.141	1.67	0.62	0.729	525.7	535.0	544.4	553.8	563.2	572.6	582.0
	28.3	21.2	0.135	1.60	0.69	0.699	525.7	535.0	544.4	553.8	563.2	572.6	582.0
32	32.0	32.0	0.199	2.37	0.00	1.000	524.2	533.5	542.9	552.3	561.6	570.9	580.3
	31.6	30.8	0.191	2.27	0.10	0.958	524.3	533.6	543.0	552.4	561.7	571.0	580.4
	31.2	29.5	0.182	2.17	0.20	0.916	524.4	533.7	543.1	552.5	561.8	571.1	580.5
	30.8	28.3 27.0	0.175	2.07	0.30	0.874	524.4 524.5	533.7 533.8	543.1 543.2	552.5 552.6	561.8 561.9	571.1 571.2	580.6 580.6
	30.0	25.8	0.160	1.90	0.47	0.802	524.5	533.8	543.2	552.6	561.9	571.2	580.6
	29.6	23.8	0.153	1.82	0.47	0.302	524.6			1	562.0	571.3	1
	29.0	23.3	0.133		1	0.735	524.6	1			562.0		580.7
	28.8	22.1	0.140	1	0.70	0.705	524.6	1			562.0	571.3	580.7
	1	20.8							543.4	1	562.1		1

	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	as of a Cu	ibic Foot	of Air.	
mor	neter, ahr.	of Dew-	of Vapor in	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.		of aCu- bic Ft. of Air.	tion = 1.000.	in. 28.0	in. 28.5	in. 29.0	29.5	in. 30.0	30.5	in. 31.0
0	0	0	in.	gr.	gr.		gr.						
33	33.0	33.0	$0.207 \\ 0.197$	2.45 $2.33$	$\begin{vmatrix} 0.00 \\ 0.12 \end{vmatrix}$	1.000 0.951	523.0 523.1	532.3	541.7	551.1	560.4 560.5	569.7 569.8	579.1 579.2
	32.0	30.2	0.187	2.22	0.12	0.906	523.2	532.5 532.6	541.8 541.9	551.2 551.3	560.6	569.9	579.3
	31.5	28.8	0.137	2.11	0.23	0.862	523.3	532.7	542.0	551.4	560.7	570.0	579.4
	31.0	27.4	0.169	2.01	0.44	0.821	523.3	532.7	542.0	551.4	560.7	570.0	579.4
	30.5	26.0	0.161	1.91	0.54	0.780	523.4	532.8	542.1	551.5	560.8	570.1	579.5
	30.0	24.6	0.153	1.82	0.63	0.743	523.4	532.8	542.1	551.5	560.8	570.1	579.5
	29.5	23.2	0.145	1.74	0.71	0.711	523.5	532.9	542.2	551.6	560.9	570.2	579.6
	29.0	21.8	0.138	1.65	0.80	0.674	523.5	532.9	542.2	551.6	560.9	570.2	579.6
	28.5	20.4	0.131	1.57	0.88	0.641	523.6	533.0	542.3	551.7	561.0	570.3	579.7
34	34.0	34.0	0.214	2.53	0.00	1.000	521.9	531.2	540.6	549.9	559.2	568.5	577.8
	33.5	32.7	0.204	2.42	0.11	0.957	522.0	531.4	540.7	550.0	559.3	568.6	577.9
	33.0	31.4	0.195	2.31	0.22	0.913	522.0	531.4	540.7	550.0	559.3	568.6	577.9
	32.5	30.1	0.186	2.21	0.32	0.874	522.1	531.5	540.8	550.1	559.4	568.7	578.0
	32.0	28.8	0.178	2.11	0.42	0.834	522.1	531.5	540.8	550.1	559.4	568.7	578.0
	31.5	27.5	0.170	2.01	0.52	0.795	522.2	531.6	540.9	550.2	559.5	568.8	578.1
	31.0	26.2	0.162	1.91	0.62	0.755	522.3	531.7	541.0	550.3	559.6	568.9	578.2
	30.5	24.9	0.155	1.83	0.70	0.724	522.3	531.7	541.0	550.3	559.6	568.9	578.2
	30.0	23.6	0.147	1.75	0.78	0.692	522.4	531.8	541.1	550.4	559.7	569.0	578.3
	29.5	22.3	0.141	1.67	0.86	0.660	522.4	531.8	541.1	550.4	559.7	569.0	578.3
	29.0	21.0	0.134	1.59	0.94	0.629	522.5	531.9	541.2	550.5	559.8	569.1	578.4
35	35	35.0	0.222	2.62	0.00	1.000	520.8	530.1	539.4	548.7	558.0	567.3	576.6
50	34	32.5	0.222	2.40	0.00	0.916	520.8	530.1	539.5	548.8	558.1	567.4	576.7
	33	30.0	0.203	2.19	0.43	0.836	521.0	530.3	539.6	548.9	558.3	567.5	576.8
	32	27.5	0.170	2.00	0.62	0.764	521.1	530.4	539.7	549.0	558.4	567.6	576.9
	31	25.0	0.155	1.83	0.79	0.698	521.2	530.5	539.8	549.1	558.5	567.7	577.0
	30	22.5	0.142	1.68	0.94	0.641	521.3	530.6	539.9	549.2	558.6	567.8	577.1
	29	20.0	0.129	1.53	1.09	0.584	521.3	530.7	540.0	549.3	558.6	567.9	577.2
	28	17.5	0.117	1.39	1.23	0.531	521.4	530.8	540.1	549.4	558.7	568.0	577.3
	27	15.0	0.108	1.27	1.35	0.485	521.5	530.9	540.2	549.5	558.7	568.1	577.4
		05.0	0.5-0	2	0.00	7.000		#2C 5	<b>***</b>		***	F00 T	
36	36	36.0	0.230	2.71	0.00	1.000	519.7	529.0	538.3	547.5	556.8	566.1	575.4
	35	33.5	0.210	2.48	0.23	0.915	519.8	529.1		547.6	556.9	566.2	575.5 575.6
	34	31.0	0.192	2.27	0.44	0.838	519.9	529.2	538.5	547.7	557.0 557.1	566.3 566.4	575.7
	33 32	28.5 26.0	0.176	2.07 1.89	0.64	0.764 0.698	520.0 520.1	529.3 529.4	538.6 538.7	547.8 547.9	557.2	566.5	575.8
	31	23.5	0.147	1.74	0.97	0.642	520.2	529.5	538.8	548.0	557.3	566.6	575.9
	30	21.0	0.134	1.58	1.13	0.583	520.3	529.6	538.9	548.1	557.4	566.7	576.0
	29	18.5	0.122	1.45	1.26	0.535	520.4	529.7	539.0	548.2	557.5	566.8	576.1
	28	16.0	0.112	1.32	1.39	0.487	520.5	529.8	539.1	548.3	557.6	566.9	576.2
				<u> </u>		1				<u> </u>		<u> </u>	

her- eter, ar. Wet.	Temp. of Dew- Point, Fahr.	of Vapor in	Tno	Reqd.	Hu-		_			bic Foot		
Wet.	Fahr.		In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	n English	Inches.	
		English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0 37	37.0	in. 0.238	gr. 2.80	gr. 0.00	1.000	gr. 518.6	gr. 527.8	gr. 53 <b>7.1</b>	gr. 546.3	gr. 555.6	gr. 564.8	gr. 574.1
36	34.5	0.235	2.56	0.24	0.914	518.7	527.9	537.2	546.4	555.7	564.9	574.2
35	32.0	0.199	2.35	0.45	0.839	518.8	528.0	537.3	546.5	555.8	565.0	574.3
34	29.5	0.182	2.14	0.66	0.764	518.9	528.1	537.4	546.6	555.9	565.1	574.4
33	27.0	0.167	1.96	0.84	0.700	519.0	528.2	537.5	546.7	556.0	565.2	574.5
32	24.5	0.152	1.79	1.01	0.640	519.1	528.3	537.6	546.8	556.1	565.3	574.6
31	22.0	0.139	1.64	1.16	0.586	519.2	528.4	537.7	546.9	556.2	565.4	574.7
30	19.5	0.127	1.50	1.30	0.536	519.3	528.5	537.8	547.1	1		574.8
29	17.0	0.116	1.37	1.43	0.489	519.4	528.6	537.9	547.2	556.4	565.6	574.9
38	38.0	0.246	2.89	0.00	1,000	517.4	526.6	535.9	545.1	554.4	563.6	572.9
					1	1	526.7	536.0	545.2	554.5	563.7	573.0
36	33.0	0.207	2.43	0.46	0.841	517.6	526.8	536.1	545.3	554.6	563.8	573.1
35	30.5	0.189	2.22	0.67	0.768	517.7	526.9	536.2	545.4	554.7	563.9	573.2
34	28.0	0.173	2.03	0.86	0.703	517.8	527.0	536.3	545.5	554.8	564.0	573.3
33	25.5	0.158	1.85	1.04	0.640	517.9	527.1	536.4	545.6	554.9	564.1	573.4
32	23.0	0.144	1.70	1.19	0.588	518.0	527.2	536.5	545.7	555.0	564.2	573.5
31	20.5		1.54	1.35	0.533	518.1		1		1		573.6
30	18.0	0.120	1.39	1.50	0.481	518.2	527.4	536.7	545.9	555.2	564.4	573.7
20	39.0	0.255	2.99	0.00	1.000	516.3	525.5	534.7	543.9	553.2	562.4	571.6
		1	1	0.25	1		525.6	534.8	544.0	553.3	562.5	571.7
37	34.0	0.214	2.51	0.48	0.840	516.5	525.7	534.9	544.1	553.4	562.6	571.8
36	31.5	0.196	2.30	0.69	0.769	516.6	525.8	535.0	544.2	553.5	562.7	571.9
35	29.0	0.179	2.10	0.89	0.703	516.7	525.9	535.1	544.3	553.6	562.8	572.1
34	26.5	0.164	1.91	1.08	0.639	516.8	526.0	535.2	544.4	553.7	562.9	572.2
	1)		1	1		1					l .	572.3
	il .		1			1		1				572.4 572.6
31 30	16.5	0.125	1.46	1.53	0.488	517.1	526.3	535.6	544.9	554.1	563.4	572.7
40	40.0	0.264	3.09	0.00	1.000	515.2	524.4	533.6	542.8	552.0	561.2	570.4
39	37.8	0.245	2.86	0.23	0.926	515.3	524.5	533.7	542.9	552.1	561.3	570.5
38	35.6	0.227	2.65	0.44	0.858	515.4	524.6	533.8	543.0	552.2	561.4	570.6
37	33.4				l .	1	l .	1			1	570.7
36	31.2	0.194	2.27	0.82	0.734	515.6	524.8	534.0	543.2	552.4	561.6	570.8
35	29.0	1	2.09	1.00	0.676	515.7			1			1
34	26.8	1	1.94		1			1	1	1	1	
33	NI .		1.79		1	1	1				1	571.1
	11					1	1	1				571.2 571.3
	1)	1	1			1					1	1
90	10.0	0.120	1.42	1.07	0.499	510.1	020.0	004.0	040.0	030.0	002.2	0.1.1
	34 33 32 31 30 29 38 37 36 35 34 33 32 31 30 39 38 37 36 35 31 30 30 31 30 31 31 31 31 31 31 31 31 31 31 31 31 31	34         29.5           33         27.0           32         24.5           31         22.0           30         19.5           29         17.0           38         38.0           37         35.5           36         33.0           35         28.0           32         23.0           31         20.5           32         23.0           36.5         34.0           36.5         37.3           36.5         29.0           34         26.5           33         24.0           32         21.5           31         19.0           30         16.5           40         40.0           39         37.8           38         35.6           37         33.4           36         31.2           35         29.0           34         26.8           37         33.4           36         31.2           35         29.0           34         26.8           37         34.2           36 </td <td>34         29.5         0.182           33         27.0         0.167           32         24.5         0.152           31         22.0         0.139           30         19.5         0.127           29         17.0         0.116           38         38.0         0.246           37         35.5         0.226           36         33.0         0.207           35         30.5         0.189           34         28.0         0.173           33         25.5         0.158           32         23.0         0.144           31         20.5         0.132           30         18.0         0.120           39         39.0         0.255           38         36.5         0.234           37         34.0         0.214           36         31.5         0.196           35         29.0         0.179           34         26.5         0.164           33         24.0         0.153           32         21.5         0.114           40         40.0         0.264           39</td> <td>34         29.5         0.182         2.14           33         27.0         0.167         1.96           32         24.5         0.152         1.79           31         22.0         0.139         1.64           30         19.5         0.127         1.50           29         17.0         0.116         1.37           38         38.0         0.246         2.89           37         35.5         0.226         2.65           36         33.0         0.207         2.43           35         30.5         0.189         2.22           34         28.0         0.173         2.03           33         25.5         0.158         1.85           32         23.0         0.144         1.70           31         20.5         0.132         1.54           30         18.0         0.120         1.39           39         39.0         0.255         2.99           38         36.5         0.234         2.74           37         34.0         0.214         2.51           36         31.5         0.196         2.30           35</td> <td>34         29.5         0.182         2.14         0.66           33         27.0         0.167         1.96         0.84           32         24.5         0.152         1.79         1.01           31         22.0         0.139         1.64         1.16           30         19.5         0.127         1.50         1.30           29         17.0         0.116         1.37         1.43           38         38.0         0.246         2.89         0.00           37         35.5         0.226         2.65         0.24           36         33.0         0.207         2.43         0.46           35         30.5         0.189         2.22         0.67           34         28.0         0.173         2.03         0.86           33         25.5         0.189         2.22         0.67           34         28.0         0.173         2.03         0.86           33         25.5         0.158         1.85         1.04           32         23.0         0.144         1.70         1.19           31         20.5         0.132         1.54         1.35     <!--</td--><td>34         29.5         0.182         2.14         0.66         0.764           33         27.0         0.167         1.96         0.84         0.700           32         24.5         0.152         1.79         1.01         0.640           31         22.0         0.139         1.64         1.16         0.586           30         19.5         0.127         1.50         1.30         0.536           29         17.0         0.116         1.37         1.43         0.489           38         38.0         0.246         2.89         0.00         1.000           37         35.5         0.226         2.65         0.24         0.917           36         33.0         0.207         2.43         0.46         0.841           35         30.5         0.189         2.22         0.67         0.768           34         28.0         0.173         2.03         0.86         0.703           33         25.5         0.158         1.85         1.04         0.640           32         23.0         0.144         1.70         1.19         0.588           31         20.5         0.132</td><td>34         29.5         0.182         2.14         0.66         0.764         518.9           33         27.0         0.167         1.96         0.84         0.700         519.0           32         24.5         0.152         1.79         1.01         0.640         519.1           31         22.0         0.139         1.64         1.16         0.586         519.2           30         19.5         0.127         1.50         1.30         0.536         519.3           29         17.0         0.116         1.37         1.43         0.489         519.4           38         38.0         0.246         2.89         0.00         1.000         517.4           37         35.5         0.226         2.65         0.24         0.917         517.5           36         33.0         0.207         2.43         0.46         0.841         517.6           35         30.5         0.189         2.22         0.67         0.768         517.7           34         28.0         0.173         2.03         0.86         0.703         517.8           33         25.5         0.158         1.85         1.04</td><td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5           29         17.0         0.116         1.37         1.43         0.489         519.4         528.6           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6           37         35.5         0.226         2.65         0.24         0.917         517.5         526.7           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8           35         30.5         0.189         2.22         0.67         0.768         517.7         526.9           34         28.0         0.173</td><td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5         537.8           29         17.0         0.116         1.37         1.43         0.489         519.4         528.6         537.9           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6         535.9           37         35.5         0.226         2.65         0.24         0.917         517.5         526.7         536.0           36         33.0         0.207         2.43         0.46         0.841         517.5         526.7         536.2           34         28.0         0</td><td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7         546.9           30         19.5         0.127         1.50         1.30         0.536         519.3         528.6         537.9         547.1           30         19.5         0.127         1.50         1.30         0.586         519.3         528.6         537.9         547.1           30         19.5         0.226         2.65         0.24         0.917         517.5         526.6         535.9         545.1           37         35.5         0.226         2.65         0.24         0.917         517.5         526.6         535.9         545.1           36         33.0         0.121         1.30</td><td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6         555.9           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7         556.0           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8         556.1           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7         546.9         556.2           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5         537.9         547.2         556.4           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6         535.9         545.1         554.4           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8         536.1         545.3         546.7           36         30.5         0.189         2.22         0.67         0.768         517.7         526.9&lt;</td><td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6         555.9         565.1           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7         556.0         565.2           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8         556.1         565.2           31         22.0         0.137         1.50         1.30         0.536         519.2         528.4         537.7         546.9         566.2         565.4           30         19.5         0.116         1.37         1.43         0.489         519.4         528.6         537.9         547.1         556.3         565.6           33         3.50         0.246         2.89         0.00         1.000         517.4         526.6         535.9         545.1         554.4         563.6           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8         536.1         545.2         554.5         563.7</td></td>	34         29.5         0.182           33         27.0         0.167           32         24.5         0.152           31         22.0         0.139           30         19.5         0.127           29         17.0         0.116           38         38.0         0.246           37         35.5         0.226           36         33.0         0.207           35         30.5         0.189           34         28.0         0.173           33         25.5         0.158           32         23.0         0.144           31         20.5         0.132           30         18.0         0.120           39         39.0         0.255           38         36.5         0.234           37         34.0         0.214           36         31.5         0.196           35         29.0         0.179           34         26.5         0.164           33         24.0         0.153           32         21.5         0.114           40         40.0         0.264           39	34         29.5         0.182         2.14           33         27.0         0.167         1.96           32         24.5         0.152         1.79           31         22.0         0.139         1.64           30         19.5         0.127         1.50           29         17.0         0.116         1.37           38         38.0         0.246         2.89           37         35.5         0.226         2.65           36         33.0         0.207         2.43           35         30.5         0.189         2.22           34         28.0         0.173         2.03           33         25.5         0.158         1.85           32         23.0         0.144         1.70           31         20.5         0.132         1.54           30         18.0         0.120         1.39           39         39.0         0.255         2.99           38         36.5         0.234         2.74           37         34.0         0.214         2.51           36         31.5         0.196         2.30           35	34         29.5         0.182         2.14         0.66           33         27.0         0.167         1.96         0.84           32         24.5         0.152         1.79         1.01           31         22.0         0.139         1.64         1.16           30         19.5         0.127         1.50         1.30           29         17.0         0.116         1.37         1.43           38         38.0         0.246         2.89         0.00           37         35.5         0.226         2.65         0.24           36         33.0         0.207         2.43         0.46           35         30.5         0.189         2.22         0.67           34         28.0         0.173         2.03         0.86           33         25.5         0.189         2.22         0.67           34         28.0         0.173         2.03         0.86           33         25.5         0.158         1.85         1.04           32         23.0         0.144         1.70         1.19           31         20.5         0.132         1.54         1.35 </td <td>34         29.5         0.182         2.14         0.66         0.764           33         27.0         0.167         1.96         0.84         0.700           32         24.5         0.152         1.79         1.01         0.640           31         22.0         0.139         1.64         1.16         0.586           30         19.5         0.127         1.50         1.30         0.536           29         17.0         0.116         1.37         1.43         0.489           38         38.0         0.246         2.89         0.00         1.000           37         35.5         0.226         2.65         0.24         0.917           36         33.0         0.207         2.43         0.46         0.841           35         30.5         0.189         2.22         0.67         0.768           34         28.0         0.173         2.03         0.86         0.703           33         25.5         0.158         1.85         1.04         0.640           32         23.0         0.144         1.70         1.19         0.588           31         20.5         0.132</td> <td>34         29.5         0.182         2.14         0.66         0.764         518.9           33         27.0         0.167         1.96         0.84         0.700         519.0           32         24.5         0.152         1.79         1.01         0.640         519.1           31         22.0         0.139         1.64         1.16         0.586         519.2           30         19.5         0.127         1.50         1.30         0.536         519.3           29         17.0         0.116         1.37         1.43         0.489         519.4           38         38.0         0.246         2.89         0.00         1.000         517.4           37         35.5         0.226         2.65         0.24         0.917         517.5           36         33.0         0.207         2.43         0.46         0.841         517.6           35         30.5         0.189         2.22         0.67         0.768         517.7           34         28.0         0.173         2.03         0.86         0.703         517.8           33         25.5         0.158         1.85         1.04</td> <td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5           29         17.0         0.116         1.37         1.43         0.489         519.4         528.6           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6           37         35.5         0.226         2.65         0.24         0.917         517.5         526.7           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8           35         30.5         0.189         2.22         0.67         0.768         517.7         526.9           34         28.0         0.173</td> <td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5         537.8           29         17.0         0.116         1.37         1.43         0.489         519.4         528.6         537.9           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6         535.9           37         35.5         0.226         2.65         0.24         0.917         517.5         526.7         536.0           36         33.0         0.207         2.43         0.46         0.841         517.5         526.7         536.2           34         28.0         0</td> <td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7         546.9           30         19.5         0.127         1.50         1.30         0.536         519.3         528.6         537.9         547.1           30         19.5         0.127         1.50         1.30         0.586         519.3         528.6         537.9         547.1           30         19.5         0.226         2.65         0.24         0.917         517.5         526.6         535.9         545.1           37         35.5         0.226         2.65         0.24         0.917         517.5         526.6         535.9         545.1           36         33.0         0.121         1.30</td> <td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6         555.9           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7         556.0           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8         556.1           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7         546.9         556.2           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5         537.9         547.2         556.4           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6         535.9         545.1         554.4           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8         536.1         545.3         546.7           36         30.5         0.189         2.22         0.67         0.768         517.7         526.9&lt;</td> <td>34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6         555.9         565.1           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7         556.0         565.2           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8         556.1         565.2           31         22.0         0.137         1.50         1.30         0.536         519.2         528.4         537.7         546.9         566.2         565.4           30         19.5         0.116         1.37         1.43         0.489         519.4         528.6         537.9         547.1         556.3         565.6           33         3.50         0.246         2.89         0.00         1.000         517.4         526.6         535.9         545.1         554.4         563.6           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8         536.1         545.2         554.5         563.7</td>	34         29.5         0.182         2.14         0.66         0.764           33         27.0         0.167         1.96         0.84         0.700           32         24.5         0.152         1.79         1.01         0.640           31         22.0         0.139         1.64         1.16         0.586           30         19.5         0.127         1.50         1.30         0.536           29         17.0         0.116         1.37         1.43         0.489           38         38.0         0.246         2.89         0.00         1.000           37         35.5         0.226         2.65         0.24         0.917           36         33.0         0.207         2.43         0.46         0.841           35         30.5         0.189         2.22         0.67         0.768           34         28.0         0.173         2.03         0.86         0.703           33         25.5         0.158         1.85         1.04         0.640           32         23.0         0.144         1.70         1.19         0.588           31         20.5         0.132	34         29.5         0.182         2.14         0.66         0.764         518.9           33         27.0         0.167         1.96         0.84         0.700         519.0           32         24.5         0.152         1.79         1.01         0.640         519.1           31         22.0         0.139         1.64         1.16         0.586         519.2           30         19.5         0.127         1.50         1.30         0.536         519.3           29         17.0         0.116         1.37         1.43         0.489         519.4           38         38.0         0.246         2.89         0.00         1.000         517.4           37         35.5         0.226         2.65         0.24         0.917         517.5           36         33.0         0.207         2.43         0.46         0.841         517.6           35         30.5         0.189         2.22         0.67         0.768         517.7           34         28.0         0.173         2.03         0.86         0.703         517.8           33         25.5         0.158         1.85         1.04	34         29.5         0.182         2.14         0.66         0.764         518.9         528.1           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5           29         17.0         0.116         1.37         1.43         0.489         519.4         528.6           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6           37         35.5         0.226         2.65         0.24         0.917         517.5         526.7           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8           35         30.5         0.189         2.22         0.67         0.768         517.7         526.9           34         28.0         0.173	34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5         537.8           29         17.0         0.116         1.37         1.43         0.489         519.4         528.6         537.9           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6         535.9           37         35.5         0.226         2.65         0.24         0.917         517.5         526.7         536.0           36         33.0         0.207         2.43         0.46         0.841         517.5         526.7         536.2           34         28.0         0	34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7         546.9           30         19.5         0.127         1.50         1.30         0.536         519.3         528.6         537.9         547.1           30         19.5         0.127         1.50         1.30         0.586         519.3         528.6         537.9         547.1           30         19.5         0.226         2.65         0.24         0.917         517.5         526.6         535.9         545.1           37         35.5         0.226         2.65         0.24         0.917         517.5         526.6         535.9         545.1           36         33.0         0.121         1.30	34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6         555.9           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7         556.0           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8         556.1           31         22.0         0.139         1.64         1.16         0.586         519.2         528.4         537.7         546.9         556.2           30         19.5         0.127         1.50         1.30         0.536         519.3         528.5         537.9         547.2         556.4           38         38.0         0.246         2.89         0.00         1.000         517.4         526.6         535.9         545.1         554.4           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8         536.1         545.3         546.7           36         30.5         0.189         2.22         0.67         0.768         517.7         526.9<	34         29.5         0.182         2.14         0.66         0.764         518.9         528.1         537.4         546.6         555.9         565.1           33         27.0         0.167         1.96         0.84         0.700         519.0         528.2         537.5         546.7         556.0         565.2           32         24.5         0.152         1.79         1.01         0.640         519.1         528.3         537.6         546.8         556.1         565.2           31         22.0         0.137         1.50         1.30         0.536         519.2         528.4         537.7         546.9         566.2         565.4           30         19.5         0.116         1.37         1.43         0.489         519.4         528.6         537.9         547.1         556.3         565.6           33         3.50         0.246         2.89         0.00         1.000         517.4         526.6         535.9         545.1         554.4         563.6           36         33.0         0.207         2.43         0.46         0.841         517.6         526.8         536.1         545.2         554.5         563.7

Re	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weight	in Grain	ns of a Cu	abic Foot	of Air.	
mo	meter,	of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n Englisl	n Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.						
41	41	38.8	$0.274 \\ 0.253$	3.19 $2.96$	0.00	1.000 0.928	514.1 514.2	523.3 523.4	532.5	541.6	550.8 550.9	560.0	569.2 569.3
	40 39	36.6	0.235	2.74	0.45	0.859	514.2	523.5	532.6 532.7	541.7 541.8	551.0	560 1 560.2	569.4
	38	34.4	0.217	2.54	0.65	0.796	514.4	523.6	532.8	541.9	551.1	560.3	569.5
	37	32.2	0.201	2.35	0.84	0.737	514.5	523.7	532.9	542.0	551.2	560.4	569.6
	36	30.0	0.186	2.16	1.03	0.677	514.6	523.8	533.0	542.1	551.3	560.5	569.7
	35	27.8	0.172	2.01	1.18	0.630	514.7	523.9	533.1	542.2	551.4	560.6	569.8
	34	25.6	0.158	1.85	1.34	0.580	514.8	524.0	533.2	542.3	551.5	560.7	569.9
	33	23.4	$0.146 \\ 0.135$	1.71 1.58	1.48	$0.536 \\ 0.495$	514.9 514.9	524.1 524.1	533.3 533.3	542.4 542.5	551.6 551.7	560.8 560.9	570.0 570.1
	31	19.0	0.135	1.46	1.73	0.458	515.0	524.2	533.4	542.6	551.8	561.0	570.1
1	01	13.0	0.120	1.40	1.10	0.400	010.0	024.2	000.4	042.0	991.0	001.0	010.2
42	42	42.0	0.283	3.30	0.00	1.000	513.0	522.2	531.3	540.5	549.6	558.8	567 9
i	41	39.8	0.263	3.06	0.24	0.927	513.1	522.3	531.4	540.6	549.7	558.9	568.0
	40	37.6	0.243	2.83	0.47	0.858	513.2	522.4	531.5	540.7	549.9	559.0	568.1
	39	35.4	0.225	2.63	0.67	0.797	513.3	522.5	531.6	540.8	550.0	559.1	568.2
	38	33.2	0.208	2.43	0.87	0.736	513.4	522.6	531.7	540.9	550.1	559.2	568.3
	37	31.0	0.192	2.24	1.06	0.679	513.5	522.7	531.8	541.0	550.2	559.3	568.4
1	36	28.8	0.178	2.08	1.22	0.631	513.6	522.8	531.9	541.1	550.3	559.4	568.5
H	35	26.6	0.164	1.91	1.39	0.579	513.7	522.9	532.0	541.2	550.4	559.5	568.6
	34	24.4	0.152	1.77	1.53	0.536	513.8	523.0	532.1	541.3	550.5	559.6	568.7
	33	22.2	0.140	1.63	1.67	0.494	513.9	523.1	532.2	541.4	550.6	559.7	568.8
	32	20.0	0.129	1.51	1.79	0.458	513.9	523.1	532.3	541.5	550.6	559.8	569.0
43	43	43.0	0.293	3.41	0.00	1.000	511.8	520.9	530.1	539.3	548.4	557.5	566.7
	42	40.8	0.272	3.16	0.25	0.927	511.9	521.0	530.2	539.4	548.6	557.7	566.9
	41	38.6	0.252	2.93	0.48	0.859	512.0	521.1	530.3	539.5	548.7	557.8	567.0
	40	36.4	0.233	2.71	0.70	0.795	512.1	521.2	530.4	539.6	548.8	557.9	567.1
	39	34.2	0.216	2.51	0.90	0.736	512.2	521.3	530.5	539.7	548.9	558.0	567.2
}}	38	32.0	0.199	2.32	1.09	0.680	512.3	521.4	530.7	539.8	549.0	558.1	567.3
	37	29.8	0.184	2.15	1.26	0.630	512.4	521.5	530.8	539.9	549.1	558.2	567.4
	36	27.6	0.170	1.98	1.43	0.581	512.5	521.6	530.9	540.0	549.2	558.3	567.5
	35	25.4	0.157	1.82	1.59	0.534	512.6	521.7	531.0	540.1	549.3	558.4	567.6
	34	23.2	0.145	1.69	1.72	0.495	512.7	521.8	531.1	540.2	549.4	558.5	567.7
	33	21.0	0.134	1.56	1.85	0.458	512.9	522.0	531.2	540.3	549.5	558.6	567.8
44	44	44.0	0.304	3.52	0.00	1.000	510.8	519.9	529.0	538.1	547.3	556.4	565.5
	43	41.8	0.282	3.27	0.25	0.929	510.9	520.0	529.1	538.2	547.5	556.5	565.7
	42	39.6	0.261	3.02	0.50	0.858					547.6		
	41	37.4	0.241	2.80	0.72	0.796	511.1	520.2	529.3	538.4	547.7	556.7	565.9
	40	35.2	0.223	2.60	0.92	0.739	511.2	520.3	529.4	538.5	547.8	556.8	566.0
	39	33.0	0.207	2.40	1.12	0.682	511.3	520.4	529.5	538.6	547.9	556.9	566.1
	38	30.8	0.191	2.22	1.30	0.631	511.4	520.5	529.6	538.7	548.0	557.0	566.2
	37	28.6	0.177	2.05	1.47	0.582	511.5	520.6	529.7	538.8	548.1	557.1	566.3
	36	26.4	0.163	1.89	1.63	0.537	511.6	520.7	529.8	538.9	548.2	557.2	566.4
1	35	24.2	0.151	1.75	1.77	0.497	511.7	520.8	529.9	539.0	548.3	557.3	566.5
11	34	22.0	0.139	1.62	1	0.460		520.8	530.0		548.3	557.4	566.6

	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cr	ıbic Foot	of Air.	
mo	meter, ahr.	of Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height	of the Bar	rometer i	n Englisl	n Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0		0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr. 555.2	gr. 564.3
45	45	45.0 42.9	$0.315 \\ 0.292$	3.64	0.00	1.000 0.931	509.7 509.8	518.8 518.9	527.9 528.0	537.0 537.1	546.1	555.3	564.5
	43	40.8	0.272	3.14	0.50	0.863	509.9	519.0	528.1	537.2	546.4	555.4	564.6
	42	38.7	0.253	2.92	0.72	0.802	510.0	519.1	528.2	537.3	546.5	555.5	564.7
	41	36.6	0.235	2.70	0.94	0.742	510.1	519.2	528.3	537.4	546.6	555.6	564.8
	40	34.5	0.218	2.52	1.12	0.692	510.2	519.3	528.4	537.5	546.7	555.7	564.9
	39	32.4	0.202	2.34	1.30	0.643	510.3	519.4	528 5	537.6	546.8	555.8	565.0
	38	30.3	0.188	2.16	1.48	0.593	510.4	519.5	528.6	537.7	546.9	555.9	565.1
	37	28.2	0.174	2.01	1.63	0.552	510.5	519.6	528.7	537.8	547.0	556.0	565.2
	36	26.1	0.161	1.87	1.77	0.514	510.6	519.7	528.8	537.9	547.1	556.1	565.3
	35	24.0	0.150	1.73	1.91	0.475	510.7	519.8	528.9	538.0	547.2	556.3	565.4
46	46	46.0	0.326	3.76	0.00	1.000	508.6	517.7	526.7	535.8	544.9	554.0	563.1
	45	43.9	0.303	3.50	0.26	0.931	508.7	517.8	526.8	535.9	545.0	554.1	563.2
	44	41.8	0.282	3.25	0.51	0.864	508.8	517.9	526.9	536.0	545.1	554.2	563.3
	43	39.7	0.262	3.02	0.74	0.803	508.9	518.0	527.0	536.1	545.2	554.3	563.4
	42	37.6	0.243	2.80	0.96	0.745	509.0	518.1	527.2	536.3	545.4	554.5	563.6
	41	35.5	0.226	2.61	1.15	0.694	509.1	518.2	527.3	536.4	545.5	554.6	563.7
	40	33.4	0.210	2.42	1.34	0.643	509.2	518.3	527.4	536.5	545.6	554.7	563.8
	39	31.3	0.194	2.24	1.52	0.596	509.3	518.4	527.5	536.6	545.7	554.8	563.9
	38	29.2	0.180	2.08	1.68	0.553	509.4	518.5	527.6	536.7	545.8	554.9	564.0
	37	27.1	0.167	1.93	1.83	0.514	509.5	518.6	527.7	536.8	545.9	555.0	564.1
	36	25.0	0.155	1.79	1.97	0.476	509.5	518.6	527.7	536.8	545.9	555.0	564.1
47	47	47.0	0.337	3.88	0.00	1.000	507.5	516.5	525.6	534.7	543.8	552.8	561.9
1	46	44.9	0.313	3.62	0.26	0.933	507.6	516.6	525.7	534.8	543.9	552.9	562.0
	45	42.8	0.291	3.36	0.52	0.866	507.8	516.7	525.9	535.0	544.1	553.1	562.2
	44	40.7	0.271	3.12	0.76	0.804	507.9	516.8	526.0	535.1	544.2	553.2	562.3
	43	38.6	0.252	2.90	0.98	0.747	508.0	516.9	526.1	535.2	544.3	553.3	562.4
	42	36.5	0.234	2.70	1.18	0.696	508.1	517.0	526.2	535.3	544.4	553.4	562.5
	41	34.4	0.217	2.51	1.37	0.647	508.2	517.1	526.3	535.4	544.5	553.5	562.6
	40	32.3	0.201	2.32	1.56	0.598	508.3	517.2	526.4	535.5	544.6	553.6	562.7
	39	30.2	0.187	2.16	1.72	0.557	508.4	517.3	526.5	535.6	544.7	553.7	562.8
	38 37	28.1 26.0	0.173 0.161	2.00 1.85	1.88 2.03	0.515	508.5 508.5	517.4 517.6	526.6 526.7	535.7 535.8	544.8 544.9	553.8 554.0	562.9 563.1
48	48	48.0	0.349	4.01	0.00	1.000	506.4	515.4	524.5	533.5	542.6	551.6	560.7
	47	45.9	0.324	3.73	0.28	0.930	506.5	515.5	524.6	533.7	542.8	551.8	560.9
	46	43.8	0.302	3.47	0.54	0.865	506.6	515.6	524.7	533.8	542.9	551.9	561.0
1	45	41.7	0.281	3.23	0.78	0.805	506.7	515.7	524.8	533.9	543.0	552.0	561.1
H	44	39.6	0.261	3.00	1.01	0.748	506.8	515.8	524.9	534.0	543.1	552.1	561.2
	43	37.5	0.242	2.79	1.22	0.696	506.9	515.9	525.0	534.1	543.2	552.2	561.3
	42	35.4	0.225	2.60	1.41	0.648	507.0	516.0	525.1	534.2	543.3	552.3	561.4
	41	33.3	0.209	2.40	1.61	0.598	507.1	516.1	525.2	534.4	543.5	552.5	561.5
	40	31.2	0.194	2.24	1.77	0.558	507.2	516.2	525.3	534.5	543.5	552.5	561.6
	39	29.1	0.180	2.07	1.94	0.516	507.3	516.3	525.4	534.6	543.6	552.6	561.6
	38	27.0	0.167	1.92	2.09	0.479	507.4	516.4	525.5	534.7	543.6	552.7	561.7
	37	24.9	0.155	1.77	2.24	0.441	507.4	516.4	525.6	534.7	543.7	552.8	561.8

of	ading Ther-	Temp.	Force of		ight apor Reqd.	Hu-		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	
	meter, ahr.	of Dew-	Vapor in	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	tion = 1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	7 000	gr.						
49	49 48	49.0	0.361 $0.336$	4.14 3.85	0.00	1.000 0.930	505.3	514.3	523.3	532.3	541.4	550.4	559.4
	47	44.8	0.312	3.59	0.55	0.867	505.4	514.4	523.4	532.4 $532.6$	541.5 541.7	550.5	559.5
	46	42.7	0.290	3.34	0.80	0.807	505.7	514.7	523.6 523.7	532.7	541.7	550.7 550.8	559.7 559.8
	45	40.6	0.270	3.10	1.04	0.749	505.9	514.9	523.8	532.9	542.0	551.0	560.0
	44	38.5	0.251	2.88	1.26	0.696	506.0	515.0	523.9	533.0	542.1	551.1	560.1
	43	36.4	0.233	2.68	1.46	0.647	506.1	515.1	524.0	533.1	542.2	551.2	560.2
	42	34.3	0.216	2.49	1.65	0.601	506.2	515.2	524.1	533.2	542.3	551.3	560.3
	41	32.2	0.201	2.32	1.82	0.560	506.3	515.3	524.2	533.3	542.4	551.4	560.4
	40	30.1	0.186	2.14	2.00	0.517	506.3	515.3	524.3	533.4	542.5	551.5	560.5
	39	28.0	0.173	1.99	2.15	0.481	506.4	515.4	524.4	533.5	542.6	551.6	560.6
	38	25.9	0.160	1.84	2.30	0.444	506.4	515.4	524.4	533.5	542.6	551.6	560.6
50	50	50.0	0.373	4.28	0.00	1.000	504.1	513.1	522.1	531.1	540.2	549.2	558.2
	49	48.0	0.349	3.99	0.29	0.932	504.2	513.2	522.2	531.2	540.3	549.3	558.3
	48	46.0	0.326	3.73	0.55	0.871	504.4	513.4	522.4	531.4	540.5	549.5	558.5
	47	44.0	0.304	3.48	0.80	0.813	504.5	513.5	522.5	531.5	540.6	549.6	558.6
	46	42.0	0.283	3.25	1.03	0.759	504.6	513.6	522.6	531.6	540.7	549.7	558.7
	45	40.0	0.264	3.03	1.25	0.708	504.8	513.8	522.8	531.8	540.9	549.9	558.9
	44	38.0	0.246	2.82	1.46	0.659	504.9	513.9	522.9	532.0	541.0	550.0	559.0
	43	36.0	0.230	2.63	1.65	0.614	505.1	514.1	523.1	532.1	541.2	550.2	559.2
	42	34.0	0.214	2.45	1.83	0.572	505.2	514.2	523.2	532,2	541.3	550.3	559.3
	41	32.0	0.199	2.28	2.00	0.533	505.3	514.3	523.3	532.3	541.4	550.4	559.4
	40 39	30.0	0.186	2.12	2.16	0.495	505.4	514.4	523.4	532.4	541.5	550.5	559.5
51	51	51.0	$0.173 \\ 0.386$	1.97 $4.42$	2.31 0.00	0.460 1.000	505.5	514.5	523.5	532.5	541.6	550.6	559.6
91	50	49.0	0.361	4.12	0.30	0.932	503.1 503.2	512.1 512.2	521.1 $521.2$	530.0 530.1	539.0 539.1	548.0 548.1	557.0 557.1
	49	47.0	0.337	3.85	0.57	0.332	503.2	512.2	521.2	530.3	539.3	548.3	557.8
	48	45.0	0.315	3.60	0.52	0.814	503.4	512.4	521.4	530.4	539.4	548.4	557.4
	47	43.0	0.293	3.36	1.06	0.760	503.5	512.5	521.5	530.5	539.5	548.5	557.5
	46	41.0	0.274	3.13	1.29	0.708	503.7	512.7	521.7	530.7	539.7	548.7	557.7
	45	39.0	0.255	2.92	1.50	0.661	503.8	512.8	521.8	530.8	539.8	548.8	557.8
	44	37.0	0.238	2.72	1.70	0.615	503.9	512.9	521.9	530.9	539.9	548.9	557.9
	43	35.0	0.222	2.54	1.88	0.575	504.0	513.0	522.0	531.0	540.0	549.0	558.0
	42	33.0	0.207	2.36	2.06	0.534	504.1	513.1	522.1	531.1	540.1	549.1	558.
	41	31.0	0.192	2.20	2.22	0.498	504.2	513.2	522.2	531.2	540.3	549.3	558.
	40	29.0	0.179	2.05	2.37	0.464	504.3	513.3	522.3	531.3	540.4	549.4	558.4
52	52	52.0	0.400	4.56	0.00	1.000	502.1	511.0	520.0	528.9	537.9	546.8	555.8
	51	50.0	0.373	4.26	0.30	0.934	502.2	511.1	520.1	529.0	538.0	546.9	555.9
	50	48.0	0.349	3.98	0.58	0.873	502.4	511.3	520.3	529.2	538.2	547.1	556.1
	49	46.0	0.326	3.72	0.84	0.816	502.5	511.4	520.4	529.3	538.3	547.2	556.2
	48	44.0	0.304	3.47	1.09	0.761	502.6	511.5	520.5	529.4	538.4	547.3	556.3
	47	42.0	0.283	3.23	1.33	0.709	502.8	511.7	520.7	529.6	538.6	547.5	556.5
	46	40.0	0.264	3.02	1.54	0.662	502.9	511.8	520.8	529.7	538.7	547.6	556.6
	45	38.0	0.246	2.81	1.75	0.616	502.9	511.9	520.9	529.8	538.8	547.8	556.8
	44	36.0	0.230	2.63	1.93	0.577	503.1	512.0	521.0	529.9	539.0	548.0	557.0
	43	34.0	0.214	2.44	2.12	0.535	503.2	512.1	521.1	530.0	539.1	548.1	557.1
	42	32.0 30.0	0.199	2.28	2.28	0.500	503.3	512.3	521.3	530.2	539.2	548.2 548.3	557.2 557.3
	71	50.0	0.100	2.13	2.43	0.467	503.4	512.4	521.4	530.3	539.3	040.0	007.0

	nding		Force		ight apor			Weigh	t in Grain	as of a Ci	ubie Foot	of Air.	
mor	Ther- neter, ahr.	Temp. of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	Hu- midity, Satura-		Height	of the Ba	rometer i	in Englis	h Inches	
Dry.	Wet.	Point, Fabr.	English Inches.			tion = 1.000.	28.0	28.5	29.0	29.5	30.0	in. 3 <b>0.5</b>	31.0
0	0	0	in.	gr.	gr.	7 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
53	53 52	53.0	$0.414 \\ 0.386$	4.71	0.00	1.000 0.934	500.9	509.8	518.8 519.0	527.7 527.9	536.7 536.9	545.6 545.8	554.6 554.8
	51	49.0	0.361	4.11	0.60	0.873	501.2	510.1	519.1	528.0	537.0	545.9	554.9
11	50	47.0	0.337	3.84	0.87	0.815	501.4	510.3	519.3	528.2	537.2	546.1	555.1
	49	45.0	0.315	3.58	1.13	0.760	501.5	510.4	519.4	528.3	537.3	546.2	555.2
	48	43.0	0.293	3.34	1.37	0.709	501.6	510.5	519.5	528.4	537.4	546.3	555.8
	47	41.0	0.274	3.12	1.59	0.662	501.7	510.6	519.6	528.5	537.5	546.4	555.4
	46	39.0	0.255	2.91	1.80	0.618	501.8	510.7	519.7	528.6	537.6	546.5	555.5
	45	37.0	0.238	2.71	2.00	0.575	502.0	510.9	519.9	528.8	537.8	546.7	555.7
li	44	35.0	0.222	2.53	2.18	0.537	502.1	511.0	520.0	528.9	537.9	546.8	555.8
	43	33.0	0.207	2.35	2.36	0.499	502.1	511.0	520.0	528.9	538.0	546.9	555.9
	42	31.0	0.192	2.18	2.53	0.463	502.2	511.1	520.1	529.0	538.1	547.0	556.0
54	54	54.0	0.428	4.86	0.00	1.000	499.9	508.8	517.8	526.7	535.6	544.5	553.5
	53	52.0	0.400	4.54	0.32	0.934	500.0	508.9	517.9	526.8	535.7	544.6	553.6
-	52	50.0	0.373	4.25	0.61	0.875	500.2	509.1	518.1	527.0	535.9	544.S	553.8
	51	48.0	0.349	3.96	0.90	0.815	500.3	509.2	518.2	527.1	536.0	544.9	553.9
	50	46.0	0.326	3.70	1.16	0.761	500.4	509.3	518.3	527.2	536.1	545.0	554.0
	49	44.0	0.304	3.45	1.41	0.709	500.6	509.5	518.5	527.4	536.3	545.2	554.2
	48	42.0	0.283	3.23	1.63	0.665	500.7	509.6	518.6	527.5	536.4	545.3	554.3
	47	40.0	0.264	3.01	1.85	0.619	500.8	509.7	518.7	527.6	536.5	545.4	554.4
	46	38.0	0.246	2.80	2.06	0.576	500.9	509.8	518.8	527.7	536.7	545.6	554.6
	45	36.0	0.230	2.61	2.25	0.537	501.0	509.9	518.9	527.8	536.8	545.7	554.7
	44	34.0	0.214	2.43	2.43	0.500	501.1	510.0	519.0	527.9	536.9	545.8	554.8
	43	32.0	0.199 0.186	2.27	2.59	0.467	501.2	510.1	519.1	528.0	537.0	545.9	554.9 555.0
}	42	30.0	0.150	$\frac{2.10}{1.96}$	$\begin{bmatrix} 2.76 \\ 2.90 \end{bmatrix}$	0.432 $0.403$	501.3 501.4	510.2 510.3	519.2 519.3	528.1 528.2	537.1 537.2	546.0 546.1	555.1
	40	26.0	0.161	1.82	3.04	0.375	501.4	510.4	519.4	528.3	537.3	546.2	555.2
==	۳.	55.0	0.449	# 00	0.00	1 000	100.0	500 0	51C C	505 5	5914	5 19 9	552.2
55	55 54	53.3	0.442	5.02 4.74	$0.00 \\ 0.28$	0.944	498.8	507.7 507.9	516.6 516.8	525.5 525.7	534.4	543.3 543.5	552.4
	53	51.6	0.394	4.74	0.25	0.888	499.1	.508.0	516.9	525.8	534.7	543.6	552.5
	52	49.9	0.372	4.23	0.79	0.843	499.3	508.2	517.1	526.0	534.9	543.8	552.7
	51	48.2	0.351	3.98	1.04	0.793	499.4	508.3	517.2	526.1	535.0	543.9	552.8
	50	46.5	0.331	3.76	1.26	0.749	499.5	508.4	517.3	526.2	535.1	544.0	552.9
	49	44.8	0.312	3.55	1.47	0.707	499.7	508.6	517.5	526.3	535.3	544.2	553.1
1	48	43.1	0.295	3.34	1.68	0.665	499.8	508.7	517.6	526.5	535.4	544.3	553.3
	47	41.4	0.278	3.14	1.88	0.626	499.8	508.7	517.6	526.6	535.5	544.4	553.4
	46	39.7	0.262	2.97	2.05	0.591	499.9	508.8	517.7	526.7	535.6	544.5	553.5
	45	38.0	0.246	2.79	2.23	0.556	500.0	508.9	517.9	526.8	535.7	544.6	553.6
	44	36.3	0.232	2.64	2.38	0.526	500.1	509.0	518.0	526.9	535.8	544.7	553.7
	43	34.6	0.219	2.47	2.55	0.492	500.2	509.1	518.1	527.0	535.9	544.8	553.8
	42	32.9	0.206	2.32	2.70	0.462	500.3	509.2	518.2	527.1	536.0	544.9	553.9
	41	31.2	0.194	2.20	2.82	0.438	500.4	509.3	518.3	527.1	536.0	544.9	554.0
	40	29.5	0.182	2.07	2.95	0.412	500.5	509.3	518.4	527.2	536.1	545.0	554.1
	39	27.8	0.172	1.95	3.07	0.388	500.6	509.4	518.5	527.3	536.2	545.1	554.2
	38	26.1	0.161	1.83	3.19	0.365	500.7	509.5	518.6	527.4	536.2	545.1	554.2

Rea	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a C	ubic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	in. 30.5	31.0
56	o 56	56.0	in. 0.458	gr. 5.18	gr. 0.00	1.000	gr. 497.7	gr. 506.6	gr. 515.5	gr. 524.4	gr. 533.2	gr. " 542.1	gr. 551.0
30	55	54.3	0.432	4.89	0.29	0.944	497.9	506.8	515.7	524.4	533.4	542.3	551.0
	54	52.6	0.408	4.61	0.57	0.890	498.0	506.9	515.8	524.7	533.5	542.4	551.3
	53	50.9	0.385	4.37	0.81	0.844	498.2	507.1	516.0	524.9	533.7	542.6	551.5
	52	49.2	0.363	4.11	1.07	0.793	498.3	507.2	516.1	525.0	533.8	542.7	551.6
	51	47.5	0.343	3.87	1.31	0.747	498.4	507.3	516.2	525.1	533.9	542.8	551.7
	50	45.8	0.323	3.66	1.52	0.706	498.6	507.5	516.4	525.3	534.1	543.0	551.9
	49	44.1	0.305	3.45	1.73	0.666	498.6	507.5	516.4	525.3	534.2	543.1	552.0
	48	42.4	0.287	3.25	1.93	0.627	498.7	507.6	516.5	525.4	534.3	543.2	552.1
	47	40.7	0.271	3.07	2.11	0.593	498.8	507.7	516.6	525.5	534.4	543.3	552.2
	46	39.0	0.255	2.89	2.29	0.558	498.9	507.8	516.7	525.6	534.5	543.4	552.3
	45	37.3	0.240	2.73	2.45	0.527	499.0	507.9	516.8	525.7	534.6	543.5	552.4
	44	35.6	0.227	2.56	2.62	0.494	499.1	508.0	516.9	525.8	534.7	543.6	552.5
	43	33.9	0.213	2.41	2.77	0.465	499.2	508.1	517.0	525.9	534.8	543.7	552.6
	42	32.2	0.201	2.27	2.91	0.438	499.3	508.2	517.1	526.0	534.9	543.S	552.7
	41	30.5	0.189	2.14	3.04	0.413	499.4	508.3	517.2	526.1	535.0	543.9	552.8
	40	28.8	0.178	2.01	3.17	0.388	499.5	508.4	517.3	526.2	535.1	544.1	552.9
	39	27.1	0.167	1.89	3.29	0.365	499.5	508.4	517.3	526.2	535.1	544.1	552.9
57	57	57.0	0.473	5.34	0.00	1.000	496.6	505.5	514.4	523.2	532.1	540.9	549.8
•	56	55.3	0.447	5.05	0.29	0.946	496.8	505.7	514.6	523.4	532.3	541.1	550.0
	55	53.6	0.422	4.76	0.58	0.891	496.9	505.8	514.7	523.5	532.4	541.2	550.1
	54	51.9	0.398	4.50	0.84	0.843	497.1	506.0	514.9	523.7	532.6	541.4	550.3
	53	50.2	0.376	4.25	1.09	0.796	497.2	506.1	515.0	523.8	532.7	541.5	550.4
	52	48.5	0.355	4.00	1.34	0.749	497.3	506.2	515.1	523.9	532.8	541.6	550.5
	51	46.8	0.335	3.78	1.56	0.709	497.5	506.4	515.3	524.1	533.0	541.8	550.7
	50	45.1	0.316	3.56	1.78	0.667	497.6	506.5	515.4	524.2	533.1	541.9	550.8
	49	43.4	0.298	3.36	1.98	0.629	497.7	506.6	515.5	524.3	533.2	542.0	550.9
	48	41.7	0.281	3.17	2.17	0.594	497.8	506.7	515.6	524.4	533.3	542.1	551.0
	47	40.0	0.264	2.99	2.35	0.560	497.9	506.8	515.7	524.5	533.4	542.2	551.2
	46	38.3	0.249	2.81	2.53	0.526	498.0	506.9	515.8	524.6	533.5	542.3	551.3
	45	36.6	0.235	2.65	2.69	0.496	498.1	507.0	515.9	524.7	533.6	542.4	551.4
	44	34.9	0.221	2.50	2.84	0.468	498.2	507.1	516.0	524.8	533.7	542.5	551.5
	43	33.2	0.208	2.35	2.99	0.440	498.3	507.2	516.1	524.9	533.8	542.6	551.6
	42	31.5	0.196	2.21	3.13	0.414	498.3	507.2		524.9	533.8	542.6	551.6
4	41	29.8	0.184	2.08	3.26	0.390	498.4	507.3	516.2	525.1	533.9	542.7	551.7
	40	28.1	0.173	1.96	3.38	0.367	498.5	507.4	516.3	525.2	534.0	542.8	551.8

Dept.   Political Process   Political Proc		ading	Temp	Force	Wei of V		Hu-		Weight	in Grain	ns of a Cu	ibic Foot	of Air.	
Dry.   Wet   Fair.   English   Foot of arCar.   Foot of Arcar.   Fair.   Series   Foot of Arcar.   Fair.   Series   Foot of Arcar.   Series   Ser	mon	neter,	of Dew-				Satura-		Height o	f the Bar	ometer i	n English	Iuches.	
58         58, 60, 0,489         5.51         0.00         1,000         495.5         504.3         513.2         522.0         530.9         537.7         548           56         54.6         0.437         4.92         0.59         0.893         495.8         504.6         513.5         522.3         531.1         530.9         548           55         52.9         0.412         4.64         0.87         0.812         496.0         504.8         513.7         522.3         531.2         540.0         548           53         49.5         0.367         4.14         1.37         0.797         496.1         504.9         513.8         522.7         531.6         540.4         549           51         46.1         0.327         3.68         1.83         0.668         496.5         505.3         514.1         523.0         531.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9 <t< th=""><th>Dry.</th><th>Wet.</th><th></th><th>English</th><th>Foot of</th><th>of aCu- bic Ft.</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>31.0</th></t<>	Dry.	Wet.		English	Foot of	of aCu- bic Ft.								31.0
57         56.3         0.462         5.21         0.30         0.946         495.7         504.5         513.4         522.2         531.1         539.9         548.6           55         55.2.9         0.412         4.64         0.87         0.812         496.0         504.8         513.7         522.5         531.1         540.2         540.0         548           54         51.2         0.369         4.39         1.12         0.797         496.1         504.9         513.8         522.7         531.6         540.4         549.5           52         47.8         0.346         3.90         1.61         0.708         496.4         505.2         514.1         523.1         540.5         540.5         540.5         540.4         540.5         560.3         514.2         523.1         532.0         540.5							1 000							gr. 548.6
56         54.6         0.437         4.92         0.59         0.893         495.8         504.6         513.5         522.3         531.2         540.0         548         555         52.9         0.412         4.64         0.87         0.812         496.0         504.8         513.7         522.5         531.4         540.2         549.5         53.4         49.6         504.8         513.8         522.7         531.6         540.2         549.5         531.6         540.2         549.5         531.6         540.5         549.6         549.6         505.0         513.8         522.7         531.6         540.7         549.5         540.5         540.5         540.5         540.5         540.5         540.7         549.5         540.5         540.5         540.7         549.5         540.5         540.5         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.5         540.5         540.4         522.1         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9         540.7         540.9	30					]								548.8
55         52.9         0.412         4.64         0.87         0.842         496.0         504.8         513.7         522.5         531.4         540.2         549         1.12         0.797         486.1         504.9         513.8         522.7         531.6         540.4         549         513.8         522.7         531.6         540.4         549         548         540.4         549         548         540.4         549         548         540.4         549         540.4         549         540.4         549         540.4         540.4         540.5         540.4         540.5         540.4         540.8         540.8         540.7         549         540.8         540.7         549         540.8         540.8         540.8         540.8         540.8         540.8         560.4         514.4         523.0         531.9         540.8         540.8         540.8         540.6         505.4         514.4         523.1         532.0         540.8         540.8         540.8         540.5         505.3         514.4         523.3         532.4         541.0         549         480.8         505.6         514.5         523.4         532.3         541.0         549         480.8         540.9		1												548.9
53         49.5         0.367         4.14         1.37         0.751         496.2         505.0         513.9         522.8         531.7         540.5         549           52         47.8         0.346         3.90         1.61         0.708         496.4         505.2         514.1         523.1         532.0         540.5         549           50         44.4         0.308         3.48         2.03         0.632         496.6         505.4         514.3         523.2         532.1         540.9         549         49         42.7         0.290         3.28         2.23         0.595         496.6         505.4         514.3         523.2         532.1         540.9         549         48         41.0         0.274         3.08         2.43         0.559         496.8         505.6         514.5         523.4         532.3         541.1         550         447         39.3         0.258         2.91         2.60         0.528         496.9         505.7         514.6         523.5         582.4         541.2         550         441.2         53.3         541.2         530.4         541.2         530.4         541.2         530.4         541.2         530.4         541.2 <th></th> <th></th> <th>1</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>531.4</th> <th></th> <th>549.1</th>			1									531.4		549.1
52         47.8         0.346         3.90         1.61         0.708         496.4         505.2         514.1         523.0         531.9         540.7         549.8         549.5         505.3         514.2         523.1         532.0         540.8         549.8         549.8         540.8         549.8         540.8         549.8         540.8         549.8         540.8         549.8         540.8         549.8         540.8         540.8         549.8         505.6         514.4         523.3         532.2         541.0         549.8         540.9         550.5         514.4         523.3         532.2         541.0         549.9         549.8         505.6         514.5         523.4         532.3         541.0         549.9         549.9         505.7         514.6         523.5         532.4         541.0         549.9         549.9         505.7         514.6         523.5         532.4         541.0         549.9         549.9         505.7         514.6         523.5         532.4         541.0         549.4         440.2         440.0         420.2         30.2         30.49         497.1         505.9         514.8         523.7         532.6         541.3         550.4         541.9         523.8<					4.39	l .	0.797		ſ	1	522.7	531.6	540.4	549.3
51         46.1         0.327         3.68         1.83         0.668         496.5         505.3         514.2         523.1         532.0         540.8         549           50         44.4         0.308         3.48         2.03         0.632         496.6         505.4         514.3         523.2         532.1         540.9         549         540.6         505.5         514.4         523.3         532.2         541.0         549         647         305.5         505.5         514.6         523.4         532.3         541.1         530         447         39.3         0.258         2.91         2.60         0.528         496.9         505.7         514.6         523.5         532.4         541.2         530         447         30.9         0.243         2.74         2.77         0.497         497.0         505.8         514.7         523.6         532.5         541.3         550         442         33.6         0.229         2.58         2.93         0.469         497.1         505.9         514.8         523.7         532.5         541.3         550         444         31.2         0.216         2.43         3.08         0.441         497.2         506.0         514.8         523.7		53	49.5	0.367	4.14	1.37	0.751	496.2	505.0	513.9	522.8	531.7	540.5	549.4
50         44.4         0.308         3.48         2.03         0.632         496.6         505.4         514.3         523.2         532.1         540.9         549           49         42.7         0.290         3.28         2.23         0.559         496.7         505.5         514.4         523.3         532.2         541.0         549           48         41.0         0.274         3.08         2.43         0.559         496.9         505.7         514.6         523.5         532.4         541.2         530           46         37.6         0.243         2.74         2.77         0.497         497.0         505.8         514.7         523.6         532.5         541.3         530           43         32.5         0.203         2.99         3.22         0.414         497.2         506.0         514.9         523.8         532.7         541.5         550           42         30.8         0.191         2.15         3.36         0.390         497.4         506.2         515.2         524.1         532.9         541.6         550           41         29.1         0.180         2.03         3.18         0.368         497.5         506.3 <td></td> <td>52</td> <td>47.8</td> <td>0.346</td> <td>3.90</td> <td>1.61</td> <td>0.708</td> <td>496.4</td> <td>505.2</td> <td>514.1</td> <td>523.0</td> <td>531.9</td> <td>540.7</td> <td>549.6</td>		52	47.8	0.346	3.90	1.61	0.708	496.4	505.2	514.1	523.0	531.9	540.7	549.6
49         42.7         0.290         3.28         2.23         0.595         496.7         505.5         514.4         523.3         532.2         541.0         549           48         41.0         0.274         3.08         2.43         0.559         496.8         505.6         514.5         523.4         532.3         511.1         550           46         37.6         0.243         2.74         2.77         0.497         497.0         505.8         514.7         523.6         532.5         541.3         550           45         35.9         0.229         2.58         2.93         0.469         497.1         505.9         514.8         523.7         532.6         541.4         550           44         34.2         0.216         2.43         3.08         0.441         497.2         506.0         514.9         523.8         532.7         541.5         550           42         30.8         0.191         2.15         3.36         0.390         497.4         506.2         515.2         524.2         533.0         541.8         550           41         29.1         0.180         2.03         3.48         0.368         497.5         506.3 <td></td> <td>51</td> <td>46.1</td> <td>0.327</td> <td>3.68</td> <td>1.83</td> <td>0.668</td> <td>496.5</td> <td>505.3</td> <td>514.2</td> <td>523.1</td> <td></td> <td>540.8</td> <td>549.7</td>		51	46.1	0.327	3.68	1.83	0.668	496.5	505.3	514.2	523.1		540.8	549.7
48         41.0         0.274         3.08         2.43         0.559         496.8         505.6         514.5         523.4         532.3         541.1         550           46         37.6         0.243         2.74         2.77         0.497         497.0         505.8         514.7         523.6         532.4         541.2         550           45         35.9         0.229         2.58         2.93         0.469         497.1         505.9         514.8         523.7         532.6         541.4         550           44         34.2         0.216         2.43         3.08         0.441         497.2         506.0         514.9         523.8         532.7         541.5         550           42         30.8         0.191         2.15         3.36         0.390         497.4         506.2         515.2         524.1         532.9         541.5         550           40         27.4         0.169         1.91         3.60         0.347         497.5         506.3         515.3         524.2         533.0         541.8         550           40         27.4         0.169         1.91         3.60         0.347         497.5         506.3 <td></td> <td>50</td> <td>44.4</td> <td></td> <td>§</td> <td>1</td> <td>ł</td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td>549.8</td>		50	44.4		§	1	ł		1					549.8
47         39.3         0.258         2.91         2.60         0.528         496.9         505.7         514.6         523.5         532.4         541.2         550           46         37.6         0.243         2.74         2.77         0.497         497.0         505.8         514.7         523.6         532.5         541.3         550           45         35.9         0.229         2.58         2.93         0.469         497.1         505.9         514.8         523.7         532.6         541.4         550           43         32.5         0.203         2.29         3.22         0.416         497.3         506.1         515.1         523.9         532.8         541.6         550           41         29.1         0.180         2.03         3.48         0.368         497.5         506.3         515.3         524.2         533.0         541.8         550           40         27.4         0.169         1.91         3.60         0.347         497.5         506.3         515.3         524.2         533.0         541.8         550           59         59         59.0         0.506         5.69         0.00         1.000         494.5			ll .			1								549.9
46         37.6         0.243         2.74         2.77         0.497         497.0         505.8         514.7         523.6         532.5         541.3         550           45         35.9         0.229         2.58         2.93         0.469         497.1         505.9         514.8         523.7         532.6         541.4         550           43         32.5         0.203         2.29         3.22         0.416         497.3         506.1         515.1         523.8         532.7         541.5         550           42         30.8         0.191         2.15         3.36         0.390         497.4         506.2         515.2         524.1         532.9         541.6         550           41         29.1         0.180         2.03         3.48         0.368         497.5         506.3         515.3         524.2         533.0         541.8         550           40         27.4         0.169         1.91         3.60         0.347         497.5         506.3         515.3         524.2         533.0         541.8         550           59         59         59.0         0.506         5.69         0.00         1.000         494.5				ł		i				1	1	1	1	550.0
45         35,9         0.229         2.58         2.93         0.469         497.1         505.9         514.8         523.7         532.6         541.4         550           44         34.2         0.216         2.43         3.08         0.441         497.2         506.0         514.9         523.8         532.7         541.5         550           42         30.8         0.191         2.15         3.36         0.390         497.4         506.2         515.2         524.1         532.9         541.7         550           41         29.1         0.180         2.03         3.48         0.368         497.5         506.3         515.3         524.2         533.0         541.8         550           40         27.4         0.169         1.91         3.60         0.347         497.5         506.3         515.3         524.2         533.0         541.8         550           59         59         59.0         0.506         5.69         0.00         1.000         494.5         503.3         512.2         521.0         529.8         538.6         547           57         55.6         0.452         5.08         0.61         0.893         494.7		47	39.3	0.258	2.91	2.60	0.528	496.9	505.7	514.6	523.5	532.4	541.2	550.1
44         34.2         0.216         2.43         3.08         0.441         497.2         506.0         514.9         523.8         532.7         541.5         550.4         43         32.5         0.203         2.29         3.22         0.416         497.3         506.1         515.1         523.9         532.8         541.6         550.4         41         29.1         0.180         2.03         3.48         0.368         497.5         506.3         515.3         524.2         533.0         541.8         550.4         40         27.4         0.169         1.91         3.60         0.347         497.5         506.3         515.3         524.2         533.0         541.8         550.5         550.3         550.3         512.2         521.0         529.8         538.6         547.8         550.5         550.3         541.8         550.3         541.8         550.5         550.3         541.8         550.3         550.3         541.2         533.0         541.8         550.5         550.3         541.8         550.3         550.3         541.2         521.0         529.8         538.6         547.8         550.3         541.8         550.3         541.8         550.3         550.3         541.8		46	37.6	0.243	2.74	2.77	0.497	497.0	505.8	514.7	523.6	532.5	541.3	550.2
43       32.5       0.203       2.29       3.22       0.416       497.3       506.1       515.1       523.9       532.8       541.6       550         42       30.8       0.191       2.15       3.36       0.390       497.4       506.2       515.2       524.1       532.9       541.7       550         41       29.1       0.180       2.03       3.48       0.368       497.5       506.3       515.3       524.2       533.0       541.8       550         40       27.4       0.169       1.91       3.60       0.347       497.5       506.3       515.3       524.2       533.0       541.8       550         59       59       59.0       0.506       5.69       0.00       1.000       494.5       503.3       512.2       521.0       529.8       538.6       547         58       57.3       0.478       5.37       0.32       0.944       494.6       503.4       512.3       521.1       529.9       538.7       547         56       53.9       0.426       4.79       0.90       0.842       494.8       503.6       512.5       521.3       530.1       538.8       547         55		45	35.9	0.229	2.58	2.93	0.469	497.1	505.9	514.8	523.7	532.6	541.4	550.3
42         30.8         0.191         2.15         3.36         0.390         497.4         506.2         515.2         524.1         532.9         541.7         550           41         29.1         0.180         2.03         3.48         0.368         497.5         506.3         515.3         524.2         533.0         541.8         550           59         59         59.0         0.506         5.69         0.00         1.000         494.5         503.3         512.2         521.0         529.8         538.6         547           57         55.6         0.452         5.08         0.61         0.893         494.7         503.5         512.4         521.2         520.0         538.8         547           56         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.4         520.2         530.0         538.8         547           54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.2         530.0         539.3         548           52         47.1         0.338         3.80         1.89         0.668		44	34.2	0.216	2.43	3.08	0.441	497.2	506.0	514.9	523.8	532.7	541.5	550.4
41         29.1         0.180         2.03         3.48         0.368         497.5         506.3         515.3         524.2         533.0         541.8         550           59         59         59.0         0.506         5.69         0.00         1.000         494.5         503.3         512.2         521.0         529.8         538.6         547.8           57         55.6         0.452         5.08         0.61         0.893         494.7         503.5         512.4         521.1         529.9         538.7         547           56         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.3         530.1         538.9         544           55         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.3         548           54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.4         530.3         539.3         548           52         47.1         0.338         3.80         1.89         0.668         495.4 <td></td> <td>43</td> <td>32.5</td> <td>0.203</td> <td>2.29</td> <td>3.22</td> <td>0.416</td> <td>497.3</td> <td>506.1</td> <td>515.1</td> <td>523.9</td> <td>532.8</td> <td>541.6</td> <td>550.5</td>		43	32.5	0.203	2.29	3.22	0.416	497.3	506.1	515.1	523.9	532.8	541.6	550.5
59         59         59.0         0.506         5.69         0.00         1.000         494.5         503.3         512.2         521.0         529.8         538.6         547.8           58         57.3         0.478         5.37         0.32         0.944         494.6         503.4         512.3         521.1         529.9         538.7         547.5         55.6         0.452         5.08         0.61         0.893         494.7         503.5         512.4         521.2         530.0         538.8         547.7           56         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.3         530.1         538.9         542.5         530.0         538.8         547.5         55.5         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.1         548.5         548.5         521.4         530.3         539.3         548.5         548.5         521.4         530.3         539.5         548.5         549.5         549.5         549.5         549.5         549.5         549.5         549.5         549.5         549.5         549.5		42	30.8	0.191	2.15	3.36	0.390	497.4	506.2	515.2	524.1	532.9		550.6
59         59         59.0         0.506         5.69         0.00         1.000         494.5         503.3         512.2         521.0         529.8         538.6         547.5           58         57.3         0.478         5.37         0.32         0.944         494.6         503.4         512.3         521.1         529.9         538.7         547.5         547.5         55.6         0.452         5.08         0.61         0.893         494.7         503.5         512.4         521.2         530.0         538.8         547.5         56.5         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.3         530.1         538.9         547.5         55.5         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.1         548.5         548.5         521.4         530.3         539.3         548.5         521.4         530.3         539.3         548.5         521.4         530.3         539.3         548.5         521.4         530.3         539.5         548.5         521.4         530.3         539.5         548.5         521.4         530.3<		41	29.1	0.180	2.03	3.48		497.5	506.3	515.3				550.7
58         57.3         0.478         5.37         0.32         0.944         494.6         503.4         512.3         521.1         529.9         538.7         547           57         55.6         0.452         5.08         0.61         0.893         494.7         503.5         512.4         521.2         530.0         538.8         547           56         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.3         530.1         538.9         547           55         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.1         548           54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.6         530.5         539.3         548           52         47.1         0.338         3.80         1.89         0.668         495.4         504.2         513.1         521.9         530.8         539.6         548           51         45.4         0.319         3.60         2.09         0.633         495.5         504.3 <th></th> <th>40</th> <th>27.4</th> <th>0.169</th> <th>1.91</th> <th>3.60</th> <th>0.347</th> <th>497.5</th> <th>506.3</th> <th>515.3</th> <th>524.2</th> <th>533.0</th> <th>541.8</th> <th>550.7</th>		40	27.4	0.169	1.91	3.60	0.347	497.5	506.3	515.3	524.2	533.0	541.8	550.7
58         57.3         0.478         5.37         0.32         0.944         494.6         503.4         512.3         521.1         529.9         538.7         547           57         55.6         0.452         5.08         0.61         0.893         494.7         503.5         512.4         521.2         530.0         538.8         547           56         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.3         530.1         538.9         547           55         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.1         548           54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.6         530.5         539.3         548           52         47.1         0.338         3.80         1.89         0.668         495.4         504.2         513.1         521.8         530.7         539.5         548           51         45.4         0.319         3.60         2.09         0.633         495.5         504.3 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>														
58         57.3         0.478         5.37         0.32         0.944         494.6         503.4         512.3         521.1         529.9         538.7         547           57         55.6         0.452         5.08         0.61         0.893         494.7         503.5         512.4         521.2         530.0         538.8         547           56         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.3         530.1         538.9         547           55         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.1         548           54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.6         530.5         539.3         548           52         47.1         0.338         3.80         1.89         0.668         495.4         504.2         513.1         521.9         530.8         539.6         548           51         45.4         0.319         3.60         2.09         0.633         495.5         504.2 <td>59</td> <td>59</td> <td>59.0</td> <td>0.506</td> <td>5.69</td> <td>0.00</td> <td>1.000</td> <td>494.5</td> <td>503.3</td> <td>512.2</td> <td>521.0</td> <td>529.8</td> <td>538.6</td> <td>547.5</td>	59	59	59.0	0.506	5.69	0.00	1.000	494.5	503.3	512.2	521.0	529.8	538.6	547.5
56         53.9         0.426         4.79         0.90         0.842         494.8         503.6         512.5         521.3         530.1         538.9         548           55         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.1         548           54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.6         530.5         539.3         548           52         47.1         0.338         3.80         1.89         0.668         495.4         504.2         513.1         521.9         530.8         539.6         518           51         45.4         0.319         3.60         2.09         0.633         495.5         504.3         513.2         522.0         530.9         539.7         548           50         43.7         0.301         3.39         2.30         0.596         495.7         504.5         513.4         522.2         531.1         539.9         548           49         42.0         0.283         3.19         2.50         0.561         495.8         504.5 <td></td> <td></td> <td>   </td> <td></td> <td>5.37</td> <td>0.32</td> <td>0.944</td> <td>494.6</td> <td>503.4</td> <td>512.3</td> <td>521.1</td> <td>529.9</td> <td>538.7</td> <td>547.6</td>					5.37	0.32	0.944	494.6	503.4	512.3	521.1	529.9	538.7	547.6
55         52.2         0.402         4.53         1.16         0.796         494.9         503.7         512.6         521.4         530.3         539.1         548           54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.6         530.5         539.3         548           53         48.8         0.358         4.03         1.66         0.708         495.3         504.1         513.0         521.8         530.7         539.5         548           52         47.1         0.338         3.80         1.89         0.668         495.4         504.2         513.1         521.9         530.8         539.6         518           51         45.4         0.319         3.60         2.09         0.633         495.5         504.3         513.2         522.0         530.9         539.7         548           50         43.7         0.301         3.39         2.30         0.596         495.7         504.5         513.4         522.2         531.1         539.9         548           49         42.0         0.283         3.19         2.50         0.561         495.8         504.5 <td>Ł</td> <td>57</td> <td>55.6</td> <td>0.452</td> <td>5.08</td> <td>0.61</td> <td>0.893</td> <td>494.7</td> <td>503.5</td> <td>512.4</td> <td>521.2</td> <td>530.0</td> <td>538.8</td> <td>547.7</td>	Ł	57	55.6	0.452	5.08	0.61	0.893	494.7	503.5	512.4	521.2	530.0	538.8	547.7
54         50.5         0.380         4.28         1.41         0.752         495.1         503.9         512.8         521.6         530.5         539.3         548           53         48.8         0.358         4.03         1.66         0.708         495.3         504.1         513.0         521.8         530.7         539.5         548           52         47.1         0.338         3.80         1.89         0.668         495.4         504.2         513.1         521.9         530.8         539.6         548           51         45.4         0.319         3.60         2.09         0.633         495.5         504.3         513.2         522.0         530.9         539.7         548           50         43.7         0.301         3.39         2.30         0.596         495.7         504.5         513.4         522.2         531.1         539.9         548           49         42.0         0.283         3.19         2.50         0.561         495.8         504.6         513.4         522.2         531.1         539.9         548           48         40.3         0.267         3.01         2.68         0.529         495.9         504.7 <td></td> <td>56</td> <td>53.9</td> <td>0.426</td> <td>4.79</td> <td>0.90</td> <td>0.842</td> <td>494.8</td> <td>503.6</td> <td>512.5</td> <td>521.3</td> <td>530.1</td> <td>538.9</td> <td>547.8</td>		56	53.9	0.426	4.79	0.90	0.842	494.8	503.6	512.5	521.3	530.1	538.9	547.8
53       48.8       0.358       4.03       1.66       0.708       495.3       504.1       513.0       521.8       530.7       539.5       548.5         52       47.1       0.338       3.80       1.89       0.668       495.4       504.2       513.1       521.9       530.8       539.6       548.5         51       45.4       0.319       3.60       2.09       0.633       495.5       504.3       513.2       522.0       530.9       539.7       548.5         50       43.7       0.301       3.39       2.30       0.596       495.7       504.5       513.4       522.2       531.1       539.9       548.5         49       42.0       0.283       3.19       2.50       0.561       495.8       504.6       513.4       522.2       531.1       539.9       548.0         48       40.3       0.267       3.01       2.68       0.529       495.9       504.7       513.5       522.4       531.3       540.1       549.0         47       38.6       0.252       2.84       2.85       0.499       496.0       504.8       513.6       522.5       531.4       540.2       549.0         45	1	55	52.2	0.402	4.53	1.16	0.796	494.9	503.7	512.6	521.4	530.3	539.1	548.0
52         47.1         0.338         3.80         1.89         0.668         495.4         504.2         513.1         521.9         530.8         539.6         548.5           51         45.4         0.319         3.60         2.09         0.633         495.5         504.3         513.2         522.0         530.9         539.7         548.5           50         43.7         0.301         3.39         2.30         0.596         495.7         504.5         513.4         522.2         531.1         539.9         548.5           49         42.0         0.283         3.19         2.50         0.561         495.8         504.6         513.4         522.2         531.1         539.9         548.5           48         40.3         0.267         3.01         2.68         0.529         495.9         504.7         513.5         522.4         531.3         540.1         549.4           47         38.6         0.252         2.84         2.85         0.499         496.0         504.8         513.6         522.5         531.4         540.2         549.4           45         35.2         0.223         2.51         3.18         0.411         496.2		54	50.5	0.380	4.28	1.41	0.752	495.1	503.9	512.8	521.6	530.5	539.3	548.2
51		53	48.8	0.358	4.03	1.66	0.708	495.3	504.1	513.0	521.8	530.7	539.5	548.4
50         43.7         0.301         3.39         2.30         0.596         495.7         504.5         513.4         522.2         531.1         539.9         548           49         42.0         0.283         3.19         2.50         0.561         495.8         504.6         513.4         522.3         531.2         540.0         548           48         40.3         0.267         3.01         2.68         0.529         495.9         504.7         513.5         522.4         531.3         540.1         549           47         38.6         0.252         2.84         2.85         0.499         496.0         504.8         513.6         522.5         531.4         540.2         549           46         36.9         0.237         2.67         3.02         0.469         496.1         504.9         513.7         522.6         531.5         540.2         549           45         35.2         0.223         2.51         3.18         0.441         496.2         505.0         513.8         522.7         531.6         540.4         549           44         33.5         0.210         2.37         3.32         0.417         496.3         505.1 <td></td> <td>52</td> <td>47.1</td> <td>0.338</td> <td>3.80</td> <td>1.89</td> <td>0.668</td> <td>495.4</td> <td>504.2</td> <td>513.1</td> <td>521.9</td> <td>530.8</td> <td>539.6</td> <td>548.5</td>		52	47.1	0.338	3.80	1.89	0.668	495.4	504.2	513.1	521.9	530.8	539.6	548.5
49 42.0 0.283 3.19 2.50 0.561 495.8 504.6 513.4 522.3 531.2 540.0 548 48 40.3 0.267 3.01 2.68 0.529 495.9 504.7 513.5 522.4 531.3 540.1 549. 47 38.6 0.252 2.84 2.85 0.499 496.0 504.8 513.6 522.5 531.4 540.2 549.  46 36.9 0.237 2.67 3.02 0.469 496.1 504.9 513.7 522.6 531.5 540.3 549. 45 35.2 0.223 2.51 3.18 0.441 496.2 505.0 513.8 522.7 531.6 540.4 549. 44 33.5 0.210 2.37 3.32 0.417 496.3 505.1 513.9 522.8 531.7 540.5 549. 43 31.8 0.198 2.23 3.46 0.392 496.4 505.2 514.1 522.9 531.8 540.6 549. 42 30.1 0.186 2.09 3.60 0.367 496.5 505.3 514.2 523.0 531.9 510.7 549. 41 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549.		51	45.4	0.319	3.60	2.09	0.633	495.5	504.3	513.2	1	i		548.6
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		50	43.7	0.301	3.39	2.30	0.596	495.7	504.5	513.4				548.8
47 38.6 0.252 2.84 2.85 0.499 496.0 504.8 513.6 522.5 531.4 540.2 549  46 36.9 0.237 2.67 3.02 0.469 496.1 504.9 513.7 522.6 531.5 540.3 549  45 35.2 0.223 2.51 3.18 0.441 496.2 505.0 513.8 522.7 531.6 540.4 549  44 33.5 0.210 2.37 3.32 0.417 496.3 505.1 513.9 522.8 531.7 540.5 549  43 31.8 0.198 2.23 3.46 0.392 496.4 505.2 514.1 522.9 531.8 540.6 549  42 30.1 0.186 2.09 3.60 0.367 496.5 505.3 514.2 523.0 531.9 510.7 549  41 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549					1		1							548.9
46 36.9 0.237 2.67 3.02 0.469 496.1 504.9 513.7 522.6 531.5 540.3 549.4   45 35.2 0.223 2.51 3.18 0.441 496.2 505.0 513.8 522.7 531.6 540.4 549.4   44 33.5 0.210 2.37 3.32 0.417 496.3 505.1 513.9 522.8 531.7 540.5 549.4   43 31.8 0.198 2.23 3.46 0.392 496.4 505.2 514.1 522.9 531.8 540.6 549.4   42 30.1 0.186 2.09 3.60 0.367 496.5 505.3 514.2 523.0 531.9 510.7 549.4   41 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549.8   49 540.8 540.8 549.8   41 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549.8   41 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549.8   42 30.1 0.186 2.09 3.60 0.367 496.5 505.3 514.2 523.0 531.9 510.7 549.8   43 31.8 0.198 2.23 3.46 0.367 496.5 505.3 514.2 523.0 531.9 510.7 549.8   44 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549.8   44 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549.8   45 45 45 45 45 45 45 45 45 45 45 45 45 4			NI .					1					1	549.0
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		47	38.6	0.252	2.84	2.85	0.499	496.0	504.8	513.6	522.5	531.4	540.2	949.1
44   33.5   0.210   2.37   3.32   0.417   496.3   505.1   513.9   522.8   531.7   540.5   549.			H				1				1			549.2
43   31.8   0.198   2.23   3.46   0.392   496.4   505.2   514.1   522.9   531.8   540.6   545.4   545.			11				1				1			
42 30.1 0.186 2.09 3.60 0.367 496.5 505.3 514.2 523.0 531.9 510.7 548 41 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549.8			11						1			1	1	549.4 549.5
41 28.4 0.175 1.97 3.72 0.346 496.6 505.4 514.3 523.1 532.0 540.8 549			11			i i				I.	1			
11 201 0110 1111 1111 1111 1111 1111 11			H	1			1						1	549.7
20.1 0.100 1.00 0.01 0.010 0.011 0.011 0.011			II.		1	1				1				549.7
		40	20.7	0.100	1.00	9.04	0.020	400.0	000.4	011.0	020.1	032.0	10.0	

	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Graiı	ns of a Cu	abic Foot	of Air.	
	neter, ahr.	of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height (	of the Ba	rometer i	n Englis	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
60	60	60.0	in. 0.523	gr. 5.87	gr. 0.00	1.000	gr. 493.4	gr. 502.2	gr. 511.0	gr. 519.8	gr. 528.6	gr. 537.4	gr. 546.2
00	59	58.3	0.323	5.54	0.33	0.944	493.6	502.4	511.0	520.0	528.8	537.6	546.4
	58	56.6	0.467	5.24	0.63	0.893	493.7	502.5	511.3	520.1	528.9	537.7	546.5
	57	54.9	0.441	4.95	0.92	0.843	493.8	502.6	511.4	520.2	529.0	537.8	546.6
	56	53.2	0.416	4.68	1.19	0.797	494.0	502.8	511.6	520.4	529.2	538.0	546.8
	55	51.5	0.393	4.41	1.46	0.751	494.2	503.0	511.8	520.6	529.4	538.2	547.0
	54	49.8	0.371	4.17	1.70	0.710	494.4	503.2	512 0	520.8	529.6	538.4	547.2
	53	48.1	0.350	3.92	1.95	0.668	494.5	503.3	512.1	520.9	529.7	538.5	547.4
}	52	46.4	0.330	3.70	2.17	0.630	494.7	503.4	512.3	521.1	529.9	538.7	547.6
.	51	44.7	0.311	3.49	2.38	0.595	494.8	503.5	512.4	521.2	530.0	538.8	547.7
	50	43.0	0.293	3.29	2.58	0.561	494.8	503.6	512.5	521.3	530.1	538.9	547.8
	49	41.3	0.277	3.10	2.77	0.528	494.9	503.7	512.6	521.4	530.2	539.0	547.9
	48	39.6	0.261	2.93	2.94	0.499	495.0	503.8	512.7	521.5	530.3	539.1	548.0
	47	37.9	0.246	2.75	3.12	0.468	495.1	503.9	512.8	521.6	530.4	539.2	548.1
	46	36.2	0.231	2.60	3.27	0.443	495.2	504.0	512.9	521.7	530.5	539.3	548.2
	45	34.5	0.218	2.45	3.42	0.417	495.3	504.1	513.0	521.8	530.6	539.4	548.3
	44	32.8	0.205	2.31	3.56	0.394	495.4	504.2	513.1	521.9	530.7	539.5	548.4
	43	31.1	0.193	2.17	3.70	0.370	495.5	504.3	513.2	522.0	530.8	539.6	548.5
	42	29.4	0.182	2.04	3.83	0.348	495.6	504.4	513.3	522.1	530.9	539.7	548.6
	41	27.7	0.171	1.92	3.95	0.327	495.6	504.4	513.3	522.1	530.9	539.7	548.7
61	61	61.0	0.541	6.06	0.00	1.000	492.3	501.1	509.9	518.7	527.5	536.3	545.1
	60	59.3	0.511	5.72	0.34	0.944	492.5	501.3	510.1	518.9	527.7	536.5	545.3
	59	57.6	0.483	5.40	0.66	0.891	492.6	501.4	510.2	519.0	527.8	536.6	545.4
	58 57	55.9	0.456	5.11	0.95	0.843	492.8	501.6	510.4	519.2	528.0 528.2	536.S 537.0	545.6 545.8
	34	54.2	0.491	4.83	1.23	0.191	493.0	901.3	510.6	519.4	920.2	337.0	040.0
	56	52.5	0.407	4.55	1.51	0.751	493.1	501.9	510.7	519.5	528.3	537.1	545.9
	55	50.8	0.383	4.30	1.76	0.710	493.3	502.1	510.9	519.7	528.5	537.3	546.1
	54	49.1	0.362	4.05	2.01	0.668	493.4	502.2	511.0	519.8	528.6	537.4	546.2
	53	47.4	0.342	3.83	2.23	0.632	493.5	502.3	511.1	519.9	528.7	537.5	546.3
	52	45.7	0.322	3.61	2.45	0.596	493.6	502.4	511.2	520.0	528.8	537.6	546.4
	51	44.0	0.304	3.40	2.66	0.561	493.8	502.6	511.4	520.2	529.0	537.8	546.6
	50	42.3	0.286	3.21	2.85	0.530	493.9	502.7	511.5	520.3	529.1	537.9	546.7
	49	40.6	0.270	3.02	1	0.498		502.8			529.2		546.8
	48	38.9	0.254	2.85	3.21	0.470	494.1	502.9	511.7	520.5	529.3	538.1	546.9
	47	37.2	0.240	2.69	3.37	0.444	494.2	503.0	511.8	520.6	529.4	538.2	547.0
	46	35.5	0.226	2.53	3.53	0.417	494.3	503.1	511.9	520.7	529.5	538.3	547.1
	45	33.8	0.213	2.38	3.68	0.393	494.4	503.2			529.6		547.2
	44	32.1	0.200	2-24	3.82	0.370	494.5	503.3	₹	520.9	529.7		547.3
1	43	30.4	0.188	2.11	3.95	0.348	494.6	503.4	1	521.0	529.8	538.6	547.4
	42	28.7	0.177	1.99	4.07	0.328	494.7	503.5	512.3	521.1	529.9	538.7	547.5
	41	27.0	0.167	1.87	4.19	0.309	494.7	503.5	512.3	521.1	529.9	538.7	547.5

	ading Ther-	Temp.	Force		eight *	IIu-		Weigh	t in Grai	ns of a C	ubic Foot	t of Air.	
moi	meter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer	in Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	in. 30.5	31.0
62	62	62.0	in. 0.559	gr. 6.25	gr. 0.00	1.000	gr. 491.2	gr. 499.9	gr. 508.7	gr. 517.5	gr. 526.3	gr. 535.1	gr. 543.9
02	61	60.3	0.528	5.91	0.34	0.946	491.4	500.1	508.9	517.7	526.5	535.3	544.1
	60	58.6	0.499	5.58	0.67	0.893	491.5	500.2	509.0	517.8	526.6	535.4	544.2
	59	56.9	0.472	5.27	0.98	0.843	491.7	500.4	509.2	518.0	526.8	535.6	544.4
	58	55.2	0.445	4.99	1.26	0.798	491.9	500.6	509.4	518.2	527.0	535.8	544.6
	57	53.5	0.421	4.70	1.55	0.752	492.0	500.7	509.5	518.3	527.1	535.9	544.7
	56	51.8	0.397	4.44	1.81	0.710	492.1	500.7	509.5	518.4	527.3	536.1	544.9
	55	50.1	0.375	4.19	2.06	0.670	492.2	500.9	509.7	518.5	527.4	536.2	545.0
	54	48.4	0.354	3.95	2.30	0.632	492.4	501.1	509.9	518.7	527.6	536.4	545.2
	53	46.7	0.333	3.72	2.53	0.595	492.5	501.3	510.1	518.9	527.7	536.5	545.3
	52	45.0	0.315	3.52	2.73	0.563	492.7	501.5	510.3	519.1	527.9	536.7	545.5
/	51	43.3	0.297	3.31	2.94	0.530	492.8	501.6	510.4	519.2	528.0	536.8	545.6
	50	41.6	0.280	3.13	3.12	0.501	492.9	501.7	510.5	519.3	528.1	536.9	545.7
	49	39.9	0.263	2.95	3.30	0.472	493.0	501.8	510.6	519.4	528.2	537.0	545.8
	48	38.2	0.248	2.77	3.48	0.443	493.1	501.9	510.7	519.5	528.3	537.1	545.9
	47	36.5	0.234	2.61	3.64	0.418	493.2	502.0	510.8	519.6	528.4	537.2	546.0
	46	34.8	0.220	2.47	3.78	0.395	493.3	502.1	510.9	519.7	528.5	537.3	546.1
	45	33.1	0.207	2.32	3.93	0.371	493.3	502.1	511.0	519.7	528.6	537.3	546.1
	44	31.4	0.195	2.18	4.07	0.349	493.4	502.2	511.0	519.8	528.6	537.4	546.2
	43	29.7 28.0	0.184	2.06	4.19	0.330	493.4	502.2	511.1	519.8	528.6	537.4	546.2
	42	26.3	0.173	1.94 1.83	4.31	0.311	493.5 493.6	502.3 502.4	511.2	519.9	528.7	537.5	546.3
	411	20.0	0.105	1.00	4.42	0.233	455.0	302.4	511.3	520.0	528.8	537.6	546.4
63	63	63.0	0.578	6.45	0.00	1.000	490.2	498.9	507.7	516.4	525.2	533.9	542.7
	62	61.3	0.546	6.10	0.35	0.946	490.4	499.1	507.9	516.6	525.4	534.1	542.9
	61	59.6	0.516	5.76	0.69	0.893	490.5	499.2	508.0	516.7	525.5	534.2	543.0
	60	57.9	0.488	5.44	1.01	0.843	490.7	499.4	508.2	516.9	525.7	534.4	543.2
	59	56.2	0.461	5.15	1.30	0.798	490.9	499.6	508.4	517.1	525.9	534.6	543.4
	58	54.5	0.435	4.86	1.59	0.753	491.0	499.7	508.5	517.2	526.0	534.7	543.5
	57	52.8	0.411	4.59	1.86	0.712	491.1	499.8	508.6	517.3	526.2	534.9	543.7
	56	51.1	0.388	4.33	2.12	0.671	491.2	499.9	508.7	517.4	526.3	535.0	543.8
	55 54	49.4	0.366	4.09	2.36	0.634	491.3	500.0	508.8	517.5	526.4	535.1	543.9
			0.345	3.85	2.60	0.597	491.5	500.2	509.0	517.7	526.6	535.3	544.1
	53	46.0	0.326	3.63	2.82	0.563	491.7	500.4	509.2	518.0	526.8	535.5	544.3
	52	44.3	0.307	3.43	3.02	0.532	491.8	500.5	509.3	518.1	526.9	535.6	544.4
	51 50	42.6	$0.289 \ 0.273$	3.24	3.21	$0.502 \ 0.473$	491.9	500.6 500.7	509.4	518.2	527.0 527.1	535.7	544.5
	49	39.2	0.273	2.07	3.58	0.445	492.1	500.7	509.5	518.3 518.4	527.1	535.8 535.9	544.6 544.7
	48	37.5	0.242	2.71	3.74	0.420	492.2	500.9	509.7	518.5	527.3	536.0	544.8
								1	1		- 1		
	47 46	35.8 34.1	0.228	2.56	3.89	0.397	492.3	501.0	509.8	518.6	527.4	536.1	544.9
	45	32.4	$0.215 \mid 0.202 \mid$	$\begin{bmatrix} 2.41 \\ 2.26 \end{bmatrix}$	4.04 4.19	$0.374 \\ 0.351$	492.4 492.5	501.1 501.2	509.9 510.0	518.7 518.8	527.5 527.6	536.2 536.3	545.0 545.1
	44	30.7	0.190	2.13	4.19	0.330	492.5	501.2	510.0	518.8	527.6	536.3	545.1
	43	29.0	0.179	2.00	4.45	0.310	492.6	501.3	510.0	518.9	527.7	536.4	545.2
	42	27.3	0.168	1.87	4.58	0.290	492.7	1	1			536.5	545.3

	eading Ther-	Temp.	Force	Wei of V	ght apor.	Hu-		Weight	t in Grain	ns of a Cu	ibie Foot	of Air.	
mo	ometer, Fahr.	of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	cometer is	n English	Inches.	
Dry	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
64	64 63	$64.0 \\ 62.3$	0.597 $0.565$	6.65	$0.00 \\ 0.36$	0.946	489.1 489.3	497.8	506.6 506.8	515.3 515.5	$524.0 \\ 524.2$	532.7 532.9	541.5 541.7
1	62	60.6	0.534	5.94	0.71	0.893	489.5	498.2	507.0	515.7	524.4	533.1	541.9
	61	58.9	0.504	5.61	1.04	0.843	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	60	57.2	0.476	5.31	1.34	0.798	489.9	498.6	507.4	516.1	524.8	533.5	542.3
	59	55.5	0.450	5.01	1.64	0.753	490.0	498.7	507.5	516.2	524.9	533.6	542.4
	58	53.8	0.425	4.73	1.92	0.711	490.1	498.8	507.6	516.3	525.1	533.8	542.6
	57	52.1	0.401	4.47	2.18	0.672	490.2	498.9	507.7	516.4	525.2	533.9	542.7
l	56	50.4	0.379	4.23	2.42	0.636	490.4	499.1	507.9	516.6	525.4	534.1	542.9
	55	48.7	0.357	3.98	2.67	0.598	490.5	499.2	508.0	516.7	525.5	534.2	543.0
	54	47.0	0.337	3.75	2.90	0.564	490.7	499.4	508.2	516.9	525.7	534.4	543.2
	53	45.3	0.318	3.55	3.10	0.534	490.8	499.5	508.3	517.0	525.8	534.5	543.3
	52	43.6	0.300	3.34	3.31	0.502	490.9	499.6	508.4	517.1	525.9	534.6	543.4
	51	41.9	0.282	3.15	3.50	0.473	491.0	499.7	508.5	517.2	526.0	534.7	543.5
	50	40.2	0.266	2.96	3.69	0.445	491.2	499.9	508.7	517.4	526.1	534.9	543.7
	49 48	38.5 36.8	$0.251 \\ 0.236$	2.79	3.86	0.419	491.3	500.0	508.8	517.5	526.2	535.0	543.8 543.9
	47	35.1	0.230	$\begin{vmatrix} 2.63 \\ 2.47 \end{vmatrix}$	4.18	0.372	491.4	500.1	508.9	517.6 517.7	526.3 526.4	535.1 535.2	544.0
il	46	33.4	0.210	2.33	4.32	0.372	491.6	500.2	509.0	517.8	526.5	535.3	544.1
	45	31.7	0.197	2.19	4.46	0.330	491.7	500.4	509.2	517.9	526.6	535.4	544.2
	44	30.0	0.186	2.06	4.59	0.310	491.7	500.4	509.2	517.9	526.6	535.4	544.2
	43	28.3	0.175	1.94	4.71	0.292	491.8	500.5	509.3	518.0	526.7	535.5	544.3
	42	26.6	0.164	1.83	4.82	0.275	491.9	500.6	509.4	518.1	526.8	535.6	544.4
65	65	65.0	0.617	6.87	0.00	1.000	488.1	496.8	505.5	514.2	522.9	531.6	540.3
	64	63.4	0.586	6.51	0.36	0.947	488.3	497.0	505.7	514.4	523.1	531.8	540.5
	63	61.8	0.555	6.17	0.70	0.898	488.5	497.2	505.9	514.6	523.3	532.0	540.7
	62	60.2	0.527	5.85	1.02	0.851	488.7	497.4	506.1	514.8	523.5	532.2	540.9
	61	58.6	0.499	5.55	1.32	0.808	488.9	497.6	506.3	515.0	523.7	532.4	541.1
1	60	57.0	0.473	5.25	1.62	0.765	489.0	497.7	506.5	515.2	523.9	532.6	541.3
1	59	55.4	0.449	4.98	1.89	0.725	489.1	497.8	506.6	515.3	524.0	532.7	541.5
	58	53.8	0.425	4.72	2.15	0.687	489.3	498.0	506.8	515.5	524.2	532.9	541.7
	57	52.2	0.402	4.47	2.40	0.651	489.4	498.1	506.9	515.6	524.3	533.0	541.8
	56	50.6	0.381	4.23	2.64	0.616	489.6	498.3	507.1	515.8	524.5	533.2	542.0
	55	49.0	0.361	4.01	2.86	0.584	489.7	493.4	507.2	515.9	524.6	533.3	542.1
	54	47.4	0.342	3.79	3.08	0.552	489.8	498.5	507.3	516.0	524.7	533.4	542.2
	53 52	45.8	0.323	3.60	3.27	0.524	489.9	498.6	507.4	516.1	524.8	533.5 533.6	542.3 542.4
	51	44.2	$0.306 \\ 0.289$	3.39	3.48	0.493	490.0	498.7 498.8	507.5	516.2	525.0	533.7	542.5
	50	41.0	0.259	3.04	3.83	0.442	490.1	498.9	507.7	516.4	525.1	533.8	542.6
1	19	39.4	0.274	2.87	4.00	0.418	490.3	499.0	507.8	516.5	525.2	533.9	542.7
	48	37.8	0.245	2.72	4.15	0.396	490.3	499.0	507.8	516.5	525.2	533.9	542.7
	47	36.2	0.231	2.57	4.30	0.374	490.4	499.1	507.9	516.6	525.3	534.0	542.8
	46	31.6	0.219	2.43	4.44	0.354	490.5	499.2	508.0	516.7	525.4	534.1	542.9
	45	33.0	0.207	2.31	4.56	0.336	490.6	499.3	508.1	516.8	525.5	534.2	543.0
	44	31.4	0.195	2.17	4.70	0.316	490.7	499.4	508.2	516.9	525.6	534.3	543.1
	43	29 8	0.181	2.05	4.82	0.299	490.7	499.4	508.2	516.9	525.6	534.3	543.1
-	42	28.2	0.174	1.94	4.93	0.283	490.8	499.5	508.3	517.0	525.7	534.4	543.2

	iding	Temp.	Force		ight apor	Hu-		Weight	in Grain	ns of a Cu	ıbic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n Englisl	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
66	66	66.0	iu. 0.638	gr. 7.08	gr. 0.00	1.000	gr. 487.0	gr. 495.7	gr. 504.4	gr. 513.1	gr. 521.8	gr. 530.5	gr. 539.2
00	65	64.4	0.605	6.72	0.36	0.949	487.2	495.9	504.6	513.3	522.0	530.7	539.4
	64	62.8	0.574	6.35	0.73	0.897	487.3	496.0	504.7	513.4	522.1	530.8	539.5
	63	61.2	0.544	6.04	1.04	0.853	487.5	496.2	504.9	513.6	522.3	531.0	539.7
	62	59.6	0.516	5.72	1.36	0.808	487.7	496.4	505.1	513.8	522.5	531.2	539.9
	61	58.0	0.489	5.42	1.66	0.766	487.9	496.6	505.3	514.0	522.7	531.4	540.1
	60	56.4	0.464	5.14	1.94	0.726	488.0	496.7	505.4	514.1	522.8	531.5	540.2
	59	54.8	0.440	4.88	2.20	0.689	488.1	496.8	505.5	514.2	523.0	531.7	540.4
	58	53.2	0.416	4.62	2.46	0.652	488.2	496.9	505.6	514.3	523.1	531.8	540.5
	57	51.6	0.394	4.37	2.71	0.619	488.4	497.1	505.8	514.5	523.3	532.0	540.7
	56	50.0	0.373	4.15	2.93	0.586	488.5	497.2	505.9	514.6	523.4	532.1	540.8
	55	48.4	0.354	3.92	3.16	0.553	488.6	497.3	506.1	514.8	523.5	532.2	541.0
	54	46.8	0.335	3.72	3.36	0.525	488.8	497.5	506.3	515.0	523.7	532.4	541.2
	53	45.2	0.317	3.51	3.57	0.496	488.9	497.6	506.4	515.1	523.8	532.5	541.3
	52	43.6	0.300	3.33	3.75	0.470	489.0	497.7	506.5	515.2	523.9	532.6	541.4
	51	42.0	0.283	3.14	3.94	0.443	489.1	497.8	506.6	515.3	524.0	532.7	541.5
	50	40.4	0.268	2.97	4.11	0.419	489.2	497.9	506.7	515.4	524.1	532.8	541.6
	49	38.8	0.253	2.81	4.27	0.397	489.3	498.0	506.8	515.5	524.2	532.9	541.7
	48	37.2	0.240	2.66	4.42	0.376	489.4	498.1	506.9	515.6	524.3	533.0	541.8
	47	35.6	0.227	2.51	4.57	0.355	489.4	498.1	506.9	515.6	524.3	533.0	541.8
	46	34.0	0.214	2.37	4.71	0.335	489.5	498.2	507.0	515.7	524.4	533.1	541.9
	45	32.4	0.202	2.24	4.84	0.316	489.6	498.3	507.1	515.8	524.5	533.2	542.0
	44	30.8	0.191	2.12	4.96	0.299	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	43	29.2	0.180	2.00	5.08	0.283	489.7	498.4	507.2	515.9	524.6	533.3	542.1
					-								
67	67	67.0	0.659	7.30	0.00	1.000	485.9	494.6	503.3	512.0	520.6	529.3	538.0
	66	65.4	0.626	6.93	0.37	0.949	486.1	494.8	503.5	512.2	520.8	529.5	538.2
	65	63.8	0.593	6.55	0.75	0.897	486.3	495.0	503.7	512.4	521.0	529.7	538.4
	64	62.2	0.563	6.23	1.07	0.853	486.5	495.2	503.9	512.6	521.2	529.9	538.6
	63	60.6	0.534	5.91	1.39	0.810	486.7	495.4	504.1	512.8	521.4	530.1	538.8
	62	59.0	0.506	5.60	1.70	0.767	486.8	495.5	504.2	512.9	521.6	530.3	539.0
	61	57.4	0.480	5.31	1.99	0.728	486.9	495.6	504.3	513.0	521.7	530.4	539.1
	60	55.8	0.455	5.04	2.26	0.691	487.1	495.8	504.5	513.2	521.9	530.6	539.3
	59	54.2	0.431	4.77	2.53	0.653	487.2	495.9	504.6	513.3	522.0	530.7	539.4
	58	52.6	0.408	4.52	12.78	0.619	487.3	496.0	504.7	513.4	522.1	530.8	539.5
	57	51.0	0.386	4.28	3.02	0.586	487.5	496.2	504.9	513.6			
	56	49.4	0.366	4.05	3.25	0.555	487.6	496.3	.505.0	513.7		1	539.8
	55	47.8	0.346	3.83	3.47	0.524	487.8	496.5	505.1	513.8	522.6	1	549.9
	54	46.2	0.328	3.62	3.68	0.496	487.9	496.6		513.9	522.7		540.0
	53	44.6	0.310	3.43	3.87	0.470	488.0	496.7	505.3	514.0	522.8		540.1
	52	43.0	0.293	3.25	4.05	0.445	488.1	496.8	504.4	514.1	522.9	531.5	540.2
	51	41.4	0.278	3.08	4.22	0.422	488.2	496.9	505.5	514.2	523.0	531.6	540.3
	50	39.5	0.263	2.91	4.39	0.399	488.4	497.1	505.7				540.5
	49	38.2	0.248	2.75	4.55	0.377	488.5	497.2	505.8	514.5	523.2	531.9	540.6

Path	a	ns of a	n Grai	Weight		Hu-	ight apor		Force	Temp.	ading Ther-	Re
Dry.   Wet.   Fabric   Color of Air.   Color	teı	romete	the Ba	eight o		Satura-				of Dew-	meter,	mo
67							bic Ft.			Fahr.	Wet.	Dry.
48						0.377						
47											l i	07
46										1		
68 68.0 0.681 7.53 0.00 1.000 484.9 493.5 502.2 510.8 519.5 528 66 66.4 0.646 7.15 0.38 0.949 485.1 493.8 502.5 511.1 519.7 523.6 66 64.8 0.613 6.77 0.76 0.899 485.3 494.0 502.6 511.2 519.9 528 65 63.2 0.582 6.43 1.10 0.854 485.5 494.2 502.8 511.4 520.1 528 63 60.0 0.523 5.78 1.75 0.768 485.8 494.5 503.0 511.6 520.3 528 63 60.0 0.523 5.78 1.75 0.768 485.8 494.5 503.1 511.8 520.5 528 62 58.4 0.496 5.47 2.06 0.726 485.9 494.4 503.0 511.6 520.3 528 61 56.8 0.470 5.20 2.33 0.691 486.0 494.7 503.4 512.1 520.8 521.6 56 55.2 0.445 4.93 2.60 0.655 486.2 494.9 503.6 512.3 521.0 528 59 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 520.8 52 52 52 52 52 52 52 52 52 52 52 52 52		1		1					0.210	33.4	46	
68 68 68.0 0.681 7.53 0.00 1.000 484.9 493.5 502.2 510.8 519.5 528 67 66.4 0.646 7.15 0.38 0.949 485.1 493.8 502.5 511.1 519.7 528 65 63.2 0.582 6.43 1.10 0.854 485.5 494.2 502.8 511.4 520.1 528 63 60.0 0.523 5.78 1.75 0.768 485.8 494.5 503.0 511.6 520.3 528 63 60.0 0.523 5.78 1.75 0.768 485.8 494.5 503.1 511.8 520.5 528 61 56.8 0.470 5.20 2.33 0.691 486.0 494.7 503.4 512.1 520.8 520 60 55.2 0.445 4.93 2.60 0.655 486.2 494.9 503.6 512.3 521.0 520 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529 559 53.6 0.422 4.67 2.86 0.620 486.3 495.5 504.0 512.7 521.4 531 550 550 550 550 550 550 550 550 550 55	1.	514	506.1	97.5	488.8	0.301	5.11	2.19	0.198	31.8	45	
67         66.4         0.646         7.15         0.38         0.949         485.1         493.8         502.5         511.1         519.7         526         66         64.8         0.613         6.77         0.76         0.899         485.3         494.0         502.6         511.2         519.9         528         66         63.2         0.582         6.43         1.10         0.854         485.5         494.2         502.8         511.4         520.1         522         64         61.6         0.552         6.10         1.43         0.810         485.7         494.4         503.0         511.6         520.3         522         63         60.0         0.523         5.78         1.75         0.768         485.8         494.5         503.1         511.8         520.5         522         63         60.0         0.522         0.33         0.691         486.0         494.7         503.4         512.0         520.7         522         61         568.8         0.470         5.26         0.620         486.3         495.0         503.7         512.4         521.1         529         52.8         52.0         0.400         4.42         3.11         0.587         486.4         495.1         503.8	1.	514	506.2	97.6	488.9	0.284	5.23	2.07	0.187	30.2	44	
66         64.8         0.613         6.77         0.76         0.899         485.3         494.0         502.6         511.2         519.9         526           65         63.2         0.582         6.43         1.10         0.854         485.5         494.2         502.8         511.4         520.1         528           64         61.6         0.552         6.10         1.43         0.810         485.7         494.4         503.0         511.6         520.3         526           63         60.0         0.523         5.78         1.75         0.768         485.8         494.5         503.3         512.0         520.5         526           61         56.8         0.470         5.20         2.33         0.691         486.0         494.7         503.4         512.1         520.8         526           60         55.2         0.445         4.93         2.60         0.655         486.2         494.9         503.6         512.3         521.0         526         59         53.6         0.422         4.67         2.86         0.620         486.3         495.1         503.6         512.3         521.2         522         52.2         52.6         0.620 <td>0.</td> <td>510</td> <td>502.2</td> <td>93.5</td> <td>484.9</td> <td>1.000</td> <td>0.00</td> <td>7.53</td> <td>0.681</td> <td>68.0</td> <td>68</td> <td>68</td>	0.	510	502.2	93.5	484.9	1.000	0.00	7.53	0.681	68.0	68	68
65         63.2         0.582         6.43         1.10         0.854         485.5         494.2         502.8         511.4         520.1         522           64         61.6         0.552         6.10         1.43         0.810         485.7         494.4         503.0         511.6         520.3         528           63         60.0         0.523         5.78         1.75         0.768         485.8         494.5         503.1         511.6         520.3         528           62         58.4         0.496         5.47         2.06         0.726         485.9         494.6         503.3         512.0         520.7         529           61         56.8         0.470         5.20         2.33         0.691         486.0         494.7         503.4         512.1         520.8         522           59         53.6         0.422         4.67         2.86         0.620         486.3         495.0         503.7         512.4         521.1         522           59         53.6         0.422         4.67         2.86         0.620         486.3         495.3         504.0         512.7         521.1         532           57	1.	511	502.5	93.8	485.1	0.949	0.38	7.15	0.646	66.4	67	
64         61.6         0.552         6.10         1.43         0.810         485.7         494.4         503.0         511.6         520.3         522           63         60.0         0.523         5.78         1.75         0.768         485.8         494.5         503.1         511.8         520.5         528           62         58.4         0.496         5.47         2.06         0.726         485.9         494.6         503.3         512.0         520.7         522           61         56.8         0.470         5.20         2.33         0.691         486.0         494.7         503.4         512.1         520.8         522           60         55.2         0.445         4.93         2.60         0.655         486.2         494.9         503.6         512.3         521.0         528           59         53.6         0.422         4.67         2.86         0.620         486.3         495.0         503.7         512.4         521.1         522           58         52.0         0.400         4.42         3.11         0.587         486.4         495.1         503.8         512.5         521.2         522           57	1.	511	502.6		485.3							
63         60.0         0.523         5.78         1.75         0.768         485.8         494.5         503.1         511.8         520.5         522           62         58.4         0.496         5.47         2.06         0.726         485.9         494.6         503.3         512.0         520.7         522           61         56.8         0.470         5.20         2.33         0.691         486.0         494.7         503.4         512.1         520.8         522           60         55.2         0.445         4.93         2.60         0.655         486.2         494.9         503.6         512.3         521.0         522           59         53.6         0.422         4.67         2.86         0.620         486.3         495.0         503.7         512.4         521.1         522           58         52.0         0.400         4.42         3.11         0.587         486.4         495.1         503.8         512.5         521.2         522           57         50.4         0.379         4.19         3.34         0.556         486.4         495.1         503.8         512.5         521.2         522           57		1			- 1					1		
62 58.4 0.496 5.47 2.06 0.726 485.9 494.6 503.3 512.0 520.7 529.6 61 56.8 0.470 5.20 2.33 0.691 486.0 494.7 503.4 512.1 520.8 529.6 60 55.2 0.445 4.93 2.60 0.655 486.2 494.9 503.6 512.3 521.0 529.8 529.5 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 520.8 529.5 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 520.8 529.5 52.0 0.400 4.42 3.11 0.587 486.4 495.1 503.8 512.5 521.2 529.5 57 50.4 0.379 4.19 3.34 0.556 486.6 495.3 504.0 512.7 521.4 530.5 55 47.2 0.339 3.75 3.78 0.498 486.8 495.5 504.2 512.9 521.6 530.5 44.0 0.304 3.35 4.18 0.445 487.0 495.7 504.4 513.1 521.8 530.5 52.4 42.4 0.287 3.17 4.36 0.421 487.1 495.8 504.5 513.2 521.9 530.5 50.4 0.230 2.57 2.84 4.69 0.377 487.3 496.0 504.7 513.4 522.1 530.5 50.2 50.2 50.2 50.2 50.2 50.2 50.2 5											1	
61 56.8 0.470 5.20 2.33 0.691 486.0 494.7 503.4 512.1 520.8 522.6 53 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529.5 53.6 0.422 4.67 2.86 0.620 486.3 495.0 503.7 512.4 521.1 529.5 53 52.0 0.400 4.42 3.11 0.587 486.4 495.1 503.8 512.5 521.2 529.5 57 50.4 0.379 4.19 3.34 0.556 486.6 495.3 504.0 512.7 521.4 530.5 55 47.2 0.339 3.75 3.78 0.498 486.8 495.5 504.2 512.9 521.6 530.5 44.0 0.304 3.35 4.18 0.445 487.0 495.7 504.4 513.1 521.8 530.5 52 42.4 0.287 3.17 4.36 0.421 487.1 495.8 504.5 513.2 521.9 530.5 51 40.8 0.272 3.00 4.53 0.399 487.2 495.9 504.6 513.3 522.0 530.5 50.2 513.9 522.6 530.5 50.2 513.9 522.4 530.5 50.2 513.9 522.4 530.5 50.2 513.2 522.2 530.5 50.5 50.2 513.2 522.2 530.5 50.5 50.2 513.2 522.2 530.5 50.5 50.2 513.2 522.2 530.5 50.5 50.2 513.2 522.2 530.5 50.5 50.2 513.2 522.2 530.5 50.5 50.2 50.5 50.2 513.5 522.2 530.5 50.5 50.2 513.5 522.2 530.5 50.5 50.2 50.5 50.2 513.5 522.2 530.5 50.5 50.5 50.5 50.5 50.5 50.5 50.	1.	511	503.1	194.5	485.8	0.768	1.75	5.78		60.0	63	- need
60         55.2         0.445         4.93         2.60         0.655         486.2         494.9         503.6         512.3         521.0         522           59         53.6         0.422         4.67         2.86         0.620         486.3         495.0         503.7         512.4         521.1         522           58         52.0         0.400         4.42         3.11         0.587         486.4         495.1         503.8         512.5         521.2         522           57         50.4         0.379         4.19         3.34         0.556         486.6         495.3         504.0         512.7         521.4         530           56         48.8         0.358         3.96         3.57         0.526         486.7         495.4         504.1         512.8         521.5         531           54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.0         521.7         536           54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.1         521.8         536           52	2.	512	503.3	194.6	485.9						l f	
59         53.6         0.422         4.67         2.86         0.620         486.3         495.0         503.7         512.4         521.1         522           58         52.0         0.400         4.42         3.11         0.587         486.4         495.1         503.8         512.5         521.2         522           57         50.4         0.379         4.19         3.34         0.556         486.6         495.3         504.0         512.7         521.4         536           56         48.8         0.358         3.96         3.57         0.526         486.7         495.4         504.1         512.8         521.5         536           54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.0         521.7         536           53         44.0         0.304         3.35         4.18         0.445         487.0         495.7         504.4         513.1         521.8         536           52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         536           51												
58         52.0         0.400         4.42         3.11         0.587         486.4         495.1         503.8         512.5         521.2         522         527         50.4         0.379         4.19         3.34         0.556         486.6         495.3         504.0         512.7         521.4         530           56         48.8         0.358         3.96         3.57         0.526         486.7         495.4         504.1         512.8         521.5         530           55         47.2         0.339         3.75         3.78         0.498         486.8         495.5         504.2         512.9         521.6         530           54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.0         521.7         530           53         44.0         0.304         3.35         4.18         0.445         487.0         495.7         504.4         513.1         521.8         531           52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         530         513.2         521.9         530 </td <td></td> <td>1</td> <td></td> <td></td> <td></td> <td>1</td> <td>1</td> <td></td> <td></td> <td>1</td> <td></td> <td></td>		1				1	1			1		
57         50.4         0.379         4.19         3.34         0.556         486.6         495.3         504.0         512.7         521.4         536           56         48.8         0.358         3.96         3.57         0.526         486.7         495.4         504.1         512.8         521.5         536           55         47.2         0.339         3.75         3.78         0.498         486.8         495.5         504.2         512.9         521.6         536           54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.0         521.7         536           53         44.0         0.304         3.35         4.18         0.445         487.0         495.7         504.4         513.1         521.8         536           52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         536           51         40.8         0.227         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         536           49												
56         48.8         0.358         3.96         3.57         0.526         486.7         495.4         504.1         512.8         521.5         536           55         47.2         0.339         3.75         3.78         0.498         486.8         495.5         504.2         512.9         521.6         536           54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.0         521.7         536           53         44.0         0.304         3.35         4.18         0.445         487.0         495.7         504.4         513.1         521.8         536           52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         536           51         40.8         0.272         3.00         4.53         0.399         487.2         495.9         504.6         513.3         522.0         536           50         39.2         0.257         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         536           49		1					F					
55         47.2         0.339         3.75         3.78         0.498         486.8         495.5         504.2         512.9         521.6         53           54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.0         521.7         536           53         44.0         0.304         3.35         4.18         0.445         487.0         495.7         504.4         513.1         521.8         536           52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         536           50         39.2         0.257         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         536           49         37.6         0.243         2.68         4.85         0.356         487.4         496.1         504.8         513.5         522.2         536           48         36.0         0.230         2.54         4.99         0.337         487.5         496.2         504.9         513.6         522.3         53           47												
54         45.6         0.321         3.54         3.99         0.470         486.9         495.6         504.3         513.0         521.7         536           53         44.0         0.304         3.35         4.18         0.445         487.0         495.7         504.4         513.1         521.8         536           52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         536           50         39.2         0.257         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         536           49         37.6         0.243         2.68         4.85         0.356         487.4         496.1         504.8         513.5         522.2         536           48         36.0         0.230         2.54         4.99         0.337         487.5         496.2         504.9         513.6         522.3         53           47         34.4         0.217         2.40         5.13         0.319         487.6         496.3         505.0         513.7         522.4         53           45										1		
53         44.0         0.304         3.35         4.18         0.445         487.0         495.7         504.4         513.1         521.8         53           52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         53           51         40.8         0.272         3.00         4.53         0.399         487.2         495.9         504.6         513.3         522.0         53           50         39.2         0.257         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         53           49         37.6         0.243         2.68         4.85         0.356         487.4         496.1         504.8         513.5         522.2         53           48         36.0         0.230         2.54         4.99         0.337         487.5         496.2         504.9         513.6         522.3         53           47         34.4         0.217         2.40         5.13         0.319         487.6         496.3         505.0         513.7         522.4         53           45         3							1			1		
52         42.4         0.287         3.17         4.36         0.421         487.1         495.8         504.5         513.2         521.9         53           51         40.8         0.272         3.00         4.53         0.399         487.2         495.9         504.6         513.3         522.0         53           50         39.2         0.257         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         53           49         37.6         0.243         2.68         4.85         0.356         487.4         496.1         504.8         513.5         522.2         53           48         36.0         0.230         2.54         4.99         0.337         487.5         496.2         504.9         513.6         522.3         53           47         34.4         0.217         2.40         5.13         0.319         487.6         496.3         505.0         513.7         522.4         53           46         32.8         0.205         2.27         5.26         0.302         487.6         496.3         505.0         513.7         522.4         53           45         3		1								1		
51         40.8         0.272         3.00         4.53         0.399         487.2         495.9         504.6         513.3         522.0         53           50         39.2         0.257         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         53           49         37.6         0.243         2.68         4.85         0.356         487.4         496.1         504.8         513.5         522.2         53           48         36.0         0.230         2.54         4.99         0.337         487.5         496.2         504.9         513.6         522.3         53           47         34.4         0.217         2.40         5.13         0.319         487.6         496.3         505.0         513.7         522.4         53           46         32.8         0.205         2.27         5.26         0.302         487.6         496.3         505.0         513.7         522.4         53           45         31.2         0.194         2.15         5.38         0.286         487.7         496.4         505.1         513.8         522.5         53           44         2						1	1					
50         39.2         0.257         2.84         4.69         0.377         487.3         496.0         504.7         513.4         522.1         536           49         37.6         0.243         2.68         4.85         0.356         487.4         496.1         504.8         513.5         522.2         536           48         36.0         0.230         2.54         4.99         0.337         487.5         496.2         504.9         513.6         522.2         53           47         34.4         0.217         2.40         5.13         0.319         487.6         496.3         505.0         513.7         522.4         53           46         32.8         0.205         2.27         5.26         0.302         487.6         496.3         505.0         513.7         522.4         53           45         31.2         0.194         2.15         5.38         0.286         487.7         496.4         505.1         513.8         522.5         53           44         29.6         0.183         2.04         5.49         0.271         487.8         496.4         505.1         513.8         522.5         53           69 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>}</td><td></td><td></td><td></td><td>l l</td><td>Į.</td><td></td></td<>						}				l l	Į.	
49         37.6         0.243         2.68         4.85         0.356         487.4         496.1         504.8         513.5         522.2         53           48         36.0         0.230         2.54         4.99         0.337         487.5         496.2         504.9         513.6         522.3         53           47         34.4         0.217         2.40         5.13         0.319         487.6         496.3         505.0         513.7         522.4         53           46         32.8         0.205         2.27         5.26         0.302         487.6         496.3         505.0         513.7         522.4         53           45         31.2         0.194         2.15         5.38         0.286         487.7         496.4         505.1         513.8         522.5         53           44         29.6         0.183         2.04         5.49         0.271         487.8         496.5         505.2         513.9         522.6         53           49         69         69.0         0.704         7.76         0.00         1.000         483.8         492.4         501.1         509.7         518.3         52           6	2	512	5017	196.0	187 3	0.377	1.60	281	0.257	39.2	50	
48 36.0 0.230 2.54 4.99 0.337 487.5 496.2 504.9 513.6 522.3 53 47 34.4 0.217 2.40 5.13 0.319 487.6 496.3 505.0 513.7 522.4 53 46 32.8 0.205 2.27 5.26 0.302 487.6 496.3 505.0 513.7 522.4 53 45 31.2 0.194 2.15 5.38 0.286 487.7 496.4 505.1 513.8 522.5 53 44 29.6 0.183 2.04 5.49 0.271 487.8 496.5 505.2 513.9 522.6 53  69 69 69.0 0.704 7.76 0.00 1.000 483.8 492.4 501.1 509.7 518.3 52 68 67.4 0.668 7.37 0.39 0.950 484.0 492.6 501.3 509.9 518.5 52 67 65.8 0.634 7.00 0.76 0.902 484.2 492.8 501.5 510.1 518.7 52 66 64.2 0.601 6.63 1.13 0.854 484.4 493.0 501.7 510.3 518.9 52 65 62.6 0.570 6.29 1.47 0.810 484.6 493.2 501.9 510.5 519.1 52		1					1					
47       34.4       0.217       2.40       5.13       0.319       487.6       496.3       505.0       513.7       522.4       53         46       32.8       0.205       2.27       5.26       0.302       487.6       496.3       505.0       513.7       522.4       53         45       31.2       0.194       2.15       5.38       0.286       487.7       496.4       505.1       513.8       522.5       53         44       29.6       0.183       2.04       5.49       0.271       487.8       496.5       505.2       513.9       522.6       53         69       69       69.0       0.704       7.76       0.00       1.000       483.8       492.4       501.1       509.7       518.3       52         68       67.4       0.668       7.37       0.39       0.950       484.0       492.6       501.3       509.9       518.5       52         67       65.8       0.634       7.00       0.76       0.902       484.2       492.8       501.5       510.1       518.7       52         66       64.2       0.601       6.63       1.13       0.854       484.4       493.0       5		1					1		1	il		
69     69     69.0     0.704     7.76     0.00     1.000     483.8     492.4     501.1     509.7     518.3     522.6     53       69     69     69.0     0.704     7.76     0.00     1.000     483.8     492.4     501.1     509.7     518.3     52       68     67.4     0.668     7.37     0.39     0.950     484.0     492.6     501.3     509.9     518.5     52       66     64.2     0.601     6.63     1.13     0.854     484.4     493.0     501.7     510.3     519.1     52       65     62.6     0.570     6.29     1.47     0.810     484.6     493.2     501.9     510.5     519.1     52							1					
69     69     69.0     0.704     7.76     0.00     1.000     483.8     492.4     501.1     509.7     518.3     52       68     67.4     0.668     7.37     0.39     0.950     484.0     492.6     501.3     509.9     518.5     52       67     65.8     0.634     7.00     0.76     0.902     484.2     492.8     501.5     510.1     518.7     52       66     64.2     0.601     6.63     1.13     0.854     484.4     493.0     501.7     510.3     518.9     52       65     62.6     0.570     6.29     1.47     0.810     484.6     493.2     501.9     510.5     519.1     52	3.	513	505.0	196.3	487.6	0.302	5.26	2.27	0.205	32.8	46	
69 69 69.0 0.704 7.76 0.00 1.000 483.8 492.4 501.1 509.7 518.3 52° 68 67.4 0.668 7.37 0.39 0.950 484.0 492.6 501.3 509.9 518.5 52° 67 65.8 0.634 7.00 0.76 0.902 484.2 492.8 501.5 510.1 518.7 52° 66 64.2 0.601 6.63 1.13 0.854 484.4 493.0 501.7 510.3 518.9 52° 65 62.6 0.570 6.29 1.47 0.810 484.6 493.2 501.9 510.5 519.1 52°	3.	513		196.4	487.7		5.38	}				
68   67.4   0.668   7.37   0.39   0.950   484.0   492.6   501.3   509.9   518.5   52   67   65.8   0.634   7.00   0.76   0.902   484.2   492.8   501.5   510.1   518.7   52   66   64.2   0.601   6.63   1.13   0.854   484.4   493.0   501.7   510.3   518.9   52   65   62.6   0.570   6.29   1.47   0.810   484.6   493.2   501.9   510.5   519.1   52	3.	513	505.2	196.5	487.8	0.271	5.49	2.01	0.183	29.6	44	
67   65.8   0.634   7.00   0.76   0.902   484.2   492.8   501.5   510.1   518.7   52   66   64.2   0.601   6.63   1.13   0.854   484.4   493.0   501.7   510.3   518.9   52   65   62.6   0.570   6.29   1.47   0.810   484.6   493.2   501.9   510.5   519.1   52	9.	509	501.1	192.4	483.8	1.000	0.00	7.76		69.0	69	69
66 64.2 0.601 6.63 1.13 0.854 484.4 493.0 501.7 510.3 518.9 52' 65 62.6 0.570 6.29 1.47 0.810 484.6 493.2 501.9 510.5 519.1 52'									1	i i	1	
65 62.6 0.570 6.29 1.47 0.810 484.6 493.2 501.9 510.5 519.1 52							1			1.		
						1		{		II.		
04 01.0 0.311 3.37 1.73 0.703 454.5 433.4 502.1 310.7 519.3 520						1				11	1	
						1			1			
63 59.4 0.513 5.65 2.11 0.728 485.0 493.6 502.3 510.9 519.5 529		-						3		11		
62 57.8 0.486 5.37 2.39 0.693 485.1 493.7 502.4 511.0 519.6 529		1				1	1			II .	1	
61   56.2   0.461   5.09   2.67   0.657   485.1   493.7   502.6   511.2   519.8   526   60   54.6   0.437   4.82   2.94   0.621   485.2   493.9   502.7   511.3   519.9   526		1				1	1	1	7	II .		
60   54.6   0.437   4.82   2.94   0.621   485.2   493.9   502.7   511.3   519.9   526   59   53.0   0.414   4.57   3.19   0.589   485.4   494.1   502.8   511.5   520.1   526						1		1	1	11	1	
58 51.4 0.392 4.33 3.43 0.558 485.5 494.2 502.9 511.6 520.2 528						1			1	11	1	

	ding	Temp.	Force		ght apor Reqd.	Hu-		Weigh	t in Grain	ns of a Cu	bic Foot	of Air.	
mor	neter, anr.	of Dew-	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Ba	ometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.		of aCu- bic Ft. of Air.	1.000.	in. 28.0	in. 28.5	in. 29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	0 ==0	gr.	gr.	gr.	gr.	gr. 520.2	gr. 528.9	gr. 537.6
69	58 57	51.4 49.8	0.392	4.33	3.43	0.558	485.5	494.2	502.9 503.1	511.6 511.8	520.2	529.1	537.8
ì	56	48.2	0.351	3.87	3.89	0.499	485.8	494.5	503.1	511.9	520.5	529.2	537.9
	55	46.6	0.331	3.66	4.10	0.472	485.9	494.6	503.3	512.0	520.6	529.3	538.0
	54	45.0	0.315	3.47	4.29	0.447	486.0	494.7	503.4	512.1	520.7	529.4	528.1
	53	43.4	0.298	3.29	4.47	0.424	486.1	494.8	503.5	512.2	520.8	529.5	538.2
Ì	52	41.8	0.282	3.11	4.65	0.401	486.2	494.9	503.6	512.3	520.9	529.6	538.3
			0.200	201		0.000	100.0	107.0	~00 ~	F10.4	501.0	500 m	E90 4
	51	40.2	0.266	2.94	4.82	0.379	486.3	495.0	503.7	512.4	521.0	529.7 529.8	538.4 538.5
	50	38.6	0.252	$\begin{vmatrix} 2.78 \\ 2.63 \end{vmatrix}$	4.98 5.13	0.358	486.4	495.1 495.2	503.8 503.9	512.5 512.6	521.1	529.8	538.6
	49	37.0	0.238 $0.225$	2.49	5.13	0.339	486.6	495.3	504.0	512.6	521.2	530.0	538.7
	48	33.4	0.223	2.49	5.42	0.302	486.7	495.4	504.0	512.7	521.4	530.1	538.8
	46	32.2	0.213	2.34	5.56	0.302	486.8	495.5	504.1	512.9	521.5	530.2	538.9
	45	30.6	0.190	2.06	5.70	0.266	486.8	495.5	504.2	512.9	521.5	530.2	538.9
	10		0,100										
70	70	70.0	0.727	8.00	0.00	1.000	482.8	491.4	500.0	508.6	517.2	525.8	534.4
1	69	68.5	0.692	7.62	0.38	0.953	483.0	491.6	500.2	508.8	517.4	526.0	534.6
	68	67.0	0.659	7.26	0.74	0.907	483.2	491.8	500.4	509.0	517.6	526.2	534.8
	67	65.5	0.628	6.91	1.09	0.865	483.3	491.9	500.5	509.1	517.7	526.3	534.9
	66	64.0	0.597	6.57	1.43	0.822	483.5	492.1	500.7	509.3	517.9	526.5	535.1
	65	62.5	0.568	6.25	1.75	0.781	483.7	492.3	500.9	509.5	518.1	526.7	535.3
	64	61.0	0.541	5.95	2.05	0.744	483.8	492.4	501.0	509.6	518.3	526.9	535.5
	63	59.5	0.515	5.66	2.34	0.708	484.0	492.6	501.2	509.8	518.5	527.1	535.7
	62	58.0	0.489	5.38	2.62	0.672	484.2	492.8	501.4	510.0	518.7	527.3	535.9
	61	56.5	0.465	5.12	2.88	0.640	484.3	492.9	501.5	510.1	518.8	527.4	536.0
	60	55.0	0.442	4.87	3.13	0.609	484.4	493.0	501.6	510.2	518.9	527.5	536.1
	59	53.5	0.421	4.62	3.38	0.578	484.6	493.2	501.8	510.4	519.1	527.7	536.3
	58	52.0	0.400	4.40	3.60	0.550	484.7	493.3	501.9	510.5	519.2	527.8	536.4
	57	50.5	0.380	4.18	3.82	0.522	484.8	493.4	502.0	510.6	519.3	527.9	536.5
	56	49.0	0.361	3.96	4.04	0.495	484.9	493.5	502.1	510.7	519.4	528.0	536.6
1	55	47.5	0.343	3.76	4.24	0.470	485.1	493.7		510.9	519.6	528.2	536.8
	54	46.0	0.326	3.57	4.43	0.446	485.2		1	511.0	519.7		536.9
	53	44.5	0.309	3.40	4.60	0.425	485.3	493.9	502.5	511.1	519.8	528.4	537.0
	52	43.0	0.292	3.23	4.77	0.404	485.4			511.2	519.9		537.1
	51	41.5	0.279								1	1	537.2
	50	40.0	0.264	2.81	5.19	0.351	485.5	494.1	502.7	511.3	520.0	528.6	537.2
	49	38.5	0.251	2.76	5.24	0.345	485.6	494.2	502.8	511.4	520.1	528.7	537.3
	48	37.0		2.63				1	502.9	511.5	520.2	528.8	537.4
	47	35.5	0.226	2.50	5.50	0.313	485.8	494.4	503.0	511.6	520.3	528.9	537.5
1	46	34.0	0.214	2.37	5.63	0.296	485.8	494.4	503.0	1	1		
	45	32.5	0.203	2.24	5.76	0.280	485.9	494.5	1	511.7		1	1
	44	31.0								1			537.7
	43	29.5	0.182	2.01	5.99	0.251	486.1	494.7	503.3	511.9	520.6	529.2	537.8

of T	ding Ther- neter,	Temp.	Force of	of V	apor Reqd.	Hu- midity,			t in Grain				
	thr.	Dew- Point,	Vapor in	In a Cubic	for Sat'n.	Satura- tion =		Height	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCn- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	_ ^ ^ ^	gr.	gr.	gr.	gr.	gr.	gr	gr.
71	71	71.0	0.751	8.25	0.00	1.000	481.6	490.2	498.8	507.4	516.0	524.6	533.2
	70	69.5	0.715	7.86	0.39	0.953	481.8	490.4	499.0	507.6	516.2	524.8	533.4
	69	68.0	0.681	7.48	0.77	0.907	482.0	490.6	499 2	507.8	516.4	525.0	533.6
	68	66.5	0.648	7.13	1.12	0.865	482.2	490.8	499.4	508.0	516.6	525.2	533.8
	67	65.0	0.617	6.79	1.46	0.823	482.4	491.0	499.6	508.2	516.8	525.4	534.0
	66	63.5	0.588	6.45	1.80	0.782	482.6	491.2	499.8	508.4	517.0	525.6	534.2
	65	62.0	0.559	6.14	2.11	0.744	482.8	491.4	500.0	508.6	517.2	525.8	534.4
	64	60.5	0.532	5.85	2.40	0.709	483.0	491.6	500.2	508.8	517.4	526.0	534.6
	63	59.0	0.506	5.56	2.69	0.674	483.1	491.7	500.3	508.9	517.5	526.1	534.7
	62	57.5	0.481	5.28	2.97	0.640	483.2	491.8	500.4	509.0	517.7	526.3	534.9
	61	56.0	0.458	5.03	3.22	0.609	483.3	491.9	500.5	509.1	517.8	526.4	535.0
	60	54.5	0.435	4.78	3.47	0.579	483.5	492.1	500.7	509.3	518.0	526.6	535.1
	59	53.0	0.414	4.54	3.71	0.550	483.6	492.2	500.8	509.4	518.1	526.7	535.2
	58	51.5	0.393	4.31	3.94	0.522	483.8	492.4	501.0	509.6	518.3	526.9	535.4
	57	50.0	0.373	4.10	4.15	0.497	483.9	492.5	501.1	509.7	518.4	527.0	535.5
	56	48.5	0.355	3.89	4.36	0.471	484.0	492.6	501.2	509.9	518.5	527.1	535.6
	55	47.0	0.337	3.69	4.56	0.447	484.1	492.7	501.3	510.0	518.6	527.2	535.7
	54	45.5	0.320	3.51	4.74	0.425	484.2	492.8	501.4	510.1	518.7	527.3	535.8
	53	44.0	0.304	3.33	4.92	0.404	484.3	492.9	501.5	510.2	518.8	527.4	535.9
	52	42.5	0.288	3.16	5.09	0.383	484.4	493.0	501.6	510.3	518.9	527.5	536.0
	51	41.0	0.274	3.00	5.25	0.364	484.5	493.1	501.7	510.4	519.0	527.6	536.1
	50	39.5	0.260	2 85	5.40	0.345	484.6	493.2	501.S	510.5	519.1	527.7	536.2
	49	38.0	0.246	2.70	5.55	0.327	484.7	493.3	501.9	510.6	519.2	527.8	536.3
	48	36.5	0.234	2.57	5.68	0.312	484.7	493.3	501.9	510.6	519.2	527.8	536.3
	47	35.0	0.222	2.44	5.81	0.296	484.8	493.4	502.0	510.7	519.3	527.9	536.4
	46	33.5	0.210	2.31	5.94	0.280	484.9	493.5	502.1	510.8	519.4	528.0	536.5
	45	32.0	0.199	2.19	6.06	0.265	485.0	493.6	502.2	510.9	519.5	528.1	536.6
	44	30.5	0.189	2.08	6.17	0.252	485.0	493.6	502.2	510.9	519.5	528.1	536.6
			,										
72	72	72.0	0.776	8.50	0.00	1.000	480.6	489.2	497.8	506.4	514.9	523.5	532.1
	71	70.5	0.739	8.10	0.40	0.953	480.8	489.4	498.0	506.5	515.1	523.7	532.3
	70	69.0	0.704	7.71	0.79	0.907	481.0	489.6	498.2	506.7	515.3	523.9	532.5
	69	67.5	0.670	7.35	1.15	0.865	481.2	489.8	498.4	506.9	515.5	524.1	532.7
	68	66.0	0.638	7.00	1.50	0.824	481.4	490.0	498.5	507.1	515.7	524.3	532.9
	67	64.5	0.607	6.66	1.84	0.784	481.6	490.2	498.7	507.3	515.9	524.5	533.1
	66	63.0	0.578	6.33	2.17	0.745	481.7	490.3	498.8	507.4	516.1	524.7	533.3
	65	61.5	0,550	6.03	2.47	0.710	481.8	490.4	499.0	507.6	516.2	524.8	533.4
	64	60.0	0.523	5.73	2.77	0.674	482.0	490.6	499.2	507.8	516.4	525.0	533.6
	63	58.5	0.498	5.15	3.05	0.641	482.1	490.7	499.3	507.9	516.5	525.1	533.7
	62	57.0	0.473	5.18	3.32	0.610	482.3	490.9	499.5	508.I	516.7	525.3	533.9
	61	55.5	0.450	4.93	3.57	0.580	482.5	491.1	499.7	508.3	516.9	525.5	534.1
	60	54.0	0.428	4.68	3.82	0.551	482.6	491.2	499.8	508.4	517.0	525.6	534.2
	0.0												

В

	ading Ther-	Temp_	Force	of V	ight apor	Hu-		Weight	t in Grain	ns of a Cu	ibic Foot	of Air.	
mo	meter, ahr.	of Dew- Point,	of Vapor in		Reqd. for Sat'n.	midity, Satura- tion ==		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1 000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	52.5	in. 0.407	gr.	gr	0.523	gr.	gr.	gr. 500.0	gr. 508.6	gr. 517.2	gr. 525.8	gr. 534.4
72	59	1		4.45	4.05		482.8	491.4		508.7	517.2	525.9	534.5
	58	51.0	0.386	4.23	4.27	0.498	482.9	491.5	500.1 500.2	508.8	517.4	526.0	534.6
	57	49.5	0.367 $0.349$		4.48	0.449	483.0 483.1		500.2	508.9	517.5	526.1	534.7
	56	48.0		3.82		0.449	483.2	491.7	500.4	509.0	517.6	526.2	534.8
	55	46.5	0.331		4.87				500.4	509.1	517.7	526.2	534.9
	54 53	45.0 43.5	0.315 $0.299$	3.45	5.05	0.406	483.3 483.3	491.9 492.0	500.6	509.2	517.8	526.3	535.0
	0.5	19.0	0.200	0.20	0.22	0.000	100.0	40210	0000	000.2	01110	02010	
	52	42.0	0.283	3.11	5.39	0.366	483.5	492.1	500.7	509.3	517.9	526.4	535.1
	51	40.5	0.269	2.95	5.55	0.347	483.6	492.2	500.8	509.4	518.0	526.5	535.2
	50	39.0	0.255	2.80	5.70	0.329	483.7	492.3	500 9	509.5	518.1	526.6	535.5
	49	37.5	0.242	2.66	5.84	0.313	483.8	492.4	501.0	509.6	518.2	526.7	535.
	48	36.0	0.230	2.52	5.98	0.296	483.8	492.4	501.0	509.6	518.2	526.7	535.
	47	34.5	0.218	2.39	6.11	0.281	483.9	492.5	501.2	509.7	518.3	526.8	535.
	46	33.0	0.207	2.27	6.23	0.267	484.0	492.6	501.3	509.8	518.4	526.9	535.0
	45	31.5	0.196	2.16	6.34	0.254	484.1	492.7	501.3	509.9	518.5	527.1	535.
73	73	73.0	0.801	8.76	0.00	1.000	479.6	488.1	496.7	505.2	513.8	522.3	530.
	72	71.5	0.736	8.35	0.41	0.953	479.8	488.3	496.9	505.4	514.0	522.5	531.
	71	70.0	0.727	7.95	0.81	0.908	480.0	488.5	497.1	505.6	514.2	522.7	531.
	70	68.5	0.692	7.57	1.19	0.864	480.2	488.7	497.3	505.8	514.4	522.9	531.
	69	67.0	0.659	7.21	1.55	0.823	480.4	488.9	497.5	506.0	514.6	523.1	531.
	68	65.5	0.628	6.87	1.89	0.784	480.5	489.0	497.6	506.1	514.8	523.3	531.
	67	64.0	0.597	6.53	2.23	0.745	480.7	489.2	497.8	506.3	515.0	523.5	532.
	66	62.5	0.568	6.22	2.54	0.710	480.8	489.3	497.9	506.4	515.1	523.6	532.
	65	61.0	0.541	5.92	2.84	0.676	481.0	489.5	498.1	506.6	515.3	523.8	532.
	64	59.5	0.515	5.63	3.13	0.643	481.1	489.6	498.2	506.8	515.4	524.0	532.
	63	53.0	0.489	5.34	3.42	0.610	481.2	489.8	498.4	507.0	515.6	524.2	532.
	62	56.5	0.465	5.09	3.67	0.581	481.4	490.0	498.6	507.2	515.8	524.4	533.
	61	55.0	0.442	4.84	3.92	0.553	481.6	490.2	498.8	507.4	516.0	524.6	533.
	60	53.5	0.421	4.59	4.17	0.524	481.7	490.3	498.9	507.5	516.1	524.7	533.
	59	52.0	0.400	4.37	4.39	0.499	481.8	490.4	499.0	507.6	516.2	524.8	533.
	58	50.5	0.380	4.16	4.60	0.475	482.0	490.6	499.2	507.8	516.4	525.0	533.
	57	49.0	0.361	3.94	4.82	0.450	482.1	490.7	499.3	507.9	516.5	525.1	533.
	56	47.5	0.343	3.74	5.02	0.427	482.2	490.8	499.4	508.0	516.6	525.2	533.
	55	46.0	0.326	1	5.20	0.406	482.3	1	1	508.1	516.7	525.3	
	54	44.5	0.309	3.38	5.38	0.386	482.4	491.0	499.6	508.2	516.8	525.4	534.
	53	43.0	0.293	3.21	5.55	0.366	482.5	491.1	499.7	508.3	516.9	525.5	534.
	52	41.5	0.279			0.348	482.6			508.4	517.0	1	1
	51	40.0	0.261		1		1	1				1	
	50	38.5	0.251	2.74	6.02	0.313	482.8	491.4	500.0	508.6	517.2	525.8	
	49	37.0	0.238	i			452.9	491.5	500.0	508.6	517.2	525.8	
	48	35.5	0.226	2.47	6.29	0.282	483.0	491.6	500.1	508.7	517.3	525.9	534.
	47	34.0				0.267		491.7	500.2	508.8	I .	1	
	46	32.5	0.203	2.22	6.54	0.253	433.3	491.9	500.4	509.1	517.6	526.2	534.

of '	ading Ther-	Temp. of Of Or Or Or Or Or Or Or Or Or Or Or Or Or			Hu-	Weight in Grains of a Cubic Foot of Air.							
	neter, ahr.		Vapor in	Cubic	for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer i	n English	l Inches	
Dry.	Wet.	Fahr.	English Inches.	Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	3 1.0
74	74	74.0	in. 0.827	gr. 9.04	gr. 0.00	1.000	gr. 478.4	gr. 486.9	gr. 495.5	gr. 504.0	gr 512.6	gr. 521.1	gr. 529.7
1.1	73	72.5	0.787	8.60	0.44	0.951	478.6	487.1	495.7	504.2	512.8	521.1	529.9
	72	71.0	0.751	8.20	0.84	0.907	478.8	487.3	495 9	504.4	513.0	521.5	530.1
	71	69.5	0.715	7.81	1.23	0.864	479.0	487.5	496.1	504.6	513.2	521.7	530.3
	70	68.0	0.681	7.44	1.60	0.823	479.2	487.7	496.3	504.8	513.4	521.9	530.5
	69	66.5	0.648	7.08	1.96	0.783	479.4	487.9	496.5	505.0	513.6	522.1	530.7
	68	65.0	0.617	6.75	2.29	0.747	479.6	488.1	496.7	505.2	513.8	522.3	530.9
	67	63.5	0.588	6.41	2.63	0.709	479.8	488.3	496.9	505.4	514.0	522.5	531.1
	66	62.0	0.559	6.10	2.94	0.675	480.0	488.5	497.1	505.6	514.2	522.7	531.3
	65	60.5	0.532	5.81	3.23	0.643	480.1	488.7	497.3	505.9	514.4	522.9	531.5
	64	59.0	0.506	5.52	3.52	0.611	480.3	488.9	497.5	506.1	514.6	523.2	531.8
	63	57.5	0.481	5.24	3.50	0.580	480.5	489.1	497.7	506.3	514.8	523.4	532.0
	62	56.0	0.458	4.99	4.05	0.552	480.6	489.2	497.8	506.4	514.9	523.5	532.1
	61	54.5	0.435	4.75	4.29	0.525	480.7	489.3	497.9	506.5	515.0	523.6	532.2
	60	53.0	0.414	4.52	4.52	0.500	480.9	489.5	498.1	506.7	515.2	523.8	532.4
	59	51.5	0.393	4.29	4.75	0.475	481.0	489.6	498.2	506.8	515.3	523.9	532.5
	58	50.0	0.373	4.08	4.96	0.451	481.1	489.7	498.3	506.9	515.4	524.0	532.6
	57	48.5	0.355	3.86	5.18	0.427	481.2	489.8	498.4	507.0	515.5	524.1	532.7
	56	47.0	0.337 $0.320$	3.66 3.48	5.38	0.405	481.3	489.9	498.5	507.1	515.6	524.2	532.8
	55 54	45.5 44.0	0.320 $0.304$	3.32	5.56 5.72	0.385 $0.367$	481.4 481.5	490.0	498.6	507.2 507.3	515.7 515.8	524.3 524.4	532.9
	0.1	11.0	0.001	0.02	0112	0.001	401.0	100.1	430.1	301.0	010.0	924.4	000.0
	53	42.5	0.288	3.15	5.89	0.348	481.6	490.2	498.8	507.4	515.9	524.5	533.1
	52	41.0	0.274	2.99	6.05	0.331	481.7	490.3	498.9	507.5	516.0	524.6	533.2
	51	39.5	0.260	2.83	6.21	0.313	481.8	490.4	499.0	507.6	516.1	524.7	533.3
	50	38.0	0.246	2.69	6.35	0.298	481.9	490.5	499.1	507.7	516.2	524.8	533.4
	49 48	36.5 35.0	$0.234 \\ 0.222$	2.55	6.49 6.62	0.282 0.268	481.9 482.0	490.5	499.1	507.7 507.8	516.2 516.3	524.8 524.9	533.4 533.5
	47	33.5	0.210	2.30	6.74	0.254	482.1	490.7	499.2	507.9	516.4	525.0	533.6
	71	00.0	0.210	2.00	0114	0.204	40241	45001	400.2	307.3	510.4	525.0	000.0
75	75	75.0	0.854	9.31	0.00	1.000	477.4	485.9	494.4	502.9	511.5	520.0	528.5
	74	73.5	0.814	8.87	0.44	0.953	477.6	486.1	494.6	503.1	511.7	520.2	528.7
	73	72.0	0.776	8.45	0.86	0.908	477.8	486.3	494.8	503.3	511.9	520.4	528.9
	72	70.5	0.739	8.05	1.26	0.865	478.0	486.5	495.0	503.5	512.1	520.6	529.1
	71	69.0	0.704	7.67	1.64	0.824	478.2	486.7	495.2	503.7	512.3	520.8	529.3
	70	67.5	0.670	7.30	2.01	0.784	478.3	486.8	495.3	503.8	512.5	521.0	529.5
	69	66.0	0.638	6.95	2.36	0.746	478.5	487.0	495.5	504.0	512.7	521.2	529.7
	68	64.5	0.607	6.62	2.69	0.711	478.7	487.2	495.7	504.2	512.9	521.4	529.9
	67	63.0	0.578	6.30	3.01	0.677	478.9	487.4	495.9	504.4	513.1	521.6	530.1
	66	61.5	0.550	5.99	3.32	0.643	479.1	487.6	496.1	504.6	513.3	521.8	530.3
	65 64	60.0	0.523	5.69	3.62	0.611	479.3	487.8	496.4	504.9	513.5	522.0	530.6
	63	58.5 57.0	0.498	5.42 5.15	3.89 4.16	0.582 0.553	479.5 479.6	488.0 488.1	496.6 496.7	505.1 505.2	513.7 513.8	522.2 522.3	530.8 530.9
	62	55.5	0.450	4.90	4.41	0.526		484.2		505.3			531.0

of	Reading of Ther- nometer, of control of Vapor  Fahr Read.  Reading of Vapor  Force of Vapor  In a for		apor	Hu- midity,	Weight in Grains of a Cubic Foot of Air.								
	ahr.	Dew-		In a Cubic		Satura-		Height o	f the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.		of aCu- bic Ft. of Air.	tion = 1.000.	28.0	in. 28.5	29.0	29.5	30.0	in. 30.5	<sup>іп.</sup>
0	0	0	in.	gr.	gr.		gr.	gr.	gr.	gr.	gr.	gr.	gr.
75	62	55.5	0.450	4.90	4.41	0.526	479.7	488.2	496.8	505.3	513.9	522.4	531.0
	61	54.0	0.428	4.66	4.65	0.501	479.9	488.4	497.0	505.5	514.1	522.6	531.2
	60	52.5	0.407	4.43	4.88	0.476	480.0	488.5	497.1	505.6	514.2	522.7	531.3
	59	51.0	0.386	4.21	5.10	0.452	480.1	488.6	497.2	505.7	514.3	522.8	531.4
	58	49.5	0.367	4.00	5.31	0.429	480.3	488.8	497.4	505.9	514.5	523.0	531.6
	57	48.0	0.349	3.79	5.52	0.407	480.4	488.9	497.5	506.0	514.6	523.1	531.7
	56	46.5	0.331	3.60	5.71	0.387	480.5	489.0	497.6	506.1	514.7	523.2	531.8
	55	45.0	0.315	3.42	5.89	0.367	480.6	489.1	497.7	506.2	514.8	523.3	531.9
	54	43.5	0.299	3.25	6.06	0.349	480.7	489.2	497.8	506.3	514.9	523.4	532.0
	53	42.0	0.289	3.09	6.22	0.332	480.7	489.3	497.9	506.4	515.0	523.5	532.0
	52	40.5	0.269	2.93	6.38	0.315	480.8	489.3	497.9	506.4	515.0	523.5	532.1
	51	39.0	0.255	2.78	6.53	0.299	480.9	489.4	497.9	506.5	515.1	523.6	532.1
	50	37.5	0.233	2.64	6.67	0.284	481.0	489.5	498.1	506.6	515.1	523.7	532.3
	49	36.0	0.242	2.51	6.80	0.270	481.1	489.6	498.1	506.7	515.2	523.8	532.4
	48	34.5	0.230	2.39	6.92	0.257	481.2	489.7	498.3	506.8	515.4	523.9	532.5
	40	94.9	0.210	2.03	0.52	0.257	401.2	403.1	490.0	300.0	010.4	920.0	002.0
											1		
76	76	76.0	0.882	9.60	0.00	1.000	476.3	484.8	493.3	501.8	510.3	518.8	527.3
10	75	74.5	0.840	9.14	0.46	0.952	476.6	485.1	493.6	502.1	510.6	519.1	527.6
	74	73.0	0.801	8.71	0.89	0.907	476.8	485.3	493.8	502.3	510.8	519.3	527.8
	73	71.5	0.763	8.30	1.30	0.865	477.0	485.5	494.0	502.6	511.1	519.6	528.1
	72	70.0	0.727	7.90	1.70	0.823	477.2	485.7	494.3	502.8	511.3	519.8	528.3
	71	68.5	0.692	7.53	2.07	0.784	477.4	485.9	494.5	503.0	511.5	520.0	528.5
	70	67.0	0.659	7.17	2.43	0.747	477.6	486.1	494.7	503.2	511.7	520.2	528.7
	**	"""	0.000			01121	11110	10012	10 111	000.2		0 - 0 - 0	
	69	65.5	0.628	6.83	2.77	0.711	477.8	486.3	494.9	503.4	511.9	520.4	528.9
	68	64.0	0.597	6.49	3.11	0.676	477.9	486.4	495.0	503.6	512.1	520.6	529.2
	67	62.5	0.568	6.16	3.44	0.642	478.1	486.6	465.2	503.8	512.3	520.8	529.4
	66	61.0	0.541	5.88	3.72	0.613	478.2	486.7	495.3	503.9	512.4	520.9	529.5
	65	59.5	0.515	5.59	4.01	0.582	478.3	486.8	495.4	504.0	512.5	521.0	529.6
	64	58.0	0.489	5.31	4.29	0.553	478.5	487.0	495.6	504.2	512.7	521.2	529.8
	63	56.5	0.465	5.06	4.54	0.527	478.6	487.1	495.7	504.3	512.8	521.3	529.9
	62		0.112		1	0.505	1000	100	107.5		F10.0	F02 =	F00.
	62	55.0	0.442	4.81	4.79	0.501	478.8	487.3	495.9	504.5	513.0	521.5	530.1
	61	53.5	0.421	4.57	5.03	0.476	479.0	487.5	496.1	504.7	513.2	521.7	530.5
	60	52.0	0.400	4.34	5.26	0.452	479.1	487.6	496.2	504.8	513.3	521.8	530.
	59	50.5	0.380	4.13	5.47	0.430	499.2	487.7	496.3	504.9	513.4	521.9	530.5
	58	49.0	0.361	3.92	5.68	0.408	499.3	487.8	496.4	505.0	513.5	522.0	530.6
	57	47.5	0.343	3.73	5.87		499.4			505.1	513.6	1	0001
	56	46.0	0.326	3.54	6.06	0.369	499.5	488.0	496.6	505.2	513.7	522.2	530.8
	55	44.5	0.309	3.36	6.24	0.351	499.6	488.1	496.7	505.3	513.8	522.3	530.9
	54	43.0	0.293	3.19	1	0.332	499.7		1	505.4		1	
1	53	41.5	0.279	3.03		0.316	499.8	488.3	496.9	505.5	514.0	522.5	531.1
	52	40.0	0.264	2.88		0.301	499.9		497.0	505.6		522.6	531.2
	51	38.5	0.251	2.73		0.384	500.0	1					531.
	50	37.0	0.238	2.59		0.269	500.1	488.6	1	505.8	1	1	531.
	49	35.5	0.236		1		1	1	497.3			1	

	ding	Temp.	Force		ight apor	Hn-		Weight	in Grain	ns of a Cr	ıbic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n	midity, Satura- tion =		Height o	of the Bar	rometer i	n Englis	n Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	in. 29.5	30.0	in. 30.5	31.0
0	0	0	in.	gr.	gr. 0.00	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
77	77	77.0 75.5	$0.910 \\ 0.868$	9.89 9.42	0.47	1.000 0.953	475.3 475.5	483.8 484.0	492.3	500.8	509.2 509.4	517 7 517.9	526.2 526.4
	75	74.0	0.827	8.99	0.90	0.909	475.7	484.2	492.7	501.2	509.6	518.1	526.6
	74	72.5	0.787	8.57	1.32	0.867	475.9	484.4	492.9	501.4	509.9	518.4	526 9
	73	71.0	0.751	8.15	1.74	0.824	176.1	484.6	493.1	501.6	510.1	518.6	527.1
	72	69.5	0.715	7.77	2.12	0.786	476.3	484.8	493.3	501.8	510.3	518.8	527.3
	71	68.0	0.681	7.40	2.49	0.748	476.5	485.0	493.5	502.0	510.5	519.0	527.5
	70	66.5	0.648	7.04	2.85	0.712	476.7	485.2	493.7	502.2	510.7	519.2	527.7
	69	65.0	0.617	6.71	3.18	0.678	476.9	485.4	493.9	502.4	510.9	519.4	527.9
	68	63.5	0.588	6.37	3.52	0.641	477.0	485.6	494.1	502.6	511.1	519.6	528.1
	67	62.0	0.559	6.06	3.83	0.613	477.2	485.8	494.3	502.8	511.3	519.8	528.3
	66	60.5	0.532	5.77	4.12	0.583	477.4	486.0	494.5	503.0	511.5	520.0	528.5
	65	59.0	0.506	5.49	4.40	0.556	477.5	486.1	494.6	503.1	511.6	520.1	528.6
	64	57.5	0.481	5.21	4.68	0.527	477.7	486.3	494.8	503.3	511.8	520.3	528.8
	63	56.0	0.458	4.96	4.93	0.501	477.9	486.5	495.0	503.5	512.0	520.5	529.0
	62	54.5	0.435	4.70	5.19	0.476	478.0	486.6	495.1	503.7	512.1	520.6	529.1
	61	53.0	0.414	4.49	5.40	0.454	478.0	486.6	495.1	503.7	512.2	520.7	529.3
	60	51.5	0.393	4.26	5.63	0.431	478.1	486.7	495.2	503.8	512.3	520.8	529.4
	59	50.0	0.373	4.05	5.84	0.410	478.2	486.8	495.3	503.9	512.4	520.9	529.5
	58	48.5	0.355	3.85	6.04	0.389	478.3	486.9	495.4	504.0	512.5	521.0	529.6
	57	47.0	0.337	3.65	6.24	0.369	478.5	487.1	495.6	504.1	512.7	521.2	529.8
	56	45.5	0.320	3.47	6.42	0.351	478.6	487.2	495.7	504.2	512.8	521.3	529.9
	55	44.0	0.304	3.29	6.60	0.333	478.7	487.3	495.8	504.3	512.9	521.4	530.0
	54	42.5	0.288	3.13	6.76	0.317	478.8	487.4	495.9	504.4	513.0	521.5	530.1
	53	41.0	0.274	2.97	6.92	0.301	478.9	487.5	496.0	504.5	513.1	521.6	530.2
	52	39.5	0.260	2.82	7.07	0.235	479.0	487.6	496.1	504.6	513.2	521.7	530.3
	51	38.0	0.246	2.67	7.22	0.270	479.1	457.7	496.2	504.7	513.3	521.8	530.4
	50	36.5	0.234	2.53	7.36	0.256	479.1	487.7	496.2	504.7	513.3	521.8	530.4
78	78	78.0	0.940	10.19	0.00	1.000	474.1	482.5	491.0	499.4	508.0	516.4	524.9
,,,	77	76.5	0.896	9.72	0.47	0.954	474.4	482.9	491.4	499.9	508.3	516.7	525.2
	76	75.0	0.854	9.25	0.94	0.908	474.7	483.2	491.6	500.1	508.6	517.1	525.6
	75	73.5	0.814	8.82	1.37	0.865	474.9	483.4	491.8	500.3	508.8	517.3	525.8
	74	72.0	0.776	8.40	1.79	0.824	475.2	483.7	492.1	500.6	509.1	517.6	526.1
	73	70.5	0.739	8.00	2.19	0.785	475.4	483.9	492.3	500.8	500.3	517.8	526.3
	72	69.0	0.704	7.62	2.57	0.748	475.6	484.1	492.5	501.0	509.5	518.0	526.5
	71	67.5	0.670	7.25	2.94	0.711	475.8	484.3	492.7	501.2	509.7	518.2	526.7
	70	66.0	0.638	6.91		0.678	475.9	484.4	492.9	501.4	509.9	518.4	526.9
	69	64.5	0.607	6.58	,	0.646	476.1	484.6	493.1	501.6	510.1	518.6	527.1
	68	63.0	0.578	6.26		0.614	476.3	484.8	493.3	501.S	510.3	518.S	527.3
	67	61.5	0.550	5.96	4.23	0.585	476.4	484.9	493.4	501.9	510.4	518.9	527.4
	66	60.0	0.523	5.66	4.53	0.555	476.6	485.1	493.6	502.1	510.6	519.1	527.6
	65	58.5	0.498	5.38	4.81	0.528	476.8	485.3	493.8	502.3	510.8	519.3	527.8

Rea of '	ding	Temp. of Vapor Reqd.		Hu-	Weight in Grains of a Cubic Foot of Air.								
mon	neter,	Dew-	Vapor in	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Bar	ometer in	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of		tion = 1.000.	in. 28.0	in. 28.5	29.0	in. 29.5	30.0	in. 30.5	31.0
0	0	0 5	in.	gr. 5.38	gr. 4.81	0.528	gr.	gr.	gr.	gr.	gr. 510.8	gr. 519.3	gr. 527.8
78	64	58.5 57.0	0.498 $0.473$	5.12	5.07	0.502	476.8 476.8	485.3	493.8 493.9	502.3 502.4	510.9	519.4	527.9
	63	55.5	0.450	4.88	5.31	0.479	476.9	485.4	494.0	502.5	511.0	519.5	528.0
	62	54.0	0.428	4.63		0.454	477.1	485.6	494.2	502.7	511.2	519.7	528.2
	61	52.5	0.407	4.40	5.79	0.432	477.2	485.7	494.3	502.8	511.3	519.8	528.3
	60	51.0	0.386	4.18	6.01	0.409	477.3	485.8	494.4	502.9	511.4	519.9	528.4
	59	49.5	0.367	3.98	6.21	0.391	477.4	485.9	494.5	503.0	511.5	520.0	528.5
	58	48.0	0.349	3.78	6.41	0.371	477.5	486.0	494.6	503.1	511.6	520.1	528.6
	57	46.5	0.331	3.59	6.60	0.352	477.6	486.1	494.7	503.2	511.7	520.2	528.7
	56	45.0	0.315	3.41	6.78	0.335	477.8	486.3	494.8	503.3	511.9	520.4	528.9
	55	43.5	0.299	3.24	6.95	0.318	477.9	486.4	494.9	503.4	512.0	520.5	529.0
	54	42.0	0.283	3.07	7.12	0.301	478.0	486.5	495.0	503.5	512.1	520.6	529.1
	53	40.5	0.269	2.92	7.27	0.287	478.1	486.5	495.0	503.5	512.1	520.6	529.1
	52	39.0	0.255	2.77	7.42	0.272	478.2	486.6	495.1	503.6	512.2	520.7	529.2
	51	37.5	0.242	2.63	7.56	0.258	478.3	486.7	495.2	503.7	512.3	520.8	529.3
	79	79.0	0.970	10.50	0.00	1.000	400 1	101 5	400.0	100 1	506.9	E15 9	523.8
79	78	77.5	0.925	10.01		0.953	473.1	481.5	490.0	498.4	507.2	515.3	524.1
	77	76.0	0.525	9.54	1	0.909	473.7	482.1	490.6	499.0	507.5	515.9	524.4
	76	74.5	0.840	9.10	1	0.867	473.8	482.2	490.7	499.2	507.7	516.2	524.7
	75	73.0	0.801	8.66		0.825	474.0	482.4	490.9	499.4	507.9	516.4	524.9
	74	71.5	0.763	8.25		0.786	474.3	482.7	491.2	499.7	508.2	516.7	525.2
	73	70.0	0.727	7.86	1	0.749	474.5	482.9	491.4	499.9	508.4	516.9	525.4
	72	68.5	0.692	7.48	3.02	0.712	474.7	483.1	491.6	500.1	508.6	517.1	525.6
	71	67.0	0.659	7.12	3.38	0.678	474.9	483.4	491.9	500.4	508.8	517.3	525.8
	70	65.5	0.628	6.79	3.71	0.647	475.1	483.6	462.1	500.6	509.0	517.5	526.0
}	69	64.0	0.597	6.45	4.05	0.614	475.3	483.8	492.3	500.8	509.2	517.7	526.2
	68	62.5	0.568	6.14	4.36	0.585	475.4	483.9	492.4	500.9	509.3	517.8	526.3
	66	61.0	0.541	5.84 5.55		0.556	475.6 475.7	484.1	492.6	501.1	509.5	518.0	526.5 526.6
	65	58.0	0.489	5.28		0.503	475.8	484.3	492.8	501.3	509.8	518.3	526.8
	64	56.5	0.465	5.02		0.478	476.0	484.5	493.0	501.5	510.0	518.5	527.0
	63	55.0	0.442	4.78	1	0.455	476.1	484.6		501.6	510.1	518.6	527.1
	62	53.5	0.421	4.54	1	0.432	476.3	484.8	493.3	501.8	510.3	518.8	527.3
	61	52.0	0.400	4.31		0.410	476.4	484.9	1	501.9	510.4	518.9	527.4
1	60	50.5	0.380	4.10	6.40	0.390	476.5	485.0	493.5	502.0	510.5	519.0	527.5
	59	49.0	0.361	3.90	6.60	0.371	476.6	485.1	493.6	502.1	510.6	519.1	527.6
	58	47.5	0.343	3.71	6.79	0.353	476.7	485.2	493.7	502.2	510.7	519.2	527.7
	57	46.0	0.326	3.52	6.98	0.335	476.8	1		502.3	510.8	519.3	527.8
	56	44.5	0.309	3.3	7.16	0.318	476.9	485.4		502.4	510.9	519.4	527.9
	55	43.0	0.293	3.17	7.33	0.301	477.0	485.5	494.0	502.5	511.0	519.5	528.0
	54	41.5	0.279	3.01	7.49	0.287	477.1	485.6	494.1	502.6	511.1	519.6	528.1
	53	40.0	0.264				477.2	§	494.2	4	511.2	519.7	528.2
	52	3S.5	0.251	2.72	2 7.78	0.260	477.3	485.8	494.3	502.8	511.3	519.8	528.3

	iding Ther-	Temp.	Force		ght apor	Hu-		Weight	in Grain	ıs of a Cu	ibic Foot	of Air.	
	neter,	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion ==		Height o	of the Ba	rometer i	n Englis	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	80.0	in. 1.001	gr. 10.81	gr. 0.00	1 000	gr.	gr. 480.4	gr.	gr.	gr.	gr.	gr
80	80 79	78.5	0.955	10.31	0.50	1.000 0.954	472.0 472.3	480.7	488.9	497.3	505.7	514.1	522.6 522.9
	78	77.0	0.910	9.83	0.98	0.909	472.5	480.9	489.4	497.9	506.3	514.7	523.2
	77	75.5	0.868	9.37	1.44	0.867	472.7	481.1	489.6	498.1	506.5	514.9	523.4
	76	74.0	0.827	8.93	1.88	0.826	473.0	481.4	489.9	498.4	506.8	515.2	523.7
	75	72.5	0.787	8.50	2.31	0.786	473.2	481.6	490.1	498.6	507.0	515.4	523.9
	74	71.0	0.751	8.11	2.70	0.750	473.4	481.8	490.3	498.8	507.2	515.6	524.1
	73	69.5	0.715	7.71	3.10	0.713	473.6	482.1	490.6	499.1	507.5	515.9	524.4
	72	68.0	0.681	7.35	3.46	0.680	473.8	482.3	490.8	499.3	507.7	516.1	524.6
	71	66.5	0.648	6.99	3.82	0.647	474.0	482.5	491.0	499.5	507.9	516.3	524.8
	70	65.0	0.617	6.66	4.15	0.616	474.2	482.7	491.2	499.7	508.1	516.5	525.0
	69	63.5	0.588	6.33	4.48	0.586	474.4	482.9	491.4	499.9	508.3	516.7	525.2
	68	62.0	0.559	6.03	4.78	0.558	474.5	483.0 483.2	491.5	500.0	508.4	516.8	525.3 525.5
	67	60.5	0.532	5.74	5.07	0.531	474.7	455.2	491.7	500.2	508.6	517.0	929.9
	66	59.0	0.506	5.45	5.36	0.504	474.9	483.4	491.9	500.4	508.8	517.2	525.7
]	65	57.5	0.481	5.18	5.63	0.479	475.0	483.5	492.0	500.5	508.9	517.3	525.8
	64	56.0	0.458	4.93	5.96	0.456	475.2	483.7	492.2	500.7	509.1	517.5	526.0
	63	54.5	0.435	4.69	6.12	0.434	475.3	483.8	492.3	500.8	509.2	517.6	526.1
	62	53.0	0.414	4.46	6.35	0.413	475.4	483.9	492.4	500.9	509.3	517.7	526.2
	61	51.5	0.393	4.23	6.58	0.391	475.5	484.0	492.5	501.0	509.4	517.8	526.3
	60	50.0	0.373	4.02	6.79	0.372	475.6	484.1	492.6	501.1	509.5	517.9	526.4
	59	48.5	0.355	3.82	6.99	0.353	475.7	484.2	492.7	501.2	509.6	518.0	526.5
	58	47.0	0.337	3.63	7.18	0.336	475.9	484.4	492.9	501.4	509.8	518.2	526.7
ł	57	45.5	0.320	3.45	7.36	0.319	476.0	484.5	493.1	501.5	509.9	518.3	526.8
	56	44.0	0.304	3.27	7.54	0.302	476.1	484.6	493.2	501.6	510.0	518.4	526.9
	55	42.5	0.288	3.11	7.70	0.288	476.2	484.7	493.3	501.7	510.1	518.5	527.0
	54	41.0	0.274	2.96	7.85	0.274	476.3	484.8	493.4	501.8	510.2	518.6	527.1
	53	39.5	0.260	2.82	7.99	0.261	476.3	484.8	493.4	501.8	510.2	518.6	527.1
81	81	81.0	1.034	11.14	0.00	1.000	471.0	479.4	487.8	496.2	504.6	513.0	521.4
	80	79.5	0.986	10.62	0.52	0.953	471.3	479.7	488.1	496.5	504.9	513.3	521.7
	79	78.0	0.940	10.13	1.01	0.910	471.5	479.9	488.4	496.8	505.2	513.6	522.1
	78	76.5	0.896	9.65	1.49	0.866	471.7	480.1	488.6	497.0	505.4	513.8	522.3
	77	75.0	0.854	9.20	1.94	0.826	472.0	480.4	488.9	497.3	505.7	514.1	522.6
	76	73.5	0.814	8.77	i e	0.787	472.2	480.6	489.1	497.5	1	514.3	522.8
	75	72.0	0.776	8.35	2.79	0.750	472.5	480.9	489.4	497.8	506.2	514.6	523.1
	74	70.5	0.739	7.95	3.19	0.713	472.6	481.0	489.5	497.9	506.4	514.8	523.3
	73	69.0	0.704	7.57	3.57	0.680	472.8	481.2	489.7	498.1	506.6 506.8	515.0 515.2	523.5 523.7
	72 71	66.0	0.670 0.638	7.21 6.87	3.93 4.27	0.617	473.0 473.2	481.4 481.6	490.1	498.3	507.0	515.4	523.9
	70	64.5	0.635	6.54	4.60	0.517	473.2	481.8	490.1	498.7	507.0	515.6	524.1
	69	63.0	0.578	6.22	4.92	0.558	473.6	482.0	490.5	498.9	507.4	515.8	524.3
	68	61.5	0.550		5.22	0.531	473.7	482.2	490.7	499.1	507.6		524.5
	1 00	01.9	0.990	5.92	9.52	0.051	410.1	402.2	450.7	455.1	1 201.0	0.0.0	024.0

of '	ading Ther-	Temp.	Force	Wei of V	apor	Hu-		Weight	in Grain	ns of a Cu	bic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	68	61.5	in. 0.550	gr. 5.92	gr. 5.22	0.531	gr.	gr.	gr.	gr.	gr. 507.6	gr. 516.0	gr. 524.5
81	67	60.0	0.523	5.62	5.52	0.505	473.7	482.2 482.3	490.7 490.8	499.1	507.7	516.1	524.6
	66	58.5	0.498	5.31	5.83	0.477	474.0	482.5	491.0	499.4	507.9	516.3	524.8
	65	57.0	0.473	5.08	6.06	0.456	474.1	482.6	491.1	499.5	508.0	516.4	524.9
	64	55.5	0.450	4.84	6.30	0.434	474.3	482.8	491.3	499.7	508.2	516.6	525.1
	63	54.0	0.428	4.60	6.54	0.413	474.4	482.9	491.4	499.8	508.3	516.7	525.2
	62	52.5	0.407	4.37	6.77	0.392	474.5	483.0	491.5	499.9	508.4	516.8	525.3
	61	51.0	0.300	4 15	6 00	0.979	457.4.C	409.1	401.6	500.0	E00 E	5100	505.4
	61 60	51.0 49.5	0.386 $0.367$	4.15 3.95	6.99 7.19	0.373	474.6	483.1	491.6	500.0	508.5 508.6	516.9 517.0	525.4 525.5
	59	48.0	0.349	3.75	7.19	0.337	474.7	483.4	491.7	500.1	508.8	517.0	525.7
	58	46.5	0.331	3.56		0.320	475.0	483.5	492.0	500.4	508.9	517.3	525.8
	57	45.0	0.315	3.38	7.76	0.303	475.1	483.6	492.1	500.5	509.0	517.4	525.9
	56	43.5	0.299	3.21	7.93	0.289	475.2	483.7	492.2	500.6	509.1	517.5	526.0
	55	42.0	0.283	3.05	8.09	0.274	475.3	483.8	492.3	500.7	509.2	517.6	526.1
	54	40.5	0.269	2.90	8.24	0.260	475.3	483.8	492.3	500.7	509.2	517.6	526.1
82	82	82.0	1.067	11.47		1.000	470.0	478.4	486.8	495.2	503.5	511.9	520.3
	81	80.5	1.017	10.94	0.53	0.954	470.3	478.7	487.0	495.4	503.8	512.2	520.6
	80	79.0	0.970	10.44	1	0.910	470.6	479.0	487.3	495.7	504.1	512.5	520.9
	79	77.5	0.925	9.95		0.868	470.7	479.1	487.5	495.9	504.3	512.7	521.1
	78	76.0	0.882	9.49		0.827	471.0	479.4	487.8	496.2	504.6	513.0	521.4
	77	74.5	0.840	9.03 8.60		0.787	471.2	479.6 479.9	488.0	496.4	504.8	513.2	521.6 521.9
	10	10.0	0.501	3.00	2.01	0.150	471.5	413.3	400.0	450.7	303.1	313.3	321.3
	75	71.5	0.763	8.19	3.28	0.714	471.6	480.0	488.5	496.9	505.3	513.7	522.1
	74	70.0	0.727	7.81	3.66	0.681	471.8	480.2	488.6	497.1	505.5	513.9	522.4
	73	68.5	0.692	7.43	4.04	0.648	472.0	480.4	488.8	497.3	505.7	514.1	522.6
1	72	67.0	0.659	7.08	4.39	0.618	472.2	480.6	489.0	497.5	505.9	514.3	522.8
	71	65.5	0.628	6.75	1	0.588	472.4	480.8	489.2	497.7	506.1	514.5	523.0
	70	64.0	0.597	6.41		0.559	472.5	480.8	489.4	497.9	506.3	514.7	523.2
	69	62.5	0.568	6.10	5.37	0.532	472.6	481.0	489.5	498.0	506.4	514.8	523.3
	68	61.0	0.541	5.81	5.66	0.507	472.8	481.2	489.7	498.2	506.6	515.0	523.5
	67	59.5	0.515	5.52	1	0.481	473.0	481.4	489.9	498.4	506.8	515.2	523.7
	66	58.0	0.489	5.25	1	0.458	473.1	481.5	490.0	498.5	506.9	515.3	523.8
	65	56.5	0.465	4.99		0.435	473.2	481.6	490.1	498.6	507.0	515.4	523.9
	64	55.0	0.442	4.75	6.72	0.414	473.4	481.8	490.3	498.8	507.2	515.6	524.1
	63	53.5	0.421	4.51	6.96	0.393	473.5	482.0	490.5	499.0	507.4	515.8	524.3
	62	52.0	0.400	4.29	7.18	0.374	473.6	482.1	490.6	499.1	507.5	515.9	524.4
	0.1	-0-	0.000		F 00	0.050	400.00	400.0	400 =	100.0	F0= 0	F70.0	504
	61	50.5	0.380		7.39	0.356	473.7		490.7	499.2	507.6		
	60	49.0	0.361	1	7.60		473.8	1	1	1	1		1
1	59 58	47.5	0.343	1	7.79	0.320	473.9 474.0	1		499.4	507.8 507.9	516.2 516.3	
	57	44.5	0.309		8.15	0.303	474.0	1	1	1	508.0	1	524.8
	56	43.0	0.303		8.32	0.233	474.2		1	499.7	508.1	516.5	524.9
	55	41.5	0.279		8.48			482.8			508.2	1	525.1
		11 -2-5	1	1 3.00	, 5.15	1 0.200	1	1 .02.0	,	1 2000	, 000.2	1 0 2 0 1 0	

	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weight	in Grain	ıs of a Cu	ıbic Foot	of Air.	
moi	meter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	3 <sup>in.</sup>
0	0	83.0	in. 1,101	gr. 11.82	gr. 0.00	1.000	gr. 468.8	gr. 477.2	gr.	gr.	gr.	gr.	gr. 519.0
83	83 82	81.5	1.050	11.27	0.55	0.953	469.1	477.5	485.5 485.8	493.9 494.2	502.3	510.6 511.0	519.4
	81	80.0	1.001	10.75	1.07	0.909	469.4	477.8	486.1	494.5	502.9	511.3	519.7
	80	78.5	0.955	10.25	1.57	0.868	469.7	478.1	486.4	494.8	503.2	511.6	520.0
	79	77.0	0.910	9.78	2.04	0.828	470.0	478.4	486.7	495.1	503.5	511.9	520.3
	78	75.5	0.868	9.31	2.51	0.786	470.3	478.7	487.0	495.4	503.8	512.2	520.6
	77	74.0	0.827	8.88	2.94	0.751	470.5	478.9	487.2	495.6	504.0	512.4	520.8
	76	72.5	0.787	8.45	3.37	0.715	470.6	479.0	487.4	495.8	504.2	512.6	521.0
	75	71.0	0.751	8.05	3.77	0.681	470.8	479.2	487.6	496.0	504.4	512.8	521.2
	74	69.5	0.715	7.66	4.16	0.647	471.0	479.4	487.8	496.2	504.6	513.0	521.4
	73	68.0	0.681	7.30	4.52	0.618	471.2	479.6	488.0	496.4	504.8	513.2	521.6
	72	66.5	0.648	6.95	4.87	0.588	471.4	479.8	488.2	496.6	505.0	513.4	521.8
	71	65.0	0.617	6.62	5.20	0.560	471.6	480.0	488.4	496.8	505.2	513.6	522.0
	70	63.5	0.588	6.29	5.53	0.533	471.7	480.1	488.5	497.0	505.4	513.8	522.3
	69	62.0	0.559	5.99	5.83	0.507	471.9	480.3	488.7	497.2	505.6	514.0	522.5
	68	60.5	0.532	5.70	6.12	0.482	472.0	480.4	488.8	497.3	505.7	514.1	522.6
	67	59.0	0.506	5.42	6.40	0.459	472.2	480.6	489.0	497.5	505.9	514.3	522.8
	66	57.5	0.481	5.15	6.67	0.435	472.4	480.8	489.2	497.7	506.1	514.5	523.0
	65	56.0	0.458	4.90	6.92	0.414	472.4	480.8	489.3	497.8	506.2	514.6	523.1
	64	54.5	0.435	4.66	7.18	0.394	472.5	480.9	489.4	497.9	506.3	514.7	523.2
	63	53.0	0.414	4.43	7.39	0.375	472.7	481.1	489.6	498.1	506.5	514.9	523.4
	62	51.5	0.393	4.21	7.61	0.356	472.8	481.2	489.7	498.2	506.6	515.0	523.5
	61	50.0	0.373	4.00	7.82	0.339	472.9	481.3	489.8	498.3	506.7	515.1	523.6
	60	48.5	0.355	3.80	8.02	0.322	473.1	481.4	489.9	498.4	506.8	515.2	523.7
	59	47.0	0.337	3.60	8.22	0.305	473.2	481.5	490.0	498.5	506.9	515.3	523.8
	58	45.5	0.320	3.42	8.40	0.289	473.3	481.6	490.1	498.6	507.0	515.4	523.9
	57	44.0	0.304	3.25	8.57	0.276	473.4	481.7	490.2	498.7	507.1	515.5	524.0
	56	42.5	0.288	3.09	8.73	0.261	473.5	481.8	490.3	498.8	507.2	515.6	524.1
84	84	84.0	1.136	12.17	0.00	1.000	467.8	476.2	484.5	492.7	501.2	509.6	517.9
	83	82.5	1.083	11.61	0.56	0.954	468.1	476.4	484.8	493.2	501.5	509.\$	518.2
	82	81.0	1.034	11.07	1.10	0.910	468.4	476.7	485.1	493.5	501.8	510.1	518.5
	81	79.5	0.986	10.55	1.62	0.867	468.6	476.9	485.4	493.7	502.1	510.5	518.8
	80	78.0	0.940	10.07	2.10	0.827	468.9	477.3	485.7	494.0	502.4	510.8	519.1
	79	76.5	$0.896 \\ 0.854$	9.59	2.58	0.788 0.751	469.1	477.5 477.8	485.9	494.2	502.6 502.9	511.0 511.3	519.3 519.7
	78	75.0	0.004	9.14	3.03	0.751	469.4	411.0	486.1	494.5	302.3	911.0	313.1
	77	73.5	0.814	8.71	3.46	0.716	469.6	478.0	486.3	494.7	503.1	511.5	519.9
	76	72.0	0.776	8.30	1	0.682	469.8	478.2	486.5	494.9	503.3	511.7	520.1
	75	70.5	0.739	7.90	4.27	0.649	470.1	478.5	486.8	495.2	503.6	512.0	520.4
	74	69.0	0.704	7.53		0.619	470.3	478.7	487.0	495.4	503.8	512.2	520.6
	73	67.5	0.670	7.17	5.00	0.589	470.5	478.9	487.2	495.6	504.0	512.4	520.8
	72	66.0	0.638		5.34	0.561	470.6	479.0	487.4	495.8	504.2 504.3	512.6	521.0
	71	64.5	0.607	6.50	5.67	0.534	470.7	479.1	487.5	490.9	004.3	512.7	521.1

Reading of Thermometer, of Vapor		Wei of Va	apor	Hu-	Weight in Grains of a Cubic Foot of Air.								
mor		of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	a English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	29.0	29.5	30.0	30.5	in. 31.0
0	° 71	64.5	in. 0.607	gr. 6.50	gr. 5.67	0.534	gr. 470.7	gr. 479.1	gr. 487.5	gr. 495.9	gr. 504.3	gr. 512.7	gr. 521.1
84	70	63.0	0.578	6.18	5.99	0.508	470.9	479.3	487.7	496.1	504.5	512.9	521.3
	69	61.5	0.550	5.87	6.30	0.482	471.1	479.5	487.9	496.3	504.7	513.1	521.5
	68	60.0	0.523	5.59	6.58	0.459	471.2	479.6	488.0	496.4	504.8	513.2	521.6
	67	58.5	0.498	5.31	6.86	0.436	471.4	479.8	488.2	496.6	505.0	513.4	521.8
	66	57.0	0.473	5.05	7.12	0.415	471.6	480.0	488.3	496.7	505.2	513.6	522.1
	65	55.5	0.450	4.81	7.36	0.395	471.6	480.0	488.4	496.8	505.3	513.7	522.2
	CI	54.0	0.428	1 57	7.60	0.375	471.7	480.1	488.5	496.9	505.4	513.8	522.3
	64	52.5	0.428	4.57	7.82	0.357	471.8	480.2	488.6	497.0	505.5	513.9	522.4
	63 62	51.0	0.386	4.13	8.04	0.339	471.9	480.4	488.8	497.2	505.7	514.0	522.5
	61	49.5	0.367	3.93	8.24	0.323	471.9	480.5	488.9	497.3	505.8	514.1	522.6
	60	48.0	0.349	3.73	8.44	0.306	472.2	480.6	489.0	497.4	505.9	514.2	522.7
	59	46.5	0.331	3.55	8.62	0.292	472.3	480.7	489.1	497.5	506.0	514.3	522.8
	58	45.0	0.315	3.37	8.80	0.277	472.4	480.8	489.2	497.6	506.1	514.4	522.9
ì	57	43.5	0.299	3.20	8.97	0.263	472.5	480.9	489.3	497.7	506.2	514.5	523.0
										107.0	-00 1	-00 -	5100
85	85	85.0	1.171	12.53		1.000	466.8	475.2	483.5	491.8	500.1	508.5	516.8
	84	83.5	1.118	11.95	0.58	0.954	467.1	475.4	483.7	492.1	500.4	508.7	517.1
	83	82.0	1.067	11.40	1.13	0.910	467.3	475.6	484.0	492.4	500.7	509.0	517.4
	82	80.5	1.017	10.87	1.66	0.868	467.6	475.9	484.3	492.7	501.0	509.3	517.7 517.9
	81	79.0	0.970	10.38	2.15	0.829	467.8	476.1	484.5	492.9	501.2	509.5	518.2
	80	77.5	0.925	9.89	2.64	0.789	468.1	476.4	484.8	493.2	501.5 501.8	510.1	518.5
	79	76.0	0.882	9.43	3.10	0.753	468.4	476.7	485.1	493.5	301.3	510.1	310.5
	78	74.5	0.840	8.98	3.55	0.717	468.6	476.9	485.3	493.7	502.0	510.3	518.7
	77	73.0	0.801	8.55	3.98	0.682	468.7	477.1	485.5	493.9	502.2	510.5	518.9
1	76	71.5	0.763	8.15	4.38	0.650	469.0	477.4	485.8	494.2	502.5	510.8	519.2
	75	70.0	0.727	7.76	4.77	0.619	469.2	477.6	486.0	494.4	502.7	511.0	519.4
1	74	68.5	0.692	7.39	5.14	0.589	469.4	477.8	486.2	494.6	502.9	511.2	519.6
	73	67.0	0.659	7.04	5.49	0.562	469.7	478.1	486.5	494.9	503.2	511.5	519.9
	72	65.5	0.628	6.71	5.82	0.536	469.9	478.3	486.7	495.1	503.4	511.7	520.1
	71	64.0	0.597	6.37	6.16	0.508	470.1	478.5	486.9	495.3	503.6	511.9	520.3
	70	62.5	0.568	6.07	6.46	0.484	470.3	478.7	487.1	495.5	503.8	512.1	520.5
	69	61.0	0.541	5.77	6.76	0.460	470.5	478.9	487.2	495.6	504.0	512.4	520.8
	68	59.5	0.515	5.48	7.05	0.437	470.6	479.0	487.3	495.7	504.1	513.5	
	67	58.0	0.489	5.21			470.6	479.0	487.4	495.8			1
	66	56.5	0.465				470.7	479.1	487.5	1			
	65	55.0	0.442	4.72	7.81	0.377	470.8	479.2	487.6	496.0	504.4	512.8	521.2
	64	53.5	0.421	4.49	8.04	0.359	470.9	479.3	487.7	496.1	504.5	512.9	521.3
	63	52.0		1	8.27					1	504.7	513.1	521.3
	62	50.5	1		8.48	1	1	1	488.1	496.4	504.8	513.2	521.6
	61	49.0			1					496.5	504.9	513.3	521.7
H	60	47.5	1			1			488.3	496.6	505.0	513.4	521.8
	59	46.0										1	1
	58	44.5	0.309	3.3	1 9.22	0.264	471.6	480.1	488.5	496.8	505.2	513.6	522.1

Re	ading				ight			Weigh	t in Grain	10 OF 11 C1	shie Foot	of 11-	
of	Ther- meter,	Temp.	Force of		apor Reqd.	Hu- midity,							
	ahr.	Dew-	Vapor in	In a Cubic	for Sat'n.	Satura- tion =		Height	of the Bar	rometer i	n Englis	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	3 <sup>in.</sup>
0	0	0	in.	gr.	gr.		gr.	gr.	gr.	gr.	gr.	gr.	gr.
86	86	86.0	1.209	12.91	0.00	1.000	465.7	474.0	482.3	490.6	498.9	507.2	515.5
	85	84.5	1.153	12.31	0.60	0.954	466.0	474.3	482.6	490.9	499.2	507.5	515.8
	84	83.0	1.101	11.75	1.16	0.910	466.3	474.6	482.9	491.2	499.5	507.8	516.1
	83	81.5	1.050	11.20	1.71	0.868	466.5	474.8	483.2	491.5	499.8	508.1	516.5
	82	80.0	1.001	10.69	2.22	0.828	466.8	475.1	483.5	491.8	500.1	508.4	516.8
	81	78.5	0.955	10.19	2.72	0.789	467.1	475.4	483.8	492.1	500.4	508.7	517.1
	80	77.0	0.910	9.71	3.20	0.752	467.3	475.6	484.0	492.3	500.7	509.0	517.4
	79	75.5	0.868	9.25	3.66	0.717	467.5	475.8	484.2	492.5	500.9	509.2	517.6
	78	74.0	0.827	8.82	4.09	0.683	467.8	476.1	484.5	492.8	501.2	509.5	517.9
	77	72.5	0.787	8.40	4.51	0.651	468.0	476.3	484.7	493.0	501.4	509.7	518.1
	76	71.0	0.751	8.00	4.91	0.619	468.2	476.5	484.9	493.2	501.6	509.9	518.3
	75	69.5	0.715	7.62	5.29	0.590	468.3	476.6	485.0	493.4	501.8	510.2	518.6
	74	68.0	0.681	7.26	5.65	0.562	468.5	476.8	485.2	493.6	502.0	510.4	518.8
	73	66.5	0.648	6.91	6.00	0.535	468.8	477.1	485.5	493.9	502.2	510.6	519.0
	72	65.0	0.617	6.58	6.33	0.509	468.9	477.2	485.6	494.0	502.4	510.8	519.2
	71	63.5	0.588	6.26	6.65	0.485	469.1	477.4	485.8	494.2	502.6	511.0	519.4
	70	62.0	0.559	5.95	6.96	0.461	469.2	477.5	485.9	494.3	502.7	511.1	519.5
	69	60.5	0.532	5.66	7.25	0.438	469.4	477.7	486.1	494.5	502.9	511.3	519.7
	68	59.0	0.506	5.38	7.53	0.417	469.6	477.9	486.3	494.7	503.1	511.5	519.9
	67	57.5	0.481	5.11	7.80	0.396	469.8	478.1	486.5	494.9	503.3	511.7	520.1
	36	56.0	0.458	4.87	8.04	0.377	469.9	478.2	486.6	495.0	503.4	511.8	520.2
	65	54.5	0.435	4.63	8.28	0.359	470.0	478.3	486.7	495.1	503.5	511.9	520.3
	64	53.0	0.414	4.40	8.51	0.341	470.1	478.4	486.8	495.1	503.6	512.0	520.4
	63	51.5	0.393	4.19	8.72	0.325	470.2	478.5	486.9	495.2	503.7	512.1	520.5
	62	50.0	0.373	3.98	8.93	0.308	470.4	478.7	487.1	495.4	503.9	512.2	520.7
	61	48.5	0.355	3.78	9.13	0.293	470.5	478.8	487.2	495.5	504.0	512.3	520.8
	60	47.0	0.337	3.59	9.32	0.278	470.6	478.9	487.3	495.6	504.1	512.4	520.9
	59	45.5	0.320	3.40	9.51	0.263	470.7	479.0	487.4	495.7	504.2	512.5	521.0
87	87	87.0	1.247	13.29	0.00	1.000	464.5	472.8	481.1	489.4	497.7	506.0	514.3
	86	85.5	1.190	12.68	0.61	0.954	464.8	473.1	481.4	489.7	498.0	506.3	514.6
	85	84.0	1.136	12.10	1.19	0.910	465.1	473.4	481.7	490.0	498.3	506.6	514.9
	84	82.5	1.083	11.54	1.75	0.868	465.4	473.7	482.0	490.3	498.6	506.9	515.2
	83	81.0	1.034	11.01	2.28	0.828	465.7	474.0	482.3	490.6	498.9	507.2	515.5
	82	79.5	0.986	10.49	2.80	0.789	466.0	474.3	482.6	490.9	499.2	507.5	515.8
	81	78.0	0.940	10.01	3.28	0.753	466.3	474.6	482.9	491.2	499.5	507.8	516.1
	80	76.5	0.896	9.54	3.75	0.718	466.5	474.8	483.1	491.4	499.8	508.1	516.5
	79	75.0	0.854	9.09	4.20	0.684	466.8	475.1	483.5	491.8	500.1	508.4	516.8
	78	73.5	0.814	8.66	4.63	0.652	467.0	475.3	483.7	492.0	500.3	508.6	517.0
	77	72.0	0.776	8.24	5.05	0.620	467.2	475.5	483.9	492.2	500.5	508.8	517.2
	76	70.5	0.739	7.85	5.44	0.591	467.3	475.6	484.0	492.3	500.7	509.0	517.4
	75	69.0	0.704	7.48	5.81	0.563	467.5	475.8	484.2	492.5	500.9	509.2	517.6
	74	67.5	0.670	7.12		0.536	467.7		484.4	492.7	501.1	509.4	517.8
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	ading Ther-	Temp.	Force	Wei of V	apor	Hu-		Weight	t in Grain	ns of a Cu	ibic Foot	of Air.	
moi	meter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'u.	midity, Satura- tion =		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	0.596	gr.	gr.	gr.	gr.	gr.	gr.	gr.
87	74	67.5 66.0	$0.670 \\ 0.638$	7.12 6.78	6.17 $6.51$	$0.536 \\ 0.510$	467.7	476.0	484.4	492.7 492.9	501.1 501.3	509.4 509.6	517.8 518.0
	72	64.5	0.607	6.46	6.83	0.486	468.1	476.4	484.8	493.1	501.5	509.8	518,2
	71	63.0	0.578	6.14	7.15	0.462	468.3	476.6	485.0	493.3	501.7	510.1	518.5
	70	61.5	0.550	5.85	7.44	0.440	468.4	476.7	485.1	493.5	501.9	510.3	518.7
	69	60.0	0.523	5.56	7.73	0.418	468.5	476.9	485.3	493.7	502.0	510.4	518.8
	68	58.5	0.498	5.28	8.01	0.397	468.7	477.1	485.5	493.9	502.2	510.6	519.0
	67	57.0	0.473	5.02	8.27	0.378	468.8	477.2	485.6	494.0	502.3	510.7	519.1
	66	55.5	0.450	4.77	8.52	0.359	468.9	477.3	485.7	494.1	502.4	510.7	519.2
	65	54.0	0.428	4.54	8.75	0.342	469.1	477.5	485.9	494.3	502.6	510.9	519.4
	64	52.5	0.407	4.33	8.96	0.326	469.2	477.6	486.1	494.4	02.7	511.0	519.5
	63	51.0	0.386	4.12	9.17	0.310	469.3	477.7	486.2	494.5	02.8	511.1	519.6
	62	49.5	0.367	3.91	9.38	0.294	469.4	477.8	486.3	494.6	502.9	511.2	519.7
	61	48.0	0.349	3.71	9.58	0.279	469.6	477.9	486.5	494.8	503.1	511.4	519.9
	60	46.5	0.331	3.51	9.78	0.264	469.7	478.1	486.6	494.9	503.2	511.5	520.0
88	88	88.0	1.286	13.68	0.00	1.000	463.5	471.7	480.0	488.3	496.6	504.8	513.1
00	87	86.5	1.228	13.06	0.62	0.954	463.8	472.0	480.3	488.6	496.9	505.1	513.4
	86	85.0	1.171	12.46	1.22	0.911	464.2	472.4	480.7	489.0	497.3	505.6	513.9
	85	83.5	1.118	11.88	1.80	0.868	464.4	472.7	481.0	489.3	497.6	505.9	514.2
	84	82.0	1.067	11.34	2.34	0.829	464.7	473.0	481.3	489.6	497.9	506.2	514.5
	83	80.5	1.017	10.81	2.87	0.790	465.0	473.3	481.6	489.9	498.2	506.5	514.8
	82	79.0	0.970	10.31	3.37	0.754	465.2	473.5	481.8	490.1	498.4	506.7	515.0
	81	77.5	0.925	9.83	3.85	0.718	465.5	473.8	482.1	490.4	498.7	507.0	515.8
	80	76.0	0.882	9.37	1		465.8	474.1	482.4	490.7	499.0	507.3	515.6
	79	74.5	0.840	8.93	1	1	466.1	474.4	482.7	491.0	499.3	507.6	515.9
	78	73.0	0.801	8.50	5.18	0.621	466.3	474.6	482.9	491.2	499.5	507.8	516.2
	77	71.5	0.763	8.09	5.59	0.591	466.4	474.7	483.0	491.3	499.7	508.0	516.4
	76	70.0	0.727	7.71	5.97	0.563	466.6	474.9	483.2	491.5	499.9	508.2	516.6
	75	68.5	0.692	7.34	6.34	0.537	466.8	475.1	483.4	491.7	500.1	508.4	516.8
	74	67.0	0.659	6.99	Į.		467.0	475.3	1	491.9	500.3	508.6	517.0
	73	65.5	0.628	6.66			467.2	475.5		492.1	500.5	508.8	517.2
	72	64.0	0.597	6.33	1	1	467.4			492.3		509.0	517
	71	62.5	0.568	6.03	1	1	467.4	475.7		492.4	500.8	509.1	517.5
	70	61.0	0.541	5.74		1	467.6	1	1	492.6	1	1	517.5
	69 68	59.5 58.0	0.313	5.45 5.18	I.	1	1	1			1	1	518.0
	67	56.5	0.465	4.93	8.75	0.359	468.1	476.4	484.7	493.1	501.5	509.8	518.5
1	66	55.0	0.442	4.69	1	1				}	1	1	1
	65	53.5	0.421	4.47			468.3			1	1	1	
	64	52.0	0.400			t .	468.4			1	1	510.1	518.5
	63	50.5	0.380			0.295		1		1		1	
	62	49.0		3.83				1		1		510.4	518.8
	61	47.5				0.265			485.5			510.5	518.9

	ading Ther-	Temp.	Force	We of V	ight 'apor	Hu-		Weight	t in Grain	as of a Cu	ibic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	ometer i	n Englisl	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	iu.	gr.	gr	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
89	89 88	89.0	1.326 $1.266$	14.08 13.44	0.00	1.000 $0.954$	462.4	470.6 470.9	478.9 479.2	487.1	495.4	503 6 503.9	511.9 512.2
	87	86.0	1.209	12.84	1.24	0.912	463.0	471.2	479.5	487.8	496.1	504.4	512.7
	86	84.5	1.153	12.24	1.84	0.869	463.3	471.5	479.8	488.1	496.4	504.7	513.0
	85	83.0	1.101	11.68	2.40	0.830	463.6	471.8	480.1	488.4	496.7	505.0	513.3
	84	81.5	1.050	11.13	2.95	0.791	464.0	472.2	480.5	488.8	497.1	505.4	513.7
	83	80.0	1.001	10.62	3.46	0.754	464.2	472.5	480.8	489.1	497.4	505.7	514.0
		<b>*0 </b>	0.055	70.10	0.05	0 *10		4=0 =	401.0	400.0	407 0	-0-0	
	82	78.5	0.955	10.13	3.95	0.719	464.4	472.7	481.0	489.3	497.6	505.9	.514.2
	81	77.0	0.910	9.66	4.42	0.686	464.7	473.0	481.3	489.6	497.9	506.2	514.5
	80	75.5 74.0	$0.868 \\ 0.827$	9.20	4.88	0.653	464.9	473.2	481.5	489.8	498.1	506.4 506.7	514.7 515.0
	79 78	72.5	0.827	8.77 8.35	5.31	0.623 $0.593$	465.2	473.5 473.7	481.8	490.1	498.4	506.7	515.2
	77	71.0	0.751	7.96	6.12	0.565	465.6	473.9	482.2	490.5	498.8	507.1	515.4
	76	69.5	0.731	7.57	6.51	0.537	465.8	474.1	482.4	490.5	499.0	507.3	515.7
						0.001	100.0			20000	20000		
	75	68.0	0.681	7.21	6.87	0.512	466.0	474.3	482.6	490.9	499.2	507.5	515.8
1	74	66.5	0.648	6.87	7.21	0.488	466.2	474.5	482.8	491.1	499.4	507.7	516.0
	73	65.0	0.617	6.54	7.54	0.465	466.3	474.6	482.9	491.2	499.6	507.9	516.3
	72	63.5	0.588	6.22	7.86	0.442	466.5	474.8	483.1	491.4	499.8	508.1	516.5
	71	62.0	0.559	5.91	8.17	0.420	466.7	475.0	483.3	491.7	500.0	508.3	516.7
4	70	60.5	0.532	5.62	8.46	0.399	466.8	475.1	483.4	491.8	500.1	508.4	516.8
	69	59.0	0.506	5 35	8.73	0.380	467.0	475.3	483.6	492.0	500.3	508.6	517.0
	68	57.5	0.481	5.08	9.00	0.361	467.1	475.4	483.7	492.1	500.4	508.7	517.1
	67	56.0	0.458	4.84	9.24	0.343	467.2	475.5	483.8	492.2	500.5	508.8	517.2
	66	54.5	0.435	4.61	9.47	0.327	467.4	475.7	483.9	492.4	500.7	509.1	517.4
	65	53.0	0.414	4.39	9.69	0.312	467.5	475.8	484.1	492.5	500.8	509.2	517.5
	64	51.5	0.393	4.17	9.91	0.296	467.6	475.9	484.2	492.6	500.9	509.3	517.6
	63	50.0	0.373	3.96	10.12	0.281	467.7	476.1	484.3	492.7	501.0	509.4	517.7
	62	48.5	0.355	3.76	10.32	0.267	467.8	476.2	484.4	492.8	501.1	509.5	517.8
00	0.0	00.0	1.000		0.00	1 000	107.0	100 -	488.0	400.0	40.4.0	500.5	510.0
90	90	90.0	1.368	14.50	0.00	1.000	461.3	469.5	477.8	486.0	494.3	502.5	510.8
	89	88.5	1.306	13.84	0.66	0.954	461.6	469.8	478.1	486.3	494.6	502.8 503.2	511.1 511.5
	88	87.0	1.247 1.190	13.22 $12.61$	1.28	0.910	462.0	470.2	478.5	486.7	495.3	503.5	511.8
	87 86	85.5	1.136	12.61	2.47	0.870	462.3	470.9	479.2	487.4	495.7	503.9	512.1
	85	82.5	1.083	12.03	3.03	0.530	463.0	471.2	479.5	487.7	496.0	504.2	512.5
	84	81.0	1.034	10.94			463.2	471.5		488.0	496.3	504.5	512.8
		31.0	2.001	20.01	0.50	3.,00	100.2			100.0			
	83	79.5	0.986	10.43			463.4	471.7	1	488.2	496.5	504.7	513.0
	82	78.0	0.940	9.95			463.7	472.0	480.3	488.5	496.8	505.0	513.3
	81	76.5	0.896	9.48			464.0	472.3	480.6	488.8	497.1	505.3	513.6
	80	75.0	0.854	9.03			464.2	472.5	480.7	488.9	497.3	505.5	513.9
	79	73.5	0.814	8.61	5.89		464.3	472.6	480.9	489.1	497.5	505.7	514.1
	78	72.0	0.776	8.20			464.5	472.8	481.1	489.3	1	505.9	514.3
	77	70.5	0.739	7.80	6.70	0.538	464.7	473.0	481.3	489.5	497.9	506.1	514.5

of	ading Ther-	Temp.	Force	Wei of V	•	Hu-		Weigh	t in Grain	ns of a Cu	bic Foot	of Air.	
	meter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion ==		Height o	of the Bar	rometer i	English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	in. 29.5	30.0	30.5	in. 31.0
90	77	70.5	in. 0.739	gr. 7.80	gr. 6.70	0.538	gr. 464.7	gr. 473.0	gr.	gr. 489.5	gr. 497.9	gr. 506.1	gr. 514.5
90	76	69.0	0.704	7.43	7.07	0.512	465.0	473.3	481.3	489.8	497.9	506.4	514.8
	75	67.5	0.670	7.08	7.42	0.488	465.2	473.5	481.8	490.0	498.4	506.6	515.0
	74	66.0	0.638	6.74	7.76	0.465	465.4	473.7	482.0	490.2	498.6	506.8	515.2
	73	64.5	0.607	6.42	8.08	0.443	465.6	473.9	482.2	490.4	498.8	507.0	515.4
	72	63.0	0.578	6.10	8.40	0.421	465.7	474.0	482.3	490.5	498.9	507.1	515.5
	71	61.5	0.550	5.81	8.69	0.400	465.9	474.2	482.5	490.7	499.1	507.3	515.7
	70	60.0	0.523	5.52	8.98	0.381	466.1	474.4	482.8	491.0	499.3	507.5	515.9
	69	58.5	0.498	5.25	9.25	0.362	466.2	474.5	482.9	491.1	499.4	507.6	516.0
	68	57.0	0.473	4.99	9.51	0.344	466.4	474.7	483.1	491.3	499.6	507.8	516.2
	67	55.5	0.450	4.74	9.76	0.327	466.5	474.8	483.2	491.4	499.7	507.9	516.3
	66	54.0	0.428	4.52	9.98		466.6	474.9	483.3	491.5	499.8	508.0	516.4
	65	52.5	0.407	4.30	10.20		466.7	475.0	483.4	491.6	499.9	508.1	516.5
	64	51.0	0.386	4.09	10.41		466.9	475.2	483.6	491.8	500.1	508.3	516.6
Ľ	63	49.5	0.367	3.90	10.60	0.269	467.0	475.3	483.7	491.9	500.2	508.4	516.7

#### TABLE XIII.

FACTORS FOR COMPUTING THE FORCE OF VAPOR, FROM THE READINGS OF THE PSYCHROMETER, BY APJOHN'S FORMULA.

Dr. Apjohn's formula for deducing the force of vapor, and the temperature of the dew-point, from the readings of the Psychrometer, as given in the Proceedings of the Royal Irish Academy for 1840, is

$$f'' = f' - \frac{d}{88} \times \frac{h}{30},$$

when the readings of the wet-bulb thermometer are above 32° Fahr., in which formula

f'' = the force of vapor at the temperature of the dew-point in degrees of Fahr.,

f' = the force of vapor at the temperature of evaporation given by the wet-bulb thermometer,

d = the difference between the readings of the dry and wet thermometers,

h = the height of the barometer in English inches at the time of the observation. When the readings of the wet-bulb thermometer are *below* 32° Fahr., and the bulb is covered with ice, the formula becomes

$$f'' = f' - \frac{d}{96} \times \frac{h}{30}.$$

The factors in the following table, which is taken from the Greenwich Observations for 1843, represent  $\frac{d}{88} \times \frac{1}{30}$  and  $\frac{d}{96} \times \frac{1}{30}$ , computed for all differences between the wet and dry bulb thermometers, or values of d, from  $0^{\circ}$  to  $21^{\circ}$ .

#### USE OF THE TABLE.

To find out the force of vapor in the air, and the temperature of the dew-point, by means of these factors, let the factor corresponding to d, or the difference between the wet and dry thermometer in the first column, be multiplied into the observed height of the barometer, and subtract the result from the force of vapor, in Table XI., due to the temperature of evaporation, indicated by the wet-bulb thermometer; the rest is the force of vapor in the air at the time of the observation; and the temperature of the dew-point is that which is due to it in Table XI.

#### EXAMPLE.

The observation gives,

Dry-bulb thermometer = 79° Fahr., or the temperature of the air.

Wet-bulb "  $= 69^{\circ}$  " or temperature of evaporation.

Difference 10°

Height of barometer 29.7 English inches.

In the Table, 2d part, is found, — factor for a difference of  $10^{\circ} = 0.00379 \times 29.7$ , or height of barometer = 0.113, which, subtracted from the force of vapor due to 69°, in Table XI., = 0.704 — 0.113, gives force of vapor in the air = 0.591 inches, and temperature of the dew-point 62°.5.

When the temperature of the wet bulb is below 32° Fahrenheit, the factors in the first part of the Table must be used.

B

XIII. FACTOR  $\frac{d}{96} imes \frac{1}{30}$ , FOR COMPUTING THE FORCE OF VAPOR BY APJOHN'S FORMULA.

Below 32° Fahrenheit; the Wet Bulb covered with a Film of Ice.

d, or Difference					Tenths of	f Degrees.				
of Wet and Dry Bulb Therm.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0										
0	0.00000	0.00003	0.00007	0.00010	0.00014	0.00017	0.00020	0.00024	0.00027	0.0003
1	.00034	.00037	.00041	.00044	.00047	.00051	.00054	.00058	.00061	.0006
2	.00068	.00071	.00075	.00078	.00081	.00085	.00088	.00092	.00095	.00099
3	.00102	.00105	.00109	.00112	.00116	.00119	.00122	.00126	.00129	.0013
4	.00136	.00139	.00143	.00146	.00150	.00153	.00156	.00160	.00163	.00163
5	.00170	.00173	.00177	.00180	.00184	.00187	.00190	.00194	.00198	.0020
6	.00204	.00207	.00211	.00214	.00218	.00221	.00224	.00228	.00231	.0023
7	.00238	.00241	.00245	.00248	.00252	.00255	.00258		.00265	.00269
8	.00272	.00275	.00279	.00282	.00285	.00289	.00292	.00296		.0030
9	.00306	.00309	.00313	.00316	.00319	.00323	.00326	.00330		.0033
10	.00340	.00343	.00347	.00350	.00354	.00357	.00360	.00364	.00367	.0037

FACTOR  $\frac{d}{88} \times \frac{1}{30}$ .

Reading of Wet-Bulb Thermometer above 32° Fahrenheit.

d, or Difference					Tenths o	f Degrees.				
of Wet and Dry Bulb Therm.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	0.00000	0.0000.1	0.00008	0.00011	0.00015	0.00010	0.00022	0.00027	0.00030	0.0002
1	.00038	.00042	.00046	.00049	.00053	.00057	.00061	.00064	.00068	.0007
2	.00036	.00042		.00043	.00091	.00095	.00098	.00102	.001068	.0007
3	.00114	.00118		.00125	.00129	.00033	.00033	.00102	.00106	.0011
4	.00151	.00135	.00159	.00163	.00167	.00132	.00174	.00140	.00144	.0014
5	.00189	.00193	.00197	.00201	.00205	.00209	.00212	.00216	.00220	.0022
6	.00228	.00231	.00235	.00239	.00242	.00246	.00250	.00254	.00258	.0026
7	.00265	.00269	.00273	.00277	.00280	.00284	.00288	.00292	.00295	.0029
8	.00303	.00307	.00311	.00315	.00318	.00322	.00326	.00330	.00333	.0033
9	.00341	.00345	.00349	.00352	.00356	.00360	.00364	.00368	.00371	.0037
10	.00379	.00383	.00386	.00390	.00394	.00398	.00401	.00405	.00409	.0041
11	.00416	.00420	.00424	.00428	.00432	.00436	.00439	.00443	.00447	.0045
12	.00454	.00458	.00462	.00466	.00470	.00474	.00477	.00481	.00485	.0048
13	.00493	.00496	.00500	.00504	.00508	.00511	.00515	.00519	.00522	.0052
14	.00530	.00534	.00538	.00541	.00545	.00549	.00553	.00556	.00560	.0056
15	.00568	.00572	.00576	.00580	.00584	.00587	.00591	.00595	.00598	.0060
16	.00606	.00610	.00614	.00618	.00622	.00625	.00629	.00633	.00636	.0064
17	.00644	.00648	.00652	.00655	.00659	.00663	.00666	.00670	.00674	.00678
18	.00682	.00686	.00690	.00693	.00697	.00701	.00704	.00708	.00712	.0071
19	.00720	.00724	.00728	.00731	.00735	.00739	.00742	.00746	.00750	.0075
20	.00758	.00761	.00765	.00769	.00773	.00777	.00780	.00781	.00788	.0079

In the Greenwich Magnetic and Meteorological Observations for 1842 and 1843, Mr. Glaisher discussed the relation between the temperature of evaporation given by the Wet-bulb Thermometer and the temperature of the Dew-Point as given by Daniell's Hygrometer. Comparing the observations taken simultaneously every six hours with the Psychrometer, and with Daniell's Dew-Point Hygrometer, and dividing the average difference between the temperatures of the Wet and Dry bulb by the average difference of the temperature of the Dew-Point and of the Air, he obtained the empirical factors given in the following Table.

The observations from which they are deduced are those taken at the Observatory in the years 1841 to 1845, for the temperatures below 35° F., and in the years 1841 to 1843, for the temperatures above 35° F.

The observations made at Toronto Observatory, Canada West, in similar circumstances, in the years 1840 to 1842, were also compared in the same manner, and the factors derived from them showed a very close accordance for temperatures above 30° F., but were found smaller at temperatures below 30° F.

The errors in the temperature of the Dew-Point, which may result by using the Greenwich factors, though frequently within half a degree, often amount, however, to  $\pm$  2 or 3 degrees, and, in extreme cases, to  $\pm$  4 or 5 degrees, as shown in the volume of the *Greenwich Observations* for 1842, p. 60 of the *Abstracts*.

### Use of the Table.

Multiply the difference between the Wet-bulb and Dry-bulb Thermometers by the factor standing in the Table opposite the reading of the Dry-bulb, and subtract the product from the reading of the Dry-bulb; the remainder will be the temperature of the Dew-Point.

Example. — Dry-bulb =  $62^{\circ}$  F.; Wet-bulb =  $55^{\circ}$ ; Difference =  $7^{\circ}$ .

Opposite 62°, in the first column, stands the factor 1.7, which multiplied by 7°, the difference, gives 11°.9, to be subtracted from the Dry-bulb; or  $62^{\circ} - 11^{\circ}.9 = 50^{\circ}.1$ , temperature of the Dcw-Point.

XIV. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. — GLAISHER.

Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.
21°	8.5	35°	2.6	49°	2.2	63°	1.7	77°	1.5
22	8.5	36	2.6	50	2.1	64	1.7	78	1.5
23	8.5	37	2.5	51	2.1	65	1.7	79	1.5
24	7.3	38	2.5	52	2.0	66	1.6	80	1.5
25	6.4	39	2.5	53	2.0	67	1.6	81	1.5
26	6.1	40	2.4	54	2.0	68	1.6	82	1.5
27	5.9	41	2.4	55	2.0	69	1.5	83	1.5
28	5.7	42	2.4	56	1.9	70	1.5	84	1.5
29	5.0	43	2.4	57	1.9	71	1.5	85	1.5
30	4.6	44	2.3	58	1.9	72	1.5	86	1.5
31	3.6	45	2.3	59	1.8	73	1.5	87	1.5
32	3.1	46	2.3	60	1.8	74	1.5	88	1.5
33	2.8	47	2.2	61	1.8	75	1.5	89	1.5
34	2.6	48	2.2	62	1.7	76	1.5	90	1.5

## XV. WEIGHT OF VAPOR, IN GRAINS TROY, CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES BETWEEN 0° AND 94° FAHRENHEIT.

From the Greenwich Observations.

Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Graius.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.
0°	0.78	19°	1.52	38°	2.89	57°	5.34	76°	9.60
1	0.81	20	1.58	39	2.99	58	5.51	77	9.89
2	0.84	21	1.63	40	3.09	59	5.69	78	10.19
3	0.87	22	1.69	41	3.19	60	5.87	79	10.50
4	0.90	23	1.75	42	3.30	61	6.06	80	10.81
5	0.93	24	1.81	43	3.41	62	6.25	81	11.14
6	0.97	25	1.87	44	3.52	63	6.45	82	11.47
7	1.00	. 26	1.93	45	3.64	64	6.65	83	11.82
8	1.04	27	2.00	46	3.76	65	6.87	84	12.17
9	1.07	28	2.07	47	3.88	66	7.08	85	12.53
10	1.11	29	2.14	48	4.01	67	7.30	86	12.91
11	1.15	30	2.21	49	4.14	68	7.53	87	13.29
12	1.19	31	2.29	50	4.28	69	7.76	88	13.68
13	1.24	32	2.37	51	4.42	70	8.00	89	14.08
14	1.28	33	2.45	52	4.56	71	8.25	90	14.50
15	1.32	34	2.53	53	4.71	72	8.50	91	14.91
16	1.37	35	2.62	54	4.86	73	8.76	92	15.33
17	1.41	36	2.71	55	5.02	74	9.04	93	15.76
18	1.47	37	2.80	56	5.18	75	9.31	94	16.22

XVI. FACTORS TO DEDUCE THE WEIGHT OF VAPOR CONTAINED IN A CUBIC FOOT OF AIR, AT THE TIME OF A GIVEN OBSERVATION, FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS. — GREENW. OBS.

 $\mathbf{t} = \text{Temperature of Air}; \ \mathbf{t}'' = \text{Temperature of Dew-Point}.$ 

Difference or $\mathbf{t} - \mathbf{t}''$ .	Factors.	Difference or t — t".	Factors.	Difference or t-t".	Factors.	Difference or t — t".	Factors.	Difference or t — t".	Factors.
1	0.999	9	0.982	17	0.966	25	0.951	33	0.935
2	0.996	10	0.980	18	0.964	26	0.949	34	0.934
3	0.994	11	0.978	19	0.962	27	0.947	35	0.932
4	0.992	12	0.976	20	0.960	28	0.945	36	0.930
5	0.990	13	0.974	21	0.958	29	0.943	37	0.929
6	0.988	14	0.972	22	0.956	30	0.942	38	0.927
7	0.986	15	0.970	23	0.954	31	0.939	39	0.925
8	0.984	16	0.968	24	0.952	32	0.937	40	0.923

Use of Table XVI. — The difference between the temperatures of the air and of the Dew-Point being known, multiply the factor in the Table corresponding to that difference into the weight of a cubic foot of vapor at the temperature of the Dew-Point, as given in Table XV., and the product will be the weight of vapor in a cubic foot of air at the time of the observation.

Example. — Temperature of air = 60° F.; Dew-Point = 52°; Diff. = 8°.

Table gives for a difference of 8°, factor 0.984; Table XV. gives weight of a cubic foot of vapor at temperature  $52^{\circ} = 4.5^{\circ}.56$ .

Hence,  $0.984 \times 4.56 = 4^{gr}.49$ , the weight of vapor required.

#### TABLE XVII.

FOR COMPARING THE WEIGHT OF A CUBIC FOOT OF DRY AND OF SATURATED AIR.

This table is composed of two tables found in the Greenwich Meteorological Observations for 1842, pages xlvi. and li.; the first containing the weight of a cubic foot of dry air, under a barometric pressure of 30 inches, at temperatures between 0° and 90° F.; the other giving the weight of a cubic foot of saturated air under the same barometric pressure and temperature, together with the excess of the first above the last.

The weight of a cubic foot of dry air, on which the tables are based, is assumed to be 563 grains Troy, being a mean value, in round numbers, between the determinations of Shuckburgh, which is 557.7295 grains, and that of Biot and Arago, 568.7013. The true mean is 563.2154, but 563 is the number used in the calculations.

The coefficient of the expansion of the air is that of Gay-Lussac, viz. 0.00375 for 1° Centigrade, or 0.002083 of its bulk for 1° Fahrenheit.

## Use of the Table.

This table shows the amount of buoyancy imparted to the air by the addition of moisture; and from it, the temperature and the relative humidity of the air being known, the weight of a cubic foot of air, in the actual condition of the atmosphere at the time of an observation, can be deduced.

It suffices to take in the fourth column, headed "Excess," the quantity corresponding to the temperature of the air in the first, multiply it into the given Relative Humidity, and subtract the product from the number in the second column. The result will be the weight of a cubic foot of air at the existing temperature and moisture, under a barometric pressure of 30 inches.

This result will be reduced to its true value, under the barometric pressure given by the observation, by multiplying it by  $\frac{\text{Height of Barometer}}{30}$ .

## Example.

The temperature of the air is 60° F.; the relative humidity, 0.852; the barometer reads 29 inches.

The table gives, for temperature of air,  $60^{\circ}$ ; excess,  $3.35 \times 0.852 = 2.85$ , which, subtracted from 531.91 in the second column, = 529.12, weight of a cubic foot of air under 30 inches of pressure; and  $529.12 \times \frac{29 \text{ inch}}{30} = 511.48$ , the weight of a cubic foot of air in the given conditions of temperature, moisture, and barometric pressure.

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# XVII. FOR COMPARING THE WEIGHT OF A CUBIC FOOT OF DRY AND OF SATURATED AIR,

## AT TEMPERATURES BETWEEN 0° AND 90° FAHRENHEIT.

From the Greenwich Observations.

Temper- ature Fahren.	Weight of a cubic foot of Dry Air.	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.	Temper- ature Fahren.	Weight of a cubic foot of Dry Air.	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.	Temper- ature Fahren.	ora cubic	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.
0	Grains.	Grains.	Grains	0	Grains.	Grains.	Grains.		Grains.	Grains.	Grains.
0	603.21	602.77	0.44	30	565.35	564.08	1.27	60	531.97	528.62	3.35
1	601.87	601.40	0.47	31	564.17	562.86	1.31	61	530.93	527.48	3.45
2	600.52	600.03	0.49	32	563.00	561.64	1.36	62	529.88	526.32	3.56
3	599.20	598.69	0.51	33	561.84	560.42	1.42	63	528.84	525.17	3.67
4	597.87	597.34	0.53	34	560.67	559.20	1.47	64	527.81	524.03	3.78
5	596.55	596.01	0.54	35	559.51	558.01	1.50	65	526.88	522.90	3.88
6	595.24	594.69	0.55	36	558.35	556.79	1.56	66	525.76	521.75	4.01
7	593.94	593.36	0.58	37	557.21	555.61	1.60	67	524.75	520.61	4.14
8	592.63	592.04	0.59	38	556.05	554.40	1.65	68	523.72	519.46	4.26
9	591.33	590.72	0.61	39	554.91	553.20	1.71	69	522.70	518.29	4.41
10	590.04	589.40	0.64	40	553.77	552.00	1.77	70	521.70	517.17	4.53
11	588.75	588.07	0.68	41	552.65	550.80	1.84	71	520.70	516.02	4.68
12	587.48	586.78	0.70	42	551.52	549.63	1.89	72	519.69	514.87	4.82
13	586.21	585.49	0.72	43	550.39	548.44	1.95	73	518.70	513.75	4.95
14	584.94	584.18	0.75	44	549.27	547.26	2.01	74	517.70	512.61	5.09
15	583.67	582.89	0.78	45	548.16	546.06	2.10	75	516.71	511.46	5.25
16	582.41	581.61	0.80	46	547.05	544.88	2.17	76	515.73	510.32	5.41
17	581.15	580.33	0.82	47	545.97	543.75	2.22	77	514.74	509.18	5.56
18	579.91	579.06	0.85	48	544.85	542.55	2.30	78	513.77	508.04	5.73
19	578.67	577.79	0.88	49	543.75	541.36	2.39	79	512.80	506.91	5.89
20	577.44	576.54	0.90	50	542.65	540.21	2.44	80	511.82	505.74	6.08
21	576.21	575.27	0.94	51	541.55	539.04	2.51	81	510.87	504.61	6.26
22	574.98	574.01	0.97	52	540.48	537.87	2.61	82	509.89	503.45	6.44
23	573.76	572.76	1.00	53	539.41	536.71	2.70	83	508.93	502.32	6.61
24	572.55	571.50	1.05	54	538.33	535.55	2.78	84	507.97	501.16	6.81
25	571.33	570.26	1.07	55	537.27	534.39	2.88	85	507.03	500.05	6.98
26	570.13	569.01	1.12	56	536.19	533.22	2.97	86	506.07	498.87	7.20
27	568.92	567.77	1.15	57	535.12	532.06	3.06	87	505.11	497.71	7.40
28	567.73	566.53	1.20	58	534.07	530.92	3.15	88	504.19	496.58	7.61
29	566.54	565.31	1.23	59	533.03	529.77	3.26	89	503.25	495.44	7.81
30	565.35	564.08	1.27	60	531.97	528.62	3.35	90	502.32	494.28	8.04
27 28 29	568.92 567.73 566.54	567.77 566.53 565.31	1.15 1.20 1.23	57 58 59	535.12 534.07 533.03	532.06 530.92 529.77	3.06 3.15 3.26	87 88 89	505.11 504.19 503.25	4	19 <b>7.</b> 71 196.58 195.44

#### TABLE XIV'.

Mr. Glaisher published in London, in 1856, another series of Hygrometrical Tables, which were unknown to the writer when the Second Edition of this volume was issued. They are based on Regnault's Table of Elastic Forces of Vapor, and on the coefficient of the expansion of the air as determined by the same physicist. The Psychrometrical Table, however, is not computed from Regnault's formula, but by first finding out, in the manner described on page 140, the temperatures of the dewpoint from the readings of the Psychrometer, by means of the empirical factors given below, in Table XIV'., and then taking the corresponding values of the force of vapor from Regnault's table. These factors have been derived from the combination of all simultaneous observations of the dry and wet bulb thermometers with those of Daniell's hygrometer, taken at the Royal Observatory, Greenwich, from the year 1841 to 1854, with some observations taken at high temperatures in India, and others at low and medium temperatures at Toronto; they are, therefore, more correct than those given in Table XIV. page 140. The results in this new Psychrometrical Table, nevertheless, by no means entirely coincide with those given by the formula, as a comparison with those in Table VII. will show.

XIV'. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. — GLAISHER.

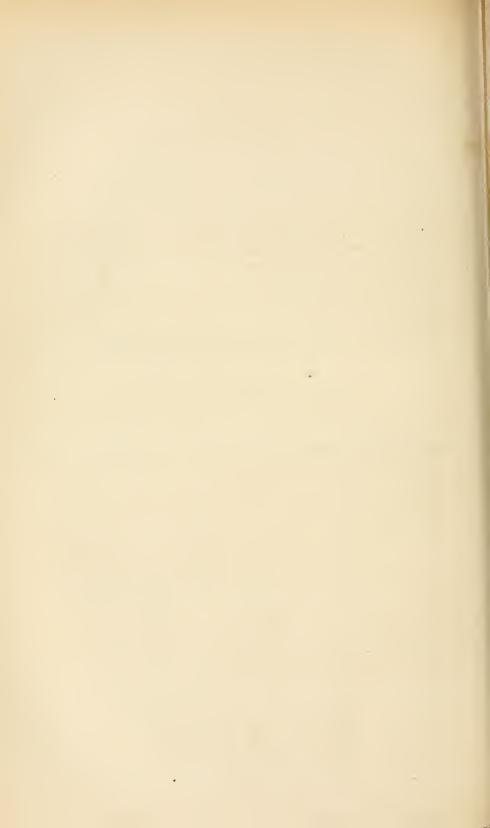
Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.
0		0		0		0		0	
10	8.78	28	5.12	46	2.14	64	1.83	82	1.67
11	8.78	29	4.63	47	2.12	65	1.82	83	1.67
12	8.78	30	4.15	48	2.10	66	1.81	84	1.66
13	8.77	31	3.70	49	2.08	67	1.80	85	1.65
14	8.76	32	3.32	50	2.06	68	1.79	86	1.65
15	8.75	33	3.01	51	2.04	69	1.78	87	1.64
16	8.70	34	2.77	52	2.02	70	1.77	88	1.64
17	8.62	35	2.60	53	2.00	71	1.76	89	1.63
18	8.50	36	2.50	54	1.98	72	1.75	90	1.63
19	8.34	37	2.42	55	1.96	73	1.74	91	1.62
20	8.14	38	2.36	56	1.94	74	1.73	92	1.62
21	7.88	39	2.32	57	1.92	75	1.72	93	1.61
22	7.60	40	2.29	58	1.90	76	1.71	94	1.60
23	7.28	41	2.26	59	1.89	77	1.70	95	1.60
21	6.92	42	2.23	60	1.88	78	1.69	96	1.59
25	6.53	43	2.20	61	1.87	79	1.69	97	1.59
26	6.08	44	2.18	62	1.86	80	1.68	98	1.58
27	5.61	45	2.16	63	1.85	81	1.68	99	1.58
28	5.12	46	2.14	64	1.83	82	1.67	100	1.57
		1							

# MISCELLANEOUS TABLES,

FOR

COMPARING THE HYGROMETRICAL RESULTS OBTAINED BY DIFFERENT AUTHORITIES.

В



#### MISCELLANEOUS TABLES.

THE object of these Tables is to afford the means of comparing the different determinations of the hygrometrical elements which have been obtained, or adopted, by various physicists, especially the values of the elastic forces of vapor given in other tables than those contained in the preceding pages.

Table XVIII., giving the elastic forces of vapor, expressed in millimetres of mercury, for Centigrade temperatures, was calculated by August from Dalton's experiments, and reduced to French measures in the translation of Kaemtz's *Meteorology*, by Chas. Martins, page 70, from which it has been taken. On these values are based the first psychrometrical tables published by August, in Berlin, 1825.

Table XIX. is the table computed by Kaemtz from his own experiments. It is found, reduced to French measures, in the same volume, page 68.

Table XX. furnishes the results of the experiments made by Professor Magnus, in Berlin, and published in Poggendorf's *Annalen*, Tom. LXI. p. 226, and also in the *Annales de Chimie et de Physique*, 3<sup>me</sup> série, Tom. XII. p. 88, from which this table was copied.

Table XXI. has been published by the Committee of Physics and Meteorology of the Royal Society, in their Report on the Objects of Scientific Inquiry in these Sciences, London, 1840, p. 89. The values which it contains are not derived from new experiments, but are probably computed from those existing at that time.

Table XXII. furnishes a synoptic view of the differences in the values of the force of vapor adopted by various authorities, prepared with the view of facilitating their comparison. A reference to their respective origin will be found below, page 152.

Table XXIII., showing the weight, in grammes, of the vapor contained in a cubic metre of saturated air, at different temperatures, is taken from Pouillet's *Eléments de Physique*, Tom. II. p. 707.

Table XXIV. gives the weights as derived from August's experiments, in Kaemtz's Vorlesungen über Meteorologie. The table is copied from the French translation, by Martins, page 73. The tensions have been added, opposite the weights, and are extracted from August's table.

Table XXV. is found in Biot's Traité de Physique, Tom. I. p. 533.

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## XVIII. ELASTIC FORCE OF AQUEOUS VAPOR,

## EXPRESSED IN MILLIMETRES OF MERCURY FOR EVERY TENTH OF A CENTIGRADE DEGREE.

#### CALCULATED BY AUGUST.

Centigrade					Tenths of	Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
-31	0.45	0.45	0.45	0.44	0.44	0.43	0.43	0.42	0.42	0.41
-30	0.50	0.49	0.49	0.48	0.48	0.47	0.47	0.46	0.46	0.45
-29	0.54	0.54	0.54	0.53	0.53	0.52	0.52	0.51	0.51	0.50
-28	0.59	0.58	0.58	0.57	0.57	0.56	0.56	0.55	0.55	0.54
-27	0.63	0.63	0.63	0.62	0.62	0.61	0.61	0.60	0.60	0.59
-26	0.70	0.69	0.68	0.68	0.67	0.66	0.66	0.65	0.64	0.64
-25	0.77	0.76	0.75	0.75	0.74	0.73	0.73	0.72	0.71	0.71
-24	0.83	0.83	0.82	0.82	0.81	0.80	0.80	0.79	0.78	0.78
-23	0.90	0.89	0.88	0.88	0.87	0.86	0.86	0.85	0.84	0.84
-22	0.99	0.98	0.97	0.96	0.95	0.95	0.94	0.93	0.92	0.91
		ļ								
-21	1.06	1.05	1.04	1.04	1.03	1.02	1.02	1.01	1.00	1.00
-20	1.15	1.14	1.13	1.12	1.11	1.11	1.10	1.09	1.08	1.07
-19	1.26	1.25	1.24	1.23	1.22	1.21	1.20	1.18	1.17	1.16
-18	1.33	1.32	1.31	1.31	1.30	1.29	1.29	1.28	1.27	1.27
-17	1.44	1.43	1.42	1.41	1.40	1.39	1.38	1.36	1.35	1.34
-16	1.56	1.54	1.53	1.52	1.51	1.50	1.49	1.47	1.46	1.45
-15	1.69	1.68	1.67	1.65	1.64	1.63	1.61	1.60	1.59	1.57
-14	1.80	1.79	1.78	1.77	1.76	1.75	1.74	1.72	1.71	1.70
-13	1.96	1.94	1.93	1.91	1.89	1.88	1.86	1.85	1.83	1.82
-12	2.12	2.10	2.09	2.07	2.05	2.04	2.02	2.01	1.99	1.98
		-						}		
-11	2.30	2.28	2.26	2.25	2.23	2.21	2.19	2.17	2.16	2.14
-10	2.48	2.46	2.44	2.43	2.41	2.39	2.37	2.35	2.34	2.32
- 9	2.66	2.64	2.62	2.61	2.59	2.57	2.55	2.53	2.52	2.50
- 8	2.86	2.84	2.82	2.80	2.78	2.76	2.74	2.72	2.70	2.68
- 7	3.09	3.06	3.04	3.02	3.00	2.97	2.95	2.93	2.91	2.88
- 6	3.32	3.29	3.27	3.25	3.23	3.20	3.18	3.16	3.14	3.11
- 5	3.56	3.56	3.54	3.51	3.48	3.46	3.43	3.40	3.37	3.35
- 4	3.83	3.80	3.78	3.75	3.72	3.70	3.67	3.64	3.61	3.59
- 3	4.11	4.07	4.05	4.02	3.99	3.97	3.94	3.91	3.88	3.86
- 2	4.40	4.37	4.34	4.32	4.29	4.26	4.23	4.20	4.17	4.14
	4.57	4.60	4 65	4.62	4.59	4.56	4.53	4.49	4.46	4.43
- 1	4.71	4.68	4.65	4.62	4.59	4.56	4.85	4.49	4.40	4.74
- 0 + 0	5.05 5.05	5.09	5.12	5.16	5.19	5.23	5.27	5.30	5.34	5.37
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centigrade					Tenths o	Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
С	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
ĭ	5.41	5.45	5.49	5.52	5.56	5.60	5.64	5.68	5.72	5.75
2	5.80	5.84	5.88	5.92	5.96	6.00	6.04	6.08	6.13	6.17
3	6.20	6.24	6.29	6.33	6.37	6.41	6.46	6.50	6.54	6.59
4	6.63	6.68	6.72	6.77	6.81	6.86	6.90	6.95	6.99	7.04
5	7.08	7.13	7.18	7.23	7.28	7.33	7.38	7.43	7.48	7.53
6	7.58	7.63	7.68	7.74	7.79	7.84	7.89	7.94	7.99	8.05
7	8.10	8.15	8.21	8.26	8.32	8.37	8.43	8.48	8.53	8.59
8	8.64	8.70	8.76	8.82	8.87	8.93	8.99	9.05	9.11	9.17
9	9.23	9.30	9.36	9.43	9.50	9.57	9.63	9.70	9.77	9.84
10	9.90	9.96	10.02	10.08	10.14	10.20	10.25	10.31	10.37	10.43
11	10.49	10.56	10.63	10.69	10.76	10.83	10.90	10.96	11.03	11.10
12	11.17	11.24	11.31	11.38	11.45	11.52	11.59	11.66	11.73	11.80
13	11.86	11.94	12.02	12.10	12.18	12.26	12.34	12.42	12.50	12.58
14	12.66	12.74	12.82	12.90	12.98	13.05	13.13	13.21	13.29	13.37
15	13.44	13.52	13.61	13.69	13.77	13.86	13.94	14.02	14.11	14.19
16	14.28	14.37	14.47	14.56	14.65	14.74	14.84	14.93	15.02	15.11
17	15.20	15.29	15.38	15.46	15.55	15.64	15.73	15.82	15.90	15.99
18	16.08	16.17	16.27	16.36	16.45	16.54	16.64	16.73	16.82	16.91
19	17.01	17.13	17.25	17.37	17.49	17.61	17.73	17.85	17.97	18.09
20	18.20	18.31	18.43	18.54	18.65	18.76	18.88	18.99	19.10	19.21
21	19.33	19.45	19.56	19.68	19.80	19.92	20.03	20.15	20.27	20.39
22	20.51	20.63	20.76	20.88	21.01	21.13	21.25	21.38	21.50	21.63
23	21.75	21.88	22.00	22.13	22.26	22.38	22.51	22.63	22.76	22.89
24	23.01	23.13	23.24	23.36	23.48	23.60	23.71	23.83	23.95	24.07
25	24.18	24.34	24.50	24.67	24.83	24.99	25.15	25.32	25.48	25.64
26	25.81	25.97	26.13	26.28	26.44	26.60	26.76	26.92	27.07	27.23
27	27.39	27.55	27.71	27.86	28.02	28.18	28.34	28.50	28.65	28.81
28	28.96	29.13	29.29	29.46	29.63	29.79	29.96	30.13	30.30	30.46
29	30.63	30.81	30.98	31.16	31.33	31.51	31.69	31.86	32.04	32.21
30	32.39	32.57	32.76	32.94	33.13	33.31	33.50	33.68	33.87	34.05
31	34.24	34.43	34.63	34.82	35.02	35.21	35.40	35.60	35.79	35.99
32	36.18	36.38	36.59	36.79	36.99	37.20	37.40	37.60	37.80	38.01
33	38.21	38.43	38.64	38.86	39.08	39.29	39.51	39.73	39.94	40.16
34	40.38	40.60	40.82	41.04	41.26	41.49	41.71	41.93	42.15	42.37
35	42.59	42.82	43.05	43.28	43.51	43.74	43.97	44.20	44.43	44.66
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

## XIX. ELASTIC FORCE OF AQUEOUS VAPOR,

#### EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES.

#### By KAEMTZ.

Temper- ature Centi- Grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor,
0	Millim.	0	Millim.	0	Millim.	0	Millim.	0	Millim.
-25	0.68	-12	1.92	ő	4.58	12	10.24	24	21.43
-24	0.72	-11	2.05	1	4.92	13	10.91	25	22.74
-23	0.79	-10	2.21	2	5.26	14	11.62	26	24.16
-22	0.86	- 9	2.39	3	5.64	15	12.38	27	25.56
-21	0.92	- 8	2.57	4	6.01	16	13.17	28	27.07
-20	1.01	- 7	2.78	5	6.45	17	14.03	29	28.67
-19	1.10	- 6	2.98	6	6.90	18	14.93	30	30.36
-18	1.20	- 5	3.20	7	7.38	19	15.86	31	32.17
-17	1.29	- 4	3.45	8	7.89	20	16.87	32	33.95
-16	1.40	- 3	3.70	9	8.41	21	17.91	33	35.95
-15	1.51	- 2	3.97	10	9.00	22	19.04	34	37.99
-14	1.62	- 1	4.26	11	9.58	23	20.21	35	40.15
-13	1.76	0	4.58	12	10.24	24	21.43	36	42.40

## XX. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES.

#### By MAGNUS.

Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.
0	Millim.	0	Millim.	0	Millim.	0	Millim.	0	Millim.
-20	0.916	-7	2.671	6	6.939	19	16.345	32	35.419
-19	0.999	-6	2.886	7	7.436	20	17.396	33	37.473
-18	1.089	-5	3.115	8	7.964	21	18.505	34	39.630
-17	1.186	-4	3.361	9	8.525	22	19.675	35	41.893
-16	1.290	-3	3.624	10	9.126	23	20.909	36	44.268
-15	1.403	-2	3.905	11	9.751	24	22.211	37	46.758
-14	1.525	-1	4.205	12	10.421	25	23.582	38	49.368
-13	1.655	0	4.525	13	11.130	26	25.026	39	52.103
-12	1.796	+1	4.867	14	11.882	27	26.547	40	54.964
-11	1.947	2	5.231	15	12.677	28	28.148	41	57.969
-10	2.109	3	5.619	16	13.519	29	29.832	42	61.109
- 9	2.284	4	6.032	17	14.409	30	31.602	43	64.396
- 8	2.471	5	6.471	18	15.351	31	33.464	44	67.833

## XXI. ELASTIC FORCE OF AQUEOUS VAPOR,

## EXPRESSED IN ENGLISH INCHES OF MERCURY, FOR TEMPERATURES OF FAHRENHEIT.

From the Royal Society's Report.

Temperature of Air.	Force of Vapor.	Temperature of Air.	Force of Vapor.	Temperature of Air.	Force of Vapor.	Temperature of Air.	Force of Vapor.
Fahrenheit.	Eng. Inches.	Fahrenheit.	Eng Inches.	Fahrenheit.	Eng. Inches.	Fahrenheit.	Eng. Inches.
0°	0.051	31°	0.179	62°	0.551	93°	1.514
1	0.053	32	0.186	63	0.570	94	1.562
2	0.056	33	0.193	64	0.590	95	1 610
3	0.058	34	0.200	65	0.611	96	1.660
4	0.060	35	0.208	66	0.632	97 *	1.712
5	0.063	36	0.216	37	0.654	98	1.764
6	0.066	37	0.224	68	0.676	99	1.819
7	0.069	38	0.233	69	0.699	100	1.874
8	0.071	39	0.242	70	0.723	101	1.931
9	0.074	40	0.251	71	0.748	102	1.990
10	0.078	41	0.260	72	0.773	103	2.050
11	0.081	42	0.270	73	0.799	104	2.112
12	0.084	43	0.280	74	0.826	105	2.176
13	0.088	4.4	0.291	75	0.854	106	2.241
14	0.092	45	0.302	76	0.882	107	2.307
15	0.095	46	0.313	77	0.911	108	2.376
16	0.099	47	0.324	78	0.942	109	2.447
17	0.103	48	0.336	79	0.973	110	2.519
18	0.107	49	0.349	80	1.005	111	2.593
19	0.112	50	0.361	81	1.036	112	2.669
20	0.116	51	0.375	82	1.072	113	2.747
21	0.121	52	0.389	83	1.106	114	2.826
22	0.126	53	0.402	84	1.142	115	2.908
23	0.131	54	0.417	85	1.179	116	2.992
24	0.136	55	0.432	86	1.217	117	3.078
25	0.142	56	0.447	87	1.256	118	3.166
26	0.147	57	0.463	88	1.296	119	3.257
27	0.153	58	0.480	89	1.337	120	3.349
28	0.159	59	0.497	90	1.380	121	3.444
29	0.165	60	0.514	91	1.423	122	3.542
30	0.172	61	0.532	92	1.468	123	3.641
31	0.179	62	0.551	93	1.514	124	3.743

#### TABLE XXII.

FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR ADOPTED BY DIFFERENT AUTHORITIES.

The following synoptic view of the values of the elastic force of vapor adopted by various authorities, furnishes the means of readily comparing them, and of appreciating the amount of the differences which they exhibit. The values are given both in English and in French measures.

Dalton's values are copied from the Edinburgh Encyclopædia, Art. Hygrometry. Those adopted in the Greenwich Observations are found in the same article, and also in the volumes published annually by that Observatory. Biot's table of tensions is, in fact, the same, computed by Pouillet from Dalton's results, by Biot's formula, and published in Biot's Traité de Physique, Tom. I. p. 531. Dr. Ure's results are taken from his Memoir in the Philosophical Transactions for 1818, p. 347. In the column headed "Daniell" are given the forces of vapor as found in the table published in his Meteorological Essays, 2d edition, p. 596, a table computed by Galbraith, from Dr. Ure's experiments, by the formula of Ivory.

For the columns headed Royal Society, August, Kaemtz, Magnus, and Regnault, see above, p. 147.

## XXII. FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR, ADOPTED BY DIFFERENT AUTHORITIES.

FORCE OF VAPOR EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES  $\hspace{1.5cm} \text{OF FAHRENHEIT.}$ 

Temper-				Force of	Vapor acc	ording to				Temper-
ature of Air, Fahren- heit.	Dalton.	Green- wich Observa- tions.	Ure.	Daniell.	Royal Society.	August.	Kaemtz.	Magnus.	Regnault.	ature of Air, Fahren- heit.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	0
0	0.064	0.061		0.068	0.051	0.053	0.048	0.044	0.043	0
10	0.090	0.089		0.098	0.078	0.082	0.074	0.070	0.068	10
20	0.129	0.129		0.140	0.116	0.124	0.112	0.108	0.108	20
30	0.186	0.186		0.200	0.172	0.184	0.166	0.164	0.167	30
32	0.200	0.199	0.200	0.216	0.186	0.199	0.180	0.178	0.181	32
40	0.263	0.264	0.250	0.280	0.251	0.269	0.244	0.245	0.248	40
50	0.375	0.373	0.360	0.400	0.361	0.390	0.354	0.359	0.361	50
60	0.524	0.523	0.516	0.560	0.516	0.547	0.505	0.517	0.518	60
70	0.721	0.727	0.726	0.770	0.723	0.766	0.710	0.733	0.733	70
80	1.000	1.001	1.010	1.060	1.005	1.058	0.988	1.025	1.023	80
90	1.360	1.368	1.360	1.430	1.380	1.442	1.354	1.412	1.410	90
95	1.580	1.594	1.640	1.636	1.562	1.677	1.581	1.649	1.647	95
100	1.860	1.852	1.860		1.874			1.921	1.918	100

## FORCE OF VAPOR EXPRESSED IN MILLIMETRES FOR CENTIGRADE TEMPERATURES.

Temper-				Force of	Vapor acc	ording to				Temper-
ature of Air, Centi- grade.	Dalton.	Green- wich Observa- tions.	Biot.	Daniell.	Royal Society.	August.	Kaemtz.	Magnus.	Regnault.	ature of Air, Centi- grade.
0	Millim.	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	0
-20			1.33			1.15	1.01	0.91	0.91	-20
-15	1.93	1.88	1.88	2.11	1.60	1.69	1.51	1.40	1.38	-15
-10	2.64	2.62	2.63	2.92	2.34	2.48	2.21	2.11	2.08	-10
- 5	3.66	3.66	3.66	4.01	3.33	3.56	3.20	3.11	3.13	- 5
0	5.08	5.06	5.06	5.49	4.72	5.05	4.58	4.52	4.60	0
+ 5	6.93	6.95	6.95	7.42	6.60	7.08	6.45	6.47	6.53	+ 5
10	9.52	9.48	9.47	10.16	9.17	9.90	9.00	9.13	9.16	10
15	12.88	12.85	12.84	13.79	12.62	13.44	12.38	12.68	12.70	15
20	17.17	17.30	17.31	18.34	17.17	18.20	16.87	17.40	17.39	20
25	23.11	23.12	23.09	24.54	23.14	24.18	22.74	23.58	23.55	25
30	30.73	30.70	30.64	32.33	30.91	32.39	30.36	31.60	31.55	30
35	40.13	40.47	40.40	41.55	40.89	42.59	40.15	41.89	41.83	35
40			53.00		53.64			54.96	54.91	40

XXIII. WEIGHT OF VAPOR, IN GRAMMES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN  $-20^{\circ}$  AND  $+40^{\circ}$  CENTIGRADE. - POUILLET.

Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor,	Weight of Vapor.
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Centigrade.	Millim	Grammes.
-20°	1.3	1.5	11°	10.1	10.3	26°	24.4	23.8
-15	1.9	2.1	12	10.7	10.9	27	25.9	25.1
-10	2.6	2.9	13	11.4	11.6	28	27.4	26.4
- 5	3.7	4.0	14	12.1	12.2	29	29.0	27.9
0	5.0	5.4	15	12.8	13.0	30	30.6	29.4
+ 1	5.4	5.7	16	13.6	13.7	31	32.4	31.0
2	5.7	6.1	17	14.5	14.5	32	34.3	32.6
3	6.1	6.5	18	15.4	15.3	33	36.2	34.3
4	6.5	6.9	19	16.3	16.2	34	38.3	36.2
5	6.9	7.3	20	17.3	17.1	35	40.4	38.1
6	7.4	7.7	21	18.3	18.1	36	42.7	40.2
7	7.9	8.2	22	19.4	19.1	37	45.0	42.2
8	8.4	8.7	23	20.6	20.2	38	47.6	44.4
9	8.9	9.2	24	21.8	21.3	39	50.1	46.7
10	9.5	9.7	25	23.1	22.5	40	53.0	49.2

XXIV. WEIGHT OF VAPOR, IN GRAMMES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN  $-25^\circ$  AND  $+36^\circ$  CENTIGR. - KAEMTZ.

Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.
-25°	0.77	0.93	-4°	3.83	4.37	16°	14.28	14.97
-24	0.83	1.01	-3	4.11	4.70	17	15.20	15.84
-23	0.90	1.10	-2	4.40	5.01	18	16.08	16.76
-22	0.99	1.19	-1	4.71	5.32	19	17.01	17.75
-21	1.06	1.26	0	5.05	5.66	20	18.20	18.77
-20	1.15	1.38	+1	5.41	6.00	21	19.33	19.82
-19	1.26	1.47	2	5.80	6.42	22	20.51	20.91
-18	1.33	1.60	3	6.20	6.84	23	21.75	22.09
-17	1.44	1.74	4	6.63	7.32	24	23.01	23.36
-16	1.56	1.84	5	7.08	7.77	25	24.18	24.61
-15	1.69	2.00	6	7.58	8.25	26	25.81	25.96
-14	1.80	2.14	7	8.10	8.79	26	27.39	27.34
-13	1.96	2.33	8	8.64	9.30	28	28.96	28.81
-12	2.12	2.48	9	9.23	9.86	29	30.63	30.35
-11	2.30	2.63	10	9.90	10.57	30	32.39	31.93
-10	2.48	2.87	11	10.49	11.18	31	34.24	33.65
- 9	2.66	3.08	12	11.17	11.53	32	36.18	35.45
- 8	2.86	3.30	13	11.86	12.57	33	38.21	37.20
- 7	3.09	3.53	14	12.66	13.33	34	40.38	39.12
- 6	3.32	3.80	15	13.44	14.17	35	42.59	41.13
- 5	3.56	4.08	16	14.28	14.97	36	44.96	43.17
			1		, , , , , ,	11		

## XXV. FORCES OF VAPOR AND RELATIVE HUMIDITY,

CORRESPONDING TO THE DEGREES OF SAUSSURE'S HAIR-HYGROMETER, AT THE TEMPERATURE OF 10° CENTIGRADE.

From the Experiments of Gay-Lussac.

The force of vapor is expressed in hundredths, the tension at full saturation being represented by 100.

		1				[]		1
Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.	Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.	Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.
			0			0		
0	0.00	0.000	34	17.10	0.100	67	43.73	
1	0.45		35	17.68 18.30	0.177	68	44.89 46.04	
2	0.90		36			69 70	47.19	0 (20
3	1.35		37	18.92				0.472
4	1.80		38	19.54		71	48.51	
5	2.25	0.022	39	20.16		72	49.82	0.500
6	2.71	0.022	40	20.78	0.208	73	51.14	0.500
7	3.18		41	21.45	0.200	74	52.45	
8	3.64		42	22.12		75	53.76	0.538
9	4.10		43	22.79		76	55.25	0.550
,	4.10		40	22.10			55.20	
10	4.57	0.046	44	23.46		77	56.74	
11	5.05	0.040	45	24.13	0.241	78	58.24	
12	5.52		46	24.86	0.211	79	59.73	
13	6.00		47	25.59		80	61.22	0.612
14	6.48		48	26.32		81	62.89	0.012
**	0.40		10	20.02	}	01	02.00	
15	6.96	0.070	49	27.06		82	64.57	
16	7.46		50	27.79	0.278	83	66.24	
17	7.95		51	28.58		84	67.92	
18	8.45		52	29.38		85	69.59	0.696
19	8.95		53	30.17		86	71.49	
20	9.45	0.094	54	30.97	-	87	73.39	
21	9.97		55	31.76	0.318	88	75.29	
22	10.49		56	32.66		89	77.19	
23	11.01		57	33.57		90	79.09	0.791
24	11.53		58	34.47		91	81.09	
25	12.05	0.120	59	35.37		92	83.08	
26	12.59		60	36.28	0.363	93	85.08	
27	13.14		61	37.31		94	87.07	
28	13.69		62	38.34		95	89.06	0.891
29	14.23		63	39.36		96	91.25	
				10.50			*	
30	14.78	0.148	64	40.39		97	93.44	
31	15.36		65	41.42	0.414	98	95.63	
32	15.94		66	42.58		99	97.81	
33	16.52		67	43.73		100	100.00	1.000

#### XXVI.

#### TABLE

FOR

DEDUCING THE RELATIVE HUMIDITY IN HUNDREDTHS, FROM THE INDICATIONS OF SAUSSURE'S HAIR-HYGROMETER;

Calculated from the Experiments of Melloni.

By M. T. HAEGHENS.

The Hair-Hygrometer of Saussure having been formerly used for long series of observations, and being still employed by some meteorologists, notwithstanding the imperfection of this instrument, on account of its giving directly the relative humidity without calculation, it was desirable to ascertain the correspondence of the degrees of that hygrometer with the relative humidity expressed in hundredths, as in the preceding table. Though these instruments compared with each other, show very often great discrepancies in their indications, yet a large number of them agree sufficiently well with the experiments of Melloni, August, and others, to allow the following table of comparison to be constructed, which table may be considered as giving good approximations. For the calculation of it, Mr. Haeghens used the results of Melloni, which agree also satisfactorily with a series of observations very carefully made by M. Deleros. See Annuaire Météorologique de la France, pour 1850.

#### RELATIVE HUMIDITY IN HUNDREDTHS.

Degrees of Saussure's Hygrome		Degrees of Saussure's Hygrometer.  Units.													
ter. Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity					
0	0	0	1	1	2	3	3	4	4	5					
1	5	6	6	7	8	8	9	10	11	11					
2	12	12	13	14	15	16	17	18	18	19					
3	19	20	21	22	23	24	24	25	26	26					
4	27	27	28	28	29	30	31	32	33	34					
5	35	36	37	37	38	39	40	41	42	43					
6	44	45	46	47	49	50	51	52	53	55					
7	56	57	58	59	61	62	63	65	66	68					
8	69	70	72	73	75	77	78	79	81	82					
		•													
9	83	85	87	88	9١	91	93	95	97	98					
10	100														

#### TABLE XXVII.

The following Table shows the Relative Humidity, in hundredths, corresponding to the degrees of Saussure's Hair-Hygrometer, as determined by various physicists. It is found in Kaemtz, *Vorlesungen über Meteorologie*, page 100; also in the French translation by Martins, *Cours de Météorologie*, page 80.

XXVI. RELATIVE HUMIDITY, CORRESPONDING TO THE DEGREES OF SAUSSURE'S HAIR-HYGROMETER.

Saturation = 100.

Degrees		Relative Humid	ity according to		Degrees
Hair- Hygrometer.	Gay-Lussac.	Prinsep.	August.	Melloni.	Hair- Hygrometer.
100°	100.0	100.0	100.0	100.0	100°
95	89.1	88.7	94.0	90.8	95
90	79.1	78.2	86.0	83.1	90
85	69.6	68.3	79.0	76.5	85
80	61.2	59.2	71.0	68.9	80
75	53.8	50.6	64.0	62.0	75
70	47.2	43.6	56.0	55.6	70
65	41.4	37.2	48.0	49.6	65
60	36.3	31.5	41.0	44.0	60
55	31.8	26.3	36.0	39.1	55
50	27.8	21.8	31.0	34.6	50
45	24.1	17.7	27.0	29.8	45
40	20.8	14.3	23.0	27.0	40
35	17.7	11.4	19.0	23.8	35
30	14.8	9.1	16.0	19.0	30
		312	2010	1	
25	12.0	7.1	13.0	16.4	25
20	9.4	4.9	10.0	11.7	20
15	7.0	3.0	7.0	8.3	15
10	4.6	1.6	4.0	5.0	10
5	2.2	0.6	2.0	2.6	5
0	0.0	0.0	0.0	0.0	0



## APPENDIX

TO

THE HYGROMETRICAL TABLES.

В



#### TABLES

FOR

## COMPARING THE QUANTITIES OF RAIN-WATER.

The three kinds of measures which are most in use for noting the quantities of rain and melted snow, are the Centimetres and Millimetres in France, the Paris or French inches and lines in Germany, and the English inches and decimals in England, America, and also in Russia, the Russian foot being the same as the English foot. The following tables will facilitate the comparison of these various measures with each other.

A glance at the tables will show that the first column on the left contains the numbers to be converted, and the heads of the following columns the fractions of these numbers, or units, each of which is one tenth of those in the first column. Shorter tables, at the bottom, give, when necessary, the value of proportional parts still smaller than those found in the larger tables.

#### Example.

Let 13 Centimetres be converted into French inches and lines.

Take, in Table II., the line beginning with 10 Centimetres in the first column, follow that line as far as the column headed 3 Centimetres, and there will be found the number of 4 inches 9.63 lines, which is the corresponding value in French inches of 10 + 3, or 13 Centimetres.

If the number is followed by a fraction, as for instance, 13.5 Centimetres, or 135 Millimetres, we find,—

In the larger table 13 Centimetres = 4.9,63In the smaller table at the bottom 5 Millimetres = 2,216Or 13.5 Centimetres = 4.11,846

When the measures which are to be compared are both subdivided into decimal parts, the equivalents of the numbers greater than 9.9 may be found by moving the decimal point.

## Example.

Let 346.7 Centimetres be converted into English inches.

In Table I., in the column headed 4, on the fourth line,

we find 3.4 Centimetres = 1.3386 English inches.

Moving the decimal point by two places we have

340 Centimetres = 133.86 English inches.

Then, in the column headed 7, on the

line beginning with 6, we find 6.7 Centimetres = 2.64

Making together  $\overline{346.7}$  Centimetres =  $\overline{136.50}$  English inches.

B 161

					1	Centimetr	e = 0.3937	079 English	Inch.					
Centi-							Mill	imetres.						
metres		0.	1		2.	3.	4.	5.	6.	7.	8.	9.		
		Eng.Inc	-		Eng.Incl	1 -				1 -	_			
0		0.000			0.0787	-			0.2362	0.2756	0.3150	0.3543		
1 2		0.393 0.787	1		$0.4724 \\ 0.8662$					0.6693	0.7087	0.7480		
3		1.181			1.2599	•		1	1.0236	1.4567	1.1024	1.1418 1.5355		
4		1.574	-		1.6536		1		1.8111	1.8504	1.8898	1.9292		
5	-	1.968			2.0478	1			2.2048	2.2441	2.2835	2.3229		
6	Ì	2.362			2.4410			1	2.5985	2.6378	2.6772	2.7166		
7		2.756	0 2.79	53	2.8347		1	2.9528	2.9922	3.0316	3.0709	3.1103		
8		3.149	7 3.18	90	3.2284	3.2678	3.3071	3.3465	3.3859	3.4253	3.4646	3.5040		
9		3.543	4 3.58	27	3.6221	3.6615	3.7009	3.7402	3.7796	3.8190	3.8583	3.8977		
II. CO	NV	ERSIO	N OF	CEI				CH INCI		ES, AN	D DECIM	IALS.		
	-	Units.												
Centi- metres.		0.	1.		2.	3.	4.	5.	6.	7.	8.	9.		
	Fi	In. Lin.	Fr.In. Li	n. F	r.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.		
0		0,00			0. 8,87			1.10,16						
10	:	3. 8,33	4. 0,	6 -	4. 5,20	4. 9,63	5. 2,06	5. 6,49	5.10,93	6. 3,36	6. 7,79	7. 0,23		
20		4,66			, ,			9. 2,82						
30		,		- 1	, ,	, ,	,	12.11,15	, ,		,	-, -		
40								16. 7,48						
50					, ,	, ,		20. 3,81	, ,		,	- ,-		
60 70		,		- 1	. 1		,	24. 0,14 27. 8,47	,		,	,		
80				- 1			-	31. 4,80	- 1					
90				- [	- 1			35. 1,13	- 1	- 1	,	,		
	_		Fr.ln. Li					Fr.In. Lin.			· · · · ·	Fr.In. Lin.		
		100	36.11,3	- 11	- 1	73.10.59		110.9,89		147.9,18	500	184.8,48		
		CONVI	ERSION	OF	CENT	IMETRE	SINTO	FRENCH	LINES	AND DE	CINALS.			
Centi-							U	nits.						
metres.		0.	1.		2.	3.	4.	5.	6.	7.	8.	9.		
		Fr. Line	1	- 1	Fr. Lines	1	l .	1	1	Fr. Lines.	Fr. Lines.	Fr. Lines.		
0		0.00	1	13	8.87	)	17.73	22.16	26.60	31.03	35.46	39.90		
10		44.33	1	- 1	53.20	1	62.06	66.49	70.93	75.36	79.79	84.23		
20 30		88.66	1	- 1	97.53 141.85		106.39 150.72	110.82	115.26 159.59	119.69 164.02	124.12 168.45	128.56 172.89		
40		177.35	1	- 1	186.18	146.29	195.05	199.48	203.92	208.35	212.78	217.22		
50		221.63		- 1	230.51	234.95	239.38	243.81	248.25	252.68	257.11	261.54		
60		265.98			274.84		283.71	288.14	292.58	297.01	301.44	305.87		
70		310.3		1	319.17		328.04	332.47	336.90	341.34	345.77	350.20		
80		354.6		- 1	363.50			376.80	381.23	385.67	390.10	394.53		
90		398.9	7 403.	10	407.83	412.26	416.70	421.13	425.56	430.00	434.43	438.86		
		CONVE	RSION	of	MILL	IMETRES	INTO	FRENCH	LINES .	AND DE	CIMALS.			
		0.	1.		2.	3.	4.	5.	6.	7.	8.	9.		
		Fr. Line	s. Fr. Li.		Fr. Lines		Fr. Lines 1.773	Fr. Lines. 2.216	Fr. Lines. 2.660	Fr. Lines. 3.103	Fr. Lines. 3.546	Fr. Lines. 3.990		

I English Inch = 2.53995 Centimetres.

			<del></del>	······		τ	Jnits.				
English Inches	0		1.	2.	3.	4.	5.	6.	7.	8.	9.
	Cen		Centin						Centim.	Centim.	Centim.
0	11	.00	2.5					1	17.78	20.32	22.86
10	11	.40	27.9					1	43.18	45.72	48.26
20	II.	.80	53.3	1			1	(	68.58	71.12	73.66
30	11	.20	78.7	1					93.98	96.52	99.06
40	101		104.1	)	1		1		119.38	121.92	124.46
50 60	127 152		129.5	1					144.78	147.32	149.86
70	177		154.9					1	170.18 195.58	172.72 198.12	175.26 200.66
80	203		205.7						220.98	223.52	226.06
90	228		231.1		1	ì			246.38	248.92	251.46
100	254		256.5			1			271.78	274.32	276.85
100	204	.00	250.5	299.00	201.0	204.10	200.70	203.24	211.10	214.02	270.80
110	279	.39	281.9	3 284.43	287.0	1 289.55	292.09	294.63	297.17	299.71	302.25
120	304		307.3						322.57	325.11	327.65
130	330		332.7	1					347.97	350.51	353.05
140	355		358.1			1	1		373.37	375.91	378.45
150	380		383.5					}	398.77	401.31	403.85
160	406		408.9						424.17	426.71	429.25
170	431	.79	434.3	3 436.87	7 439.4	441.93	444.49	447.03	449.57	452.11	454.65
180	457	19	459.7	3 462.27	464.8	467.33	469.89	472.43	474.97	477.51	480.05
190	482	59	485.13	3 487.67	490.2				500.37	502.91	505.45
200	507	.99	510.5	3 513.07	515.6	1 518.15	520.69	523.23	525.77	528.31	530.85
	i i		· <u>·</u>			Tenths	of an Inch.		<u>'</u>		
	0	•	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Cent		Centim			1		1	Centim.	Centim.	Centim.
	0.0		0.254	0.508 OF EN	0.762	1.016	1.270 NTO FR	1.524	1.778	2.032	2.286
						= 0. inches	11.2595 Pa		TOTTES A	IND LIN	es.
Eng.						Un	its.	,			
Inches.	0.		1.	2.	3.	4.	5.	6.	7.	8.	9.
				Fr.In. Lin.							
0				1.10,52							
10		- 1		11. 3,11		,		,		,	,
20				20. 7,71		,		1			,
30				30. 0,30		,			,		,
40 50				39. 4,90		, ,	,				,
60				48. 9,49 58. 2,09	,	,	,	, ,	,	,	,
70		- 1		67. 6,68				, ,			,
80				76.11,28				, ,		, ,	, .
90				86. 3,87							
				Eng.Inch.							
	100		3.9,95		187.7,90		281.5,85		375.3,80		469.1,75
li li						Tenths of	an Inch.				

В

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2.

3.

Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr.In. Lin. | Fr

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#### V. CONVERSION OF FRENCH INCHES INTO CENTIMETRES.

I French Inch = 2.7070 Centimetres.

French	Units.										
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	
0	0.00	2.71	5.41	8.12	10.83	13.53	16.24	18.95	21.66	24.36	
10	27.07	29.78	32.48	35.19	37.90	40.60	43.31	46.02	48.73	51.43	
20	54.14	56.85	59.55	62.26	64.97	67.67	70.38	73.09	75.80	78.50	
30	81.21	83.92	86.62	89.33	92.04	94.74	97.45	100.16	102.87	105.57	
40	108.28	110.99	113.69	116.40	119.11	121.81	124.52	127.23	129.94	132.64	
50	135.35	138.06	140.76	143.47	146.18	148.88	151.59	154.30	157.01	159.71	
			:								
60	162.42	165.13	167.83	170.54	172.25	175.95	178.66	181.37	184.08	186.78	
70	189.49	192.20	194.90	197.61	200.32	203.02	205.73	208.44	211.15	213.85	
80	216.56	219.27	221.97	224.68	227.39	230.09	232.80	235.51	238.22	240.92	
90	243.63	246.34	249.04	251.75	254.46	257.16	259.87	262.58	265.29	267.99	
100	270.70	273.41	276.11	278.82	281.53	284.23	286.94	289.65	292.36	295.06	
110	297.77	300.48	303.18	305.89	308.60	311.30	314.01	316.72	319.42	322.13	
120	324.84	327.55	330.25	332.96	335.67	338.37	341.08	343.79	346.49	349.20	
130	351.91	354.62	357.32	360.03	362.74	365.44	368.15	370.86	373.56	376.27	
140	378.98	381.69	384.39	387.10	389.81	392.51	395.22	397.93	400.63	403.34	
150	406.05	408.76	411.46	414.17	416.88	419.58	422.29	425.00	427.70	430.41	
160	433.12	435.83	438.53	441.24	443.95	446.65	449.36	452.07	454.77	457.48	
170	460.19	462.90	465.60	468.31	471.02	473.72	476.43	479.14	481.84	484.55	
180	487.26	489.97	492.67	495.38	498.09	500.79	503.50	506.21	508.91	511.62	
190	514.33	517.04	519.74	522.45	525.16	527.86	530.57	533.28	535.98	538.69	
200	541.40	544.11	546.81	549.52	552.23	554.93	557.64	560.35	563.05	565.76	

#### CONVERSION OF FRENCH LINES INTO CENTIMETRES.

#### 1 French Line = 0.22558 Centimetre.

French Lines.	Tenths of a Line.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	
0	0.000	0.023	0.045	0.068	0.090	0.113	0.135	0.158	0.180	0.203	
1	0.226	0.248	0.271	0.293	0.316	0.338	0.361	0.383	0.406	0.429	
2	0.451	0.474	0.496	0.519	0.541	0.564	0.587	0.609	0.632	0.654	
3	0.677	0.699	0.722	0.744	0.767	0.790	0.812	0.835	0.857	0.880	
4	0.902	0.925	0.947	0.970	0.993	1.015	1.038	1.060	1.083	1.105	
5	1.128	1.150	1.173	1.196	1.218	1.241	1.263	1.286	1.308	1.331	
6	1.353	1.376	1.399	1.421	1.444	1.466	1.489	1.511	1.534	1.557	
7	1.579	1.602	1.624	1.647	1.669	1.692	1.714	1.737	1.760	1.782	
8	1.805	1.827	1.850	1.872	1.895	1.917	1.940	1.963	1.985	2.008	
9	2.030	2.053	2.075	2.098	2.120	2.143	2.166	2.188	2.211	2.233	
10	2.256	2.278	2.301	2.324	2.346	2.369	2.391	2.414	2.436	2.459	
11	2.481	2.504	2.527	2.549	2.572	2.594	2.617	2.639	2.662	2.684	
12	2.707	2.730	2.752	2.775	2.797	2.820	2.842	2.865	2.887	2.910	

1 French Inch = 1.065765 English Inch.

French	Units.										
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Eng.Inch.	Eng.Inch.	Eng.lnch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Éng.Inch.	Eng.Inch.	
0	0.000	1.066	2.132	3.197	4.263	5.329	6.395	7.460	8.526	9.592	
10	10.658	11.723	12.789	13.855	14.921	15.986	17.052	18.118	19.184	20.250	
20.	21.315	22.381	23.447	24.513	25.578	26.644	27.710	28.776	29.841	30.907	
30	31.973	33.039	34.104	35.170	36.236	37.302	38.368	39.433	40.499	41.565	
40	42.631	43.696	44.762	45.828	46.894	47.959	49.025	50.091	51.157	52.222	
50	53.288	54.354	55.420	56.486	57.551	58.617	59.683	60.749	61.814	62.880	
60	63.946	65.012	66.077	67.143	68.209	69.275	70.340	71.407	72.472	73.538	
70	74.604	75.669	76.735	77.801	78.867	79.932	80.998	82.064	83.130	84.195	
80	85.261	86.327	87.393	88.458	89.524	90.590	91.656	92.722	93.787	94.853	
90	95.919	96.985	98.050	99.116	100.182	101.248	102.314	103.379	104.445	105.511	
100	106.576	107.642	108.708	109.774	110.840	111.905	112.971	114.037	115.103	116.168	
						1					
110	117.234	118.300	119.366	120.431	121.497	122.563	123.629	124.695	125.760	126.826	
120	127.892	128.958	130.023	131.089	132.155	133.221	134.286	135.352	136.418	137.484	
130	138.549	139.615	140.681	141.747	142.813	143.878	144.944	146.010	147.076	148.141	
140	149.207	150.273	151.339	152.404	153.470	154.536	155.602	156.667	157.733	158.799	
150	159.865	160.931	161.996	163.062	164.128	165.194	166.259	167.325	168.391	169.457	
160	170.522	171.588	172.654	173.720	174.785	175.851	176.917	177.983	179.049	180.114	
170				184.377			187.575	188.640	189.706	190.772	
180			193.969				198.232		200.364	201.430	
190			204.627			207.824				212.087	
200						218.482				222.745	

#### CONVERSION OF FRENCH LINES INTO ENGLISH INCHES.

I French Line = 0.088814 English Inch.

French Lines.	Tenths of a Line.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng. Inch.	Eng Inch	
0	0.0000	0.0089	0.0178	0.0266	0.0355	0.0444	0.0533	0.0622	0.0711	0.0799	
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.1687	
2	0.1776	0.1865	0.1954	0.2043	0.2132	0.2220	0.2309	0.2398	0.2487	0.2576	
3	0.2664	0.2753	0.2842	0.2931	0.3020	0.3108	0.3197	0.3286	0.3375	0.3464	
4	0.3553	0.3641	0.3730	0.3819	0.3908	0.3997	0.4085	0.4174	0.4263	0.4352	
5	0.4441	0.4530	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.5240	
6	0.5329	0.5418	0.5506	0.5595	0.5684	0.5773	0.5862	0.5951	0.6039	0.6128	
7	0.6217	0.6306	0.6395	0.6483	0.6572	0.6661	0.6750	0.6839	0.6927	0.7016	
8	0.7105	0.7194	0.7283	0.7372	0.7460	0.7549	0.7638	0.7727	0.7816	0.7904	
9	0.7993	0.8082	0.8171	0.8260	0.8349	0.8437	0.8526	0.8615	0.8704	0.8793	
10	0.8881	0.8970	0.9059	0.9148	0.9237	0.9325	0.9414	0.9503	0.9592	0.9681	
11	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0302	1.0391	1.0480	1.0569	
12	1.0658	1.0746	1.0835	1.0924	1.1013	1.1102	1.1191	1.1279	1.1368	1.145	



# METEOROLOGICAL TABLES.

III.

BAROMETRICAL TABLES.



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### COMPARISON

OF

# THE BAROMETRICAL SCALES,

OR

#### TABLES

FOR CONVERTING THE INDICATIONS OF THE ENGLISH, METRICAL, OLD FRENCH,
AND RUSSIAN BAROMETERS INTO EACH OTHER.



#### COMPARISON

OF

### THE BAROMETRICAL SCALES.

The following tables are intended for converting into each other the four most important Barometrical Scales. They are sufficiently detailed to save the labor of any calculation or even of interpolation for the ordinary wants of Meteorology. But before making use of them, for comparing the observations taken with barometers of different scales, it is necessary to reduce the observed heights to the temperature of the freezing point, or to any other temperature, provided it be the same for all, by means of the tables calculated for this purpose, and which will be found below. The reason of it may be readily understood.

The length of the bars of metal, or of other substances, which represent the standard measures of length which obtain among different nations, varying with the temperature, it was necessary to determine a fixed point of temperature at which they really ought to have the length adopted as the standard unit of measure. This temperature is the *normal* temperature of the standard, and the length of the standard-bar, at this temperature, is the *true* length of it.

If the normal temperature of the various standards used for dividing Barometrical Scales were the same, the heights of the barometrical column, taken with these scales, could be compared directly, provided the scales be made of the same substance, brass, for instance, because their variations above or below this normal temperature would remain parallel with each other. But unfortunately it is not so. The English Yard is a standard at the temperature of 62° Fahrenheit; the Old French Toise, at 13° Reaumur; the Metre, at the freezing point, or zero Centigrade. Thus metallic rods intended to represent these various units of measure give the true or standard length only when at these respective temperatures; at any other temperature they are longer or shorter than the standard, and their subdivisions, inches, lines, or millimetres, partake of the error.

It is obvious, therefore, that the barometrical heights, taken with different scales, cannot be compared directly by means of the following tables, which give the relation between these scales at their respective normal temperatures. For suppose the temperature of the three barometers to be the freezing point, or 32° Fahrenheit,

the scale of the Metrical Barometer alone will actually represent the standard length, and the millimeters will have the true length; while the inches and lines of the Old French and of the English Barometers will be too short, causing thus the barometrical column to appear too high. If the temperature of the instruments be 62° Fahrenheit, the divisions of the English Barometer will have the true standard length, and those of the Old French Barometer nearly so; but the millimeters of the Metrical Barometer will be too long, causing the barometrical column to appear too low. It is to neutralize the effect of those inequalities arising from the expansion of the scale that it is necessary, before comparing the observations taken with the three barometers, to reduce them to the same temperature. This is done by means of the tables above mentioned, for reducing the barometer to the freezing point, which suppose the scales to be of brass from top to bottom, and which take into account the expansion or contraction they undergo by the variations of temperature.

But in doing so, we must be aware that the accuracy of the comparison depends in part upon the correctness of the indications of the attached thermometers, which determine the amount of the correction to be applied for reducing the barometers to the freezing point. If the thermometers do not agree, an error is introduced which will affect the height of the reduced columns, and the final comparison. Therefore the correction of the attached thermometers ought to be ascertained and applied to them before the reduction is made; or if this correction is unknown, it will be well to place the instruments to be compared in the most favorable conditions for taking the same temperature, and then to take the temperature given by one of the thermometers to reduce both barometers. If the correction of the attached thermometer has not been applied before the reduction, it will be contained, after the reduction, in the total correction of the instrument. If it be so, this circumstance must be indicated.

In computing the following tables, the value of the Metre, as determined by Capt. Kater, (Philosoph. Transact. for 1818, p. 109, and Baily's Astronomical Tables, p. 192,) has been adopted, viz. 1 Metre, at 0° Centigrade = 39.37079 English inches, at 62° Fahrenheit. The relation of the Metre (legal) to the Old French system of measures is known to be 1 Metre = 443.296 French or Paris lines. From these equations are derived the elements used in the computations, which are found at the head of each table.

Besides the larger Tables I. - VIII., a set of smaller ones, Tables IX. - XVI., has been added, which will be found useful for comparing Barometrical differences, such as ranges, amount of variation in a given time, &c., expressed in measures of different scales, in which only small quantities occur that are not found in the large tables.

I. - II.

#### COMPARISON

OF

### THE ENGLISH BAROMETER

WITH

THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

# TABLES

FOR CONVERTING ENGLISH INCHES INTO MILLIMETRES, AND INTO FRENCH OR PARIS LINES AND DECIMALS;

GIVING THE VALUES CORRESPONDING TO EVERY TENTH OF AN INCH, FROM 9

TO 19 INCHES; AND TO EVERY HUNDREDTH, FROM

19 TO 31.5 ENGLISH INCHES.

#### USE OF TABLE I.

#### Example.

THE English Barometer reads 20.657 inches. What would be the corresponding height in the Metrical Barometer?

In Table I., first column on the left, look out the line of 20 inches 6 tenths; on that line, in the sixth column, headed 5 hundredths, is found the value in millimetres for

At the bottom of the page, for 
$$0.007$$
 "  $= 0.18$  "  $= 0.007$  "  $= 0.18$  "  $= 0.007$  "  $= 0.18$  "  $= 0.007$  "  $= 0.18$  "  $= 0.007$  "  $= 0.007$  "  $= 0.18$  "  $= 0.007$  "  $= 0.$ 

which would be the reading of the Metrical Barometer.

This example may serve for all tables, throughout the volume, which are constructed on the same plan.

1 English Inch = 25.39954 Millimetres.

English Inches.	0.	1.		1		·				
9	7.7.111		2.	3.	4.	5.	6.	7.	8.	9.
9	Millim.	Millim.	Millim.	Millim.	Millim.	Millim	. Millim.	Millim.	Millim.	Millim.
	228.60	231.14	233.68	236.22	238.76	241.3	243.84	246.38	248.92	251.46
10	254.00	256.54	259.08	261.62	264.16	266.70	269.24	271.78	274.32	276.85
11	279.39	281.93	284.47	287.01	289.55	292.09	9 294.63	297.17	299.71	302.25
12	304.79	307.33	309.87	312.41	314.95	317.49	320.03	322.57	325.11	327.65
13	330 19	332.73	335.27	337.81	340.35	342.89	345.43	347.97	350.51	353.05
14	355.59	358.13	360.67	363.21	365.75	368.29	370.83	373.37	375.91	378.45
15	380.99	383.53	386.07	388.61	391.15	393.69	396.23	398.77	401.31	403.85
16	406.39	408.93	411.47	414.01	416.55	419.09	421.63	424.17	426.71	429.25
17	431.79	434.33	436.87	439.41	441.95	444.49	447.03	449.57	452.11	454.65
18	457.19	459.73	462.27	464.81	467.35	469.89	472.43	474.97	477.51	480.05
					Hundredth	of an l	lnch	1		1
English Inches and tenths.					l	1	1		1	1
tenens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millin		Millim	Millim.	Millim.
19.0	482.59	482.85	483.10	483.35	483.61	483.8	1	484.37	484.62	484.88
1	485.13	485.39	485.64	485.89	486.15	486.4	1	486.91	487.16	487.42
2	487.67	487.93	488.18	488.43	488.69	488.9		489.45	489.70	489.96
3	490.21	490.47	490.72	490.97	491.23	491.4	1	491.99	492.24	492.50
4	492.75	493.01	493.26	493.51	493.77	494.0	2   494.28	494.53	494.78	495.04
5	495.29	495.55	495.80	496.05	496.31	496.5	6 496.81	497.07	497.32	497.58
6	497.83	498.08	493.34	498.59	498.85	499.1	0 499.35	499.61	499.86	500.124
7	500.37	500.62	500.88	501.13	501.39	501.6	4 501.89	502.15	502.40	502.66
8	502.91	503.16	503.42	503.67	503.93	504.1	8 504.43	504.69	504.94	505.20
9	505.45	505.70	505.96	506.21	506.47	506.7	2 506.97	507.23	507.48	507.74
20.0	507.99	508.24	508.50	508.75	509.01	509.2	6 509.51	509.77	510.02	510.28
1	510.53	510.78	511.04	511.29	511.55	511.8	0 512.05	512.31	512.56	512.82
2	513.07	513.32	513.58	513.83	514.09	514.3		514.85	515.10	515.36
3	515.61	515.86	516.12	516.37	516.63	516.8		517.39	517.64	517.90
4	518.15	518.40	518.66	518.91	519.17	519.4		519.93	520.18	520.44
5	520.69	520.94	521.20	521.45	521.71	521.9	6 522.21	522.47	522.72	522.98
6	523.23	523.48	523.74	523.99	524.25	524.5	0 524.75	525.01	525.26	525.52
7	525.77	526.02	526.28	526.53	526.79	527.0	4 527.29	527.55	527.80	528.06
8	528.31	528.56	528.82	529.07	529.33	529.5	8   529.83	530.09	530.34	530:60
9	530.85	531.10	531.36	531.61	531.87	532.1	2 532.37	532.63	532.88	533.14
					dths of an	Inch.				
0.	1.	2.	3.	4	•	5.	6.	7.	8.	9.
0.0	0.03	0.05	0.08	8 0.	10	0.13	0.15	0.18	0.20	0.23

English					Hundredth	s of an Inc	h.			
Inches an tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
010	Millim.	Millim								
21.0	533.39	533.64	533.90 536.44	534.15	534.41	534.66	534.91	535.17	535.42	535.68
$\frac{1}{2}$	535.93 538.47	536.18 538.72	538.98	536.69	536.95	537.20 539.74	537.45	537.71	537.96	538.23
3	541.01	541.26	541.52	541.77	542.03	542.28	542.53	540.25	540.50	540.70
4	543.55	543.80	544.06	544.31	544.57	544.82	545.07	545.33	545.58	543.30
5	546.09	546.34	546.60	546.85	547.11	547.36	547.61	547.87	548.12	548.38
6	548.63	548.88	549.14	549.39	549.65	549.90	550.15	550.41	550.66	550.93
7	551.17	551.42	551.68	551.93	552.19	552.44	552.69	552.95	553.20	553.40
8	553.71	553.96	554.22	554.47	554.73	554.98	555.23	555.49	555.74	556.00
9	556.25	556.50	556.76	557.01	557.27	557.52	557.77	558.03	558.28	558.5
22.0	558.79	559.04	559.30	559.55	559.81	560.06	560.31	560.57	560.82	561.08
1	561.33	561.58	561.84	562.09	562.35	562.60	562.85	563.11	563.36	563.62
2	563.87	564.12	564.38	564.63	564.89	565.14	565.39	565.65	565.90	566.10
3 4	566.41 568.95	566.66 569.20	566.92 569.46	567.17 569.71	567.43 569.97	567.68 570.22	567.93 570.47	568.19 570.73	568.44 570.98	568.70
5	571.49	571.74	572.00	572.25	572.51	572.76	573.01	573.27	573.52	573.78
6	574.03	574.28	574.54	574.79	575.05	575.30	575.55	575.81	576.06	576.32
7	576.57	576.82	577.08	577.33	577.59	577.84	578.09	578.35	578.60	578.86
8	579.11	579.36	579.62	579.87	580.13	580.38	580.63	580.89	581.14	581.40
9	581.65	581.90	582.16	582.41	582.67	582.92	583.17	583.43	583.68	583.9
23.0	584.19	584.44	584.70	584.95	585.21	585.46	585.71	585.97	586.22	586.48
· 1	586.73	586.98	587.24	587.49	587.75	588.00	588.25	588.51	588.76	589.02
2	589.27	589.52	589.78	590.03	590.29	590.54	590.79	591.05	591.30	591.56
3	591.81	592.06	592.32	592.57	592.83	593.08	593.33	593.59	593.84	594.10
4	594.35	594.60	594.86	595.11	595.37	595.62	595.87	596.13	596.38	596.6
5	596.89	597.14	597.40	597.65	597.91	598.16	598.41	598.67	598.92	599.18
6	599.43	599.68	599.94	600.19	600.45	600.70	600.95	601.21	601.46	601.72
7 8	601.97	602.22	602.48	602.73	602.99	603.24	603.49	603.75	604.00	604.26
9	604.51 607.05	604.76 607.30	605.02 607.56	605.27 607.81	605.53 608.06	605.78 608.32	606.03 608.57	606.29 608.83	606.54 609.08	606.79 609.33
24.0	609.59	609.84	610.10	610.35	610.60	610.86	611.11	611.37	611.62	611.87
1	612.13	612.38	612.64	612.89	613.14	613.40	613.65	613.91	614.16	614.41
2	614.67	614.92	615.18	615.43	615.68	615.94	616.19	616.45	616.70	616.95
3	617.21	617.46	617.72	617.97	618.22	618.48	618.73	618.99	619.24	619.49
4	619.75	620.00	620.26	620.51	620.76	621.02	621.27	621.53	621.78	622.03
	J			Thous	andths of	an Inch.				
0.	1.	2.	3.	4.	5		6.	7.	s.	9.
0.0	0.03	0.05	0.08	0.10	0 0.	13 0	).15	0.18	0.20	0.23

24.5 6 7 8 9	Millim. 622.29 624.83 627.37 629.91 632.45	Millim. 622.54 625.08 627.62 630.16 632.70	Millim. 622.80 625.34 627.88 630.42	Millim. 623.05 625.59 628.13	4. Millim. 623.30	5.	6.	7.	8.	9.
6 7 8 9 <b>25.</b> 0	622.29 624.83 627.37 629.91 632.45	622.54 625.08 627.62 630.16	622.80 625.34 627.88	623.05 625.59		Detition				
6 7 8 9 <b>25.</b> 0	624.83 627.37 629.91 632.45	625.08 627.62 630.16	625.34 627.88	625.59	1.623.30	1	Millim.	Millim.	Millim.	Millim.
7 8 9 <b>25</b> .0	627.37 629.91 632.45	627.62 630.16	627.88		1	623.56	623.81	624.07	624.32	624.57
8 9 <b>25</b> .0	629.91 632.45	630.16		600 10	625.84	626.10	626.35	626.61	626.86	627.11
9 <b>25</b> .0 1	632.45		630.42	020.10	628.38	628.64	628.89	629.15	629.40	629.65
<b>25</b> .0		632.70	0001111	630.67	630.92	631.18	631.43	631.69	631.94	632.19
1	634.99		632.96	633.21	633.46	633.72	633.97	634.23	634.48	634.73
		635.24	635.50	637.75	636.00	636.26	636.51	636.77	637.02	637.27
	637.53	637.78	638.04	638.29	638.54	638.80	639.05	639.31	639.56	639.81
2	640.07	640.32	640.58	640.83	641.08	641.34	641.59	641.85	642.10	642.35
3	642.61	642.86	643.12	643.37	643.62	643.88	644.13	644.39	644.64	644.89
4	645.15	645.40	645.66	645.91	646.16	646.42	646.67	646.93	647.18	647.43
5	647.69	647.94	648.20	648.45	648.70	648.96	649.21	649.47	649.72	649.97
6	650.23	650.48	650.74	650.99	651.24	651.50	651.75	652.01	652.26	652.51
7	652.77	653.02	653.28	653.53	653.78	654.04	654.29	654.55	654.80	655.05
8	655.31	655.56	655.82	656.07	656.32	656.58	656.83	657.09	657.34	657.59
9	657.85	658.10	658.36	658.61	658.86	659.12	659.37	659.63	659.88	660.13
<b>26</b> .0	660.39	660.64	660.90	661.15	661.40	661.66	661.91	662.17	662.42	662.67
1	662.93	663.18	663.44	663.69	663.94	664.20	664.45	664.71	664.96	665.21
2	665.47	665.72	665.98	666.23	666.48	666.74	666.99	667.25	667.50	667.75
	668.01		66S.52				}			
3		668.26		668.77	669.02	669.28	669.53	669.79	670.04	670.29
4	670.55	670.80	671.06	671.31	671.56	671.82	672.07	672.33	672.58	672.83
5	673.09	673.34	673.60	673.85	674.10	674.36	674.61	674.87	675.12	675.37
6	675.63	675.88	676.14	676.39	676.64	676.90	677.15	677.41	677.66	677.91
7	678.17	678.42	678.68	678.93	679.18	679.44	679.69	679.95	680.20	680.45
8	680.71	680.96	681.22	681.47	681.72	681.98	682.23	682.49	682.74	682.99
9	683.25	683.50	683.76	684.01	684.26	684.52	684.77	685.03	685.28	685.53
<b>27</b> .0	685.79	686.04	686.30	686.55	686.80	687.06	687.31	687.57	687.82	688.07
1	688.33	688.58	688.84	689.09	689.34	689.60	689.85	690.11	690.36	690.61
2	690.87	691.12	691.38	691.63	691.88	692.14	692.39	692.65	692.90	693.15
3	693.41	693.66	693.92	694.17	694.42	694.68	694.93	695.19	695.44	695.69
4	695.95	696.20	696.46	696.71	696.96	697.22	697.47	697.73	697.98	698.23
5	698,49	698.74	699.00	699.25	699.50	699.76	700.01	700.27	700.52	700.77
i									703.06	703.31
						2	1	1	705.60	705.85
								1	708.14	708.39
9	708.65	708.90	709.16	709.41	709.66	709.92	710.17	710.43	710.68	710.93
5 6 7 8 9	698.49 701.03 703.57 706.11 708.65	698.74 701.28 703.82 706.36 708.90	699.00 701.54 704.08 706.62 709.16	699.25 701.79 704.33 706.87 709.41	699.50 702.04 704.58 707.12 709.66	699.76 702.30 704.84 707.38 709.92	700.01 702.55 705.09 707.63 710.17	700.27 702.81 705.35 707.89 710.43	703 705 708	.06 .60
				Thous	sandths of	an Inch.				
0.	1.	2.	3.	4.		5.	6.	7.	8.	9.
0.0	0.03	0.05	0.08	0.1	0 0	.13	0.15	0.18	0.20	0.23

English				1	Hundredth	s of an	Inch				
Inches and tenths.	0.	1.	2.	3.	4.	5.	•	6.	7.	8.	9.
	Millim.	Millim,	Millim.	Millim.	Millim.	Milli	- 1	Millim.	Millim.	Millim.	Millim.
28.0	711.19	711.44	711.70	711.95	712.20	712.		712.71	712.97	713.22	713.47
1	713.73	713.98	714.24	714.49	714.74	715.0	00	715.25	715 51	715.76	716.01
2	716.27	716.52	716.78	717.03	717.28	717.	54	717.79	718.04	718.30	718.55
3	718.81	719.06	719.31	719.57	719.82	720.0	08	720.33	720.58	720.84	721.09
4	721.35	721.60	721.85	722.11	722.36	722.6	62	722.87	723.12	723.38	723.63
5	723.89	724.14	724.39	724.65	724.90	725.	16	725.41	725.66	725.92	726.17
6	726.43	726.68	726.93	727.19	727.44	727.7	70	727.95	728.20	728.46	728.71
7	728.97	729.22	729.47	729.73	729.98	730.2	24	730.49	730.74	731.00	731.25
8	731.51	731.76	732.01	732.27	732.52	732.7	78	733.03	733.28	733.54	732.79
9	734.05	734.30	734.55	734.81	735.06	735.3	32	735.57	735.82	736.08	736.33
<b>29</b> .0	736.59	736.84	737.09	737.35	737.60	737.8	36	738.11	738.36	738.62	738.87
1	739.13	739.38	739.63	739.89	740.14	740.	- 1	740.65	740.90	741.16	741.41
2	741.67	741.92	742.17	742.43	742.68	742.9		743.19	743.44	743.70	743.95
3	744.21	744.46	744.71	744.97	745.22	745.		745.73	745.98	746.24	746.49
4	746.75	747.00	747.25	747.51	747.76	748.0		748.27	748.52	748.78	749.03
5	749.29	749.54	749 79	750.05	750.30	750.5	56	750.81	751.06	751.32	751.57
6	751.83	752.08	752.33	752.59	752.84	753.1	10	753.35	753.60	753.86	754.11
7	754.37	754.62	754.87	755.13	755.38	755.6	64	755.89	756.14	756.40	756.65
8	756.91	757.16	757.41	757.67	757.92	758.1	- 1	758.43	758.68	758.94	759.19
9	759.45	759.70	759.95	760.21	760.46	760.7	72	760.97	761:22	761.48	761.73
30.0	761.99	762.24	762.49	762.75	763.00	763.2	26	763.51	763.76	764.02	764.27
1	764.53	764.78	765.03	765.29	765.54	765.8	30	766.05	766.30	766.56	766.81
2	767.07	767.32	767.57	767.83	768.08	768.3	34	768.59	768.84	769.10	769.35
3	769.61	769.86	770.11	770.37	770.62	770.9	38	771.13	771.38	771.64	771.89
4	772.15	772.40	772.65	772.91	773.16	773.4		773.67	773.92	774.18	774.43
5	774.69	774.94	775.19	775.45	775.70	775.9	06	776.21	776.46	776.72	776.97
6	777.23	777.48	777.73	777.99	778.24	778.5	60	778.75	779.00	779.26	779.51
7	779.77	780.02	780.27	780.53	780.78	781.0		781.29	781.54	781.80	782.05
S.	782.31	782.56	782.81	783.07	783.32	783.5	- 1	783.S3	784.08	784.34	784.59
9	784.85	785.10	785.35	785.61	785.86	786.1	- 1	786.37	786.62	786.88	787.13
1.0	787.39	787.64	787.89	788.15	788.40	788.6	66	788.91	789.16	789.42	789.67
1	789.93	790.18	790.43	790.69	790.94	791.2	0	791.45	791.70	791.96	792.21
2	792.47	792.72	792.97	793.23	793.48	793.7	- 1	793.99	794.24	794.50	794.75
3	795.01	795.26	795.51	795.77	796.02	796.2		796.53	796.78	797.04	797.29
4	797.55	797.80	798.05	798.31	798.56	798.8	- 1	799.07	799.32	799.58	799.83
				Thous	sandths of	an Incl	h.				
0.	1.	2.	3.	4.		5.	(	6.	7.	8.	9.
0.0	0.03	0.05	0.08	0.1	0 0.	13	0	.15	0.18	0.20	0.23

1 English Inch = 11.2595 French or Paris Lines.

			T Engusu	inen = 1	1.2595 Frei	nelı or Pari	s Lines.			
English					Tenths o	f an Ineh.			2	
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par lines.	Par.lines.	Par.lines.	Par.lines.	Par line
11	123.85	124.98	126.11	127.23	128.36	129.48	130.61	131.74	132.86	133.9
12	135.11	136.24	137.37	138.49	139.62	140.74	141.S7	143.00	144.12	145.2
13	146.37	147.50	148.63	149.75	150.88	152.00	153.13	154.26	155.38	156.5
14	157.63	158.76	159.88	161.01	162.14	163.26	164.39	165.51	166.64	167.7
15	168.89	170.02	171.14	172.27	173.40	174.52	175.65	176.77	177.90	179.0
16	180.15	181.28	182.40	183.53	184.66	185.78	186.91	188.03	189.16	190.2
				Hundre	edths of an	Inch.				
0.	1.	2.	3.	4.		5.	6.	7.	8.	9.
0.000	0.113	0.225	0.338	0.45	0.	563 0	.676	0.788	0.901	1.013
English				I	Inndredth	s of an Inc	h.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par lines.	Par.lines.	Par.lines.	Par.lines.	Par.line
17.0	191.41	191.52	191.64	191.75	191.86	191.97	192.09	192.20	192.31	192.4
1	192.54	192.65	192.76	192.88	192.99	193.10	193.21	193.33	193.44	193.5
2	193.66	193.78	193.89	194.00	194.11	194.23	194.34	194.45	194.56	194.6
3	194.79	194.90	195.01	195.13	195.24	195.35	195.46	195.58	195.69	195.8
4	195.92	196.03	196.14	196.25	196.37	196.48	196.59	196.70	196.82	196.9
5	197.04	197.15	197.27	197.38	197.49	197.60	197.72	197.83	197.94	198.0
6	198.17	198.28	198.39	198.50	198.62	198.73	198.84	198.96	199.07	199.1
7	199.29	199.41	199.52	199.63	199.74	199.86	199.97	200.08	200.19	200.3
8	200.42	200.53	200.64	200.76	200.87	200.98	201.09	201.21	201.32	201.43
9	201.55	201.66	201.77	201.88	202.00	202.11	202.22	202.33	202.45	202.5
18.0	202.67	202.78	202.90	203.01	203.12	203.23	203.35	203.46	203.57	203.68
1	203.80	203.91	204.02	204.13	204.25	204.36	204.47	204.59	204.70	204.8
2	204.92	205.04	205.15	205.26	205.37	205.49	205.60	205.71	205.82	205.9
3	206.05	206.16	206.27	206.39	206.50	206.61	206.72	206.84	206.95	207.00
4	207.17	207.29	207.40	207.51	207.63	207.74	207.85	207.96	208.08	208.19
5	208.30	208.41	208.53	208.64	208.75	208.86	208.98	209.09	209.20	209.31
6	209.43	209.54	209.65	209.76	209.88	209.99	210.10	210.21	210.33	210.4
7	210.55	210.67	210.78	210.89	211.00	211.12	211.23	211.34	211.45	211.57
8	211.68	211.79	211.90	212.02	212.13	212.24	212.35	212.47	212.58	212.69
9	212.80	212.92	213.03	213.14	213.25	213.37	213.48	213.59	213.71	213.82
19.0	213.93	214.04	214.16	214.27	214.38	214.49	214.61	214.72	214.83	214.94
1	215.06	215.17	215.28	215.39	215.51	215.62	215.73	215.84	215.96	216.07
2	216.18	216.29	216.41	216.52	216.63	216.75	216.86	216.97	217.08	217.20
3	217.31	217.42	217.53	217.65	217.76	217.87	217.98	218.10	218.21	218.32
4	218.43	218.55	218.66	218.77	218.88	219.00	219.11	219.22	219.34	219.45
5	219.56	219.67	219.79	219.90	220.01	220.12	220.24	220.35	220.46	220.57
6	220.69	220.80	220.91	221.02	221.14	221.25	221.36	221.47	221.59	221.70
7	221.81	221.92	222.04	222.15	222.26	222.38	222.49	222.60	222.71	222.83
8	222.94	223.05	223.16	223.28	223.39	223.50	223.61	223.73	223.84	223.95
9	221.06	224.18	224.29	224.40		224.63	224.74	224.85	224.96	225.08

1 English Inch = 11.2595 French or Paris Lines.

English nches and				I	Iundredths	of an Incl	n.			
Tonths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
20	Par.lines.	Par.lines.		Par.lines.	Par.lines.	Par.lines.			Par.lines.	Par.line
20.0	225.19	225.30	225.42	225.53	225.64	225.75	225.87	225.98	226.09	226.2
1	226.32	226.43	226.54	226.65	226.77	226.88	226.99	227.10	227.22	227.3
2	227.44	227.55	227.67	227.78	227.89	228.00	228.12	228.23	228.34	228.4
3	228.57	228.68	228.79	228.91	229.02	229.13	229.24	229.36	229.47	229.5
4	229.69	229.81	229.92	230.03	230.14	230.26	230.37	230.48	230.59	230.7
5	230.82	230.93	231.04	231.16	231.27	231.38	231.50	231.61	231.72	231.8
6	231.95	232.06	232.17	232.28	232.40	232.51	232.62	232.73	232.85	232.9
7	233.07	233.18	233.30	233.41	233.52	233.63	233.75	233.86	233.97	234.0
8	234.20	234.31	234.42	234.54	234.65	234.76	234.87	234.99	235.10	235.2
9	235.32	235.44	235.55	235.66	235.77	235.89	236.00	236.11	236.22	236.3
21.0	236.45	236.56	236.67	236.79	236.90	237.01	237.13	237.24	237.35	237.4
1	237.58	237.69	237.80	237.91	238.03	238.14	238.25	238.36	238.48	238.5
2	238.70	238.81	238.93	239.04	239.15	239.26	239.38	239.49	239.60	239.7
3	239.83	239.94	240.05	240.17	240.28	240.39	240.50	240.62	240.73	240.8
4	240.95	241.07	241.18	241.29	241.40	241.52	241.63	241.74	241.85	241.9
5	242.08	242.19	242.30	242.42	242.53	242.64	242.75	242.87	242.98	243.0
6	243.21	243.32	243.43	243.54	243.66	243.77	243.88	243.99	244.11	244.2
7	244.33	244.44	244.56	244.67	244.78	244.89	245.01	245.12	245.23	245.3
8	245.46	245.57	245.68	245.79	245.91	246.02	246.13	246.25	246.36	246.4
9	246.58	246.70	246.81	246.92	247.03	247.15	247.26	247.37	247.48	247.6
22.0	247.71	247.S2	247.93	248.05	248.16	248.27	248.38	248.50	248.61	248.7
1	248.83	248.95	249.06	249.17	249.29	249.40	249.51	249.62	249.74	249.8
2	249.96	250.07	250.19	250.30	250.41	250.52	250.64	250.75	250.86	250.9
3	251.09	251.20	251.31	251.42	251.54	251.65	251.76	251.88	251.99	252.1
4	252.21	252.33	252.44	252.55	252.66	252.78	252.89	253.00	253.11	253.2
5	253.34	253.45	253.56	253.68	253.79	253.90	254.01	254.13	254.24	254.3
6	254.46	254.58	254.69	254.80	254.92	255.03	255.14	255.25	255.37	255.4
7	255.59	255.70	255.82	255.93	256.04	256.15	256.27	256.38	256.49	256.6
8	256.72	256.83	256.94	257.05	257.17	257.28	257.39	257.50	257.62	257.7
9	257.81	257.96	258.07	258.18	258.29	258.41	258.52	258.63	258.74	258.8
23.0	258.97	259.08	259.19	259.31	259.42	259.53	259.64	259.76	259.87	259.9
1	260.09	260.21	260.32	260.43	260.54	260.66	260.77	260.88	261.00	261.1
2	261.22	261.33	261.45	261.56	261.67	261.78	261.90	262.01	262.12	262.2
3	262.35	262.46	262.57	262.68	262.80	262.91	263.02	263.13	263.25	263.3
4	263.47	Į.	263.70	263.81	263.92	264.04	264.15	264.26	1	264.4
5	264.60	264.71	264.82	264.94	265.05	265.16	265.27	265.39	265.50	265.6
6	265.72	265.84	265.95	266.06	266.17	266.29	266.40	266.51	266.62	266.7
7	266.85	266.96	267.08	267.19	267.30	267.41	267.53	267.64	267.75	267.8
8	267.98	268.09	268.20	268.31	268.43	268.54	268.65	268.76	268.88	268.9
9	269.10	269.21	269.33	269.44	269.55	269.67	269.78	269.89	270.00	270.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 English Inch = 11.2595 French or Paris Lines.

English				H	lundredths	of an Inch	1.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	L.	Par.lines.	Par.lines
24.0	270.23	270.34	270.45	270.57	270.68	270.79	270.90	271.02	271.13	271.24
1	271.35	271.47	271.58	271.69	271.80	271.92	272.03	272.14	272.25	272.37
2	272.48	272.59	272.71	272.82	272.93	273.04	273.16	273.27	273.38	273.49
3	273.61	273.72	273.83	273.94	274.06	274.17	274.28	274.39	274.51	274.62
4	274.73	274.84	274.96	275.07	275.18	275.29	275.41	275.52	275.63	275.75
5	275.86	275.97	276.03	276.20	276.31	276.42	276.53	276.65	276.76	276.87
6	276.98	277.10	277.21	277.32	277.43	277.55	277.66	277.77	277.88	278.00
7	278.11	278.22	278.33	278.45	278.56	278.67	278.79	278.90	279.01	279.12
8	279.24	279.35	279.46	279.57	279.69	279.80	279.91	280.02	280.14	280.2
9	280.36	280.47	280.59	280.70	280.81	280.92	281.04	281.15	281.26	281.38
<b>25</b> .0	281.49	281.60	281.71	281.83	281.94	282.05	282.16	282.28	282.39	282.50
1	282.61	282.73	282.84	282.95	283.06	283.18	283.29	283.40	283.51	283.63
2	283.74	283.S5	283.96	284.08	284.19	284.30	284.41	284.53	284.64	284.7
3	284.87	284.98	285.09	285.20	285.32	285.43	285.54	285.65	285.77	285.88
4	285.99	286.10	286.22	286.33	286.44	286.55	286.67	286.78	286.89	287.00
5	287.12	287.23	287.34	287.46	287.57	287.68	287.79	287.91	288.02	288.1
6	288.24	288.36	288.47	288.58	288.69	288.81	288.92	289.03	289.14	289.2
7	289.37	289.48	289.59	289.71	289.82	289.93	290.04	290.16	290.27	290.38
8	290.50	290.61	290.72	290.83	290.95	291.06	291.17	291.28	291.40	291.5
9	291.62	291.73	291.85	291.96	292.07	292.18	292.30	292.41	292.52	292.63
<b>26</b> .0	292.75	292.86	292.97	293.08	293.20	293.31	293.42	293.54	293.65	293.70
1	293.87	293.99	294.10	294.21	294.32	294.44	294.55	29-1.66	294.77	294.8
2	295.00	295.11	295.22	295.34	295.45	295.56	295.67	295.79	295.90	296.0
3	296.12	296.24	296.35	296.46	296.58	296.69	296.80	296.91	297.03	297.1-
4	297.25	297.36	297.48	297.59	297.70	297.81	297.93	298.04	298.15	298.20
5	298.38	298.49	298.60	298.71	298.83	298.94	299.05	299.17	299.28	299.3
6	299.50	299.62	299.73	299.84	299.95	300.07	300.18	300.29	300.40	300.5
7	300.63	300.74	300.85	300.97	301.08	301.19	301.30	301.42	301.53	301.6
8	301.75	301.87	301.98	302.09	302.20	302.32	302.43	302.54	302.66	302.7
9	302.88	302.99	303.11	303.22	303.33	303.44	303.56	303.67	303.78	303.8
27.0	304.01	304.12	304.23	304.34	304.46	304.57	304.68	304.79	304.91	305.0
1	305.13	305.25	305.36	305.47	305.58	305.70	305.81	305.92	306.03	306.1
2	306.26	306.37	306.48	306.60	306.71	306.82	306.93	307.05	307.16	307.2
3	307.38	307.50	307.61	307.72	307.83	307.95	308.06	308.17	308.29	308.40
4	308.51	308.62	308.74	308.85	308.96	309.07	309.19	309.30	309.41	309.5
5	309.61	309.75	309.86	309.97	310.09	310.20	310.31	310.42	310.54	310.6
6	310.76	310.87	310.99	311.10	311.21	311.33	311.44	311.55	311.66	311.78
7	311.89	312.00	312.11	312.23	312.34	312.45	312.56	312.68	312.79	312.9
8	313.01	313.13	313.21	313.35	313.46	313.58	313.69	313.80	313.91	314.03
9	314.14	314.25	314.37	314.48	314.59	314.70	314.82	314.93	315.04	315.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 English Inch = 11.2595 French or Paris Lines.

English				I	Hundredth:	of an In	ch.			
Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
20	Par.lines.	Par.lines,	Par.lines.	Par.lines.			. Par.lines	j.		1
28.0	315.27	315.38	315.49	315.60	315.72	315.83		1		316.28
1	316.39	316.50	316.62	316.73	316.84	316.95	1	317.1		317.4
2	317.52	317.63	317.74	317.86	317.97	318.08	1	318.3		318.5
3	318.64	318.76	318.87	318.98	319.09	319.21	319.32	319.4		319.6
4	319.77	319.88	319.99	320.11	320.22	320.33	320.45	320.5	6 320.67	320.7
5	320.90	321.01	321.12	321.23	321.35	321.46	1	321.6	8 321.80	321.9
6	322.02	322.13	322.25	322.36	322.47	322.58	322.70	322.8	1   322.92	323.0
7	323.15	323.26	323.37	323.49	323.60	323.71	323.82	323.9	4   324.05	324.1
8	324.27	324.39	324.50	324.61	324.72	324.84	324.95	325.0	6 325.17	325.2
9	325.40	325.51	325.62	325.74	325.85	325.96	326.08	326.1	9   326.30	326.4
<b>29</b> .0	326.53	326.64	326.75	326.86	326.98	327.09	327.20	327.3	1 327.43	327.5
1	327.65	327.76	327.88	327.99	328.10	328.21	328.33	328.4	4 328.55	328.6
2	328.78	328.89	329.00	329.12	329.23	329.34	329.45	329.5	7   329.68	329.7
3	329.90	330.02	330.13	330.24	330.35	330.47	330.58	330.6	9 330.80	330.9
4	331.03	331.14	331.25	331.37	331.48	331.59	331.70	331.8	2   331.93	332.0
5	332.16	332.27	332.38	332.49	332.61	332.72	332.83	332.9	4 333.06	333.1
6	333.28	333.39	333.51	333.62	333.73	333.84	333.96	334.0	7   334.18	334.2
7	334.41	334.52	334.63	334.74	334.86	334.97	335.08	335.2	1	335.4
8	335.53	335.65	335.76	335.87	335.98	336.10	336.21	336.3	2 336.43	336.5
9	336.66	336.77	336.88	337.00	337.11	337.22	337.33	337.4	5 337.56	337.6
30.0	337.78	337.90	338.01	338.12	338.24	338.35	338.46	338.5	7 338.69	338.8
1	338.91	339.02	339.14	339.25	339.36	339.47	339.59	339.7	1	339.9
2	340.04	340.15	340.26	340.37	340.49	340.60	(	340.8	1	341.0
3	341.16	341.28	341.39	341.50	341.61	341.73	341.84	341.9		342.1
4	342.29	342.40	342.51	342.63	342.74	342.85	342.96	343.0	S 343.19	343.3
5	343.41	343.53	343.64	343.75	343.87	343.98	344.09	344.2	0 344.32	344.4
6	314.54	344.65	344.77	344.88	344.99	345.10	345.22	345.3		345.5
7	345.67	345.78	345.89	346.00	346.12	346.23	346.34	346.4		346.6
8	346.79	346.91	347 02	347.13	347.24	347.36	347.47	347.5		347.8
9	347.92	348.03	348.14	348.26	348.37	348.48	348.59	348.7		348.9
31.0	349.04	349.16	349.27	349.38	349.49	349.61	349.72	349.8	3 349.95	350.0
1	350.17	350.28	350.40	350.51	350.62	350.73	350.85	350.9		351.1
2	351.30	351.41	351.52	351.63	351.75	351.86	351.97	352.0	1	352.3
3	352.42	352.53	352.65	352.76	352.87	352.99	353.10	353.2	1	353.4
4	353.55	353.66		353.89	354.00	354.11		354.3	1	354.50
5	354.67	354.79	354.90	355.01	355.12	355.24	355.35	355.4		355.6
6	355.80	355.91	356.03	356.14	356.25	356.36	356.48	356.5		356.8
				Thousan	dths of an	Inch.				
0.	1.	2.	3.	4.	6	5.	6.	7.	8.	9.

III. - IV.

#### COMPARISON

OF

### THE METRICAL BAROMETER

WITH

THE ENGLISH AND THE OLD FRENCH BAROMETERS,

OR

#### TABLES

FOR CONVERTING MILLIMETRES INTO ENGLISH INCHES AND DECIMALS,
AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY MILLIMETRE FROM 250 TO 600; AND TO EVERY TENTH OF A MILLIMETRE FROM 600 TO 800 MILLIMETRES.



1 Metre = 39.37079 English Inches.

Millime-					Millimetre	es. Ur	nits.				
tres.			1			<u> </u>	1				<u> </u>
Tens.	0.	1.	2.	3.	4.	5	•	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng.	·	Eng. In.	Eng. I	Eng. In.	Eng. In.
250	9.843	9.882	9.921	9.961	10.000	10.0		10.079	10.11		10.197
260	10.236	10.276	10.315	10.355	10.394	10.4	33	10.473	10.51	2 10.551	10.591
270	10.630	10.669	10.709	10.748	10.788	10.8	27	10.866	10.90	6 10.945	10.984
280	11.024	11.063	11.103	11.142	11.181	11.2	21	11.260	11.29	9 11.339	11.378
290	11.418	11.457	11.496	11.536	11.575	11.6	14	11.654	11.69	3 11.732	11.772
300	11.811	11.851	11.890	11.929	11.969	12.0	08	12.047	12.08	7 12.126	12.166
310	12.205	12.244	12.284	12.323	12.362	12.4	02	12.441	12.48	1 12.520	12.559
320	12.599	12.638	12.677	12.717	12.756	12.7	95	12.835	12.87	4 12.914	12.953
330	12.992	13.032	13.071	13.110	13.150	13.1	89	13.229	13.26	8 13.307	13.547
340	13.386	13.425	13.465	13.504	13.544	13.5	83	13.622	13.66	2   13.701	13.740
350	13.780	13.819	13.859	13.898	13.937	13.9	77	14.016	14.05	5 14.095	14.134
360	14.173	14.213	14.252	14.292	14.331	14.3	70	14.410	14.44	9 14.488	14.528
370	14.567	14.607	14.646	14.685	14.725	14.7	64	14.803	14.84	3 14.882	14.922
380	14.961	15.000	15.040	15.079	15.118	15.1	58	15.197	15.23	6 15.276	15.315
390	15.355	15.494	15.433	15.473	15.512	15.5	51	15.591	15.63	0 15.670	15.709
400	15.748	15.788	15.827	15.866	15.906	15.9	45	15.985	16.02	4 16.063	16.103
410	16.142	16.181	16.221	16.260	16.300	16.3	39	16.378	16.41	8 16.458	16.496
420	16.536	16.575	16.614	16.654	16.693	16.73	33	16.772	16.81	1 16.851	16.890
430	16.929	16.969	17.008	17.048	17.087	17.1	26	17.166	17.20	5 17.244	17.284
440	17.323	17.362	17.402	17.441	17.481	17.5	20	17.559	17.59	9 17.638	17.677
450	17.717	17.756	17.796	17.835	17.874	17.9	14	17.953	17.99	2 18.032	18.071
460	18.111	18.150	18.189	18.229	18.268	18.30	07	18.347	18.38	3 18.426	18.465
470	18.504	18.544	18.583	18.622	18.662	18.70	01	18.740	18.78	18.819	18.859
480	18.898	18.937	18.977	19.016	19.055	19.09	95	19.134	19.17	19.213	19.252
490	19.292	19.331	19.370	19.410	19.449	19.48	39	19.528	19.56	7 19.607	19.646
500	19.685	19.725	19.764	19.804	19.843	19.88	32	19.922	19.96	20.000	20.040
510	20.079	20.118	20.158	20.197	20.237	20.27	- 1	20.315	20.35	1	20.433
520	20.473	20.512	20.552	20.591	20.630	20.67		20.709	20.748		20.827
530	20.867	20.906	20.945	20.985	21.024	21.06		21.103	21.142	1	21.221
540	21.260	21.300	21.339	21.378	21.418	21.43	57	21.496	21.536	21.575	21.615
550	21.654	21.693	21.733	21.772	21.811	21.83		21.890	21.930	1	22.008
560	22.048	22.087	22.126	22.166	22.205	22.2		22.284	22.323		22.402
570	22.441	22.481	22.520	22.559	22.599	22.63		22.678	22.717		22.796
580	22.835	22.874	22.914		22.993			23.071			23.189
590	23.229	23.268	23.308	23.347	23.386	23.42	26   2	23.465	23.504	23.544	23.583
	· · · · · · · · · · · · · · · · · · ·		,	Tenths	of Millime	etres.					
0.	1.	2.	3.	4.	5	i.	6	.	7.	8.	9.
					-						
0.000	0.004	0.008	0.012	0.01	b   0.0	20	0.0	24   0	.028	0.031	0.035

1 Metre = 39.37079 English Inches.

Millime-					Tenths of	Millimetres	•			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. 1
600	23.622	23.626	23.630	23.634	23.638	23.642	23.646	23.650	23.654	23.6
601	23.662	23.666	23.670	23.674	23.678	23.682		23.689	23.693	23.69
602	23.701	23.705	23.709	23.713		23.721	23.725	23.729	23.733	23.7
603	23.741	23.745	23.748	23.752	23.756	23.760	23.764	23.768 23.808	23.772	23.7
604	23.780	23.784	23.788	23.792	23.796	23.800	23.804	23.808	23.811	23.8
605	23.819	23.823	23.827	23.831	23.835	23.839	23.843	23.847	23.851	23.8
606	23.859	23.863	23.867	23.871	23.874	23.878	23.882	23.886	23.890	23.8
607	23.898	23.902	23.906	23.910	23.914	23.918	23.922	23.926	23.930	23.9
608	23.937	23.941	23.945	23.949	23.953	23.957	23.961	23.965	23.969	23.9
609	23.977	23.981	23.985	23.989	23.993	23.996	24.000	24.004	24.008	24.0
610	24.016	24.020	24.024	24.028	24.032	24.036	24.040	24.044	24.048	24.0
611	24.056	24.059	24.063	24.067	24.071	24.075	24.079	24.083	24.087	24.0
612	24.095	24.099	24.103	24.107	24.111	24.115	24.119	24.122	24.126	24.1
613	24.134	24.138	24.142	24.146	24.150	24.154	24.158	24.162	24.166	24.1
614	24.174	24.178	24.182	24.185	24.189	24.193	24.197	24.201	24.205	24.2
615	24.213	24.217	24.221	24.225	24.229	24.233	24.237	24.241	24.245	24.2
616	24.252	24.256	24.260	24.264	24.268	24.272	24.276	24.280	24.284	24.2
617	24.292	24.296	24.300	24.304	24.308	24.311	24.315	24.319	24.323	24.3
618	24.331	24.335	24.339	24.343	24.347	24.351	24.355	24.359	24.363	24.3
619	24.371	24.374	24.378	24.382	24.386	24.390	24.394	24.398	24.402	24.4
620	24.410	24.414	24.418	24.422	24.426	24.430	24.434	24.437	24.441	24.4
621	24.449	24.453	24.457	24.461	24.465	24.469	24.473	24.477	24.481	24.48
622	24.489	24.493	24.497	24.500	24.504	24.508	24.512	24.516	24.520	24.5
623	24.528	24.532	24.536	24.540	24.544	24.548	24.552	24.556	24.559	24.50
624	24.567	24.571	24.575	24.579	24.583	24.587	24.591	24.595	24.599	24.6
625	24.607	24.611	24.615	24.619	24.622	24.626	24.630	24.634	24.638	24.6
626	24.646	24.650	24.654	24.658	24.662	24.666	24.670	24.674	24.678	24.6
627	24.685	24.689	24.693	24.697	24.701	24.705	24.709	24.713	24.717	24.7
628	24.725	24.729	24.733	24.737	24.741	24.745	24.748	24.752	24.756	24.7
629	24.764	24.768	24.772	24.776	24.780	24.784	24.788	24.792	24.796	24.8
630	24.804	24.808	24.811	24.815	24.819	24.823	24.827	24.831	24.835	24.8
631	24.843	24.808	24.851	24.855	24.819	24.863	24.827	24.831	24.835	24.8
632	24.882	24.886	24.890	24.894	24.898	24.503	24.807	24.910	24.914	24.9
633	24.922	24.926	24.930	24.934	24.937	24.941	24.945	24.910	24.953	24.9
634	24.961	24.965	24.969	24.973		24.981	24.985	24.989	24.993	
635	25.000	25.004	25.008	25.012	25.016	25.020	25.024	25.028	25.032	25.0
636	25.040	25.044	25.048	25.052	25.056	25.060	25.063	25.067	25.071	25.07
637	25.079	25.083	25.087	25.091	25.095	25.099	25.103	25.107	25.111	25.1
638	25.119	25.123	25.126	25.130	25.134	25.138	25.142	25.146	25.150	25.13
639	25.158	25.162	25.166	25.170	25.174	25.178	25.182	25.185	25.189	25.19
	0.	1.	2.	3.				7.	8.	9.

1 Metre = 39.37079 English Inches

640 25.19 641 25.29 642 25.29 643 25.33 644 25.34 645 25.49 646 25.49 647 25.47 648 25.5 650 25.56 651 25.66 652 25.66 653 25.77 655 25.77 656 25.89 659 25.99 660 25.98 661 26.06									
640         25.19           641         25.22           642         25.22           643         25.3           644         25.33           645         25.44           647         25.47           648         25.53           650         25.56           651         25.66           652         25.67           654         25.77           655         25.86           657         25.86           659         25.99           660         25.98           661         26.00           663         26.14           664         26.14           665         26.36           667         26.36           669         26.33           670         26.37           671         26.41           672         26.41           673         26.41           674         26.53           675         26.53	0.	1. 2.	3.	4.	5.	6.	7.	8.	9.
641         25.2:           642         25.2:           643         25.3:           644         25.3:           645         25.4:           647         25.4:           648         25.5:           650         25.5:           651         25.6:           652         25.6:           653         25.7:           654         25.7:           655         25.8:           657         25.8:           659         25.9:           660         25.9:           661         26.0:           662         26.0:           663         26.1:           664         26.1:           665         26.3:           666         26.2:           667         26.3:           668         26.3:           669         26.3:           670         26.3:           671         26.4:           672         26.1:           673         26.4:           674         26.5:           675         26.5:		ng. In. Eng. 1 5.201 25.20		Eng In. 25.213	Eng. In. 25.217	Eng. In. 25.221	Eng. In. 25.225	Eng. In. 25.229	Eng. Ir 25.23
642         25.2'           643         25.3'           644         25.3'           645         25.3'           646         25.4'           647         25.5'           648         25.5'           650         25.5'           651         25.6'           652         25.6'           653         25.7'           654         25.7'           655         25.8'           657         25.8'           659         25.9'           660         25.9'           661         26.0'           662         26.0'           663         26.1'           664         26.1'           665         26.3'           666         26.2'           667         26.2'           668         26.3'           670         26.3'           671         26.4'           672         26.1'           673         26.4'           674         26.5'           675         26.5'		5.241 25.2		25.252	25 256	25.260	25.264	25.268	25.27
643         25.3           644         25.3           645         25.3           646         25.4           647         25.4           648         25.5           650         25.5           651         25.6           652         25.6           653         25.7           654         25.7           655         25.8           657         25.8           659         25.9           660         25.9           661         26.0           662         26.0           663         26.1           664         26.1           665         26.3           667         26.2           668         26.3           669         26.3           670         26.3           671         26.41           672         26.41           673         26.41           674         26.53           675         26.55		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	25.292	25.296	25.300	25.304	25.203	25.21
644         25.33           645         25.33           646         25.43           647         25.47           648         25.5           649         25.53           650         25.53           651         25.63           652         25.67           653         25.77           656         25.83           657         25.86           659         25.93           660         25.98           661         26.06           662         26.06           663         26.14           665         26.33           667         26.26           668         26.33           670         26.37           671         26.41           672         26.13           673         26.41           674         26.53           675         26.55		5.319 25.33		25.331	25.335	25.339	25.343	25.347	25.35
646         25.44           647         25.4           648         25.5           649         25.5           650         25.55           651         25.66           652         25.67           653         25.77           654         25.78           657         25.86           658         25.96           661         26.06           662         26.06           663         26.16           664         26.14           665         26.36           669         26.33           670         26.33           671         26.41           672         26.13           673         26.44           674         26.53           675         26.55		$\begin{bmatrix} 25.35 \\ 25.36 \end{bmatrix}$	1	25.371	25.374	25.378	25.382	25.386	25.39
647         25.4'           648         25.5'           649         25.5'           650         25.5'           651         25.6'           652         25.6'           653         25.7'           654         25.7'           655         25.9'           657         25.8'           658         25.9'           661         26.0'           662         26.0'           663         26.1'           664         26.2'           667         26.2'           668         26.3'           669         26.3'           670         26.3'           671         26.41           672         26.1'           673         26.1'           674         26.5'           675         26.5'	5.394 25	5.398 25.40	25.406	25.410	25.414	25.418	25.422	25.426	25.43
648         25.5           649         25.5           650         25.55           651         25.6           652         25.6           653         25.7           654         25.7           655         25.8           657         25.8           658         25.9           661         26.0           662         26.0           663         26.1           664         26.2           667         26.2           668         26.3           669         26.3           670         26.3           671         26.41           672         26.1           673         26.4           674         26.5           675         26.5	5.434 25	5.437 25.4-	11 25.445	25.449	25.453	25.457	25.461	25.465	25.46
649         25.53           650         25.53           651         25.63           652         25.63           653         25.76           654         25.78           655         25.83           657         25.86           659         25.99           661         26.02           662         26.06           663         26.16           664         26.26           667         26.26           668         26.33           669         26.33           670         26.37           671         26.41           672         26.13           673         26.42           674         26.53           675         26.53	5.473 25	5.477 25.48	25.485	25.489	25.493	25.497	25.500	25.504	25.50
650 25.58 651 25.63 652 25.67 653 25.76 654 25.77 655 25.88 657 25.86 658 25.90 660 25.99 661 26.01 662 26.00 663 26.11 664 26.24 667 26.26 669 26.33 670 26.33 670 26.35 671 26.41 672 26.41 673 26.45 674 26.53	5.512 25	5.516 25.53	20 25.524	25.528	25.532	25.536	25.540	25.544	25.54
651         25.63           652         25.63           653         25.76           654         25.77           655         25.78           656         25.83           657         25.86           658         25.99           661         26.03           662         26.06           663         26.14           665         26.26           667         26.26           668         26.33           669         26.33           670         26.37           671         26.41           672         26.13           673         26.43           674         26.53           675         26.55	5.552 25	5.556 25.56	30 25.563	25.567	25.571	25.575	25.579	25.583	25.58
652         25.6°           653         25.7°           654         25.7°           655         25.8°           656         25.8°           657         25.8°           658         25.9°           660         25.9°           661         26.0°           662         26.0°           663         26.1°           664         26.1°           665         26.3°           666         26.3°           667         26.3°           670         26.3°           671         26.41°           672         26.15°           673         26.44°           674         26.5°           675         26.5°	5.591 25	5.595 25.59	9 25.603	25.607	25.611	25.615	25.619	25.623	25.62
653         25.76           654         25.77           655         25.78           656         25.83           657         25.86           658         25.99           669         25.98           661         26.02           662         26.06           663         26.14           664         26.14           665         26.36           669         26.33           670         26.37           671         26.41           672         26.13           673         26.44           674         26.53           675         26.55		$6.634 \mid 25.63$		25.646	25.650	25.654	25.658	25.662	25.66
654   25.77 655   25.78 656   25.89 657   25.86 658   25.99 660   25.98 661   26.02 662   26.06 663   26.14 665   26.18 666   26.26 667   26.26 669   26.33 670   26.37 671   26.41 672   26.13 673   26.45 674   26.55 675   26.57	1	5.674  25.67	1	25.686	25.689	25.693	25.697	25.701	25.70
655 25.78 656 25.89 657 25.86 658 25.99 660 25.98 661 26.06 662 26.06 663 26.16 664 26.14 665 26.28 667 26.26 668 26.36 669 26.38 670 26.37 671 26.41 672 26.43 673 26.44 674 26.55		5.713 25.71	1	25.725	25.729	25.733	25.737	25.741	25.74
656         25.82           657         25.86           658         25.96           659         25.95           660         25.98           661         26.02           662         26.06           663         26.16           664         26.18           665         26.26           667         26.26           668         26.33           670         26.33           671         26.41           672         26.42           673         26.43           674         26.53           675         26.55	5.748   25	5.752   25.75	25.760	25.764	25.768	25.772	25.776	25.780	25.78
657         25.86           658         25.90           659         25.9-           660         25.98           661         26.06           662         26.06           663         26.10           664         26.13           665         26.26           667         26.26           668         26.33           670         26.33           671         26.41           672         26.12           673         26.49           674         26.53           675         26.55		5.792 25.79		25.804	25.808	25.811	25.815	25.819	25.82
658         25.96           659         25.9-           660         25.9-           661         26.06           662         26.06           663         26.16           664         26.18           665         26.26           667         26.26           668         26.33           670         26.33           671         26.41           672         26.16           673         26.49           674         26.53           675         26.55		$\begin{array}{c c} \textbf{0.831} & \textbf{25.83} \\ \end{array}$		25.843	25.847	25.851	25.855	25.859	25.86
659         25.9-1           660         25.98-1           661         26.02-1           662         26.06-1           663         26.16-1           664         26.18-1           665         26.26-1           667         26.26-1           668         26.33-1           670         26.33-1           671         26.41-1           672         26.15-1           673         26.49-1           674         26.53-1           675         26.55-1		.871 25.87	1	25.882	25.886	25.890	25.894	25.898	25.90
660 25.98 661 26.00 662 26.00 663 26.10 664 26.14 665 26.26 667 26.26 668 26.33 670 26.33 670 26.34 672 26.44 672 26.45 673 26.49 674 26.53	1	.910 25.91		25.922	25.926	25.930	25.934	25.937	25.94
661         26.02           662         26.06           663         26.10           664         26.13           665         26.26           667         26.26           668         26.33           670         26.37           671         26.41           672         26.43           673         26.44           674         26.53           675         26.53	$\begin{vmatrix} 5.945 & 25. \end{vmatrix}$	25.95	3 25.957	25.961	25.965	25.969	25.973	25.977	25.98
662         26.06           663         26.16           664         26.14           665         26.18           666         26.22           667         26.36           669         26.33           670         26.37           671         26.41           672         26.42           673         26.43           674         26.53           675         26.53	5.985 25.	.989 25.99	3 25.997	26.000	26.004	26.008	26.012	26.016	26.02
663         26.16           664         26.14           665         26.18           666         26.22           667         26.26           668         26.33           670         26.33           671         26.41           672         26.45           673         26.45           674         26.53           675         26.55	6.024 26.	.028  26.03	2   26.036	26.040	26.044	26.048	26.052	26.056	26.06
664 26.14 665 26.18 666 26.29 667 26.26 668 26.33 670 26.33 670 26.37 671 26.41 672 26.15 673 26.45 674 26.55	6.063 26.	26.07	1 26.075	26.079	26.083	26.087	26.091	26.095	26.09
665 26.18 666 26.26 667 26.26 668 26.33 669 26.33 670 26.37 671 26.41 672 26.15 673 26.45 674 26.55	6.103 26.	.107  26.11	1 26.115	26.119	26.123	26.126	26.130	26.134	26.13
666   26 22 667   26.26 668   26.33 669   26.33 670   26.33 671   26.41 672   26.42 673   26.43 674   26.53 675   26.53	5.142 26.	3.146 26.15	0 26.154	26.158	26.162	26.166	26.170	26.174	26.17
667 26.26 668 26.33 669 26.33 670 26.41 672 26.41 673 26.49 674 26.53 675 26.53	6.182 26.	3.186 26.18	9 26.193	26.197	26.201	26.205	26.209	26.213	26.21
668 26.33 669 26.33 670 26.43 671 26.41 672 26.43 673 26.49 674 26.53 675 26.53	221 26.	.225   .26.22	9 26.233	26.237	26.241	26.245	26.249	26.252	26.25
669         26.33           670         26.37           671         26.41           672         26.45           673         26.49           674         26.53           675         26.57	-	26.26		26.276	26.280	26.284	26.288	26.292	26.29
670 26.37 671 26.41 672 26.45 673 26.48 674 26.53 675 26.53		[.304 ] 26.30		26.315	26.319	26.323	26.327	26.331	26.33
671 26.41 672 26.45 673 26.45 674 26.53 675 26.57	$\begin{bmatrix} 3.339 & 26. \end{bmatrix}$	3.343 26.34	7 26.351	26.355	26.359	26.363	26.367	26.371	26.37
672 26.45 673 26.49 674 26.55 675 26.57	6.378 26.	3.382 26.38	6 26.390	26.394	26.398	26.402	26.406	26.410	26.41
673   26.49 674   26.53 675   26.57	6.418 26.	.422 26.42	6 26.430	26.434	26.437	26.441	26.445	26.449	26.45
674   26.58 675   26.57	6.157 26.	.461 26.46	5 26.469	26.473	26.477	26.481	26.485	26.489	26.49
675 26.57		26.50		26.512	26.516	26.520	26.524	26.528	26.53
	6.536 26.	26.540	4 26.548	26.552	26.556	26.560	26.563	26.567	26.57
676 26.61		3.579 26.58		26.591	26.595	26.599	26.603	26.607	26.61
		.619 26.62	1	26.630	26.634	26.638	26.642	26.646	26.65
677   26.63		6.658   26.66		26.670	26.674	26.678	26.682	26.686	26.68
678 26.69		6.697 26.70		26.709	26.713	26.717	26.721	26.725	26.72
679 26.73 <b>0.</b>	.733   26.	26.74	1 26.745	26.749	26.752	26.756	26.760	26.764	26.76

1 Metre = 39.37079 English Inches.

Millime-					Tenths of I	Iillimetres.				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. I
680	26.772	26.776	26.780	26.784	26.788	26.792	26.796	26.800	26.804	26.80
681	26.812	26.815	26.819	26.823	26.827	26.831	26.835	26.839	26.843	26.84
682	26.851	26.855	26.859	26.863	26.867	26.871	26.875	26.878	26.882	26.88
683	26.890	26.894	26.898	26.902	26.906	26.910	26.914	26.918	26.922	26.92
684	26.930	26.934	26.937	26.941	26.945	26.949	26.953	26.957	26.961	26.96
685	26.969	26.973	26.977	26.981	26.985	26.989	26.993	26.997	27.000	27.00
686	27.008	27.012	27.016	27.020	27.024	27.028	27.032	27.036	27.010	27.04
687	27.048	27.052	27.056	27.060	27.063	27.067	27.071	27.075	27.079	27.08
688	27.087	27.091	27.095	27.099	27.103	27.107	27.111	27.115	27.119	27.12
689	27.126	27.130	27.134	27.138	27.142	27.146	27.150	27.154	27.158	27.16
690	27.166	27.170	27.174	27.178	27.182	27.186	27.189	27.193	27.197	27.20
691	27.205	27.209	27.213	27.217	27.221	27.225	27.229	27.233	27.237	27.24
692	27.245	27.249	27.252	27.256	27.260	27.264	27.268	27.272	27.276	27.28
693	27.284	27.288	27.292	27.296	27.300	27.304	27.308	27.312	27.315	27.31
694	27.323	27.327	27.331	27.335	27.339	27.343	27.347	27.351	27.355	27.35
695	27.363	27.367	27.371	27.375	27.378	27.382	27.386	27.390	27.394	27.39
696	27.402	27.406	27.410	27.414	27.418	27.422	27.426	27.430	27.434	27.43
697	27.441	27.445	27.449	27.453	27.457	27.461	27.465	27.469	27.473	27.47
698	27.481	27.485	27.489	27.493	27.497	27.500	27.504	27.508	27.512	27.51
699	27.520	27.524	27.528	27.532	27.536	27.540	27.544	27.548	27.552	27.55
700	27.560	27.563	27.567	27.571	27.575	27.579	27.583	27.587	27.591	27.59
701	27.599	27.603	27.607	27.611	27.615	27.619	27.623	27.626	27.630	27.63
702	27.638	27.642	27.646	27.650	27.654	27.658	27.662	27.666	27.670	27.67
703	27.678	27.682	27.686	27.689	27.693	27.697	27.701	27.705	27.709	27.71
704	27.717	27.721	27.725	27.729	27.733	27.737	27.741	27.745	27.749	27.78
705	27.756	27.760	27.764	27.768	27.772	27.776	27.780	27.784	27.788	27.79
706	27.796	27.800	27.804	27.808	27.812	27.815	27.819	27.823	27.827	27.83
707	27.835	27.839	27.843	27.847	27.851	27.855	27.859	27.863	27.867	27.87
708	27.875	27.878	27.882	27.886	27.890	27.894	27.898	27.902	27.906	27.91
709	27.914	27.918	27.922	27.926	27.930	27.934	27.938	27.941	27.945	27.9
710	27.953	27.957	27.961	27.965	27.969	27.973	27.977	27.981	27.985	27.98
711	27.993	27.997	28.001	28.004	28.008	28.012	28.016	28.020	28.024	28.02
712	28.032	28.036	28.010	28.044	28.048	28.052	28.056	28.060	28.063	28.06
713	28.071	28.075	28.079	28.083	28.087	28.091	28.095	28.099	28.103	28.10
714	28.111	28.115		28.123	28.126	28.130		28.138		28.1
715	28.150	28.154	28.158	28.162	28.166	28.170	28.174	28.178	28.182	28.18
716	28.189	28.193	28.197	28.201	28.205	28.209	28.213	28.217	28.221	28.22
717	28.229	28.233	28.237	28.241	28.245	28.249	28.252	28.256	28.260	28.26
718	28.268	28.272	28.276	28.280	28.284	28.288	28.292	28.296	28.300	28.30
719	28.308	28.312	28.315	28.319	28.323	28.327	28.331	28.335	28.339	28.3
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches.

Millime-					Tenths of	Millimetres	•			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
720	Eng. ln. 28.347	Eng. In. 28.351	Eng. In. 28.355	Eng. In. 28.359	Eng. In. 28.363	Eng. In. 28.367	Eng. In. 28.371	Eng. In. 28.375	Eng. In. 28.378	Eng. In 28.382
721	28.386	28.390	28.394	28.398	28.402	28.406	28.410	28.414	28.418	28.42
722	28.426	28.430	28.434	28.438	28.441	28.445	28.449	28.453	28.457	28.46
723	28.465	28.469	28.473	28.477	28.481	28.485	28.489	28.493	28.497	28.50
724	28.504	28.508	28.512	28.516	28.520	28.524	28.528	28.532	28.536	28.54
725	28.544	28.548	28.552	28.556	28.560	28.564	28.567	28.571	28.575	28.57
726	28.583	28.587	28.591	28.595	28.599	28.603	28.607	28.611	28.615	28.61
727	28.623	28.627	28.630	28.634	28.638	28.642	28.646	28.650	28.654	28.65
728	28.662	28.666	28.670	28.674	28.678	28.682	28.686	28.689	28.693	28.69
729	28.701	28.705	28.709	28.713	28.717	28.721	28.725	28.729	28.733	28.73
730	28.741	28.745	28.749	28.752	28.756	28.760	28.764	28.768	28.772	28.77
731	28.780	28.784	28.788	28.792	28.796	28.800	28.804	28.808	28.812	28.81
732	28.819	28.823	28.827	28.831	28.835	28.839	28.843	28.847	28.851	28.85
733	28.859	28.863	28.867	28.871	28.875	28.878	28.882	28.886	28.890	28.89
734	28.898	28.902	28.906	28.910	28.914	28.918	28.922	28.926	28.930	28.93
735	28.938	28.941	28.945	28.949	28.953	28.957	28.961	28.965	28.969	28.97
736	28.977	28.981	28.985	28.989	28.993	28.997	29.001	29.004	29.008	29.01
737	29.016	29.020	29.024	29.028	29.032	29.036	29.040	29.044	29.048	29.05
738	29.056	29.060	29.064	29.067	29.071	29.075	29.079	29.083	29.087	29.09
739	29.095	29.099	29.103	29.107	29.111	29.115	29.119	29.123	29.127	29.13
740	29.134	29.138	29.142	29.146	29.150	29.154	29.158	29.162	29.166	29.17
741	29.174	29.178	29.182	29.186	29.190	29.193	29.197	29.201	29.205	29.20
742	29.213	29.217	29.221	29.225	29.229	29.233	29.237	29.241	29.245	29.24
743	29.252	29.256	29.260	29.264	29.268	29.272	29.276	29.280	29.284	29.28
744	29.292	29.296	29.300	29.304	29.308	29.312	29.315	29.319	29.323	29.32
745	29.331	29.335	29.339	29.343	29.347	29.351	29.355	29.359	29.363	29.36
746	29.371	29.375	29.378	29.382	29.386	29.390	29.394	29.398	29.402	29.40
747	29.410	29.414	29.418	29.422	29.426	29.430	29.434	29.438	29.441	29.44
748 749	29.449 29.489	29.453 29.493	29.457 29.497	29.461 29.501	29.465 29.504	29.469 29.508	29.473 29.512	29.477 29.516	29.481 29.520	29.48 $29.52$
750	29.528	29,532	29.536	29.540	29.544	29.548	29.552	29.556	29.560	29.56
751	29.567	29.571	29.575	29.579	29.583	29.587	29.591	29.595	29.599	29.60
752	29.607	29.611	29.615	29.619	29.623	29.627	29.630	29.634	29.638	29.64
753	29.646	29.650	29.654	29.658	29.662	29.666	29.670	29.674	29.678	29.68
754	29.686	29.690	29.693	29.697	29.701	29.705	29.709	29.713	29.717	29.72
755	29.725	29.729	29.733	29.737	29.741	29.745	29.749	29.753	29.756	29.76
756	29.764	29.768	29.772	29.776	29.780	29.784	29.788	29.792	29.796	29.80
757	29.804	29.808	29.812	29.815	29.819	29.823	29.827	29.831	29.835	29.83
758	29.843	29.847	29.851	29.855	29.859	29.863	29.867	29.871	29.875	29.87
759	29.882	29.886	29.890	29.894	29.898	29.902	29.906	29.910	29.914	29.91
	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches.

Millime-					Tenths of	Millimetre	8.			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
***	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.		Eng. In	Eng. In. 29.953	
760	29.922	29.926	29.930 29.969	29.934 29.973	29.938 29.977	29.941 29.981	29.945	29.949		29.95
761	29.961	29.965			30.016	30.020	29.985	29.989		29.99
762	30.001	30.004	30.008 30.048	30.012 30.052	30.056	30.020	30.024	30.028	!	30.030
763	30.040	30.011	30.045	30.032	30.095	30.099	30.064	30.067	1	30 07
764	30.079	30.053	50.057	50.031	50.095	50.099	30.103	30.107	30.111	30.11
765	30.119	30.123	30.127	30.130	30.134	30.138	30.142	30.146	30.150	30.15
766	30.158	30.162	30.166	30.170	30.174	30.178	30.182	30.186		30.19
767	30.197	30.201	30.205	30.209	30.213	30.217	30.221	30.225	30.229	30.23
768	30.237	30.241	30.245	30.249	30.253	30.256	30.260	30.264	30.268	30.27
<b>7</b> 69	30.276	30.280	30.284	30.288	30.292	30.296	30.300	30.304	30.308	30.31
770	30.316	30.319	30.323	30.327	30.331	30.335	30.339	30.343	30.347	30.35
771	30.355	30.359	30.363	30.367	30.371	30.375	30.379	30.382	30.386	30.39
772	30.394	30.398	30.402	30.406	30.410	30.414	30.418	30.422		30.43
773	30.434	30.438	30.411	30.445	30.449	30.453	30.457	30.461	30.465	30.46
774	30.473	30.477	30.481	30.485	30.489	30.493	30.497	30.501	30.504	30.50
Pay sky #5	00 - 10	00 710	20.720	00.704	00 500	00 500	00 700	90.540	00 711	00 **
775	30.512	30.516	30.520	30.524	30.528	30.532	30.536	30.540	30.544	30.54
776	30.552	30.556	30.560	30.561	30.567	30.571	30.575	30.579	30.583	30.58
777	30.591	30.595	30.599	30.603	30.607	30.611	30.615	30.619	30.623	30.62
778	30.630	30.634	30.638	30.612	30.646	30.650	30.654	30.658	30.662	30.66
779	30.670	30.674	30.678	30.682	30.686	30.690	30.693	30.697	30.701	30.70
780	30.709	30.713	30.717	30.721	30.725	30.729	30.733	30.737	30.741	30.74
781	30.749	30.753	30.756	30.760	30.764	30.768	30.772	30.776	30.780	30.78
782	30.788	30.792	30.796	30.800	30.804	30.808	30.812	30.816	30.819	30.82
783	30.827	30.831	30.835	30.839	30.843	30.847	30.851	30.855	30.859	30.86
784	30.867	30.871	30.875	30.879	30.882	30.886	30.890	30.894	30.898	30.90
785	30.906	30.910	30.914	30.918	30.922	30.926	30.930	30.934	30.938	30.94
786	30.945	30.949	30.953	30.957	30.961	30.965	30.969	30.973	30.977	30.98
787	30.985	30.989	30.993	30.997	31.001	31.004	31.008	31.012	31.016	31.02
788	31.024	31.028	31.032	31.036	31.040	31.044	31.048	31.052	31.056	31.06
789	31.064	31.067	31.071	31.075	31.079	31.083	31.087	31.091	31.095	31.09
790	31.103	31.107	31.111	31.115	31.119	31.123	31.127	31.130	31.134	31.138
791	31.142	31.146	31.150	31.154	31.158	31.162	31.166	31.170	31.174	31.178
792	31.182	31.186	31.190	31.193	31.197	31.201	31.205	31.209	31.213	31.21
793	31.221	31.225	31.229	31.233	31.237	31.241	31.245	31.249	31.253	31.25
994	31.260	31.264	31.268	31.272	31.276	31.280	31.284	31.288	31.292	31.29
795	31.300	31.304	31.308	31.312	31.316	31.319	31.323	31.327	31.331	31.33
796	31.339	31.343	31.347	31.351	31.355	31.359	31.363	31.367	31.371	31.373
797	31.379	31.382	31.386	31.390	31.394	31.398	31.402		31.410	31.41-
798	31.418	31.422	31.426	31.430	31.434	31.438	31.442	31.445	31.449	31.458
799	31.457	31.461	31.465	31.469	31.473	31.477	31.481	31.485	31.489	31.498
800	31.497	31.501	31.505	31.508	31.512		31.520	31.521	31.528	31.532
			*	Hundredth	s of Millin	netres.				
0.	1.	2.	3.	4.	5	.	6.	7.	8.	9.

1 Millimetre = 0.443296 French or Paris Line.

Millimetres.					Millimetr	es. Uı	nits.				
Tens.	0.	1.	2.	3.	4.	5	•	6.	7.	8.	9.
	Par.lines.	Par.lines	Par.lines.	Par.lines	Par.lines.	Par.li	nes.	Par.lines.	Par,lines	Par.lines.	Par.lines.
300	132.99	133.43	133.88	134.32	134.76	135.	21	135.65	136.09	136.54	136.98
310	137.42	137.87	138.31	138.75	139.19	139.	64	140.08	140.52	140.97	141.41
320	141.85	142.30	142.74	143.18	143.63	144.		144.51	144.96	145.40	145.84
330	146.29	146.73	147.17	147.62	148.06	148.	.50	148.95	149.39	149.83	150.28
340	150.72	151.16	151.61	152.05	152.49	152.	.94	153.38	153.82	154.27	154.71
350	155.15	155.60	156.04	156.48	156.93	157.	37	157.81	158.26	158.70	159.14
360	159.59	160.03	160.47	160.92	161.36	161.	80	162.25	162.69	163.13	163.58
370	164.02	164.46	164.91	165.35	165.79	166.	.24	166.68	167.12	167.57	168.01
380	168.45	168.90	169.34	169.78	170.23	170.	67	171.11	171.56	172.00	172.44
390	172.89	173.33	173.77	174.22	174.66	175.	.10	175.55	175.99	176.43	176.88
400	177.32	177.76	178.20	178.65	179.09	179.	.53	179.98	180.42	180.86	181.31
410	181.75	182.19	182.64	183.08	183.52	183.	.97	184.41	184.85	185.30	185.74
420	186.18	186.63	187.07	187.51	187.96	188.	.40	188.84	189.29	189.73	190.17
430	190.62	191.06	191.50	191.95	192.39	192	.83	193.28	193.72	194.16	194.61
440	195.05	195.49	195.94	196.38	196.82	197	.27	197.71	198.15	198.60	199.04
450	199.48	199.93	200.37	200.81	201.26	201	.70	202.14	202.59	203.03	203.47
460	203.92	204.36	204.80	205.25	205.69	206	.13	206.58	207.02	207.46	207.91
470	208.35	208.79	209.24	209.68	210.12	210	.57	211.01	211.45	211.90	212.34
480	212.78	213.23	213.67	214.11	214.56	215	.00	215.44	215.88	216.33	216.77
490	217.22	217.66	218.10	218.54	218.99	219	.43	219.87	220.32	220.76	221.20
500	221.65	222.09	222.53	222.98	223.42	223	.86	224.31	224.75	225.19	225.64
510	226.08	226.52	226.97	227.41	227.85	228	.30	228.74	229.18	229.63	230.07
520	230.51	230.96	231.40	231.84	232.29	232	.73	233.17	233.62	234.06	234.50
530	234.95	235.39	235.83	236.28	236.72	237	.16	237.61	238.05	238.49	238.94
540	239.38	239.82	240.27	240.71	241.15	241	.60	242.04	242.48	242.93	243.37
550	243.81	244.26	244.70	245.14	245.59	246	.03	246.47	246.92	247.36	247.80
560	248.25	248.69	249.13	249.57	250.01	250	.46	250.91	251.35	251.79	252.24
570	252.68	253.12	253.57	254.01	254.45	254	.90	255.34	255.78	256.23	256.67
580	257.11	257.55	258.00	258.44	258.88	259	.32	259.77	260.21	260.66	261.10
590	261.54	261.99	262.43	262.87	263.32	263	.76	264.20	264.65	265.09	265.53
	<u> 11</u>	1	1	Tenths	of Millin	netres.			1		
0.	1.	2.	3.	4.	1 6	5.		6.	7.	8.	9.
0.000	0.011	0.089	0.133	0.17	7 0.:	222	0.	266	0.310	0.355	0.399
	1		<u> </u>	Hundred	ths of Mill	imetre	S.				
0.000	0.004	0.009	0.013	0.018	8 0.0	022	0.	027	0.031	0.035	0.040

1 Millimetre = 0.443296 French Line.

Millime-				7	Tenths of I	Villimetres				
tres.	0.	11.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.line
600	265.98	266.02	266.07	266.11	266.15	266.20	266.24	266.29	266.33	266.3
601	266.42	266.47	266.51	266.55	266.60	266.64	266.69	266.73	266.78	266.8
602	266.86	266.91	266.95	267.00	267.04	267.09	267.13	267.17	267.22	267.2
603	267.31	267.35	267.40	267.44	267.48	267.53	267.57	267.62	267.66	267.7
604	267.75	267.80	267.84	267.88	267.93	267.97	268.02	268.06	268.11	268.1
605	268.19	268.24	268.28	268.33	268.37	268.42	268.46	268.50	268.55	268.5
606	268.64	268.68	268.73	268.77	268.81	268.86	268.90	268.95	268.99	269.0
607	269.08	269.13	269.17	269.21	269.26	269.30	269.35	269.39	269.44	269.4
608	269.52	269.57	269.61	269.66	269.70	269.75	269.79	269.83	269.88	269.9
609	269.97	270.01	270.06	270.10	270.14	270.19	270.23	270.28	270.32	270.3
610	270.41	270.45	270.50	270.54	270.59	270.63	270.68	270.72	270.77	270.8
611	270.85	270.90	270.94	270.99	271.03	271.08	271.12	271.16	271.21	271.2
612	271.30	271.34	271.39	271.43	271.47	271.52	271.56	271.61	271.65	271.7
613	271.74	271.78	271.S3	271.87	271.92	271.96	272.01	272.05	272.10	272.1
614	272.18	272.23	272.27	272.32	272.36	272.41	272.45	272.49	272.54	272.5
615	272.63	272.67	272.72	272.76	272.80	272.85	272.89	272.94	272.98	273.0
616	273.07	273.11	273.16	273.20	273.25	273.29	273.34	273.38	273.42	273.4
617	273.51	273.56	273.60	273.65	273.69	273.74	273.78	273.82	273.87	273.9
618	273.96	274.00	274.05	274.09	274.13	274.18	274.22	274.27	274.31	274.3
619	274.40	274.44	274.49	274.53	274.58	274.62	274.67	274.71	274.75	274.8
620	274.84	274.89	274.93	274.98	275.02	275.07	275.11	275.15	275.20	275.2
621	275.29	275.33	275.38	275.42	275.46	275.51	275.55	275.60	275.64	275.6
622	275.73	275.77	275.82	275.86	275.91	275.95	276.00	276.04	276.08	276.1
623	276.17	276.22	276.26	276.31	276.35	276.38	276.44	276.48	276.53	276.5
624	276.62	276.66	276.71	276.75	276.79	276.84	276.88	276.93	276.97	277.0
625	277.06	277.10	277.15	277.19	277.24	277.28	277.33	277.37	277.41	277.4
626	277.50	277.55	277.59	277.64	277.58	277.72	277.77	277.81	277.86	277.9
627	277.95	277.99	278.04	278.08	278.12	278.17	278.21	278.26	278.30	278.3
628	278.39	278.43	278.48	278.52	278.57	278.61	278.66	278.70	278.74	278.7
629	278.83	278.88	278.92	278.97	279.01	279.05	279.10	279.14	279.19	279.2
630	279.28	279.32	279.37	279.41	279.45	279.50	279.54	279.59	279.63	279.6
631	279.72	279.76	279.81	279.85	279.90	279.94	279.99	280.03	280.07	280.1
632	280.16	280.21	280.25	280.30	280.34	280.38	280.43	280.47	280.52	280.5
633	280.61	280.65	280.70	280.74	280.78	280.83	280.87	280.92	280.96	281.0
634	281.05	281.09	281.14	281.18	281.23	281.27	281.32	281.36	281.40	281.4
635	281.49	281.54	281.58	281.63	281.67	281.71	281.76	281.80	281.85	281.8
636	281.94	281.98	282.02	282.07	282.11	282.16	282.20	282.25	282.29	282.3
637	292.38	282.42	282.47	282.51	282.56	282.60	282.65	282.69	282.73	282.7
638	282.82	282.87	282.91	282.96	283.00	283.04	283.09	283.13	283.18	283.2
639	283.27	283.31	283.35	283.40	283.44	283.49	283.53	283.58	283.62	283.6
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line.

Millime-	-									
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
C (0		Par.lines.		Par.lines. 283.84	Par.lines.	Par.lines. 283.93	Par.lines. 283.98	Par.lines. 284.02	Par.lines.	Par.lin 284.1
640	283.71	283.75 284.20	283.80	284.29	284.33	284.37	284.42	284.46	284.51	284.5
641 642	284.15 284.60	284.64	284.24 284.68	284.73	284.77	284.82	284.86	284.91	284.95	284.9
643	285.04	285.08	285.13	285.17	285.22	285.26	285.31	285.35	285.39	285.
644	285.48	285.53	285.57	285.62	285.66	285.70	285.75	285.79	285.84	285.8
645	285.93	285.97	286.01	286.06	286.10	286.15	286.19	286.24	286.28	286.
646	286.37	286.41	286.46	286.50	286.55	286.59	286.64	286.68	286.72	286.
647	286.81	286.86	286.90	286.95	286.99	287.03	287.08	287.12	287.17	287.5
648	287.26	287.30	287.34	287.39	287.43	287.48	287.52	287.57	287.61	287.
649	287.70	287.74	287.79	287.83	287.88	287.92	287.96	288.01	288.05	288.
650	288.14	288.19	288.23	288.28	288.32	288.36	288.41	288.45	288.50	288.
651	288.59	288.63	288.67	288.72	288.76	288.S1	288.85	288.90	288.94	288.9
652	289.03	289.07	289.12	289.16	289.21	289.25	289.29	289.34	289.38	289.
653	289.47	289.52	289.56	289.61	289.65	289.69	289.74	289.78	289.83	289.
654	289.92	289.96	290.00	290.05	290.09	290.14	290.18	290.23	290.27	290.
655	290.36	290.40	290.45	290.49	290.54	290.58	290.62	290.67	290.71	290.
656	290.80	290.85	290.89	290.94	290.98	291.02	291.07	291.11	291.16	291.
657	291.25	291.29	291.33	291.38	291.42	291.47	291.51	291.56	291.60	291.
658	291.69	291.73	291.78	291.82	291.87	291.91	291.95	292.00	292.04	292.
659	292.13	292.18	292.22	292.26	292.31	292.35	292.40	292.44	292.49	292.
660	292.58	292.62	292.66	292.71	292.75	292.80	292.84	292.89	292.93	292.
661	293.02	293.06	293.11	293.15	293.20	293.24	293.28	293.33	293.37	293.
662	293.46	293.51	293.55	293.59	293.64	293.68	293.73	293.77	293.82	293.
663	293.91	293.95	293.99	294.04	294.08	294.13	294.17	294.22	294.26	294.
664	294.35	294.39	294.44	294.48	294.53	294.57	294.61	294.66	294.70	294.
665	294.79	294.84	294.88	294.92	294.97	295.01	295.06	295.10	295.15	295.
666	295.24	295.28	295.32	295.37	295.41	295.46	295.50	295.55	295.59	295.
667	295.68	295.72	295.77	295.81	295.86	295.90	295.94	295.99	296.03	296.
668 669	296.12 296.56	296.17 296.61	296.21 296.65	296.25 296.70	296.30 296.74	296.34 296.79	296.39 296.83	296.43 296.88	296.48 $296.92$	296. 296.
									20** 20	
670	297.01	297.05	297.10	297.14	297.19	297.23 297.67	297.27 297.72	297.32 297.76	297.36 297.81	297. 297.
671	297.45	297.50 297.94	297.54 297.98	297.58 298.03	297.63 298.07	297.67	298.16	298.21	298.25	298.3
672 673	298.34	297.94	297.98	298.47	298.52	298.56	298.60	298.65	298.69	298.
674	298.78	298.83	298.43	298.91	298.96	299.00	299.05	299.09	299.14	299.
675	299.22	299.27	299.31	299.36	299.40	299.45	299.49	299.54	299.58	299.6
676	299.67	299.71	299.76	299.80	299.85	299.89	299.93	299.98	300.02	300.0
677	300.11	300.16	300.20	300.24	300.29	300.33	300.38	300.42	300.47	300.5
678	300.55	300.60	300.64	300.69	300.73	300.78	300.82	300.86	300.91	300.9
679	301.00	301.04	301.09	301.13	301.18	301.22	301.26	301.31	301.35	301.
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line.

Millime-										
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	11	Par.lines.	Par.lines.				Par.lines.		Par.lines.	Par.line
680	301.44	301.49	301.53	301.57	301.62	301.66	301.71	301.75	301.80	301.8
681	301.88	301.93	301.97	302.02	302.06	302.11	302.15	302.19	302.24	302.2
682	302.33	302.37	302.42	302.46	302.51	302.55	302.59	302.64	302.68	302.7
683	302.77	302.82	302.86	302.90	302.95	302.99	303.04	303.08	303.13	303.1
684	303.21	303.26	303.30	303.35	303.39	303.44	303.48	303.52	303.57	303.6
685	303.66	303.70	303.75	303.79	303.83	303.88	303.92	303.97	304.01	304.0
686	304.10	304.15	304.19	304.23	304.28	304.32	304.37	304.41	304.46	304.5
687	304.54	304.59	304.63	304.68	304.72	304.77	304.81	304.85	304.90	304.9
688	304.99	305.03	305.08	305.12	305.16	305.21	305.25	305.30	305.34	305.3
689	305.43	305.48	305.52	305.56	305.61	305.65	305.70	305.74	305.79	305.8
690	305.87	305.92	305.96	306.01	306.05	306.10	306.14	306.18	306.23	306.2
691	306.32	306.36	306.41	306.45	306.49	306.54	306.58	306.63	306.67	306.7
692	306.76	306.81	306.85	306.89	306.94	306.98	307.03	307.07	307.12	307.1
693	307.20	307.25	307.29	307.34	307.38	307.43	307.47	307.51	307.56	307.6
694	307.65	307.69	307.74	307.78	307.82	307.87	307.91	307.96	308.00	308.0
CO.5	308.09	308.13	308.18	308.22	308.27	308.31	308.36	308.40	308.45	308.4
695	1			308.67	308.71	308.76	308.80	308.84	308.89	308.9
696	308.53 308.98	308.58 309.02	308.62 309.07	309.11	309.15	309.20	309.24	309.29	309.33	309.3
697	309.42	309.46	309.51	309.55	309.60	309.64	309.69	309.73	309.78	309.8
698 699	309.86	309.91	309.95	310.00	310.04	310.09	310.13	310.17	310.22	310.2
				212.11		010 #0	0.0 5.0	210.02	220.00	0.00
700	310.31	310.35	310.40	310.44	310.48	310.53	310.57	310.62	310.66	310.7
701	310.75	310.79	310.84	310.88	310.93	310.97	311.02	311.06	311.11	311.1
702	311.19	311.24	311.28	311.33	311.37	311.42	311.46	311.50	311.55	311.5
703	311.64	311.68	311.73	311.77	311.81	311.86	311.90	311.95	311.99	312.0
704	312.08	312.12	312.17	312.21	312.26	312.30	312.35	312.39	312.43	312.4
705	312.52	312.57	312.61	312.66	312.70	312.75	312.79	312.83	312.88	312.9
706	312.97	313.01	313.06	313.10	313.14	313.19	313.23	313.28	313.32	313.3
707	313.41	313.45	313.50	313.54	313.59	313.63	313.68	313.72	313.76	313.8
708	313.85	313.90	313.94	313.99	314.03	314.08	314.12	314.16	314.21	314.2
709	314.30	314.34	314.39	314.43	314.47	314.52	314.56	314.61	314.65	314.7
710	314.74	314.78	314.83	314.87	314.92	314.96	315.01	315.05	315.09	315.1
711	315.18	315.23	315.27	315.32	315.36	315.41	315.45	315.49	315.54	315.5
712	315.63	315.67	315.72	315.76	315.80	315.85	315.89	315.94	315.98	316.0
713	316.07	316.11	316.16	316.20	316.25	316.29	316.34	316.38	316.42	316.4
714	316.51	316.56		316.65	316.69	316.73	316.78	316.82	316.87	316.9
715	316.96	317.00	317.05	317.09	317.13	317.18	317.22	317.27	317.31	317.3
716	317.40	317.44	317.49	317.53	317.58	317.62	317.67	317.71	317.75	317.8
717	317.84	317.89	317.93	317.98	318.02	318.06	318.11	318.15	318.20	318.2
718	318.29	318.33	318.38	318.42	318.46	318.51	318.55	318.60	318.64	318.6
719	318.73	318.77	318.82	318.86	318.91	318.95	319.00	319.04	319.08	319.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line.

Millime-				5	Tenths of	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.		Par.lines.		Par.lines.	Par.lines.		Par.lines.	Par.lines.	1
720	319.17	319.22	319.26	319.31	319.35	319.39	319.44	319.48	319.53	319.5
721	319.62	319.66	319.70	319.75	319.79	319.84	319.88	319.93	319.97	320.0
722	320.06	320.10	320.15	320.19	320.24	320.28	320.33	320.37	320.41	320.4
723	320.50	320.55	320.59	320.64	320.68	320.72	320.77	320.81	320.86	320.9
724	320.95	320.99	321.03	321.08	321.12	321.17	321.21	321.26	321.30	321.3
725	321.39	321.43	321.48	321.52	321.57	321.61	321.66	321.70	321.74	321.7
726	321.83	321.88	321.92	321.97	322.01	322.05	322.10	322.14	322.19	322.2
727	322.28	322.32	322.36	322.41	322.45	322.50	322.54	322.59	322.63	322.6
728	322.72	322.76	322.81	322.85	322.90	322.94	322.99	323.03	323.07	323.1
729	323.16	323.21	323.25	323.30	323.34	323.38	323.43	323.47	323.52	323.5
730	323.61	323.65	323.69	323.74	323.78	323.83	323.87	323.92	323.96	324.0
731	324.05	324.09	324.14	324.18	324.23	324.27	324.32	324.36	324.40	324.4
732	324.49	324.54	324.58	324.63	324.67	324.71	324.76	324.80	324.85	324.8
733	324.94	324.98	325.02	325.07	325.11	325.16	325.20	325.25	325.29	325.3
734	325.38	325.42	325.47	325.51	325.56	325.60	325.65	325.69	325.73	325.7
*0"	325.82	995 55	207.01	325.96	326.00	326.04	326.09	326.13	326.18	326.2
735	(	325.87	325.91	326.40	326.44					
736	326.27 326.71	326.31	326.35	326.84	326.89	326.49 326.93	326.53 $326.98$	326.58	326.62	326.6
737	327.15	326.75 $327.20$	326.80 327.24	327.29	327.33	327.37	327.42	327.02 327.46	327.06 $327.51$	327.1 327.5
738 739	327.60	327.64	327.68	327.73	327.77	327.82	327.86	327.91	327.95	327.9
740	328.04	328.08	328.13	328.17	328.22	328.26	328.30	328.35	328.39	328.4
741	328.48	328.53	328.57	328.62	328.66	328.70	328.75	328.79	328.84	328.8
742	328.93	328.97	329.01	329.06	329.10	329.15	329.19	329.24	329.28	329.3
743	329.37	329.41	329.46	329.50	329.55	329.59	329.63	329.68	329.72	329.7
744	329.81	329.86	329.90	329.95	329.99	330.03	330.08	330.12	330.17	330.2
745	330.26	330.30	330.34	330.39	330.43	330.48	330.52	330.57	330.61	330.6
746	330.70	330.74	330.79	330.83	330.88	330.92	330.96	331.01	331.05	331.1
747	331.14	331.19	331.23	331.28	331.32	331.36	331.41	331.45	331.50	331.5
748	331.59	331.63	331.67	331.72	331.76	331.81	331.85	331.90	331.94	331.9
749	332.03	332.07	332.12	332.16	332.21	332.25	332.29	332.34	332.38	332.4
750	332.47	332.52	332.56	332.60	332.65	332.69	332.74	332.78	332.83	332.8
751	332.92	332.96	333.00	333.05	333.09	333.14	333.18	333.23	333.27	333.8
752	333.36	333.40	333.45	333.49	333.54	333.58	333.62	333.67	333.71	333.7
753	333.80	333.85	333.89	333.93	333.98	334.02	334.07	334.11	334.16	334.2
754	334.25	334.29	334.33	334.38	334.42	334.47	334.51	334.56	334.60	334.6
755	334.69	334.73	334.78	334.82	334.87	334.91	334.95	335.00	335.04	335.0
756	335.13	335.18	335.22	335.26	335.31	335.35 335.80	335.40	335.44 335.89	335.49	335.5
757	335.58	335.62	335.66	335.71	335.75	1	335.84		335.93	335.9
758 759	336.02 336.46	336.06 336.51	336.11 336.55	336.15 336.59	336.20 336.64	336.24 336.68	336.28 336.73	336.33 336.77	336.37 336.82	336.4 336.8
	0.	1.	2.	3.		5.	6.			

1 Millimetre = 0.443296 French Line

.				ŗ	Fenths of I	Aillimetres				
Millime- tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines
760	336.90	336.95	336.99	337.04	337.08	337.13	337.17	337.22	337.26	337.30
761	337.35	337.39	337.44	337.48	337.53	337.57	337.61	337.66	337.70	337.75
762	337.79	337.84	337.88	337.92	337.97	338.01	338.06	338.10	338.15	338.19
763	338.23	338.28	338.32	338.37	338.41	338.46	338.50	338.55	338.59	338.63
761	338.68	338.72	338.77	338.81	338.86	338.90	338.94	338.99	339.03	339.08
765	339.12	339.17	339.21	339.25	339.30	339.34	339.39	339.43	339.48	339.52
766	339.56	339.61	339.65	339.70	339.74	339.79	339.83	339.87	339.92	339.96
767	340.01	340.05	340.10	340.14	340.19	340.23	340.27	340.32	340.36	340.41
768	340.45	340.50	340.54	340.58	340.63	340.67	340.72	340.76	340.81	340.85
769	340.89	340.94	340.98	341.03	341.07	341.12	341.16	341.20	341.25	341.29
770	341.34	341.38	341.43	341.47	341.52	341.56	341.60	341.65	341.69	341.7
771	341.78	341.83	341.87	341.91	341.96	342.00	342.05	342.09	342.14	342.18
772	342.22	342.27	342.31	342.36	342.40	342.45	342.49	342.53	342.58	342.62
773	342.67	342.71	342.76	342.80	342.85	342.89	342.93	342.98	343.02	343.07
774	343.11	343.16	343.20	343.24	343.29	343.33	343.38	343.42	343.47	343.51
775	343.55	343.60	343.64	343.69	343.73	343.78	343.82	343.86	343.91	343.9
776	314.00	344.04	344.09	344.13	344.17	344.22	344.26	344.31	344.35	344.40
777	344.44	344.49	344.53	344.57	344.62	344.66	344.71	344.75	344.80	344.84
778	344.88	344.93	344.97	345.02	345.06	345.11	345.15	345.19	345.24	345.28
779	345.33	345.37	345.42	345.46	345.50	345.55	345.59	345.64	345.68	345.73
780	345.77	345.82	345.86	345.90	345.95	345.99	346.04	346.08	346.13	346.17
781	346.21	346.26	346.30	346.35	346.39	346.44	346.48	346.52	346.57	346.6
782	346.66	346.70	346.75	346.79	346.83	346.88	346.92	346.97	347.01	347.06
783	347.10	347.15	347.19	347.23	347.28	347.32	347.37	347.41	347.46	347.50
784	347.54	347.59	347.63	347.68	347.72	347.77	347.81	347.85	347.90	347.9
785	347.99	348.03	348.08	348.12	348.16	348.21	348.25	348.30	348.34	348.39
786	348.43	348.47	348.52	348.56	348.61	348.65	348.70	348.74	348.79	348.83
787	348.87	348.92	348.96	349.01	349.05	349.10	349.14	349.18	349.23	349.2
788	349.32	349.36	349.41	349.45	349.49	349.54	349.58	349.63	349.67	349.72
789	349.76	349.80	349.85	349.89	349.94	349.98	350.03	350.07	350.12	350.10
790	350.20	350.25	350.29	350.34	350.38	350.43	350.47	350.51	350.56	350.60
791	350.65	350.69	350.74	350.78	350.82	350.87	350.91	350.96	351.00	351.0
792	351.09	351.13	351.18	351.22	351.27	351.31	351.36	351.40	351.44	351.49
793	351.53	351.58	351.62	351.67	351.71	351.76	351.80	351.84	351.89	351.93
794	351.98	352.02	352.07	352.11	352.15	352.20	352.24	352.29	352.33	352.38
795	352.42	352.46	352.51	352.55	352.60	352.64	352.69	352.73	352.77	352.82
796	352.86	352.91	352.95	353.00	353.04	353.09	353.13	353.17	353.22	353.26
797	353.31	353.35	353.40	353.44	353.48	353.53	353.57	353.62	353.66	353.7
798	353.75	353.79	353.84	353.88	353.93	353.97	354.02	354.06	354.10	354.15
799 800	354.19 354.64	354.24 354.68	354.28 354.73	354.33	354.37	354.42	354.46	354.50 354.95	354.55	354.59
				354.77	354.81	354.86	354.90		354.99	355.0
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

### V. - VI.

### COMPARISON

OF

# THE OLD FRENCH BAROMETER

WITH

### THE ENGLISH AND THE METRICAL BAROMETERS,

OR

#### TABLES

FOR CONVERTING FRENCH OR PARIS LINES INTO ENGLISH INCHES
AND DECIMALS, AND INTO MILLIMETRES;

GIVING THE VALUES CORRESPONDING TO EVERY PARIS LINE FROM 120 TO 216 LINES, OR FROM 10 TO 18 INCHES; AND TO EVERY TENTH OF A LINE FROM 216 TO 348 LINES, OR FROM 18 TO 29 FRENCH INCHES.

#### TABLE V.

MM. J. J. Pohl and J. Schabus have published, in the number for March, 1852, of the Proceedings of the Imperial Academy of Vienna, Class of Mathematics and Natural Philosophy, a set of short Thermometrical and Barometrical Reduction Tables, among which is found a table for the reduction of the Old French Barometrical Scale into the English. As this table shows slight discrepancies from the one given in the following pages, it may not be out of place to state that they arise from an accidental error in the equation used by MM. Pohl and Schabus in computing their table. Adopting, as they do, Bird's value of the metre, viz.

1 metre = 39.37062 English inches,

the value of the Paris line is

1 Paris line = 0.088813 English inches.

But the table seems to have been computed by using the equation

which, of course, gradually diminishes in lower numbers.

1 Paris line = 0.088823 English inches,

34

which gives, at the end of the table,

 $348 \text{ lines} \times .088823 = 30.9104 \text{ English inches},$ 

instead of

C

$$348 \text{ "} \times .088813 = 30.9069 \text{ "} \text{ "}$$

thus causing an error

= 0.0035 "

1 Paris Line = 0.088814 English Inch.

			11	aris Line =	= 0.000014	English I.	ucn,			
French or Paris Lines.		1			Uı	nits.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
10 Inch.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng In	Eng. In.	Eng. In.	1		
120	10.653	10.746	10.835	10.924	11.013	11.102	11.191	11.279		11.45
130	11.546	11.635	11.723	11.812	11.901	11.990	12.079	12.168		1
140	12.431	12.523	12.612	12.700	12.789	12.878	12.967	13.050	3   13.144	13.23
150	13.322	13.411	13.500	13.589	13.677	13.766	13.855	13.94	14.033	14.12
160	14.210	14.299	14.388	14.477	14.565	14.654	14.743	14.832	2 14.921	15.01
170	15.098	15.187	15.276	15.365	15.454	15.542	15.631	15.720	15.809	15.89
180	15.987	16.075	16.164	16.253	16.342	16.431	16.519	16.608	16.697	16.78
190	16.875	16.963	17.052	17.141	17.230	17.319	17.408	17.496	17.585	17.67
200	17.763	17.852	17.940	18.029	18.118	18.207	18.296	18.38		18.56
210	18.651	18.740	18.829	18.917	19.006	1	19.184	19.278		19.45
					Ter	iths.				
Paris Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9,
18 Inch.	Eng. In.	Eng. In.	Eng. In.	Eng In	Eng. In.	Eng. In.	Eng. In.	Eng. In		Eng. Ir
216	19.184	19.193	19.202	19.210	19.219	19.228	19.237	19.246	19.255	19.26
217	19.273	19.282	19.290	19.299	19.308	19.317	19.326	19.333	19.344	19.35
218	19.361	19.370	19.379	19.388	19.397	19.406	19.415	19.424	19.433	19.44
219	19.450	19.459	19.468	19.477	19.486	19.495	19.504	19.512	19.521	19.53
220	19.539	19.548	19.557	19.566	19.575	19.583	19.592	19.601	19.610	19.61
221	19.628	19.637	19.646	19.655	19.663	19.672	19.681	19.690		19.70
222	19.717	19.726	19.734	19.743	19.752	19.761	19.770	19.779	19.788	19.79
223	19.806	19.814	19.823	19.832	19.840	19.850	19.859	19.868		19.88
224	19.894	19.903	19.912	19.921	19.930	19.939	19.948	19.957		19.97
225	19.983	19.992	20.001	20.010	20.019	20.028	20.036	20.045		20.06
226	20.072	20.081	20.001	20.099	20.107	20.116	20.030	20.134		
11										20.15
227	20.161	20.170	20.179	20.187	20.196	20.205	20.214	20.223	20.232	20.24
19 Inch.	20.250	00 070	20.26*	20.250	00.00-	90.904	20.202	00.010	00.001	20.00
, 228	20.250	20.258	20.267	20.276	20.285	20.294	20.303	20.312		20.330
229	20.338	20.347	20.356	20.365	20.374	20.383	20.392	20.401	1	20.418
230	20.427	20.436	20.445	20.454	20.463	20.472	20.481	20.489		20.507
231	20.516	20.525	20.534	20.543	20.552	20.560	20.569	20.578	1	20.596
232	20.605	20.614	20.623	20.631	20.640	20.649	20.658	20.667	1	20.683
233	20.694	20.703	20.711	20.720	20.729	20.738	20.747	20.756	20.765	20.77
234	20.782	20.791	20.800	20.809	20.818	20.827	20.836	20.845	20.854	20.86
235	20.871	20.880	20.889	20.898	20.907	20.916	20.925	20.933	20.942	20.95
236	20.960	20.969	20.978	20.987	20.996	21.005	21.013	21.022	21.031	21.040
237	21.049	21.058	21.067	21.076	21.084	21.093	21.102	21.111	21.120	21.129
233	21.133	21.147	21.155	21.164	21.173	21.182	21.191	21.200	21.209	21.218
239	21.227	21.235	21.244	21.253	21.262	21.271	21.280	21.289		21.306
				Hnndre	edths of a	Line.				
0.	1.	2.	3.	4.	5	.	6.	7.	.8.	9.
.000	.001	.002	.003	.004	.00		05	.006	.007	.008

1 Paris Line = 0.083814 English Inch.

Wan sh					Tenths	of a	Line.					
French or ParisLines.	0.	1.	2.	3.	4.	1	5.	6.	7	·•	8.	9.
20 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In		g. In.	Eng. 1	n. Eng.	In.	Eng. In.	Eng. In.
240	21.315	21.324	21.333	21.342	21.351	21	.360	21.36	69 21.3	78	21.386	21.395
241	21.404	21.413	21.422	21.431	21.440	21	.449	21.49	57 21.4	166	21.475	21.484
242	21.493	21.502	21.511	21.520	21.529	21	.537	21.5		55	21.564	21.573
243	21.582	21.591	21.600	21.608	21.617	21	.626	21.63	$35 \mid 21.6$	14	21.653	21.662
244	21.671	21.679	21.688	21.697	21.706	21	.715	21.72	$24 \mid 21.7$	33	21.742	21.751
245	21.759	21.768	21.777	21.786	21.793	21	.804	21.81	13 21.8	22	21.830	21.839
246	21.848	21.857	21.866	21.875	21.884	21	.893	21.90	2 21.9	10	21.919	21.928
247	21.937	21.946	21.955	21.964	21.973	21	.981	21.99	00   21.9	99	22.008	22.017
248	22.026	22.035	22.044	22.053	22.061	22	.070	22.07	9 22.0	SS	22.097	22.106
249	22.115	22.124	22.132	22.141	22.150	22	.159	22.16	8 22.1	77	22 186	22.195
250	22.203	22.212	22.221	22.230	22.239	22	.248	22.25	7 22.2	66	22.275	22.283
251	22.292	22.301	22.310	22.319	22.328	22	.337	22.34	6 22.3	54	22.363	22.372
21 In. =										1		
252	22.381	22.390	22.399	22.408	22.417	22	.426	22.43	4 22.4	43	22.452	22.461
253	22.470	22.479	22.488	22.497	22,505	22	.514	22.52	3 22.5	32	22.541	22.550
254	22.559	22.568	22.577	22.585	22.594	22	.603	22.61	2 22.6	21	22.630	22.639
255	22.648	22.656	22.665	22.674	22.683	22	.692	22.70	1 22.7	10	22.719	22.728
256	22.736	22.745	22.754	22.763	22.772	22	.781	22.79	0 22.7	99	22.807	22.816
257	22.825	22.834	22.843	22.852	22.861	22	.870	22.87	8 22.8	87	22.896	22.905
258	22.914	22.923	22.932	22.941	22.950	22	.958	22.96	7 22.9	76	22.985	22.994
259	23.003	23.012	23.021	23.029	23.038	23	.047	23.05	6 23.0	65	23.074	23.083
260	23.092	23.101	23.109	23.118	23.127	23	.136	23.14	5 23.1	54	23.163	23.172
261	23.180	23.189	23.198	23.207	23.216	23	.225	23.23	4 23.2	43	23.252	23.260
262	23.269	23.278	23.287	23.296	23.305	23	.314	23.32	3 23.3	31	23.340	23.349
263	23.358	23.367	23.376	23.385	23.394	23	.402	23.41	1 23.43	20	23.429	23.438
22 In. =												
264	23.447	23.456	23.465	23.474	23.482	23	.491	23.50	0 23.50	09	23.518	23.527
265	23.536	23.545	23.553	23.562	23.571	23	.580	23.58	9 23.59	98	23.607	23.616
266	23.625	23.633	23.642	23.651	23.660	23	.669	23.67	S 23.6	87	23.696	23.704
267	23.713	23.722	23.731	23.740	23.749		.758	23.76	7 23.7	76	23.784	23.793
268	23.802	23.811	23.820	23.829	23.838	1	.847	23.85		i	23.873	23.882
269	23.891	23.900	23.909	23.918	23.926	23	.935	23.94	4 23.9	53	23.962	23.971
270	23.980	23.989	23.998	24.006	24.015	24	.024	24.03	3 24.0	42	24.051	24.060
271	24.069	24.077	24.086	24.095	24.104		.113	24.12		- 1	24.140	24.149
272	24.157	24.166	24.175	24.184	24.193		.202	24.21			24.228	24.237
273	24.246	24.255	24.264	24.273	24.282		.291	24.30		- 1	24.317	24.326
274	24.335	24.344	24.353	24.362	24.371		.379	24.38			24.406	24.415
275	24.424	24.433	24.442	24.450	24.459		.468	24.47		- 1	24.495	24.504
				Hundre	dths of a	Line						
0.	1.	2.	3.	4.	1	5.	€	s.	7.	1	8.	9.
.0000	.0009	.0018	.0027	.0036	,0	044	.00	)53	.0062	-	.0071	.0080

1 Paris Line = 0.088814 English Inch.

French or					Tenths of	of a Lin	е.			
ParisLines.	0.	1.	2.	3.	4.	5.	6	. 7.	s.	9.
23 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. 1				
276	24.513	24.522	24.530	24.539	24.548	24.5	1			
277	24.601	24.610	24.619	24.628	24.637	24.6				1
278	24.690	24.699	24.708	24.717	24.726	24.73	1	1		24.770
279	24.779	24.788	24.797	24.806	24.815	24.8				1
280	24.868	24.877	24.886	24.895	24.903	24.9	1			
281	24.957	24.966	24.974	24.983	24.992	25.00	01 25.0	10 25.0	19   25.028	25.037
282	25.046	25.054	25.063	25.072	25.081	25.09	00 25.0		1	25.125
283	25.134	25.143	25.152	25.161	25.170	25.17				
284	25.223	25.232	25.241	25.250	25.259	25.20			1	
285	25.312	25.321	25.330	25.339	25.348	25.33			1	
286	25.401	25.410	25.419	25.427	25.436	25.4			1	
287	25.490	25.498	25.507	25.516	25.525	25.53	$34 \mid 25.5$	$43 \mid 25.58$	$52 \mid 25.561$	25.570
24 In. =										25 25
288	25.578	25.587	25.596	25.605	25.614	25.63				
289	25.667	25.676	25.685	25.694	25.703	25.7	1	1		i
290	25.756	25.765	25.774	25.783	25.792	25.80	1	- 1		1
291	25.845	25.854	25.863	25.872	25.880	25.88		1		25.92
292	25.934	25.943	25.951	25.960	25.969	25.97	1		1	26.01
293	26.023	26.031	26.040	26.049	26.058	26.00	67 26.0	$76 \mid 26.08$	85   26.094	26.10
294	26.111	26.120	26.129	26.138	26.147	26.18	56 26.1	65 26.1	1	
295	26.200	26.209	26.218	26.227	26.236	26.2-	26.2	$53 \mid 26.26$		1
296	26.289	26.298	26.307	26.316	26.324	26.33	33   26.3	i	1	26.369
297	26.378	26.387	26.396	26.404	26.413	26.42		1		
298	26.467	26.475	26.484	26.493	26.502	26.51	11 26.5			26.547
299	26.555	26.564	26.573	26.582	26.591	26.60	$00 \mid 26.6$	$09 \mid 26.61$	$18 \mid 26.626$	26.635
25 In. =										
300	26.644	26.653	26.662	26.671	26.680	26.68		1	į.	1
301	26.733	26.742	26.751	26.760	26.769	26.77		1		
302	26.822	26.831	26.840	26.848	26.857	26.86		1		
303	26.911	26.920	26.928	26.937	26.946	26.93		i		1
304	26.999	27.008	27.017	27.026	27.035	27.0-				27.079
305	27.088	27.097	27.106	27.115	27.124	27.13	33 27.1	42 27.1	50 27.159	27.169
306	27.177	27.186	27.195	27.204	27.213	27.22	21 27.2	30 27.25	39 27.248	27.257
307	27.266	27.275	27.284	27.293	27.301	27.31	10   27.3	19 27.3	28 27.337	1
308	27.355	27.364	27.372	27.381	27.390	27.39	9 27.4	08 27.4	17 27.426	27.435
309	27.444	27.452	27.461	27.470	27.479	27.48		1		27.523
310	27.532	27.541	27.550	27.559	27.568	27.57	77 27.5	$86 \mid 27.59$	95 27.603	27.612
311	27.621	27.630	27.639	27.648	27.657	27.66	66 27.6	74 27.68	83 27.692	27.701
		1		Hnndr	edths of a	Line.	,	•		
0.	1.	2.	3.	4.	5	5.	6.	7.	8.	9.
				-					-	
.0000	.0009	.0018	.0027	.003	00.00	044	.0053	.0062	.0071	.0080

1 Paris Line = 0.088814 English Inch.

French or					Tenths	of a Line.				
ParisLines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
26 Inches.	Eng. In.          In.	Eng. In	. Eng. In.	Eng. I						
312	27.710	27.719	27.728	27.737	27.745	27.754	27.763	27.772	27.781	27.79
313	27.799	27.808	27.817	27.825	27.834	27.843	27.852	27.861	27.870	27.87
314	27.888	27.896	27.905	27.914	27.923	27.932	27.941	27.950	27.959	27.96
315	27.976	27.985	27.994	28.003	28.012	28.021	28.030	28.039	28.047	28.05
316	28.065	28.074	28.083	28.092	28.101	28.110	28.119	28.127	28.136	28.14
317	28.154	28.163	28.172	28.181	28.190	28.198	28.207	28.216	28.225	28.23
318	28.243	28.252	28.261	28.269	28.278	28.287	28.296	28.305	28.314	28.32
319	28.332	28.341	28.349	28.358	28.367	28.376	28.385	28.394	28.403	28.41
320	28.420	28.429	28.438	28.447	28.456	28.465	28.474	28.483	28.492	28.50
321	28.509	28.518	28.527	28.536	28.545	28.554	28.563	28.571	28.580	28.58
322	28.598	28.607	28.616	28.625	28.634	28.643	28.651	28.660	28.669	28.67
323	28.687	28.696	28.705	28.714	28.722	28.731	28.740	28.749	28.758	28.76
27 In. =   324	28.776	28.785	28.793	28.802	28.811	28.820	28.829	28.838	28.847	28.85
325	28.865	28.873	28.882	28.891	28.900	28.909	28.918	28.927		28.94
326	28.953	28.962	28.971	28.980	28.989	28.998	29.007	29.016		29.03
327	29.042	29.051	29.060	29.069	29.078	29.087	29.095	29.104		29.12
328	29.131	29.140	29.149	29.158	29.167	29.175	29.184	29.193		29.21
329	29.220	29.229	29.238	29.246	29.255	29.264	29.273	29.282	29.291	29.30
990	00.000	00.010	00.000	20.00=	20.041	00.050	20 222	00.001	90, 900	29.38
330	29.309 29.397	29.318 29.406	29.326	29.335	29.344	29.353	29.362	29.371	29.380 29.468	
331 332			29.415	29.424	29.433	29.442	29.451	29.460	1	29.47
333	29.486 29.575	29.495 29.584	29.504 29.593	29.513 29.602	29.522 29.611	29.531	29.540	29.548 29.637	29.557 29.646	29.56 29.65
334	29.664	29.673	29.682			29.619	29.628	29.726	29.735	29.74
335	29.753	29.762	29.770	29.691	29.699	29.708	29.717		29.824	29.83
28 In. =	29.700	49.104	29.110	29.779	29.788	29.797	29.806	29.815	49.524	29.33
336	29.842	29.850	29.859	29.868	29.877	29.886	29.895	29.904	29.913	29.92
337	29.930	29.939	29.948	29.957	29.966	29.975	29.984	29.992	30.001	30.01
338	30.019	30.028	30.037	30.046	30.055	30.064	30.072	30.081	30.090	30.09
339	30.108	30.117	30.126	30.135	30.143	30.152	30.161	30.170	30.179	30.18
340	30.197	30.206	30.215	30.223	30.232	30.241	30.250	30.259	30.268	30.27
341	30.286	30.294	30.303	30.312	30.321	30.330	30.339	30.348	30.357	30.36
342	30.374	30.383	30.392	30.401	30.410	30.419	30.428	30.437	30.445	30.45
343	30.463	30.472	30.481	30.490	30.499	30.508	30.516	30.525	30.534	30.543
344	30.552	30.561	30.570	30.579	30.588	30.596	30.605	30.614	30.623	30.63
345	30.641	30.650	30.659	30.667	30.676	30.685	30.694	30.703	30.712	30.72
346	30.730	30.739	30.747	30.756	30.765	30.774	30.783	30.792	30.801	39.810
347	30.818	30.827	30.836	30.845	30.854	30.863	30.872	30.881	30.890	30.898
29 In. =   348	30.907	30.916	30.925	30.934	30.943	30.952	30.961	30.969	30.978	30.987
			'		dths of a				<u>'</u>	
0.	1.	2.	3.	4.	5	.   (	3.	7.	8.	9.
			1				1			

C

1 Paris Line = 2.255829 Millimetres.

French or ParisLines.	Units.											
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
10 Inch. 120	Millim. 270.70	Millim. 272.96	Millim. 275.21	Millim. 277.47	Millim. 279.72	Millim. 281.98	Millim. 284.23	Millim. 286.49		Millim. 291.00		
130	293.26	295.51	297.77	300.03	302 28	304.54	306.79	309.05		313.56		
140	315.82	318.07	320.33	322.58	324.84	327.10	329.35	331.61		336.12		
150	338.37	340.63	342.89	345.14	317.40	349.65	351.91	354.17		358.68		
160	360.93	363.19	365.44	367.70	369.96	372.21	374.47	376.72		381.24		
170	383.49	385.75	3Ś8.00	390.26	392.51	394.77	397.03	399.28	401.54	403.79		
180	406.05	408.30	410.56	412.82	415.07	417.33	419.58	421.84	424.10	426.35		
190	428.61	430.86	433.12	435.37	437.63	439.89	442.14	444.40	446.65	448.91		
200	451.17	453.42	455.68	457.93	460.19	462.44	464.70	466.96	469.21	471.47		
210	473.72	475.98	478.24	480.49	482.75	485.00	487.26	489.51	491.77	494.03		
		Tenths of a Line.										
Paris Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
18 Inch.	Millim.		Millim.									
216	487.26	487.48	487.71	487.94	488.16	488.39	488.61	488.84	1	489.29		
217	489.51	489.74	489.97	490.19	490.42	490.64	490.87	491.09		491.55		
218	491.77	492.00	492.22	492.45	492.67	492.90	493.12	493.35		493.80		
219	494.03	494.25	494.48	494.70	494.93	495.15	495.38	495.61		496.06		
220	496.28	496.51	496.73	496.96	497.18	497.41	497.64	497.86		498.31		
221	498.54	498.76	498.99	499.21	499.44	499.67	499.89	500.12	500.34	500.57		
222	500.79	501.02	501.25	501.47	501.70	501.92	502.15 502.37			502.82		
223	503.05	503.28	503.50	503.73	503.95	504.18	504.40	504.63		505.08		
224	505.31	505.53	505.76	505.98	506.21	506.43	506.66	506.88	!	507.34		
225	507.56	507.79	508.01	508.24	508.46	508.69	508.91	509.14		509.59		
226	509.82	510.04	510.27	510.49	510.72	510.95	511.17	511.40		511.85		
227 19 Inch.	512.07	512.30	512.52	512.75	512.98	513.20	513.43	513.65	513.88	514.10		
228	514.33	514.55	514.78	515.01	515.23	515.46	515.68	515.91	516.13	516.36		
229	516.58	516.81	517.04	517.26	517.49	517.71	517.94	518.16	518.39	518.61		
230	518.84	519.07	519.29	519.52	519.74	519.97	520.19	520.42	520.65	520.87		
231	521.10	521.32	521.55	521.77	522.00	522.22	522.45	522.68		523.13		
232	523.35	523.58	523.80	524.03	524.25	524.48	524.71	524.93	525.16	525.38		
233	525.61	525.83	526.06	526.28	526.51	526.74	526.96	527.19	527.41	527.64		
234	527.86	528.09	528.32	528.54	528.77	528.99	529.22	529.44	529.67	529.89		
235	530.12	530.35	530.57	530.80	531.02	531.25	531.47	531.70	531.92	532.15		
236	532.38	532.60	532.83	533.05	533.28	533.50	533.73	533.95	534.18	534.41		
237	534.63	534.86	535.08	535.31	535.53	535.76	535.98 536.3		536.44	536.66		
238	536.89	537.11	537.34	537.56	537.79	538.02	538.24	538.47	538.69	538.92		
239	539.14	539.37	539.59	539.82	540.05	540.27	540.50	540.72	540.95	541.17		
				Tent	hs of a Li	ne.						
0.	1.	2.	3.	4.	5	•	6.	7.	8.	9.		
0.00	0.23	0.45	0.68	0.90	) 1.	13 1	.35	1.58	1.80	2.03		

1 Paris Line = 2.255829 Millimetres.

Paris or	Tenths of a Line.										
French Lines.	0.	1.	2.	3.	4.	5.		6.	7.	8.	9.
20 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Milli	m.	Millim.	Millim.	Millim.	Millim.
240	541.40	541.62	541.85	542.08	542.30	542.	53	542.75	542.98	543.20	543.43
241	543.65	543.88	544.11	544.33	544.56	544.	78	545.01	545.23	545.46	545.69
242	545.91	546.14	546.36	546.59	546.81	547.	04	547.26	547.49	547.72	547.9-
243	548.17	548.39	548.62	543.54	549.07	549.	29	549.52	549.75	549.97	550.20
244	550.42	550.65	550.87	551.10	551.32	551.	55	551.78	552.00	552.23	552.48
245	552.68	552.90	553.13	553.35	553.58	553.	81	554.03	554.26	554.48	554.7
246	554.93	555.16	555.39	555.61	555.84	556.	06	556.29	556.51	556.74	556.9
247	557.19	557.42	557.64	557.87	558.09	558.	32	558.54	558.77	558.99	559.2
248	559.45	559.67	559.90	560.12	560.33	560.	57	560.80	561.02	561.25	561.4
249	561.70	561.93	562.15	562.38	562.60	562.	83	563.05	563.28	563.51	563.73
250	563.96	564.18	564.41	564.63	564.80	565.	09	565.31	565.54	565.76	565.9
251	566.21	566.44	566.66	566.89	567.12	567.	34	567.57	567.79	568.02	568.2
31 Inches.							1				
252	568.47	568.69	568.92	569.15	569.37	5		569.82	570.05	570.27	570.5
253	570.72	570.95	571.18	571.40	571.63	II.	85	572.08	572.30	572.53	572.7
254	572.98	573.21	573.43	573.66	573.88	4	1	574.33	574.56	574.79	575.0
255	575.24	575.46	575.69	575.91	576.1	576.	36	576.59	576.82	577.04	577.2
256	577.49	577.72	577.94	578.17	578.39	578.	62	578.85	579.07	579.30	579.5
257	579.75	579.97	580.20	580.42	580.63	580.	88	581.10	581.33	581.55	581.7
258	582.00	582.23	582.46	582.68	582.93	583.	13	583.36	583.58	583.81	584.0
259	584.26	584.49	584.71	584.94	585.16	585.	39	585.61	585.84	556.06	586.2
260	586.52	586.74	586.97	587.19	587.45	587.	61	587.87	588.09	588.32	588.5
261	588.77	589.00	589.22	589.45	589.63	589.	90	590.12	590.35	590.58	590.8
262	591.03	591.25	591.48	591.70	591.93	592.	16	592.38	592.61	592.83	593.0
263	593.28	593.51	593.73	593.96	594.19	594.	41	594.64	594.86	595.09	595.3
22 Inches.						1					
264	595.54	595.76	595.99	596.22	596.4	596.	67	596.89	597.12	597.34	597.5
265	597.79	598.02	598.25	598.47	598.70			599.15		599.60	599.8
266	600.05	600.28	600.50	600.73	600.93	- 10	t	601.40	i i	601.86	602.0
267	602.31	602.53	602.76	602.98	603.21	ğ		603.66	ì	604.11	604.3
268	604.56	604.79	605.01	605.24	605.46	fl .		605.92	606.14	606.37	606.5
269	606.82	607.04	607.27	607.49	607.72	8		608.17	608.40	608.62	608.8
270	609.07	609.30	609.52	609.75	609.98	610.	20	610.43	610.65	610.88	611.1
271	611.33	611.56	611.78	612.01	612.23	13	- 1	612.68	612.91	613.13	613.3
272	613.59	613.81	614.04	614.26	614.49	3	- 1	614.94	615.16	615.39	615.6
273	615.84	616.07	616.29	616.52	616.7	H		617.19	617.42	617.65	617.8
274	618.10	618.32	618.55	618.77	619.00	E .		619.45	619.68	619.90	620.1
275	620.35	620.58	620.80	621.03	621.26	N		621.71	621.93	622.16	622.3
				Hundre	edths of a	Line.			1		ı
0.	1.	2.	3.	4.		5.		6.	7.	8.	9.
0.000	0.023	0.045	0.068	3 0.09	90 0	.113	0.	.135	0.158	0.180	0.203

1 Paris Line = 2.255829 Millimetres.

	ris or				Line =		of a Line.				
	rench ines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
11	Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
- 11	276	622.61	622.83	623.06	623.29	623.51	623.74	623.96	624.19	624.41	624.64
- 11	277	624.86	625.09	625.32	625.54	625.77	625.99	626.22	626.44	626.67	626.89
11	278	627.12	627.35	627.57	627.80	628.02	628.25	628.47	628.70	628.93	629.15
11	279	629.38	629.60	629.83	630.05	630.28	630.50	630.73	630.96	631.18	631.41
11	280	631.63	631.86	632.08	632.31	632.53	632.76	632.99	633.21	633.44	633.66
	281	633.89	634.11	634.34	634.56	634.79	635.02	635.24	635.47	635.69	635.92
2	282	636.14	636.37	636.59	636.82	637.05	637.27	637.50	637.72	637.95	638.17
1 2	283	638.40	638.63	638.85	639.08	639.30	639.53	639.75	639.98	640.20	640.43
1 2	284	640.66	640.88	641.11	641.33	641.56	641.78	642.01	642.23	643.46	642.69
1 2	285	642.91	643.14	643.36	643.59	643.81	644.04	644.26	644.49	644.72	644.94
	286	645.17	645.39	645.62	645.84	646.07	646.30	646.52	646.75	646.97	647.20
1 :	287	647.42	647.65	647.87	648.10	648.33	648.55	648.78	649.00	649.23	649.45
41	Inches.										
11	288	649.68	649.90	650.13	650.36	650.58	650.81	651.03	651.26	651.48	651.71
11	289	651.93	652.16	652.39	652.61	652.84	653.06	653.29	653.51	653.74	653.96
2	290	654.19	654.42	654.64	654.87	655.09	655.32	655.54	655.77	656.00	656.22
1	291	656.45	656.67	656.90	657.12	657.35	657.57	657.80	658.03	658.25	658.48
1 2	292	658.70	658.93	659.15	659.38	659.60	659.83	660.06	660.28	660.51	660.73
1 2	293	660.96	661.18	661.41	661.63	661.86	662.09	662.31	662.54	662.76	662.99
	294	663.21	663.44	663.66	663.89	664.12	664.34	664.57	664.79	665.02	665.24
1 5	295	665.47	665.70	665.92	666.15	666.37	666.60	666.82	667.05	667.27	667.50
1 :	296	667.73	667.95	668.18	668.40	668.63	668.85	669.08	669.30	669.53	669.76
	297	669.98	670.21	670.43	670.66	670.88	671.11	671.33	671.56	671.79	672.01
11	298	672.24	672.46	672.69	672.91	673.14	673.36	673.59	673.82	674.04	674.27
11	299	674.49	674.72	674.94	675.17	675.40	675.62	675.85	676.07	676.30	676.52
25	Inches.										
:	300	676.75	676.97	677.20	677.43	677.65	677.88	678.10	678.33	678.55	678.78
:	301	679.00	679.23	679.46	679.68	679.91	680.13	680.36	680.58	680.81	681.03
:	302	681.26	681.49	681.71	681.94	682.16	682.39	682.61	682.84	683.07	683.29
:	303	683.52	683.74	683.97	684.19	684.42	684.64	684.87	685.10	685.32	685.55
:	304	685.77	686.00	686.22	686.45	686.67	686.90	687.13	687.35	687.58	687.80
	305	688.03	688.25	688.48	688.70	688.93	689.16	689.38	689.61	689.83	690.06
	306	690.28	690.51	690.73	690.96	691.19	691.41	691.64	691.86	692.09	692.31
:	307	692.54	692.77	692.99	693.22	693.44	693.67	693.89	694.12	694.34	694.57
:	308	694.80	695.02	695.25	695.47	695.70	695.92	696.15	696.37	696.60	696.83
;	309	697.05	697.28	697.50	697.73	697.95	698.18	698.40	698.63	698.86	699.08
;	310	699.31	699.53	699.76	699.98	700.21	700.43	700.66	700.89	701.11	701.34
	311	701.56	701.79	702.01	702.24	702.47	702.69	702.92	703.14	703.37	703.59
					Hundr	edths of a	Line.		<del></del>		
	0.	1.	2.	3.	4	.	5.	6.	7.	8.	9.
0	.000	0.023	0.045	0.06	8 0.0	90 0.	113	0.135	0.158	0.180	0.203

1 Paris Line = 2.255829 Millimetres.

Paris or					Tenths	of a Line.				
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
26 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
312	703.82	704.04	704.27	704.50	704.72	704.95	705.17	705.40	705.62	705.85
313	706.07	706.30	706.53	706.75	706.98	707.20	707.43	707.65	707.88	708.10
314	708.33	708.56	708.78	709.01	709.23	709.46	709.68	709.91	710.13	710.36
315	710.59	710.81	711.04	711.26	711.49	711.71	711.94	712.17	712.39	712.62
316	712.84	713.07	713.29	713.52	713.74	713.97	714.20	714.42	714.65	714.87
317	715.10	715.32	715.55	715.77	716.00	716.23	716.45	716.68	716.90	717.13
318	717.35	717.58	717.80	718.03	718.26	718.48	718.71	718.93	719.16	719.38
319	719.61	719.84	720.06	720.29	720.51	720.74	1		721.41	721.64
320	721.87	722.09	722.32	722.54	722.77	722.99			723.67	723.90
321	724.12	724.35	724.57	724.80	725.02	725.25			725.93	726.15
322	726.38	726.60	726.83	727.05	727.28	727.50			728.18	728.41
323	728.63	728.86	729.08	729.31	729.54	729.76	1	730.21	730.44	730.66
27 Inches.					,	1				.55,05
324	730.89	731.11	731.34	731.57	731.79	732.02	732.24	732.47	732.69	732.92
325	733.14	733.37	733.60	733.82	734.05	734.27	1	1	734.95	735.17
326	735.40	735.63	735.85	736.08	736.30	736.53	736.75	736.98	737.20	737.43
327	737.66	737.88	738.11	738.33	738.56	1		739.24	739.46	739.69
328	739.91	740.14	740.36	740.59	740.81	741.04	741.27	1	741.72	741.94
329	742.17	742.39	742.62	742.84	743.07	743.30	743.52		743.97	744.20
330	744.42	744.65	744.87	745.10	745.33	745.55	745.78	746.00	746.23	746.45
331	746.68	746.90	747.13	747.36	747.58	747.81		1	748.48	748.71
332	748.94	749.16	749.39	749.61	749.84	750.06		1	750.74	750.97
333	751.19	751.42	751.64	751.87	752.09		1	1	753.00	753.22
334	753.45	753.67	753.90	754.12	754.35	754.57	1	1	755.25	755.48
335	755.70	755.93	756.15	756.38	756.61	756.83	1	1	757.51	757.73
24 Inches.							10,100			
336	757.96	758.18	758.41	758.64	758.86	759.09	759.31	759.54	759.76	759.99
337	760.21	760.14	760.67	760.89	761.12	761.34	761.57	761.79	762.02	762.24
338	762.47	762.70	762.92	763.15	763.37	763.60	763.82	764.05	764.27	764.50
339	764.73	764.95	765.18	765.40	765.63	765.85	766.08	766.31	766.53	766.76
340	766.98	767.21	767.43	767.66	767.88	768.11	768.34	768.56	768.79	769.01
341	769.24	769.46	769.69	769.91	770.14	770.37	770.59	770.82	771.04	771.27
342	771.49	771.72	771.94	772.17	772.40	772.62	772.85	773.07	773.30	773.52
343	773.75	773.97	774.20	774.43	774.65				775.55	775.78
344	776.01	776.23	776.46	776.68	776.91	777.13		1	777.81	778.04
345	778.26	778.49	778.71	778.94	779.16	1		1	780.07	780.29
346	780.52	780.74	780.97	781.19	781.42			1	782.32	782.55
347	782.77	783.00	783.22	783.45	783.67	783.90	1	1	784.58	784.50
29 Inches.						1				
318	785.03	785.25	785.48	785.71	785.93	1786.16	786.38	786.61	786.83	787.06
				Hundr	edths of a	Line.				
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.000	0.023	0.045	0.068	8 0.0	90 0	.113	0.135	0.158	0.180	0.203

## VII. - VIII.

## COMPARISON

OF

# THE RUSSIAN BAROMETER

WITH

THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

## TABLES

FOR CONVERTING RUSSIAN HALF-LINES INTO MILLIMETRES,
AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY HALF-LINE FROM 440 TO 540, OR FROM 22 TO 27 INCHES; AND TO EVERY TENTH, FROM 540 TO 610 HALF-LINES, OR FROM 27 TO 30.5 ENGLISH INCHES.



## RUSSIAN BAROMETER.

A LEGULAR system of Meteorological Observations has been established by order of the Russian government throughout the extensive regions placed under its sway, and a vast amount of observations made in Europe, in Asia, and in North America have already been published. The scale of the barometer employed in this system is divided in units, each of which is equal to one half of a Russian, or English decimal line, that is, 1 = 0.05 of an inch, 600 half-lines of the Russian Barometer being = 30 inches of the English Barometer.

The conversion of this scale, which is the English scale, slightly modified in its form, is easy. It suffices to divide the Russian heights by two, and to put back, by one figure, the decimal point, in order to have them converted into English inches and decimals. This transformation is so easy to effect, that a peculiar table for it would seem superfluous.

The normal temperature of the standard being the same as that of the English, that is, 13°½ Reaumur, or 62° Fahrenheit, the reduction of the Russian Barometer to the freezing point can be made by means of the table for reducing the English Barometers. But the attached thermometer being that of Reaumur, its indications must be first converted into degrees of Fahrenheit.

Tables VII. and VIII., which follow, have been computed in order to render more easy the comparison and the use of the Barometrical Observations recorded in the large collection, published annually by order of the Emperor of Russia, under the name of Annuaire Météorologique et Magnétique du Corps des Ingénieurs des Mines.

1 Russian Half-Line = 1.269977 Millimetres.

Russian				Uni	its or Russ	an Half-Li	nes.			
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
22 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
440	558.79	560.06	561.33	562.60	563.87	565.14	566.41	567.68	568.95	570.2
450	571.49	572.76	574.03	575.30	576.57	577.84	579.11	580.38	581.65	582.9
460	584.19	585.46	586.73	588.00	589.27	590.54	591.81	593.08	594.35	595.6
470	596.89	598.16	599.43	600.70	601.97	603.24	604.51	605.78	607.05	608.3
480	609.59	610.86	612.13	613.40	614.67	615.94	617.21	618.48	619.75	621.0
24.5 In.										
490	622.29	623.56	624.83	626.10	627.37	628.64	629.91	631.18	632.45	633.7
500	634.99	636.26	637.53	638.80	640.07	641.34	642.61	643.88	645.15	646.4
510	647.69	648.96	650.23	651.50	652.77	654.04	655.31	656.58	657.85	659.1
520	660.39	661.66	662.93	664.20	665.47	666.74	668.01	669.28	670.55	671.8
530	673.09	674.36	675.63	676.90	678.17	679.44	680.71	681.98	683.25	684.5
Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
27 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
540	685.79	685.91	686.04	686.17	686.30	686.42	686.55	686.68	686.80	686.9
541	687.06	687.18	687.31	687.44	687.57	687.69	687.82	687.95	688.07	688.2
542	688.33	688.45	688.58	688.71	688.84	688.96	689.09	689.22	689.34	689.4
543	689.60	689.72	689.85	689.98	690.11	690.23	690.36	690.49	690.61	690.7
544	690.87	690.99	691.12	691.25	691.38	691.50	691.63	691.76	691.88	692.0
545	692.14	692.26	692.39	692.52	692.65	692.77	692.90	693.03	693.15	693.2
546	693.41	693.53	693.66	693.79	693.91	694.04	694.17	694.30	694.42	694.5
547	694.68	694.80	694.93	695.06	695.19	695.31	695.44	695.57	695.69	695.8
548	695.95	696.07	696.20	696.33	696.46	696.58	696.71	696.84	696.96	697.0
549	697.22	697.34	697.47	697.60	697.73	697.85	697.98	698.11	698.23	698.3
27.5 In.										
550	698.49	698.61	698.74	698.87	699.00	699.12	699.25	699.38	699.50	699.6
551	699.76	699.88	700.01	700.14	700.27	700.39	700.52	700.65	700.77	700.9
552	701.03	701.15	701.28	701.41	701.54	701.66	701.79	701.92	702.04	702.1
553	702.30	702.42	702.55	702.68	702.81	702.93	703.06	703.19	703.31	703.4
554	703.57	703.69	703.82	703.95	704.08	704.20	704.33	704.46	704.58	704.7
555	704.84	704.96	705.09	705.22	705.35	705.47	705.60	705.73	705.85	705.9
556	706.11	706.23	706.36	706.49	706.62	706.74	706.87	707.00	707.12	707.2
557	707.38	707.50	707.63	707.76	707.89	708.01	708.14	708.27	708.39	708.5
558	708.65	708.77	708.90	709.03	709.16	709.28	709.41	709.54	709.66	709.7
559	709.92	710.14	710.27	710.40	710.53	710.65	710.78	710.81	710.93	711.0
28 Inch.										
560	711.19	711.31	711.44	711.57	711.70	711.82	711.95	712.08	712.20	712.3
561	712.46	712.58	712.71	712.84	712.97	713.09	713.22	713.35	713.47	713.6
562	713.73	713.85	713.98	714.11	714.24	714.36	714.49	714.62	714.74	714.8
563	715.00	715.12	715.25	715.38	715.51	715.63	715.76	715.89	716.01	716.1
564	716.27	716.39	716.52	716.65	716.78	716.90	717.03	717.16	717.28	717.4
565	717.54	717.66	717.79	717.92	718.04	718.17	718.30	718.43	718.55	718.6
566	718.81	718.93	719.06	719.19	719.31	719.44	719.57	719.70	719.82	719.9
567	720.08	720.20	720.33	720.46	720.58	720.71	720.84	720.97	721.09	721.2
	721.35	721.47	721.60	721.73	721.85	721.98	722.11	722.24	722.36	722.49
568	141.00		141.001		141.00	141.00				

1 Russian Half-Line = 1.269977 Millimetre.

Russian					Ter	iths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
28.5 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
570	723.89	724.01	724.14	724.27	724.39	724.52	724.65	724.78	724.90	725.0
571	725.16	725.28	725.41	725.54	725.66	725.79	725.92	726.05	726.17	726.3
572	726.43	726.55	726.68	726.81	726.93	727.06	727.19	727.32	727.44	727.5
573	727.70	727.S2	727.95	728.08	728.20	728.33	728.46	728.59	728.71	728.8
574	728.97	729.08	729.21	729.34	729.46	729.59	729.73	729.85	729.97	730.1
575	730.24	730.36	730.49	730.62	730.74	730.87	731.00	731.13	731.25	731.3
576	731.51	731.63	731.76	731.89	732.01	732.14	732.27	732.40	732.52	732.6
577	732.78	732.90	733.03	733.16	733.28	733.41	733.54	733.67	733.79	733.9
578	734.05	734.17	734.30	734.43	734.55	734.68	734.81	734.94	735.06	735.1
579	735.32	735.44	735.57	735.70	735.82	735.95	736.08	736.21	736.33	736.4
29 Inch.	F90 50	700 M1	mac 0 4	mac 0m	79F 00	mor 00	****	mor 40	mom 00	
580	736.59	736.71	736.84	736.97	737.09	737.22	737.35	737.48	737.60	737.7
581	737.86	737.98	738.11	738.24	738.36	738.49	738.62	738.75	738.87	739.0
582	739.13	739.25	739.38	739.51	739.63	739.76	739.89	740.02	740.14	740.2
583 584	740.40 741.67	740.52	740.65 741.92	740.78 742.05	740.90 $742.17$	741.03 742.30	741.16 $742.43$	741.29	741.41	741.5 742.8
585	742.94	743.06	743.19	743.32	743.44	743.57	743.70	743.83	719.05	
586	744.21	744.33	743.13	744.59	744.71				743.95	744.0
587	745.48	745.60		745.86	745.98	744.84	744.97 746.24	745.10	745.22	745.3
	746.75	746.87	745.73			746.11		746.37	746.49	746.6
588 589			747.00	747.13	747.25	747.38	747.51	747.64	747.76	747.8
29.5 In.	748.02	748.14	748.27	748.40	748.52	748.65	748.78	748.91	749.03	749.1
590	749.29	749.41	749.54	749.67	749.79	749.92	750.05	750.18	750.30	750.4
591	750.56	750.68	750.81	750.94	751.06	751.19	751.32	751.45	751.57	751.7
592	751.83	751.95	752.08	752.21	752.33	752.46	752.59	752.72	752.84	752.9
593	753.10	753.22	753.35	753.48	753.60	753.73	753.86	753.99	754.11	754.2
594	754.37	754.49	754.62	754.75	754.87	755.00	755.13	755.26	755.38	755.5
595	755.64	755.76	755.89	756.02	756.14	756.27	756.40	756.53	756.65	756.7
596	756.91	757.03	757.16	757.29	757.41	757.54	757.67	757.80	757.92	758.0
597	758.18	758.30	758.43	758.56	758.68	758.81	758.94	759.07	759.19	759.3
598	759.45	759.57	759.70	759.84	759.96	760.09	760.21	760.34	760.46	760.5
599	760.72	760.84	760.97	761.10	761.22	761.35	761.48	761.61	761.73	761.S
30 Inch.										
600	761.99	762.11	762.24	762.37	762.49	762.62	762.75	762.88	763.00	763.1
601	763.26	763.38	763.51	763.64	763.76	763.89	764.02	764.15	764.27	764.4
602	764.53	764.65	764.78	764.91	765.03	765.16	765.29	765.42	765.54	765.6
603	765.80	765.92	766.05	766.18	766.30	766.43	766.56	766.69	766.81	766.9
604	767.07	767.19	767.32	767.45	767.57	767.70	767.83	767.96	768.08	768.2
605	768.34	768.46	768.59	768.72	768.84	768.97	769.10		769.35	769.4
606	769.61	769.73	769.85	769.99	770.11	770.24	770.37	770.50	770.62	770.7
607	770.88	771.00	771.13	771.26	771.38	771.51	771.64	771.77	771.89	772.0
608	772.15 773.42	772.27	772.40	772.53 773.80	772.65 773.92	772.78 774.05	772.91 774.18	773.03 774.30	773.16 774.43	773.2
					indredths.					
0.000	0.012	0.027	1 0 000	1	1		- 1 -	000 1	0.702	
0.000	0.013	0.025	0.038	0.051	0.06	53   0.0	076 0	.089	0.102	0.114

1 Russian Half-Line = 0.562976 Paris Line.

B				<del> </del>	Units or R	ıssian Half	f-Lines.			
Russian Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
22 Inch.	Par. line.	Par. line.	Par. line	Par. line.	Par line.	Par line.			Par line	Par. line
440	247.71	248.27	248.84	249.40	249.96	250.52	251.09	251.65	252.21	252.78
450	253.34	253.90	254.47	255.03	255.59	256.15	256.72	257.28	257.84	258.41
460	258.97	259.53	260.09	260.66	261.22	261.78	262.35	262.91	263.47	264.04
470	264.60	265.16	265.72	266.29	266.85	267.41	267.98	268.54	269.10	269.67
480 24.5 In.	270.23	270.79	271.35	271.92	272.48	273.04	273.61	274.17	274.73	275.30
490	275.86	276.42	276.98	277.55	278.11	278.67	279.24	279.80	280.36	280.93
500	281.49	282.05	282.61	283.18	283.74	284.30	284.87	285.43	285.99	286.55
510	287.12	287.68	288.24	288.81	289.37	289.93	290.50	291.06	291.62	292.18
520	292.75	293.31	293.87	294.44	295.00	295.56	296.13	296.69	297.25	297.81
530	298.38	298.94	299.50	300.07	300.63		301.76	302.32	302.88	303.44
980	230.00	200:04	200.00	300.07	300.03	001.13	1 301.70	302.02	002.00	000.44
Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
27 Inch.	Par. line	Par line.	Par. line.	Par. line.	Par. line.	Par line.	Par. line.	Par. line.	Par. line	Par. line
540	304.01	304.06	304.12	304.18	304.23	304.29	304.34	304.40	304.46	304.51
541	304.57	304.63	304.68	304.74	304.80	304.85	304.91	304.96	305.02	305.08
542	305.13	305.19	305.25	305.30	305.36	305.41	305.47	305.53	305.58	305.64
543	305.70	305.75	305.81	305.86	305.92	305.98	306.03	306.09	306.15	306.20
544	306.26	306.32	306.37	306.43	306.48	306.54	306.60	306.65	306.71	306.77
545	306.82	306.88	306.93	306.99	307.05	307.10	307.16	307.22	307.27	307.33
546	307.38	307.44	307.50	307.55	307.61	307.67	307.72	307.78	307.84	307.89
547	307.95	308.00	308.06	308.12	308.17	308.23	308.29	308.34	308.40	308.45
548	308.51	308.57	308.62	308.68	308.74	308.79	308.85	308.90	308.96	309.02
549 27.5 In.	309.07	309.13	309.19	309.24	309.30	309.36	309.41	309.47	309.52	309.58
550	309.64	309.69	309.75	309.81	309.86	309.92	309.97	310.03	310.09	310.14
551	310.20	310.26	310.31	310.37	310.42	310.48	310.54	310.59	310.65	310.71
552	310.76	310.82	310.88	310.93	310.99	311.04	311.10	311.16	311.21	311.27
553	311.33	311.38	311.44	311.49	311.55	311.61	311.66	311.72	311.78	311.83
554	311.89	311.95	312.00	312.06	312.11	312.17	312.23	312.28	312.34	312.40
555	312.45	312.51	312.56	312.62	312.68	312.73	312.79	312.85	312.90	312.96
556	313.01	313.07	313.13	313.18	313.24	313.30	313.35	313.41	313.47	313.52
557	313.56	313.63	313.69	313.75	313.80	313.86	313.92	313.97	314.03	314.08
558	314.14	314.20	314.25	314.31	314.37	314.42	314.48	314.53	314.59	314.65
559	314.70	314.76	314.82	314.87	314.93	314.99	315.04	315.10	315.15	315.21
28 Inch.	7.1110	3.1110	011.02	011.01	011100		310101	0.00.00	010110	010.21
560	315.27	315.32	315.38	315.44	315.49	315.55	315.60	315.66	315.72	315.77
561	315.83	315.89	315.94	316.00	316.05	316.11	316.17	316.22	316.28	316.34
562	316.39	316.45	316.51	316.56	316.62	316.67	316.73	316.79	316.84	316.90
563	316.96	317.01	317.07	317.12	317.18	317.24	317.29	317.35	317.41	317.46
564	317.52	317.57	317.63	317.69	317.74	317.80	317.86	317.91	317.97	318.03
565	318.08	318.14	318.19	318.25	318.31	318.36	318.42	318.48	318.53	318.59
566	318.64	318.70	318.76	318.81	318.87	318.93	318.98	319.04	319.09	319.15
567	319.21	319.26	319.32	319.38	319.43	319.49	319.55	319.60	319.66	319.71
568	319.77	319.83	319.88	319.94	320.00	320.05	320.11	320.16	320.22	320.28
569	320.33	320.39	320.45	320.50	320.56		320.67	320.73	320.78	320.84

## COMPARISON OF THE RUSSIAN AND OLD FRENCH BAROMETERS.

1 Russian Half-Line = 0.562976 Paris Line.

Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
28.5 Inch.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. lin
570	320.90	320.95	321.01	321.07	321.12	321.18	321.23	321.29	321.35	321.4
571	321.46	321.52	321.57	321.63	321.68	321.74	321.80	321.85	321.91	321.9
572	322.02	322.08	322.13	322.19	322.25	322.30	322.36	322.42	322.47	322.5
573	322.59	322.64	322.70	322.75	322.81	322.87	322.92	322.98	323.04	323.0
574	323.15	323.20	323.26	323.32	323.37	323.43	323.49	323.54	323.60	323.6
575	323.71	328.77	323.82	323.88	323.94	323.99	324.05	324.11	324.16	324.2
576	324.27	324.33	324.39	324.44	324.50	324.56	324.61	324.67	324.72	324.7
577	324.84	324.89	324.95	325.01	325.06	325.12	325.17	325.23	325.29	325.3
578	325.40	325.46	325.51	325.57	325.63	325.68	325.74	325.79	325.85	325.9
579	325.96	326.02	326.08	326.13	326.19	326.24	326.30	326.36	326.41	326.4
29 Inch.										
580	326.53	326.58	326.64	326.69	326.75	326.81	326.86	326.92	326.98	327.0
581	327.09	327.15	327.20	327.26	327.31	327.37	327.43	327.48	327.54	327.6
582	327.65	327.71	327.76	327.82	327.88	327.93	327.99	328.05	328.10	328.1
583	328.22	328.27	328.33	328.38	328.44	328.50	328.55	328.61	328.67	328.7
584	328.78	328.83	328.89	328.95	329.00	329.06	329.12	329.17	329.23	329.2
585	329.34	329.40	329.45	329.51	329.57	329.62	329.68	329.74	329.79	329.8
586	329.90	329.96	330.02	330.07	330.13	330.19	330.24	330.30	330.35	330.4
587	330.47	330.52	330.58	330.64	330.69	330.75	330.80	330.86	330.92	330.9
588	331.03	331.09	331.14	331.20	331.26	331.31	331.37	331.42	331.48	331.5
589 <b>29.5</b> In.	331.59	331.65	331.71	331.76	331.82	331.87	331.93	331.99	332.04	332.1
590	332.16	332.21	332.27	332.32	332.38	332.44	332.49	332.55	332.61	332.6
591	332.72	332.78	332.83	332.89	332.94	333.00	333.06	333.11	333.17	333.2
592	333.28	333.34	333.39	333.45	333.51	333.56	333.62	333.68	333.73	333.7
593	333.84	333.90	333.96	334.01	334.07	334.13	334.18	334.24	334.30	334.3
594	334.41	334.46	334.52	334.58	334.63	334.69	334.75	334.80	334.86	334.9
595	334.97	335.03	335.08	335.14	335.20	335.25	335.31	335.36	335.42	335.4
596	335.53	335.59	335.65	335.70	335.76	335.82	335.87	335.93	335.98	336.0
597	336.10	336.15	336.21	336.27	336.32	336.38	336.43	336.49	336.55	336.6
598	336.66	336.72	336.77	336.83	336.88	336.94	337.00	337.05	337.11	337.1
599	337.22	337.28	337.34	337.39	337.45	337.50	337.56	337.62	337.67	337.7
30 Inch.		30,.20	3001	3000	30,.10	30,.00	30,100	30,102	301101	55111
600	337.79	337.84	337.90	337.95	338.01	338.07	338.12	338.18	338.24	338.2
601	338.35	338.40	338.46	338.52	338.57	338.63	338.69	338.74	338.80	338.8
602	338.91	338.97	339.02	339.08	339.14	339.19	339.25	339.31	339.36	339.4
603	339.47	339.53	339.59	339.64	339.70	339.76	339.81	339.87	339.92	339.9
604	340.04	340.09	340.15	340.21	340.26	340.32	340.38	340.43	340.49	340.5
605	310.60	340.66	340.71	340.77	340.83	340.88	340.94	340.99	341.05	341.1
606	341.16	341.22	341.28	341.33	341.39	341.44	341.50	341.56	341.61	341.6
607	341.73	341.78	341.84	341.90	341.95	342.01	342.06	342.12	342.18	342.2
608	342.29	342.35	342.40	342.46	342.51	342.57	342.63	342.68	342.74	342.8
609	342.85	342.91	342.96	343.02	343.08	313.13	343.19	343.25	343.30	343.3
				H	andredths.					
0.000	0.006	0.011	0.017	0.02	2 0.0	10   0	034   0	.039	0.045	0.051



IX. - XVI.

COMPARISON

OF

# BAROMETRICAL DIFFERENCES

EXPRESSED IN MEASURES OF DIFFERENT SCALES,

OR

## TABLES

FOR CONVERTING ENGLIST/ INCHES, MILLIMETRES, PARIS LINES, AND RUSSIAN HALF-LINES INTO EACH OTHER.



## IX. CONVERSION OF ENGLISH INCHES INTO MILLIMETRES.

1 English Inch = 25.39954 Millimetres.

English				Н	undredths	of an Inc	h.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	S.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0.0	0.000	0.254	0.508	0.762	1.016	1.270	1.524	1.778	2.032	2.286
0.1	2.540	2.794	3.048	3.302	3.556	3.810	4.064	4.318	4.572	4.826
0.2	5.080	5.334	5.588	5.842	6.096	6.350	6.604	6.858	7.112	7.366
0.3	7.620	7.874	8.128	8.382	8.636	8.890	9.144	9.398	9.652	9.906
0.4	10.160	10.414	10.668	10.922	11.176	11.430	11.684	11.938	12.192	12.446
. 0.5	12.700	12.954	13.208	13.462	13.716	13.970	14.224	14.478	14.732	14.986
0.6	15.240	15.494	15.748	16.002	16.256	16.510	16.764	17.018	17.272	17.526
0.7	17.780	18.034	18.288	18.542	18.796	19.050	19.304	19.558	19.812	20.066
0.8	20.320	20.574	20.828	21.082	21.336	21.590	21.844	22.098	22.352	22.606
0.9	22.860	23.114	23.368	23.622	23.876	24.130	24.384	24.638	24.892	25.146
1.0	25.400	25.654	25.908	26.162	26.416	26.670	26.924	27.178	27.432	27.685
1.1	27.939	28.193	28.447	28.701	28.955	29.209	29.463	29.717	29.971	30.225
1.2	30.479	30.733	30.987	31.241	31.495	31.749	32.003	32.257	32.511	32.765
1.3	33.019	33.273	33.527	33.781	34.035	34.289	34.543	34.797	35.051	35.305
1.4	35.559	35.813	36.067	36.321	36.575	36.829	37.083	37.337	37.591	37.845
1.5	38.099	28.353	38.607	38.861	39.115	39.369	39.623	39.877	40.131	40.385
1.6	40.639	40.893	41.147	41.401	41.655	41.909	42.163	42.417	42.671	42.925
1.7	43.179	43.433	43.687	43.941	44.195	44.449	44.703	44.957	45.211	45.465
1.8	45.719	45.973	46.227	46.481	46.735	46.989	47.243	47.497	47.751	48.005

## X. CONVERSION OF ENGLISH INCHES INTO FRENCH OR PARIS LINES. 1 English Inch = 11.259515 Paris Lines.

English				I	Iundredths	of an Inc	h.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.
0.0	0.000	0.113	0.225	0.338	0.450	0.563	0.676	0.788	0.901	1.013
0.1	1.126	1.239	1.351	1.464	1.576	1.689	1.802	1.914	2.027	2.139
0.2	2.252	2.364	2.477	2.590	2.702	2.815	2.927	3.040	3.153	3.265
0.3	3.378	3.490	3.603	3.716	3.828	3.941	4.053	4.166	4.279	4.391
0.4	4.504	4.616	4.729	4.842	4.954	5.067	5.179	5.292	5.405	5.517
0.5	5.630	5.742	5.855	5.968	6.080	6.193	6.305	6.418	6.531	6.643
0.6	6.756	6.868	6.981	7.093	7.206	7.319	7.431	7.544	7.656	7.769
0.7	7.882	7.994	8.107	8.219	8.332	8.445	8.557	8.670	8.782	8.895
0.8	9.008	9.120	9.233	9.345	9.458	9.571	9.683	9.796	9.908	10.021
0.9	10.134	10.246	10.359	10.471	10.584	10.697	10.809	10.922	11.034	11.147
1.0	11.260	11.372	11.485	11.597	11.710	11.822	11.935	12.048	12.160	12.273
1.1	12.385	12.498	12.611	12.723	12.836	12.948	13.061	13.174	13.286	13.399
1.2	13.511	13.624	13.737	13.849	13.962	14.074	14.187	14.300	14.412	14.525
1.3	14.637	14.750	14.863	14.975	15.088	15.200	15.313	15.426	15.538	15.651
1.4	15.763	15.876	15.988	16.101	16.214	16.326	16.439	16.551	16.664	16.777
1.5	16.889	17.002	17.114	17.227	17.340	17.452	17.565	17.677	17.790	17.903
1.6	18:015	18.128	18.240	18.353	18.466	18.578	18.691	18.803	18.916	19.029
1.7	19.141	19.254	19.366	19.479	19.592	19.704	19.817	19.929	20.042	20.155
1.8	20.267	20.380	20.492	20.605	20.717	20.830	20.943	21.055	21.168	21.280

## XI. CONVERSION OF MILLIMETRES INTO ENGLISH INCHES.

1 Metre = 39.37079 English Inches.

Millime-				1	Cenths of a	Millimetr	e.			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In. 0.0000	Eng. In. 0.0039	Eng. In. 0.0079	Eng. In. 0.0118	Eng. In.	Eng. In. 0.0197	Eng. In. 0.0236	Eng. In.	Eng. In. 0.0315	Eng.
0	0.0394	0.0039	0.0079	0.0512	0.0157	0.0197	0.0230	0.0276		0.03
1	0.0394	0.0455	0.0472	0.0912	0.0945	0.0984	0.0030	0.1063	0.0709	0.07
2	1	0.0327		0.0300		0.0354	0.1024	Ī	0.1102	0.11
3	0.1181 $0.1575$		0.1260	0.1299	0.1339			0.1457	0.1496	0.15
4	0.1575	0.1614	0.1654	0.1095	0.1732	0.1772	0.1811	0.1850	0.1890	0.19
5	0.1969	0.2008	0.2047	0.2087	0.2126	0.2165	0.2205	0.2244	0.2283	0.23
6	0.2362	0.2402	0.2441	0.2480	0.2520	0.2559	0.2598	0.2638	0.2677	0.27
7	0.2756	0.2795	0.2835	0.2874	0.2913	0.2953	0.2992	0.3032	0.3071	0.31
8	0.3150	0.3189	0.3228	0.3268	0.3307	0.3347	0.3386	0.3425	0.3465	0.350
9	0.3543	0.3583	0.3622	0.3661	0.3701	0.3740	0.3780	0.3819	0.3858	0.389
10	0.3937	0.3976	0.4016	0.4055	0.4095	0.4134	0.4173	0.4213	0.4252	0.429
11	0.4331	0.4370	0.4410	0.4449	0.4488	0.4528	0.4567	0.4606	0.4646	0.468
12	0.4724	0.4764	0.4803	0.4843	0.4882	0.4921	0.4961	0.5000	0.5039	0.507
13	0.5118	0.5158	0.5197	0.5236	0.5276	0.5315	0.5354	0.5394	0.5433	0.547
14	0.5512	0.5551	0.5591	0.5630	0.5669	0.5709	0.5748	0.5788	0.5827	0.586
15	0.5906	0.5945	0.5984	0.6024	0.6063	0.6102	0.6142	0.6181	0.6221	0.626
16	0.6299	0.6339	0.6378	0.6417	0.6457	0.6496	0.6536	0.6575	0.6614	0.665
17	0.6693	0.6732	0.6772	0.6811	0.6851	0.6890	0.6929	0.6969	0.7008	0.70-
18	0.7087	0.7126	0.7165	0.7205	0.7244	0.7284	0.7323	0.7362	0.7402	0.74
19	0.7480	0.7520	0.7559	0.7599	0.7638	0.7677	0.7717	0.7756	0.7795	0.783
20	0.7874	0.7914	0.7953	0.7992	0.8032	0.8071	0.8110	0.8150	0.8189	0.822
21	0.8268	0.8307	0.8347	0.8386	0.8425	0.8465	0.8504	0.8543	0.8583	0.863
22	0.8662	0.8701	0.8740	0.8780	0.8819	0.8858	0.8898	0.8937	0.8977	0.901
23	0.9055	0.9095	0.9134	0.9173	0.9213	0.9252	0.9292	0.9331	0.9370	0.94
24	0.9449	0.9488	0.9528	0.9567	0.9606	0.9646	0.9685	0.9725	0.9764	0.980
25	0.9843	0.9882	0.9921	0.9961	1.0000	1.0040	1.0079	1.0118	1.0158	1.019
26	1.0236	1.0276	1.0315	1.0355	1.0394	1.0433	1.0473	1.0512	1.0551	1.059
27	1.0630	1.0669	1.0709	1.0748	1.0788	1.0827	1.0866	1.0906	1.0945	1.098
28	1.1024	1.1063	1.1103	1.1142	1.1181	1.1221	1.1260	1.1299	1.1339	1.137
29	1.1418	1.1457	1.1496	1.1536	1.1575	1.1614	1.1654	1.1693	1.1732	1.177
30	1.1811	1.1851	1.1890	1.1929	1.1969	1.2008	1.2047	1.2087	1.2126	1.216
31	1.2205	1.2244	1.2284	1.2323	1.2362	1.2402	1.2441	1.2481	1.2520	1.25
32	1.2599	1.2638	1.2677	1.2717	1.2756	1.2796	1.2835	1.2874	1.2914	1.295
33	1.2992	1.3032	1.3071	1.3110	1.3150	1.3189	1.3229	1.3268	1.3307	1.33
34	1.3386	1.3425	1.3465	1.3504	1.3544	1.3583	1.3622	1.3662	1.3701	1.37
35	1.3780	1.3819	1.3859	1.3898	1.3937	1.3977	1.4016	1.4055	1.4095	1.418
36	1.4173	1.4213	1.4252	1.4292	1.4331	1.4370	1.4410	1.4449	1.4488	1.452
37	1.4567	1.4607	1.4646	1.4685	1.4725	1.4764	1.4803	1.4843	1.4882	1.492
38	1.4961	1.5000	1.5040	1.5079	1.5118	1.5158	1.5197	1.5236	1.5276	1.531
39	1.5355	1.5394	1.5433	1.5473	1.5512	1.5551	1.5591	1.5630	1.5670	1.570
40	1.5748	1.5788	1.5827	1.5866	1.5906	1.5945	1.5985	1.6024	1.6063	1.610
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

## XII. CONVERSION OF MILLIMETRES INTO FRENCH OR PARIS LINES.

1 Millimetre = 0.443296 Paris Line.

Millime-				7	enths of a	Millimetre	·.			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par. line.		Par. line.	Par. line.	Par. line.	Par. line.		Par. line.	l.	Par. lin
0	0.000	0.044	0.089	0.133	0.177	0.222	0.266	0.310	0.355	0.39
1	0.443	0.488	0.532	0.576	0.621	0.665	0.709	0.754	0.798	0.84
2	0.887	0.931	0.975	1.020	1.064	1.108	1.153	1.197	1.241	1.28
3	1.330	1.374	1.419	1.463	1.507	1.552	1.596	1.640	1.685	1.72
4	1.773	1.818	1.862	1.906	1.950	1.995	2.039	2.083	2.128	2.17
5	2.216	2.261	2.305	2.349	2.394	2.438	2.482	2.527	2.571	2.61
6	2.660	2.704	2.748	2.793	2.837	2.881	2.926	2.970	3.014	3.05
7	3.103	3.147	3.192	3.236	3.280	3.325	3.369	3.413	3.458	3.50
8	3.546	3.591	3.635	3.679	3.724	3.768	3.812	3.857	3.901	3.94
9	3.990	4.034	4.078	4.123	4.167	4.211	4.256	4.300	4.344	4.38
10	4.433	4.477	4.522	4.566	4.610	4.655	4.699	4.743	4.788	4.83
11	4.876	4.921	4.965	5.009	5.054	5.098	5.142	5.187	5.231	5.27
12	5.320	5.364	5.408	5.453	5.497	5.541	5.586	5.630	5.674	5.71
13	5.763	5.807	5.851	5.896	5.940	5.984	6.029	6.073	6.117	6.16
14	6.206	6.250	6.295	6.339	6.383	6.428	6.472	6.516	6.561	6.60
15	6.649	6.694	6.738	6.782	6.827	6.871	6.915	6.960	7.004	7.04
16	7.093	7.137	7.181	7.226	7.270	7.314	7.359	7.403	7.447	7.49
17	7.536	7.580	7.625	7.669	7.713	7.758	7.802	7.846	7.891	7.93
18	7.979	8.024	8.068	8.112	8.157	8.201	8.245	8.290	8.334	8.37
19	8.423	8.467	8.511	8.556	8.600	8.644	8.689	8.733	8.777	8.82
20	8.866	8.910	8.955	8.999	9.043	9.088	9.132	9.176	9.221	9.26
21	9.309	9.354	9.398	9.442	9.487	9.531	9.575	9.620	9.664	9.70
22	9.753	9.797	9.841	9.886	9.930	9.974	10.018	10.063	10.107	10.15
23	10.196	10.240	10.284	10.329	10.373	10.417	10.462	10.506	10.550	10.59
24	10.639	10.683	10.728	10.772	10.816	10.861	10.905	10.949	10.994	11.03
25	11.082	11.127	11.171	11.215	11.260	11.304	11.348	11.393	11.437	11.48
26	11.526	11.570	11.614	11.659	11.703	11.747	11.792	11.836	11.880	11.92
27	11.969	12.013	12.058	12.102	12.146	12.191	12.235	12.279	12.324	12.36
28	12.412	12.457	12.501	12.545	12.590	12.634	12.678	12.723	12.767	12.81
29	12.856	12.900	12.944	12.989	13.033	13.077	13.122	13.166	13.210	13.25
30	13.299	13.343	13.388	13.432	13.476	13.521	13.565	13.609	13.654	13.69
31	13.742	13.786	13.831	13.875	13.919	13.964	14.008	14.052	14.097	14.14
32	14.185	14.230	14.274	14.318	14.363	14.407	14.451	14.496	14.540	14.58
33	14.629	14.673	14.717	14.762	14.806	14.850	14.895	14.939	14.983	15.02
34	15.072	15.116	15.161	15.205	15.249	15.294	15.338	15.382	15.427	15.47
35	15.515	15.560	15.604	15.648	15.693	15.737	15.781	15.826	15.870	15.91
36	15.959	16.003	16.047	16.092	16.136	16.180	16.225	16.269	16.313	16.35
37	16.402	16.446	16.491	16.535	16.579	16.624	16.668	16.712	16.757	16.80
38	16.845	16.890	16.934	16.978	17.023	17.067	17.111	17.156	17.200	17.24
39	17.289	17.333	17.377	17.422	17.466	17.510	17.555	17.599	17.643	17.68
40	17.732	17.776	17.820	17.865	17.909	17.953	17.998	18.042	18.086	18.13
	0.	1.	2.	3.	4.	5.	6.	7.	<b>S.</b>	9.

1 Paris Line = 2.255829 Millimetres.

Paris					Tenths o	f a Line.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim,
0	0.000	0.226	0.451	0.677	0.902	1.128	1.353	1.579	1.805	2.030
1	2.256	2.481	2.707	2.933	3.158	3.384	3.609	3.835	4.060	4.286
2	4.512	4.737	4.963	5.188	5.414	5.640	5.865	6.091	6.316	6.542
3	6.767	6.993	7.219	7.444	7.670	7.895	8.121	8.347	8.572	8.798
4	9.023	9.249	9.474	9.700	9.926	10.151	10.377	10.602	10.828	11.054
5	11.279	11.505	11.730	11.956	12.181	12.407	12.633	12.858	13.084	13.309
6	13.535	13.761	13.98€	14.212	14.437	14.663	14.888	15.114	15.340	15.565
7	15.791	16.016	16.242	16.468	16.693	16.919	17.144	17.370	17.595	17.821
8	18.047	18.272	18.498	18.723	18.949	19.175	19.400	19.626	19.851	20.077
9	20.302	20.528	20.754	20.979	21.205	21.430	21.656	21.882	22.107	22.333
10	22.558	22.784	23.009	23.235	23.461	23.686	23.912	24.137	24.363	24.589
11	24.814	25.040	25.265	25.491	25.716	25.942	26.168	26.393	26.619	26.844
12	27.070	27.296	27.521	27.747	27.972	28.198	28.423	28.649	28.875	29.100
13	29.326	29.551	29.777	30.003	30.228	30.454	30.679	30.905	31.130	31.356
14	31.582	31.807	32.033	32.258	32.485	32.711	32.936	33.162	33.387	33.613
15	33.837	34.063	34.289	34.514	34.740	34.965	35.191	35.417	35.642	35.868
16	36.093	36.319	36.544	36.770	36.996	37.221	37.447	37.672	37.898	38.124
17	38.349	38.575	38.800	39.026	39.251	39.477	39.703	39.928	40.154	40.379
18	40.605	40.831	41.056	41.282	41.507	41.733	41.958	42.184	42.410	42.635

XIV. CONVERSION OF FRENCH OR PARIS LINES INTO ENGLISH INCHES.  $1 \ {\rm Paris} \ {\rm Line} = 0.088814 \ {\rm English} \ {\rm Inch.}$ 

Paris					Tenths o	f a Line.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In	Eng. In.	Eng. In.	Eng. 1n.	Eng. In.	Eng. In.
0	0.0000	0.0089	0.0178	0.0266	0.0355	0.0444	0.0533	0.0622	0.0711	0.0799
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.1687
2	0.1776	0.1865	0.1954	0.2043	0.2132	0.2220	0.2309	0.2398	0.2487	0.2576
3	0.2664	0.2753	0.2842	0.2931	0.3020	0.3108	0.3197	0.3286	0.3375	0.3464
4	0.3553	0.3641	0.3730	0.3819	0.3908	0.3997	0.4085	0.4174	0.4263	0.4352
5	0.4441	0.4530	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.5240
6	0.5329	0.5418	0.5506	0.5595	0.5684	0.5773	0.5862	0.5951	0.6039	0.6128
7	0.6217	0.6306	0.6395	0.6483	0.6572	0.6661	0.6750	0.6839	0.6927	0.7016
8	0.7105	0.7194	0.7283	0.7372	0.7460	0.7549	0.7638	0.7727	0.7816	0.7904
9	0.7993	0.8082	0.8171	0.8260	0.8349	0.8437	0.8526	0.8615	0.8704	0.8793
10	0.8881	0.8970	0.9059	0.9148	0.9237	0.9325	0.9414	0.9503	0.9592	0.9681
11	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0302	1.0391	1.0480	1.0569
12	1.0658	1.0746	1.0835	1.0924	1.1013	1.1102	1.1191	1.1279	1.1368	1.1457
13	1.1546	1.1635	1.1723	1.1812	1.1901	1.1990	1.2079	1.2168	1.2256	1.2345
14	1.2434	1.2523	1.2612	1.2700	1.2789	1.2878	1.2967	1.3056	1.3144	1.3233
15	1.3322	1.3411	1.3500	1.3589	1.3677	1.3766	1.3855	1.3944	1.4033	1.4121
16	1.4210	1.4299	1.4388	1.4477	1.4565	1.4654	1.4743	1.4832	1.4921	1.5010
17	1.5098	1.5187	1.5276	1.5365	1.5454	1.5542	1.5631	1.5720	1.5809	1.5898
18	1.5987	1.6075	1.6164	1.6253	1.6342	1.6431	1.6519	1.6608	1.6697	1.6786

## XV. CONVERSION OF RUSSIAN HALF-LINES INTO MILLIMETRES.

1 Russian Half-Line = 1.269977 Millimetres.

Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.000	0.127	0.254	0.381	0.508	0.635	0.762	0.889	1.016	1.143
1	1.270	1.397	1.524	1.651	1.778	1.905	2.032	2.159	2.286	2.413
2	2.540	2.667	2.794	2.921	3.048	3.175	3.302	3.429	3.556	3.683
3	3.810	3.937	4.064	4.191	4.318	4.445	4.572	4.699	4.826	4.953
4	5.080	5.207	5.334	5.461	5.588	5.715	5.842	5.969	6.096	6.223
5	6.350	6.477	6.604	6.731	6.858	6.985	7.112	7.239	7.366	7.493
6	7.620	7.747	7.874	8.001	8.128	8.255	8.382	8.509	8.636	8.763
7	8.890	9.017	9.144	9.271	9.398	9.525	9.652	9.779	9.906	10.033
8	10.160	10.287	10.414	10.541	10.668	10.795	10.922	11.049	11.176	11.303
9	11.430	11.557	11.684	11.811	11.938	12.065	12.192	12.319	12.446	12.573
10	12.700	12.827	12.954	13.081	13.208	13.335	13.462	13.589	13.716	13.843
11	13.970	14.097	14.224	14.351	14.478	14.605	14.732	14.859	14.986	15.113
12	15.240	15.367	15.494	15.621	15.748	15.875	16.002	16.129	16.256	16.383
13	16.510	16.637	16.764	16.891	17.018	17.145	17.272	17.399	17.526	17.653
14	17.780	17.907	18.034	18.161	18.288	18.415	18.542	18.669	18.796	18.923
15	19.050	19.177	19.304	19.431	19.558	19.685	19.812	19.939	20.066	20.193
16	20.320	20.447	20.574	20.701	20.828	20.955	21.082	21.209	21.336	21.463
17	21.590	21.717	21.844	21.971	22.098	22.225	22.352	22.479	22.606	22.733
18	22.860	22.987	23.114	23.241	23.368	23.495	23.622	23.749	23.876	24.003

## XVI. CONVERSION OF RUSSIAN HALF-LINES INTO PARIS LINES.

1 Russian Half-Line = 0.562976 Paris Line.

Russian					Ter	iths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par. line	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.
0	0.000	0.056	0.113	0.169	0.225	0.281	0.338	0.394	0.450	0.507
1	0.563	0.619	0.676	0.732	0.788	0.844	0.901	0.957	1.013	1.070
2	1.126	1.182	1.239	1.295	1.351	1.407	1.464	1.520	1.576	1.633
3	1.689	1.745	1.802	1.858	1.914	1.970	2.027	2.083	2.139	2.196
4	2.252	2.308	2.364	2.421	2.477	2.533	2.590	2.646	2.702	2.759
5	2.815	2.871	2.927	2.984	3.040	3.096	3.153	3.209	3.265	3.322
6	3.378	3.434	3.490	3.547	3.603	3.659	3.716	3.772	3.828	3.885
7	3.941	3.997	4.053	4.110	4.166	4.222	4.279	4.335	4.391	4.448
8	4.504	4.560	4.616	4.673	4.729	4.785	4.842	4.898	4.954	5.010
9	5.067	5.123	5.179	5.236	5.292	5.348	5.405	5.461	5.517	5.573
10	5.630	5.686	5.742	5.799	5.855	5.911	5.968	6.024	6.080	6.136
11	6.193	6.249	6.305	6.362	6.418	6.474	6.531	6.587	6.643	6.699
12	6.756	6.812	6.868	6.925	6.981	7.037	7.093	7.150	7.206	7.262
13	7.319	7.375	7.431	7.488	7.544	7.600	7.656	7.713	7.769	7.825
14	7.882	7.938	7.994	8.051	8.107	8.163	8.219	8.276	8.332	8.388
15	8.445	8.501	8.557	8.614	8.670	8.726	8.782	8.839	8.895	8.951
16	9.008	9.064	9.120	9.177	9.233	9.289	9.345	9.402	9.458	9.514
17	9.571	9.627	9.683	9.739	9.796	9.852	9.908	9.965	10.021	10.077
18	10.134	10.190	10.246	10.302	10.359	10.415	10.471	10.528	10.584	10.640



# TABLES

FOR

# REDUCING BAROMETRICAL OBSERVATIONS,

TAKEN AT ANY TEMPERATURE,

TO THE TEMPERATURE OF THE FREEZING POINT.



#### TABLES

FOR

REDUCING THE BAROMETRICAL OBSERVATIONS TAKEN AT ANY TEMPERATURE TO THE TEMPERATURE OF THE FREEZING POINT.

The variations of the mercurial column in a stationary barometer are due to two causes, the changes of atmospheric pressure and the variations of temperature of the mercury, which affect the length of the column by changing its density. The variations of atmospheric pressure, which alone the barometer is destined to ascertain, are therefore hidden, and their observation falsified by the expansion or contraction of the mercury due to changes of temperature. For, supposing that, while the atmospheric pressure remains the same, the temperature of the instrument becomes lower, the mercurial column will become shorter, and the barometer will appear to fall; if the pressure becomes less, but the temperature increases, the expansion of the mercury will tend to compensate the diminution of pressure, and the barometer may remain stationary, or even may rise, while it ought to be falling; in other cases the action of temperature will tend to increase the amount of the changes of the barometrical height. It is therefore evident that successive observations, with the same barometer, do not give directly the actual changes of atmospheric pressure, unless they have been taken exactly at the same temperature, a case which, in practice, seldom occurs. Likewise simultaneous observations, taken with various barometers, do not give directly the actual differences of the absolute pressure of the atmosphere above the instruments. To obtain the true barometrical heights, that is, the action of the atmospheric pressure alone, the influence of the temperature must first be eliminated from the observed heights. This is done by reducing, by means of the following Tables, the various barometrical columns to the length they would have at a given temperature, which is the same for all. For the sake of convenient comparison, the freezing point has been almost universally adopted as the standard temperature to which all observations are to be reduced.

#### Construction of the Tables.

In all the following Tables the barometers are supposed to be furnished with brass scales, extending from the surface of the mercury in the cistern to the top of the mercurial column. The correction to be applied is therefore composed of two elements: the correction for the expansion of the mercury, and that for the expansion of the scale; both of which ought to be, and have been, taken into account.

Indeed, the correction for the expansion of mercury is not sufficient to reduce the readings to the height which the barometer would indicate, under the same pressure, at the temperature of the freezing point. For when the temperature rises the mercurial column expands; but then the scale also grows longer, and this will tend to lower the reading of the height. The correction for the expansion of the mercury

 $\mathbf{C}$ 

must thus be diminished by the amount of that of the scale, that is, by nearly 100 this being the proportion between the expansion of brass and that of mercury.

It is also the expansion of the scale which causes an apparent anomaly in the Tables for the Reduction of the English and Old French Barometers. It can be seen, that, though the observations are to be reduced to the freezing point, or to 32° Fahrenheit and zero Reaumur, the Tables give still a correction for observations taken at that temperature. The reason of it is, that the normal length of the English and Old French standards has not been determined at the temperature of the freezing point, as is the case with the metre, but respectively at the temperatures of 62° Fahrenheit and 13° Reaumur. It is thus only at these temperatures that the scales graduated with these standards have their true length. Above and below, the inches of the scales are longer or shorter than the inches of the standards. At the freezing point, therefore, the correction for the expansion of the mercury is null, but that for the expansion of the scale is not. The scale being too short, the reading will be too high, and a subtractive correction must still be applied, which will be gradually compensated at lower temperatures by the now additive correction of the mercurial column. Thus the point of no correction will occur at 28°.5 Fahrenheit, instead of 32°, in the English Barometer, and at -1°.5 Reaumur, instead of zero, in the Old French.

Schumacher has calculated and published in his Collection of Tables, &c., and in his Jahrbuch for 1836, 1837, and 1838, extensive tables for the reduction of the English, Old French, and Metrical Barometers, using the following general formula:—

Let h =observed height.

" t = temperature of the attached thermometer.

" T = temperature to which the observed height is to be reduced.

" m = expansion, in volume, of mercury.

" l = linear expansion of brass.

"  $\vartheta$  = normal temperature of the standard scale.

The reduction to the freezing point will be given by the formula, -

$$h \cdot \frac{m(t-T)-l(t-\vartheta)}{1+m(t-T)}$$

The following tables, which may be found more convenient for ordinary use, have been calculated from the same formula. Table XVII., published in the Instructions of the Royal Society of London, is mostly abstracted from the table of Schumacher. It gives the reduction of the English Barometer, adopting the following values:—

Let h = observed height in English inches.

" t = temperature of attached thermometer in degrees of Fahrenheit.

" m = expansion, in volume, of mercury for one degree Fahrenheit = 0.0001001.

" l = linear expansion of brass for one degree Fahrenheit = 0.0000104344.

The normal temperature of standard being  $=62^{\circ}$ .

The reduction to 32° Fahrenheit will be given then by the formula,

$$-h \cdot \frac{m(t-32)-l(t-62)}{1+m(t-32)}.$$

The elements for the other tables are found at the head of each.

## XVII.

## ENGLISH BAROMETER.

## TABLE

# GIVING THE CORRECTION TO BE APPLIED TO ENGLISH BAROMETERS,

WITH BRASS SCALES EXTENDING FROM THE CISTERN TO THE TOP OF
THE MERCURIAL COLUMN, FOR REDUCING THE OBSERVATIONS
TO THIRTY-TWO DEGREES FAHRENHEIT.



#### TABLE XVII.

The following Table, calculated after that of Schumacher, has been adopted by the Committee of Physics and Meteorology of the Royal Society of London. It gives immediately the correction for every degree of Fahrenheit, and for every half-inch from 20 up to 31 inches. The scale of the barometer is supposed to be of brass, extending from the cistern to the top of the mercurial column. The difference of expansion of brass and mercury is taken into account. The standard temperature of the yard being 62° Fahr., and not 32° Fahr., the difference of expansion of the scale and of the mercurial column carries the point of no correction down to 29° Fahr. Therefore, from 29° up the correction must be subtracted from, from 29° down it must be added to, the observed height.

## Examples of Calculation.

Barometer, observed height, . . . . . 30.231
Attached thermometer 82° Fahr.

See in the last page the column of 30 inches; go down as far as the horizontal line corresponding with 82° in the first vertical column, which contains the temperatures; you will find there the correction —.143. We have thus:—

Barometer, observed height,	•	30.231
Subtractive correction for 82° Fahr.,	•	<b>—0.14</b> 3
Barometer at 32° Fahr.,	1	30.088
Barometer, observed height,	•	29.743
Attached thermometer 25° Fahr.		
The column of 29.5 inches opposite to 25° Fahr. give	s an	
additive correction of,	•	+0.009
Barometer at 32° Fahr.,		29.752

It will be easy to apply also the correction for fractions of a degree Fahrenheit; for example:—

Barometer, observed height, . . . . . . . . . . . . 28.358
Attached thermometer 71.3

And barometer at 32° Fahr., . . . . 28.249

Degrees				English	h Inches.				Degrees
of Fah- renheit.	20	20.5	21	21.5	22	22.5	23	23.5	Degrees of Fah- renheit
0	+.051	+.053	+.054	+.055	+.056	+.058	+.059	+.060	0
1	.049	.051	.052	.053	.054	.056	.057	.058	ì
2	.048	.049	.050	.051	.052	.054	.055	.056	2
3	.046	.047	.048	.049	.050	.052	.053	.054	3
5	.044	.045	.046	.047	.048	.050	.051	.052 .050	4 5
6	+.040	+.042	+.042	+.044	+.044	+.046	+.047	+.048	6
7	.039	.040	.041	.042	.042	.044	.044	.046	7
8	.037	.038	.039	.040	.041	.041	.042	.043	8
9	.035	.036	.037	.038	.039	.039	.040	.041	9
10	.033	.034	.035	.036	.037	.037	.038	.039	10
11 12	+.031	+.032	+.033	+.034	+.035	+.035	+.036	+.037	11
13	.030 .028	.030 .029	.031	.032	.033	.033	.034	.035	12
14	.026	.029	.029	.028	.031	.031	.032	.033	13 14
15	.024	.025	.026	.026	.027	.027	.028	.029	15
16	+.022	+.023	+.024	+.024	+.025	+.025	+.026	+.026	16
17	.021	.021	.022	.022	.023	.023	.024	.024	17
18	.019	.019	.020	.020	.021	.021	.022	.022	18
19	.017	.018	.018	.018	.019	.019	.020	.020	19
20	.015	.016	.016	.016	.017	.017	.018	.018	20
21 22	+.014 $.012$	+.014 .012	+.014	+.015 .013	+.015	+.015 .013	+.015 .013	+.016	21 22
23	.012	.012	.012	.013	.013	.013	.013	.014	23
24	.008	.008	.009	.009 -	.009	.009	.009	.010	24
25	.006	.007	.007	.007	.007	.007	.007	.007	25
26	+.005	+.005	+.005	+.005	+.005	+.005	+.005	+.005	26
27	.003	.003	.003	.003	.003	.003	.003	.003	27
28	.001	.001	.001	.001	.001	.001	.001	.001	28
29	001	001	001	001	001	001	001	001	29
30	.003	.003	.003	.003	.003	.003	.003	.003	30
31 32	005 .006	005 .006	005 .007	005 .007	005 .007	005 .007	005 .007	005 .007	31 32
33	.003	.008	.008	.009	.009	.009	.009	.010	33
34	.010	.010	.010	.011	.011	.011	.011	.012	34
35	.012	.012	.012	.013	.013	.013	.013	.014	35
36	013	014	014	014	015	015	016	-016	36
37	.015	.016	.016	.016	.017	.017	.018	.018	37
38 39	.017	.017 .019	.018 .020	.018 .020	.019	.019 .021	.020 .022	.020 .022	38
40	.021	.021	.020	.022	.023	.023	.024	.024	40
41	022	023	024	024	025	025	026	026	41
42	.024	.025	.025	.026	.027	.027	.028	.028	42
43	.026	.027	.027	.028	.029	.029	.030	.031	43
44 45	.028 .030	.029 .030	.029 .031	.030	.031	.031	.032	.033 .035	44 45
46	031	032	033	034	035	035	036	037	46
47	.033	.032	.035	.034	035	.037	.038	.039	47
48	.035	.034	.037	.038	.038	.039	.040	.041	48
49	.037	.038	.039	.040	.040	.041	.042	.043	49
50	.038	.039	.040	.041	.042	.043	.044	.045	50

С

Degrees	*			English	Inches.				Degrees
of Fah- renheit.	20	20.5	21	21.5	22	22.5	23	23.5	of Fah- renheit.
51	040	041	042	043	044	045	046	047	51
52	.042	.043	.044	.045	.046	.047	.048	.049	52
53	.044	.045	.046	.047	.048	.049	.050	.052	53
54	.046	.047	.048	.049	.050	.051	.052	.054	54
55	.047	.049	.050	.051	.052	.053	.055	.056	55
56	049	050	052	053	054	055	057	058	56
57	.051	.052	.054	.055	.056	.057	.059	.060	57
58	.053	.054	.055	.057	.058	.059	.061	.062	58
59	.055	.056	.057	.059	.060	.061	.063	.064	59
60	.056	.058	.059	.061	.062	.063	.065	.066	60
61	058	060	061	062	064	065	067	068	61
62	.060	.061	.063	.064	.066	.067	.069	.070	62
63	.062	.063	.065	.066	.068	.069	.071	.072	63
64	.063	.065	.067	.068	.070	.071	.073	.075	64
65	.065	.067	.068	.070	.072	.073	.075	.077	65
66	067	069	070	072	074	075	077	079	66
67	.069	.071	.072	.074	.076	.077	.079	.081	67
68	.071	.072	.074	.076	.078	.079	.081	.083	68
69	.072	.074	.076	.078	.080	.081	.083	.085	69
70	.074	.076	.078	.080	.082	.083	.085	.087	70
71 72 73 74 75	076 .078 .079 .081 .083	078 .080 .081 .083 .085	080 .082 .083 .085 .087	082 .084 ·.085 .087 .089	083 .085 .087 .089	085 .087 .089 .091 .093	087 .089 .091 .093 .095	089 .091 .093 .095 .098	71 72 73 74 75
76	085	087	089	091	093	095	097	100	76
77	.087	.089	.091	.093	.095	.097	.100	.102	77
78	.088	.091	.093	.095	.097	.099	.102	.104	78
79	.090	.092	.095	.097	.099	.101	.104	.106	79
80	.092	.094	.096	.099	.101	.103	.106	.108	80
81	094	096	098	101	103	105	108	110	81
82	.095	.098	.100	.103	.105	.107	.110	.112	82
83	.097	.100	.102	.104	.107	.109	.112	.114	83
84	.009	.101	.104	.106	.109	.111	.114	.116	84
85	.101	.103	.106	.108	.111	.113	116	.118	85
86	103	105	108	110	113	115	118	120	86
87	.104	.107	.109	.112	.115	.117	.120	.123	87
88	.106	.109	.111	.114	.117	.119	.122	.125	88
89	.108	.111	.113	.116	.119	.121	.124	.127	89
90	.110	.112	.115	.118	.121	.123	.126	.129	90
91	111	114	-117	120	122	125	128	131	91
92	.113	.116	.119	.122	.124	.127	.130	.133	92
93	.115	.118	.121	.124	.126	.129	.132	.135	93
94	.117	.120	.122	.125	.128	.131	.134	.137	94
95	.118	.121	.124	.127	.130	.133	.136	.139	95
96	120	123	126	129	132	135	138	141	96
97	.122	.125	.128	.131	.134	.137	.140	.143	97
98	.124	.127	.130	.133	.136	.139	.142	.145	98
99	.125	.129	.132	.135	.138	.141	.144	.147	99
100	.127	.130	.134	.137	140	.143	.146	.150	100
l	)				27	1	1	1	

Degrees				English	n Inches.			•	Degrees
of Fah- renheit.	24	24.5	25	25.5	26	26.5	27	27.5	of Fah- renheit.
0	+.061	+.063	+.064	+.065	+.067	+.068	+.069	+.071	0
1	.059	.061	.062	.063	.064	.065	.067	.068	1
2 3	.057 .055	.058	.060	.061	.062	.063	.064	.066	2 3
- 4	.053	.054	.057	.056	.060	.061	.052	.063	4
5	.051	.052	.053	.054	.055	.056	.057	.058	5
6	+.049	+.050	+.051	+.052	+.053	+.054	+.055	+.056	6
7 8	.046	.047	.048	.049	.050	.051	.052	.053	7
9	.044	.045	.046	.047	.048	.049	.050	.051	8 9
10	.040	.041	.042	.042	.043	.044	.045	.046	10
11	+.038	+.039	+.039	+.040	+.041	+.042	+.042	+.043	11
12	.036	.036	.037	.038	.039	.039	.040	.041	12
13	.033	.034	.035	.036	.036	.037	.038	.038	13
14 15	.031	.032	.033	.033	.034	.035	.035	.036	14 15
16	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	16
17	.025	.025	.026	.026	.027	.027	.028	.028	17
18	.023	.023	.024	.024	.025	.025	.025	.026	18
19	.021	.021	.021	.022	.022	.023	.023	.024	19
20	.018	.019	.019	.020	.020	.020	.021	.021	20
21	+.016	+.017	+.017	+.017	+.018	+.018	+.018	+.019	21
22 23	.014	.014	.015	.015	.015	.016	.016	.016	22
24	.012	.012	.012	.013 .010	.013	.013	.013	.014	23 24
25	.008	.008	.008	.008	.008	.008	.009	.009	25
26	+.005	+.006	+.006	+.006	+.006	+.006	+.006	+.006	26
27	.003	.003	.003	.003	.004	.004	.004	.004	27
28	.001	.001	.001	.001	.001	.001	.001	.001	28
29 30	001	001	001	001	001	001	001	001	29
30	.003	.003	.003	.004	.004	.004	.004	.004	30
31 32	005 .008	006 .008	006 .008	006 .008	006 .008	006 .008	006 .008	006 .009	31 32
33	.010	.010	.010	.010	.008	.011	.011	.009	33
34	.012	.012	.012	.013	.013	.013	.013	.014	34
35	.014	.014	.015	.015	.015	.015	.016	.016	35
36	016	017	017	017	017	018	018	019	36
37	.018	.019	.019	.019	.020	.020	.021	.021	37
38 39	.020	.021	.021	.022	.022	.023	.023	.023	38
40	.023	.023 .025	.024 .026	.024	.024	.025 .027	.025	.026	39 40
41	027	027	028	- 000	- 000	- 020	- 000	003	47
42	.027	.030	028	029 .031	029 .031	030 .032	030 .033	031	41 42
43	.031	.032	.032	.033	.034	.034	.035	.036	43
44	.033	.034	.035	.035	.036	.037	.037	.038	44
45	.035	.036	.037	.038	.038	.039	.040	.041	45
46	038	038	039	040	041	042	042	043	46
47 48	.040	.041	.041	.042	.043	.044	.045	.046	47
49	.042	.043	.044	.045	.045	.046	.047	.048	48
50	.046	.045	.046	.047	.048	.049	.050 .052	.050	49 50
C					3.030	.001	1 .002	1000	1 30

 $\overline{\mathbf{C}}$ 

Degrees	English Inches.									
of Fah- renheit.	24	24.5	25	25.5	26	26.5	27	27.5	of Fah- renheit.	
51	048	049	050	051	052	053	054	055	51	
52	.050	.052	.053	.054	.055	.056	.057	.058	52	
53	.053	.054	.055	.056	.057	.058	.059	.060	53	
54	.055	.056	.057	.058	.059	.060	.062	.063	54	
55	.057	.058	.059	.060	.062	.063	.064	.065	55	
56 57 58 59 60	059 .061 .063 .065 .068	060 .062 .065 .067 .069	061 .064 .066 .068 .070	063 .065 .067 .070	064 .066 .069 .071 .073	065 .068 .070 .072 .075	066 .069 .071 .074 .076	068 .070 .073 .075	56 57 58 59 60	
61	070	071	073	074	075	077	078	080	61	
62	.072	.073	.075	.076	.078	.079	.081	.082	62	
63	.074	.076	.077	.079	.080	.082	.083	.085	63	
64	.076	.078	.079	.081	.082	.084	.086	.087	64	
65	.078	.080	.082	.083	.085	.086	.088	.090	65	
66	080	082	084	085	087	089	090	092	66	
67	.083	.084	.086	.088	.089	.091	.093	.095	67	
68	.085	.086	.088	.090	.092	.094	.095	.097	68	
69	.087	.089	.090	.092	.094	.096	.098	.100	69	
70	.089	.091	.093	.095	.096	.098	.100	.102	70	
71	091	093	095	097	099	101	102	104	71	
72	.093	.095	.097	.099	.101	.103	.105	.107	72	
73	.095	.097	.099	.101	.103	.105	.107	.109	73	
74	.097	.099	.102	.104	.106	.108	.110	.112	74	
75	.100	.102	.104	.106	.108	.110	.112	.114	75	
76	102	104	106	108	110	112	114	117	76	
77	.104	.106	.108	.110	.112	.115	117	.119	77	
78	.106	.108	.110	.113	.115	.117	.119	.122	78	
79	.108	.110	.113	.115	.117	.119	.122	.124	79	
80	.110	.113	.115	.117	.119	.122	.124	.126	80	
81	112	115	117	119	122	124	126	129	81	
82	.114	.117	.119	.122	.124	.126	.129	.131	82	
83	.117	.119	.121	.124	.126	.129	.131	.134	83	
84	.119	.121	.124	.126	.129	.131	.134	.136	84	
85	.121	.123	.126	.128	.131	.133	.136	.139	85	
86	123	126	128	131	133	136	138	141	86	
87	.125	.128	.130	.133	.136	.138	.141	.143	87	
88	.127	.130	.133	.135	.138	.141	.143	.146	88	
89	.129	.132	.135	.137	.140	.143	.146	.148	89	
90	.131	.134	.137	.140	.142	.145	.148	.151	90	
91	134	136	139	142	145	148	150	153	91	
92	.136	.139	.141	.144	.147	.150	.153	.156	92	
93	.138	.141	.144	.147	.149	.152	.155	.158	93	
94	.140	.143	.146	.149	.152	.155	.157	.161	94	
95	.142	.145	.148	.151	.154	.157	.160	.163	95	
96	144	147	150	153	156	159	162	165	96	
97	.146	.149	.152	.156	.159	.162	.165	.168	97	
98	.148	.152	.155	.158	.161	.164	.167	.170	98	
99	.151	.154	.157	.160	.163	.166	.169	.173	99	
100	.153	.156	.159	.162	.165	.169	.172	.175	100	

Degrees of				English Inche	s.			Degrees of
Fahren- heit.	28	28.5	29	29.5	30	30.5	31	Fahren- heit.
0	+.072	+.073	+.074	+.076	+.077	+.078	+.080	°o
1	.069	.071	.072	.073	.074	.076	.077	i
2	.067	.068	.069	.070	.072	.073	.074	2
3	.064	.065	.067	.068	.069	.070	.071	3
4	.062	.063	.064	.065	.066	.067	.068	4
5	.059	.060	.061	.062	.063	.065	.066	5
6	+.057	+.058	+.059	+.060	+.061	+.062	+.063	6
7	.054	.055	.056	.057	.058	.059	.060	7
8	.052	.053	.054	.054	.055	.056	.057	8
9	.049	.050	.051	.052	.053	.054	.054	9
10	.047	.047	.048	.049	.050	.051	.052	10
11	+.044	+.045	+.046	+.046	+.047	+.048	+.049	11
12	.042	.042	.043	.044	.045	.045	.046	12
13	.039	.040	.040	.041	.042	.043	.043	13
14	.037	.037	.038	.038	.039	.040	.040	14
15	.034	.035	.035	.036	.036	.037	.038	15
16	+.032	+.032	+.033	+.033	+.034	+.034	+.035	16
17	.029	.030	.030	.031	.031	.032	.032	17
18	.026	.027	.027	.028	.028	.029	.029	18
19	.024	.024	.025	.025	.026	.026	.027	19
20	.021	.022	.022	.023	.023	.023	.024	20
21	+.019	+.019	+.020	+.020	+.020	+.021	+.021	21
22	.016	.017	.017	.017	.018	.018	.018	22
23	.014	.014	.014	.015	.015	.015	.015	23
24	.011	.012	.012	.012	.012	.012	.013	24
25	.009	.009	.009	.009	.009	.010	.010	25
26	+.006	+.006	+.007	+.007	+.007	+.007	+.007	26
27	.004	.004	.004	.004	.004	.004	.004	27
28	.001	.001	.001	.001	.001	.001	.001	28
29	001	001	001	001	001	001	001	29
30	.004	.004	.004	.004	.004	.004	.004	30
31	006	006	007	007	007	007	007	31
32	.009	.009	.009	.009	.009	.010	.010	32
33	.011	.012	.012	.012	.012	.012	.012	33
34	.014	.014	.014	.015	.015	.015	.015	34
35	.016	.017	.017	.017	.018	.018	.018	35
36	019	019	020	020	020	021	021	36
37	.021	.022	.022	.022	.023	.023	.024	37
48	.024	.024	.025	.025	.026	.026	.026	38
39	.026	.027	.027	.028	.028	.029	.029	39
40	.029	.029	.030	.030	.031	.031	.032	40
41	031	032	033	033	034	034	035	41
42	.034	.034	.035	.036	.036	.037	.037	42
43	.036	.037	.038	.038	.039	.040	.040	43
44 45	.039 .041	.040	.040	.041 .044	.042 .044	.042 .045	.043	44 45
			,,,,,	.011	1023	*040	,040	40
46	044 .046	045	045	046	047	048	049	46
48	.049	.047	.048	.049	.050	.051	.051	47
	.051	.052	.051	.052	.052 .055	.053 .056	.054 .057	48
49 il								

Degrees of	English Inches.								
Fahren- heit.	28	28.5	29	29.5	30	30.5	31	Degrees of Fahren-heit.	
51	056	057	058	059	060	061	062	51	
52	.059	.060	.061	.062	.063	.064	.065	52	
53	.061	.063	.064	.065	.066	.067	.068	53	
54 55	.064 .066	.065	.066	.067	.068 .071	.070	.071	54 55	
56	069	070	071	073	074	075	076	56	
57	.071	.073	.074	.075	.076	.078	.079	57	
58	.074	.075	.077	.078	.079	.081	.082	58	
59 60	.076 .079	.078	.079	.080	.082 .085	.083 .086	.085	59 60	
61	081	083	084	086	087	089	090	61	
62	.084	.085	.087	.088	.090	.091	.093	62	
63	.086	.088	.089	.091	.093	.094	.096	63	
64	.089	.090	.092	.094	.095	.097	.098	64	
65	.091	.093	.095	.096	.098	.100	.101	65	
66	094	096	097	099	101	102	104	66	
67	.096	.098	.100	.102	.103	.105	.107	67	
68	.099	.101	.102	.104	.106	.108	.109	68	
69	.101	.103	.105	.107	.109	.110	.112	69	
70	.104	.106	.108	.109	.111	.113	.115	70	
71	106	108	110	112	114	116	118	71	
72	.109	.111	.113	.115	.117	.119	.120	72	
73 74	.111	.113	.115	.117	.119	.121	.123	73	
75	.116	.116 .118	.118 .120	.120	.122 .125	.124 .127	.126 .129	74 75	
76	119	121	123	125	127	129	131	76	
77	.121	.123	.126	.128	.130	.132	.134	77	
78	.124	.126	.128	.130	.133	.135	.137	78	
79	.126	.128	.131	.133	.135	.137	.140	79	
80	.129	.131	.133	.136	.138	.140	.143	80	
81	131	134	136	138	141	143	145	81	
82 83	.134	.136	.138	.141	.143 .	.146	.148	82	
84	.139	.139 .141	.141 .144	.143 .146	.146 .149	.148 .151	.151 .154	83 84	
85,	.141	.144	.146	.149	.151	.154	.156	85	
86	144	146	149	151	154	156	159	86	
87	.146	.149	.151	.154	.157	.159	.162	87	
88	.149	.151	.154	.157	.159	.162	.165	88	
89 90	.151 .153	.154 .156	.156 .159	.159 .162	.162 .164	.165 .167	.167 .170	89 90	
91 92	156 .158	159	162	165 .167	167 .170	170 .172	- 173	91	
93	.161	.161 .164	.164 .167	.170	.170	.172	.175 .178	92 93	
94	.163	.166	.169	.172	.175	.177	.180	94	
95	.166	.169	.172	.175	.178	.180	.183	95	
96	168	171	174	178	181	183	186	96	
97	.171	.174	.177	.180	.183	.186	.189	97	
98	.173	.176	.179	.183	.186	.188	.191	98	
100	.176 .178	.179	.182 .184	.185 .188	.188 .191	.191 .194	.194 .197	99	
100	.110	.181	1104	*100	.131	11 34	1131	100	

#### TABLE XVIII.

FOR REDUCING THE INDICATIONS OF ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO THE FREEZING POINT.

In most of the common barometers the scale is engraved upon a short plate of brass, or of ivory, fixed upon the wooden frame of the instrument. In such a case, the compound expansion of the two substances can only be guessed at, and the correction to be applied to the observations for reducing them to the freezing point cannot be determined with precision. As a near approximation for such imperfect instruments, the following table may be used. In computing this table, the expansion of glass, which is less than that of brass and greater than that of wood, has been substituted for that of brass, as an approximate value for a scale composed of these last two substances. The table thus gives the true correction, in English inches, for the barometers, the graduation of which is engraved on the glass tube itself. It answers equally for any English barometer with wooden scale, whatever be the substance of which the short plate bearing the graduation is made.

CORRECTIONS TO BE APPLIED TO ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO REDUCE THE OBSERVATIONS TO THE FREEZING POINT.

Expansion of Mercury for 1° Fahr. = 0.0001001; of Glass for 1° Fahr. = 0.00000444.

Attached Thermom-		Barometer in English Inches.											
eter, Fahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31		
								<b></b>					
°	+.076	+.077	+.079	+.080	+.082	+.083	+.085	+.086	+.088	+.089	+.090		
1	+.073	+.075	+.076	+.078	+.079	+.080	+.082	+.083	+.085	+.086	+.088		
2	+.071	+.072	+.074	+.075	+.076	+.078	+.079	+.080	+.082	+.083	+.085		
3	+.068	+.070	+.071	+.072	+.074	+.075	+.076	+.078	+.079	+.080	+.082		
4	+.066	+.067	+.069	+.070	+.071	+.072	+.074	+.075	+.076	+.077	+.079		
5	+.064	+.065	+.066	+.067	+.068	+.070	+.071	+.072	+.073	+.074	+.076		
6	+.061	+.062	+.063	+.065	+.066	+.067	+.068	+.069	+.070	+.072	+.073		
7	+.059	+.060	+.061	+.062	+.063	+.064	+.065	+.067	+.068	+.069	+.070		
8 9	+.056	+.057	+.058	+.059	+.060	+.061	+.063	+.064	+.065	+.066	+.067		
9	+.054	+.055	+.056	+.057	+.058	+.059	7.000	+.001	+.002	+.003	+.004		
10	+.051	+.052	+.053	+.054	+.055	+.056	+.057	+.058	+.059	+.060	+.061		
11	+.049	+.050	+.051	+.051	+.052	+.053	+.054	+.055	+.056	+.057	+.058		
12	+.046	+.047	+.048	+.049	+.050	+.051	+.052	+.052	+.053	+.054	+.055		
13	+.044	+.045	+.045	+.046	+.047	+.048	+.049	+.050	+.050	+.051	+.052		
14	+.041	+.042	+.043	+.044	+.044	+.045	+.046	+.047	+.048	+.048	+.049		
15	+.039	+.039	+.040	+.041	+.042	+.042	+.043	+.044	+.045	+.045	+.046		
16	+.036	+.037	+.038	+.038	+.039	+.040	+.040	+.041	+.042	+.043	+.043		
17	+.034	+.034	+.035	+.036	+.036	+.037	+.038	+.038	+.039	+.040	+.040		
18	+.031	+.032	+.032	+.033	+.034	+.034	+.035	+.036	+.036	+.037	+.037		
19	+.029	+.029	+.030	+.030	+.031	+.032	+.032	+.033	+.033	+.034	+.034		
20	+.026	+.027	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	+.031		

Barometer with Glass or Wooden Scale.

Attached Thermom-				Baro	ometer in	English I	nches.						
eter, Fahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31		
neit.	20	20.0	2.	21.0	20	28.0	23	29.9	30	30.9	91		
°	+.024	+.024	+.025	+.025	+.026	+.026	+.027	+.027	+.028	+.028	+.028		
21 22	+.021	+.022	+.022	+.023	+.022	+.023	+.024	+.024	+.025	+.025	+.025		
23	+.019	+.019	+.020	+.020	+.020	+.021	+.021	+.021	+.022	+.022	+.023		
24	+.016	+.017	+.017	+.017	+.018	+.018	+.018	+.019	+.019	+.019	+.020		
25	+.014	+.014	+.014	+.015	+.015	+.015	+.016	+.016	+.016	+.016	+.017		
26	+.011	+.012	+.012	+.012	+.012	+.013	+.013	+.013	+.013	+.013	+.014		
27	+.009	+.009	+.009	+.009	+.010	+.010	+.010	+.010	+.010	+.011	+.011		
28	+.006	+.007	+.007	+.007	+.007	+.007	+.007	+.007	<b>⊹.007</b>	+.008	+.008		
29	+.004	+.004	+.004	+.004	+.004	+.004	+.004	+.005	+.005	+.005	+.005		
30	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002		
31	001	001	001	001	001	001	001	001	001	001	001		
32	003	004	004	004	004	004	004	004	004	004	004		
33	006	006	006	006	006	007	007	007	007	007	007		
34	008	009	009	009	009	009	009	010	010	010	010		
35	011	011	011	012	012	012	012	012	013	013	013		
36	013	014	014	014	014	015	015	015	015	016	016		
37	016	016	017	017	017	017	018	018	018	019	019		
38	018	019	019	019	020	020	020	021	021	022	022		
39	021	021	022	022	022	023	023	024	034	024	025		
40	023	024	024	025	025	026	026	026	027	027	028		
41	026	026	027	027	028	028	029	029	030	030	031		
42	028	029	029	030	030	031	032	032	033	033	034		
43	031	031	032	033	033	034	033	035	036	036	037		
44	033	034	035	035	036	036	036	038	038	039	040		
45	036	036	037	038	038	039	039	041	041	042	043		
46	038	039	040	040	041	042	042	043	044	045	046		
47	041	041	042	043	044	045	044	046	047	048	049		
48	043	044	045	046	047	047	047	049	050	051	051		
49	016	046	047	048	049	050	050	052	053	054	054		
50	048	049	050	051	052	053	054	<b></b> 055	056	056	057		
51	051	052	053	054	055	055	056	057	058	059	060		
52	053	054	055	056	057	058	059	060	061	062	063		
53	056	057	058	059	060	061	062	063	064		066		
54 55	058 061	059 062	060 063	061 064	063 065	064 066	065 068	066 069	067 070	068 071	069 072		
56	063	064	065	067	068	069	070	071	073	074	075		
57	065	067	068	069	071	072	073	074	076	077	078		
58	068	069	071	072	073	074	076	077	078	080	081		
59	070	072	073	074	076 079	077	079	080 083	081 084	083	084 087		
60	073	074	076	077	079	080	081	053	054	085	057		

Barometer with Glass or Wooden Scale.

Attached Thermom-				Baro	meter in l	English Ir	nches.				
Fahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31
61	075	077	078	080	081	083	084	086	087	088	090
62	078	079	081	082	084	085	087	088	090	091	093
63	080	082	083	085	086	088	090	091	093	094	096
64	083	084	086	088	089	091	092	094	096	097	099
65	035	087	089	090	092	093	095	097	098	100	102
66	038	089	091	093	094	096	098	100	101	103	104
67	090	092	094	095	097	099	101	102	104	106	108
68	093	094	096	098	100	102	103	105	107	109	110
69	095	097	099	101	102	104	196	108	110	112	113
70	098	099	101	103	105	107	109	111	113	114	116
71	100	102	104	106	108	110	112	114	115	117	119
72	<b></b> 103	105	106	108	110	112	114	116	118	120	122
73	105	107	<b>1</b> 09	111	113	115	117	119	121	123	125
74	107	110	112	114	116	118	120	122	124	126	128
75	110	112	114	116	118	121	123	125	127	129	131
76	112	115	117	119	121	123	125	128	130	132	134
77	115	117	119	121	124	126	128	130	133	135	137
78	117	120	122	124	126	129	131	133	135	138	140
79	120	122	124	127	129	131	134	136	138	141	143
80	122	125	127	129	132	134	136	139	141	143	146
81	125	127	130	132	134	137	139	142	144	146	149
82	127	130	132	135	137	139	142	144	147	149	152
83	130	132	135	137	140	142	145	147	150	152	155
84	132	135	137	140	142	145	147	150	152	155	158
85	135	137	140	142	145	147	150	153	155	<b>158</b>	160
86	137	140	142	145	148	150	153	155	158	161	163
87	139	142	145	148	150	153	156	158	161	164	166
88	142	145	147	150	153	156	158	161	164	167	169
89	144	147	150	153	156	158	161	164	167	169	172
90	147	150	<b>153</b>	155	158	161	164	167	169	172	175
91	149	152	155	158	161	164	167	169	172	175	178
92	152	155	158	161	163	166	169	172	175	178	181
93	154			163	166	169	172	(	178		184
94 95	157 159	160 162	163 165	166 168	169 171	172 174	175 178	178 181	181 184	184 187	187 190
96	162	165	168	171	174	177	180	183	186	190	193
97	164	167	170	174	177	180	183	186	189	192	196
98	167	170	173	176	179	183	186	189	192	195	199
99	169 171	172	175	179	182	185	188	192	195	198	201
100	171	175	178	181	185	188	191	194	198	201	204

## XIX.

## METRICAL BAROMETER.

## TABLE

FOR

# REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO
THE TOP; CALCULATED FROM 260 TO 865 MILLIMETRES,
AND FOR EACH DEGREE CENTIGRADE.
By M. T. Delcros.



#### TABLE XIX.

This table has been calculated by using the following coefficients of dilatation:—
Brass, linear dilatation, from Laplace and Lavoisier for 100° C. = 0.0018782.

Mercury, dilatation in volume, from Dulong and Petit for 100° C. = 0.0180180.

Dilatation of the mercurial column for 100° C. . . . = 0.0161398.

Dilatation of the mercurial column for 1° C. . . . = 0.0001614.

Observed height reduced to freezing point,

$$H = h - h \ (0.0001614). \quad T = h - h \left(\frac{T}{6196}\right).$$

The second term of this last formula is given by the table, when the temperature T and the height h of the barometer are known; this correction must be *subtracted* from the observed height h, when the temperature is above freezing point; it is to be added when the temperature is below zero, or freezing point.

This table allows the barometrical heights taken at the highest summits, and in the deepest mines, to be corrected.

## Examples of Calculation.

Diampics of Carculation.	
Barometer, observed height,	567.49
Total, = 1.158	
Subtractive correction,	<b>—</b> 1.16
_	
Barometer at zero,	566.33
Temperature of the barometer, —7°.8.	mm. 454.17
First page, $\begin{cases} \text{for } 7.0 = 0.514 \\ \text{for } 0.8 = 0.059 \end{cases}$	
Total, $= 0.573$	
Additive correction,	+0.57
Barometer at zero,	454.74

Height of the				TEMPERA	TEMPERATURE CENTIGRADE.											
Barome-	10	2°	3°	4°	<b>5</b> °	6°	70	8°	90							
Millim.	Millim. 0.042	Millim. 0.084	Millim. 0.126	Millim. 0.168	Millim. 0.210	Millim, 0.252	Millim. 0.294	Millim. 0.336	Millim. 0.378							
265	0.042	0.084	0.128	0.103	0.210	0.252	0.294	0.342	0.378							
270	0.043	0.087	0.123	0.174	0.214	0.261	0.295	0.349	0.392							
275	0.044	0.089	0.133	0.178	0.222	0.266	0.311	0.355	0.399							
280	0.045	0.090	0.136	0.181	0.226	0.271	0.316	0.362	0.407							
285	0.046	0.092	0.138	0.184	0.230	0.276	0.322	0.368	0.414							
290	0.047	0.094	0.140	0.187	0.234	0.281	0.328	0.374	0.421							
295	0.048	0.095	0.143	0.190	0.238	0.286	0.333	0.381	0.428							
300	0.048	0.097	0.145	0.194	0.242	0.291	0.339	0.387	0.436							
305	0.049	0.098	0.148	0.197	0.246	0.295	0.345	0.394	0.443							
310	0.050	0.100	0.150	0.200	0.250	0.300	0.350	0.400	0.450							
315	0.051	0.102	0.152	0.203	0.254	0.305	0.356	0.407	0.458							
320	0.052	0.103	0.155	0.207	0.258	0.310	0.361	0.413	0.465							
325	0.052	0.105	0.157	0.210	0.262	0.315	0.367	0.420	0.472							
330	0.053	0.106	0.160	0.213	0.266	0.320	0.374	0.426	0.479							
335	0.054	0.108	0.162	0.216	0.270	0.324	0.379	0.432	0.487							
340	0.055	0.110	0.165	0.219	0.274	0.329	0.384	0.439	0.494							
345	0.056	0.111	0.167	0.223	0.278	0.334	0.390	0.445	0.501							
350	0.056	0.113	0.169	0.226	0.282	0.339	0.395	0.452	0.508							
355	0.057	0.115	0.172	0.229	0.286	0.344	0.401	0.458	0.516							
360	0.058	0.116	0.174	0.232	0.290	0.349	0.407	0.465	0.523							
365	0.059	0.118	0.177	0.236	0.294	0.353	0.412	0.471	0.530							
370	0.060	0.119	0.179	0.239	0.299	0.358	0.418	0.478	0.537							
375 380	0.060	0.121	0.182	0.242	0.303	0.363	0.424	0.484	0.545							
380	0.061	0.123	0.184	0.245	0.307	0.368	0.429	0.491	0.552							
385	0.062	0.124	0.186	0.249	0.311	0.373	0.435	0.497	0.559							
390	0.063	0.126	0.189	0.252	0.315	0.378	0.441	0.504	0.566							
395 400	0.064	0.127	0.191	0.255	0.319	0.382	0.446	0.510	0.574							
400	0.065	0.129 0.131	0.194 0.196	0.258 0.261	0.323 0.327	0.387	0.452 $0.457$	0.516 0.523	0.581 $0.588$							
100	0.000	0.191	0.190	,0.201	0.021	0.092	0.497	0.020	0.088							
410	0.066	0.132	0.198	0.265	0.331	0.397	0.463	0.529	0.596							
415	0.067	0.134	0.201	0.268	0.335	0.402	0.469	0.536	0.603							
420	0.068	0.136	0.203	0.271	0.339	0.407	0.474	0.542	0.610							
425	0.068	0.137	0.206	0.274	0.343	0.411	0.480	0.549	0.617							
430	0.069	0.139	0.208	0.278	0.347	0.416	0.486	0.555	0.625							
435	0.070	0.140	0.211	0.281	0.351	0.421	0.491	0.562	0.632							
440	0.071	0.142	0.213	0.284	0.355	0.426	0.497	0.568	0.639							
445	0.072	0.144	0.215	0.287	0.359	0.431	0 503	0.574	0.646							
450 455	0.073	0.145	0.218	0.290	0.363	0.436	0.508	0.581	0.654							
400		0.147	0.220	0.294	0.367	0.441	0.514	0.587	0.661							
	1°	2°	3°	<b>4</b> °	5°	6,	70	80	<b>9</b> 2							

Height of the	TEMPERATURE CENTIGRADE.											
Barome- ter.	1°	2°	3°	40	<b>5</b> °	<b>6</b> °	70	8°	9°			
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.			
460	0.0742	0.1485	0.2227	0.2970	0.371	0.445	0.520	0.594	0.668			
465	0.0750	0.1501	0.2251	0.3002	0.375 0.379	0.450	0.525	0.600	0.675			
470 475	0.0759	0.1517	0.2300	0.3066	0.383	0.460	0.537	0.607	0.690			
480	0.0775	0.1549	0.2324	0.3099	0.387	0.465	0.542	0.620	0.697			
485	0.0783	0.1565	0.2348	0.3131	0.391	0.470	0.548	0.626	0.704			
490	0.0791	0.1582	0.2373	0.3163	0.395	0.474	0.554	0.633	0.712			
495	0.0800	0.1598	0.2397	0.3195	0.399	0.479	0.559	0.639	0.719			
500	0.0807	0.1614	0.2421	0.3228	0.403	0.484	0.565	0.646	0.726			
505	0.0815	0.1630	0.2445	0.3260	0.407	0.489	0.570	0.652	0.734			
510	0.0823	0.1646	0.2469	0.3293	0.412	0.494	0.576	0.658	0.741			
515	0.0831	0.1662	0.2493	0.3325	0.416	0.499	0.582	0.665	0.748			
520	0.0839	0.1679	0.2518	0.3357	0.420	0.504	0.587	0.671	0.755			
525	0.0847	0.1695	0.2542	0.3389	0.424	0.508	0.593	0.678	0.763			
530	0.0855	0.1711	0.2566	0.3422	0.428	0.513	0.599	0.684	0.770			
535	0.0863	0.1727	0.2590	0.3454	0.432	0.518	0.604	0.691	0.777			
540	0.0872	0.1743	0.2615	0.3486	0.436	0.523	0.610	0.697	0.784			
545	0.0879	0.1759	0.2639	0.3518	0.440	0.528	0.616	0.704	0.792			
550	0.0888	0.1775	0.2663	0.3551	0.444	0.533	0.621	0.710	0.799			
555	0.0896	0.1791	0.2687	0.3583	0.448	0.537	0.627	0.717	0.806			
560	0.0904	0.1808	0.2712	0.3615	0.452	0.542	0.633	0.723	0.813			
565	0.0912	0.1824	0.2736	0.3647	0.456	0.547	0.638	0.730	0.821			
570	0.0920	0.1840	0.2760	0.3680	0.460	0.552	0.644	0.736	0.828			
575	0.0928	0.1856	0.2784	0.3712	0.464	0.557	0.650	0.742	0.835			
580	0.0936	0.1872	0.2808	0.3744	0.468	0.562	0.655	0.749	0.842			
585	0.0944	0.1888	0.2833	0.3777	0.472	0.566	0.661	0.755	0.850			
590	0.0952	0.1904	0.2857	0.3809	0.476	0.571	0.667	0.762	0.857			
595	0.0960	0.1921	0.2881	0.3841	0.480	0.576	0.672	0.768	0.864			
600	0.0968	0.1937	0.2905	0.3874	0.484	0.581	0.678	0.775	0.872			
605	0.0976	0.1953	0.2929	0.3906	0.488	0.586	0.683	0.781	0.879			
610	0.0985	0.1969	0.2954	0.3938	0.492	0.591	0.689	0.788	0.886			
615	0.0993	0.1985	0.2978	0.3970	0.496	0.595	0.695	0.794	0.893			
620	0.1001	0.2001	0.3002	0.4003	0.500	0.600	0.700	0.800	0.901			
625	0.1009	0.2017	0.3026	0.4035	0.504	0.605	0.706	0.807	0.908			
630	0.1017	0.2034	0.3050	0.4067	0.508	0.610	0.712	0.813	0.915			
635	0.1025	0.2050	0.3074	0.4099	0.512	0.615	0.717	0.820	0.922			
640	0.1033	$0.2066 \\ 0.2082$	0.3099 0.3123	0.4132 0.4164	$0.516 \\ 0.520$	0.620	0.723	0.826 $0.833$	0.930 0.937			
645	0.1041 0.1049	0.2082	0.3123	0.4164	0.524	0.625 0.629	0.729 0.734	0.833	0.937			
650 655	0.1049	0.2098	0.3147	0.4196	0.524	0.634	0.734	0.846	0.951			
660	0.1065	0.2130	0.3196	0.4261	0.533	0.639	0.746	0.852	0.959			
	10	2°		40	<b>5</b> °	<b>6</b> °	70	80	9°			

Height	TEMPERATURE CENTIGRADE.										
of the Barome- ter.	10	2°	3°	40	<b>5</b> °	<b>6</b> °	70	80	90		
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.		
665	0.1073	0.2146	0.3220	0.4293	0.537	0.644	0.751	0.859	0.966		
670	0.1081	0.2163	0.3244	0.4326	0.541	0.649	0.757	0.865	0.973		
675	0.1089	0.2179	0.3268	0.4358	0.545	0.654	0.763	0.871 0.878	0.980		
680	0.1097	$0.2195 \\ 0.2211$	0.3292	0.4423	0.549	0.658 0.663	0.768	0.884	0.988		
685	0.1106	0.2211	0.3317	0.4423	0.553	0.000	0.774	0.554	0.995		
690	0.1114	0.2227	0.3341	0.4455	0.557	0.668	0.780	0.891	1.002		
695	0.1122	0.2233	0.3365	0.4487	0.561	0.673	0.785	0.897	1.010		
700	0.1130	0.2260	0.3389	0.4520	0.565	0.678	0.791	0.904	1.017		
705	0.1138	0.2276	0.3414	0.4552	0.569	0.683	0.797	0.910	1.024		
710	0.1146	0.2292	0.3438	0.4584	0.573	0.688	0.802	0.917	1.031		
715	0.1154	0.2308	0.3462	0.4616	0.577	0.691	0.808	0.923	1.039		
720	0.1162	0.2324	0.3486	0.4648	0.581	0.697	0.813	0.930	1.046		
725	0.1170	0.2340	0.3510	0.4680	0.585	0.702	0.819	0.936	1.053		
730	0.1178	0.2356	0.3535	0.4713	0.589	0.707	0.825	0.943	1.060		
735	0.1186	0.2372	0.3559	0.4745	0.593	0.712	0.830	0.949	1.068		
740	0.1104	0.2389	0.3583	0.4777	0.597	0.717	0.836	0.955	1.075		
745	0.1202	0.2405	0.3607	0.4809	0.601	0.721	0.842	0.962	1.082		
750	0.1210	0.2421	0.3631	0.4842	0.605	0.726	0.847	0.968	1.089		
755	0.1218	0.2437	0.3655	0.4874	0.609	0.731	0.853	0.975	1.097		
760	0.1227	0.2453	0.3680	0.4906	0.613	0.736	0.859	0.981	1.104		
765	0.1235	0.2469	0.3704	0.4939	0.617	0.741	0.864	0.988	1.111		
770	0.1243	0.2486	0.3728	0.4971	0.621	0.746	0.870	0.994	1.118		
775	0.1251	0.2502	0.3752	0.5003	0.625	0.750	0.876	1.001	1.126		
780	0.1259	0.2518	0.3777	0.5036	0.629	0.755	0.881	1.007	1.133		
785	0.1267	0.2534	0.3801	0.5068	0.633	0.760	0.888	1.014	1.140		
790	0.1275	0.2550	0.3825	0.5100	0.637	0.765	0.893	1.020	1.148		
795	0.1283	0.2566	0.3849	0.5132	0.641	0.770	0.898	1.026	1.155		
800	0.1291	0.2582	0.3874	0.5165	0.646	0.775	0.904	1.033	1.162		
805	0.1299	0.2598	0.3898	0.5197	0.650	0.780	0.909	1.039	1.169		
810	0.1307	0.2615	0.3922	0.5230	0.654	0.784	0.915	1.046	1.177		
815	0.1315	0.2621	0.3946	0.5262	0.658	0.789	0.921	1.052	1.184		
820	0.1323	0.2647	0.3970	0.5294	0.662	0.794	0.926	1.059	1.191		
825	0.1323	0.2653	0.3994	0.5326	0.666	0.799	0.932	1.065	1.198		
830	0.1340	0.2679	0.4019	0.5358	0.670	0.804	0.938	1.072	1.206		
835	0.1348	0.2695	0.4043	0.5391	0.674	0.809	0.943	1.078	1.213		
840	0.1356	0.2712	0.4067	0.5423	0.678	0.813	0.949	1.085	1.220		
845	0.1364	0.2728	0.4091	0.5455	0.682	0.818	0.955	1.091	1.227		
850	0.1372	0.2744	0.4116	0.5488	0.686	0.823	0.960	1.097	1.235		
855	0.1380	0.2760	0.4140	0.5520	0.690	0.828	0.966	1.104	1.242		
860	0.1388	0.2776	0.4164	0.5552	0.694	0.833	0.972	1.110	1.249		
865	0.1396	0.2792	0.4188	0.5584	0.698	0.838	0.977	1.117	1.256		
	1°	2°	3°	40	<b>5</b> °	<b>6</b> °	70	80	<b>9</b> °		

## XX.

## METRICAL BAROMETER.

# TABLE

FOR

# REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO THE TOP; CALCULATED FOR THE HEIGHTS BETWEEN 605 AND 800 MILLIMETRES, AND FOR
EVERY TENTH OF A DEGREE, FROM 0° TO + AND - 35° CENTIGRADE.

By M. T. Haeghens.



### TABLE. XX.

This table has been calculated by using the same coefficients of dilatation as in the preceding table, viz.:—

Brass, linear dilatation, from Laplace and Lavoisier for 100°C. = 0.0018782. Mercury, dilatation in volume, from Dulong and Petit for 100°C. = 0.0180180. Dilatation of the mercurial column for 100°C. . . . = 0.0161398. Dilatation of the mercurial column for 1°C. . . . = 0.0001614.

This table, calculated for the reduction of long series of meteorological observations, gives immediately the value of the correction for each tenth of a degree up to 35° C. above, and down to 35° C. below, the freezing point, and for mercurial columns extending from 605 to 800 millimetres.

## Examples of Calculation.

For finding the correction, seek in the horizontal column, headed *barometer*, at the head of the pages, the corresponding height of the barometer; it will be found, p. 31, barometer 755<sup>mm</sup>. (from 752.50 to 757.50); next seek in the first vertical column, containing the temperatures, 17°, follow then horizontally this line as far as the column of 8 tenths, and you find there 2.17 millimetres, which is the correction, or the quantity to be subtracted for reducing the observed height to zero. We have thus:—

Observed height,				•		$754.17^{\text{mm.}}$
Subtractive correction	for +	17°.8 =		•	•	- 2.17
	:	Baromete	er a	t zero,		752.00

If the temperature is below zero, the correction will be additive.

						729.72
atta	ched t	herm	omete	er, —8	8°.4.	
		•	•			+0.99
	р			4		730.71
	atta	attached t	attached therm	attached thermomete	attached thermometer, —6	attached thermometer, —8°.4.

·	BAROMETER: 605 <sup>mm</sup> (from 602.51 to 607.50).										
Centigrade Degrees.					Tenths of	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millin. 0.00	Millim.	Millim, 0.02	Millim.	Millim. 0.04	Millim. 0.05	Millim.	Millim.	Millim. 0.08	Millim.	
	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.10	
1	0.10	0.11	0.12	0.13	0.14	0.13	0.10	0.17	0.13	0.19	
2 3	0.20	0.30	0.21	0.22	0.23	0.34	0.25	0.26	0.27	0.28	
4	0.39	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.33	
5	0.49	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	
3	0.40	0.50	0.01	0.02	0.00	0.01	0.00	0.50	0.57	0.00	
6	0.59	0.60	0.61	0.62	0.63	0.63	0.64	0.65	0.66	0.67	
7	0.68	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	
8	0.78	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	
9	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	
10	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.05	1.06	
11	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	
12	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	
13	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	
14	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	
15	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	
16	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64	1.65	
17	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	
18	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85	
19	1.86	1.87	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	
20	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04	
21	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	
22	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24	
23	2.25	2.26	2.27	2.28	2.29	2.29	2.30	2.31	2.32	2.33	
24	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	
25	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	
26	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	
27	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.71	2.72	
28	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	
29	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92	
30	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	
31	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12	
32	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19	3.20	3.21	
33	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31	
34 35	3.32	3.33 3.43	3.34 3.44	3.35 3.45	3.36 3.46	3.37 $3.47$	3.38	3.39 3.49	3.40	3.41 3.51	
							9.40				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

Centigrade Degrees.  O.  O.  O.  O.  O.  O.  O.  O.  O.				BAROMETER: 610 <sup>mm.</sup> (from 607.51 to 612.50).											
Millin   0.10	Tenths of Degrees.														
1 0.00 1 0.10 2 0.20 3 0.30 4 0.39 5 0.49 6 0.59 7 0.69 8 0.79 9 0.89 10 0.98 11 1.08 12 1.18 13 1.28 14 1.38 15 1.48 16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95		1.	2.	3.	4.	5.	6.	7.	8.	9.					
1 0.10 2 0.20 3 0.30 4 0.39 5 0.49 6 0.59 7 0.69 8 0.79 9 0.89 10 0.98 11 1.08 12 1.18 13 1.28 14 1.38 15 1.48 16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	lim.	Millim.	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.					
2 0.20 3 0.30 4 0.39 5 0.49 6 0.59 7 0.69 8 0.79 9 0.89 10 0.98 11 1.08 12 1.18 13 1.28 14 1.38 15 1.48 16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09					
2 0.20 3 0.30 4 0.39 5 0.49 6 0.59 7 0.69 8 0.79 9 0.89 10 0.98 11 1.08 12 1.18 13 1.28 14 1.38 15 1.48 16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19					
3   0.30 4   0.39 5   0.49 6   0.59 7   0.69 8   0.79 9   0.89 10   0.98 11   1.08 12   1.18 13   1.28 14   1.38 15   1.48 16   1.58 17   1.67 18   1.77 19   1.87 20   1.97 21   2.07 22   2.17 23   2.26 24   2.36 25   2.46 26   2.56 27   2.66 28   2.76 29   2.86 30   2.95		0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29					
4 0.39 5 0.49 6 0.59 7 0.69 8 0.79 9 0.89 10 0.98 11 1.08 12 1.18 13 1.28 14 1.38 15 1.48 16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	- 1	0.31	0.32	0.32	0.33	0.34	0.35	0.36	0.37	0.38					
5   0.49 6   0.59 7   0.69 8   0.79 9   0.89 10   0.98 11   1.08 12   1.18 13   1.28 14   1.38 15   1.48 16   1.58 17   1.67 18   1.77 19   1.87 20   1.97 21   2.07 22   2.17 23   2.26 24   2.36 25   2.46 26   2.56 27   2.66 28   2.76 29   2.86 30   2.95	1	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48					
6 0.59 7 0.69 8 0.79 9 0.89 10 0.98 11 1.08 12 1.18 13 1.28 14 1.38 15 1.48 16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	- 1	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58					
7   0.69   0.79   9   0.89   10   0.98   11   1.08   12   1.18   13   1.28   14   1.38   15   1.48   16   1.58   17   1.67   18   1.77   19   1.87   20   1.97   21   2.26   2.46   2.56															
7   0.69 8   0.79 9   0.89 10   0.98 11   1.08 12   1.18 13   1.28 14   1.38 15   1.48 16   1.58 17   1.67 18   1.77 19   1.87 20   1.97 21   2.07 22   2.17 23   2.26 24   2.36 25   2.46 26   2.56 27   2.66 28   2.76 29   2.86 30   2.95	59	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68					
9 0.89 10 0.98 11 1.08 12 1.18 13 1.28 14 1.38 15 1.48 16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78					
10 0.98  11 1.08 12 1.18 13 1.28 14 1.38 15 1.48  16 1.58 17 1.67 18 1.77 19 1.87 20 1.97  21 2.07 22 2.17 23 2.26 24 2.36 25 2.46  26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88					
11	89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.96	0.97					
12         1.18           13         1.28           14         1.38           15         1.48           16         1.58           17         1.67           18         1.77           19         1.87           20         1.97           21         2.07           22         2.17           23         2.26           24         2.36           25         2.46           26         2.56           27         2.66           28         2.76           29         2.86           30         2.95	98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07					
12															
13         1.28           14         1.38           15         1.48           16         1.58           17         1.67           18         1.77           19         1.87           20         1.97           21         2.07           22         2.17           23         2.26           24         2.36           25         2.46           26         2.56           27         2.66           28         2.76           29         2.86           30         2.95	08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17					
14         1.38           15         1.48           16         1.58           17         1.67           18         1.77           19         1.87           20         1.97           21         2.07           22         2.17           23         2.26           24         2.36           25         2.46           26         2.56           27         2.66           28         2.76           29         2.86           30         2.95	- 1	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27					
15 1.48  16 1.58  17 1.67  18 1.77  19 1.87  20 1.97  21 2.07  22 2.17  23 2.26  24 2.36  25 2.46  26 2.56  27 2.66  28 2.76  29 2.86  30 2.95	28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37					
16 1.58 17 1.67 18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95		1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47					
17	48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57					
17			7 40	7 00	1 01				7 05	1 00					
18 1.77 19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95		1.59	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66					
19 1.87 20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95		1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76					
20 1.97 21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	1	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86					
21 2.07 22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95		1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96					
22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	97	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06					
22 2.17 23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95	07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16					
23 2.26 24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95		2.18	2.19	2.20	2.21	2.22	2.23	2.23	2.24	2.25					
24 2.36 25 2.46 26 2.56 27 2.66 28 2.76 29 2.86 30 2.95		2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35					
25   2.46 26   2.56 27   2.66 28   2.76 29   2.86 30   2.95		2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45					
27 2.66 28 2.76 29 2.86 30 2.95		2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55					
27 2.66 28 2.76 29 2.86 30 2.95		0.57	0.70	0.70	0.00	0.07	0.00	0.00	0.01	9.05					
28 2.76 29 2.86 30 2.95		2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65					
29 2.86 30 2.95	1	2.67	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75					
30 2.95	- 1	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85					
	- 1	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94					
31 3.05	95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04					
1 1	05	3.06	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14					
32 3.15		3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24					
33 3.25		3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34					
34 3.35		3.36	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44					
35 3.45	45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.55	3.54					
0.	).	1.	2.	3.	4.	5.	6.	7.	8.	9.					

BAROMETER: 615<sup>mm</sup>. (from 612.51 to 617.50).

Centi-

grade Degrees.		Tenths of Degrees.												
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.				
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09				
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19				
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29				
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39				
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49				
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59				
6	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.68				
7	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78				
8	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88				
9	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98				
10	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08				
11	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18				
12	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28				
13	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38				
14	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48				
15	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58				
16	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68				
17	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78				
18	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88				
19	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98				
20	1.99	2.00	2.01	2.01	2.02	2.03	2.04	2.05	2.06	2.07				
21	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17				
22	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27				
23	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37				
24	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47				
25	2.48	2.19	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57				
26	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67				
27	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77				
28	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87				
29	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97				
30	2.98	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07				
31	3.08	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17				
32	3.18	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27				
33	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.36				
34	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.46				
35	3.47	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.56				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

		BAROMETER: 620 <sup>mm.</sup> (from 617.51 to 622.50)										
Centi- grade Degrees.					Tenths o	f Degrees.						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0	Millim.	Millim. 0.01	Millim, 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim 0.08	Millim. 0.09		
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19		
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29		
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39		
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49		
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59		
6	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69		
7	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79		
8	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89		
9	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99		
10	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09		
11	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19		
12	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29		
13	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39		
14	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49		
15	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58	1.59		
16	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69		
17	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79		
18	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89		
19	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99		
20	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09		
21	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19		
22	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29		
23	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39		
24	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49		
25	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59		
26	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.68	2.69		
27	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78	2.79		
28	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89		
29	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	2.99		
30	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09		
31	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19		
32	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29		
33	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39		
34	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49		
35	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58	3.59		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 625 <sup>mm.</sup> (from 622.51 to 627.50).											
Centigrade Degrees.	Tenths of Degrees.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Miltim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim 0.08	Millim. 0.09		
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19		
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29		
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39		
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49		
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.58	0.59	0.60		
6	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70		
7	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80		
8	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90		
9	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00		
10	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10		
11	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20		
12	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30		
13	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40		
14	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50		
15	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60		
16	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70		
17	1.71	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81		
18	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91		
19 20	1.92 $2.02$	1.93 2.03	$\frac{1.94}{2.04}$	1.95 2.05	1.96 2.06	1.97 2.07	1.98 2.08	1.99	2.00	2.01		
21	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21		
22	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31 2.41		
23 24	$\frac{2.32}{2.42}$	2.33	2.34	2.35 $2.45$	2.36 2.46	2.37 $2.47$	2.38 2.48	2.39 2.49	2.40 2.50	2.41		
25	2.42	2.43	2.54	2.45	2.56	2.57	2.48	2.49	2.60	2.61		
26	2.62	2.63	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71		
26	2.62	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.70	2.81		
28	2.82	2.83	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92		
29	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02		
30	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12		
31	3.13	3.14	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22		
32	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32		
33	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42		
34	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52		
35	3.53	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.61	3.62		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

		В	AROMI	ETER:	630 <sup>mm</sup> ·	(from	627.51	to 632.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.			1 1	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim.	Millim.	Millim.	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40
4	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50
5	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60
6	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70
7	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80
8	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90
9	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01
10	1.02	1.03	1.04	1.05	1.06	1.07_	1.08	1.09	1.10	1.11
11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21
12	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31
13	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41
14	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.52
15	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62
16 .	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72
17	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82
18	1.83	1.84	1.85	1.86	1.87	.1.88	1.89	1.90	1.91	1.92
19	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02
20	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.13
21	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23
22	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33
23	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43
24	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53
25	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63
26	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.73	2.74
27	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
-28	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94
29	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04
30	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14
31	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24
32	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.34	3.35
33	3.36	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45
34	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.55
35	3.56	3.57	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.65
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	635 <sup>mm</sup> ·	(from 6	632.51 t	o 637.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millini.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40
4	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50
5	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60
6	0.61	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71
7	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81
8	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91
9	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01
10	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12
.,	1 10	1.14	1 15	1.16	1.17	1.10	1.10	1.00	1.01	1.00
11	1.13	1.14	1.15 1.25	1.16 1.26	1.17	1.18 1.28	1.19	1.20	1.21	1.22
12	1.23 1.33	1.24	1.25	1.36	1.27	1.28	1.29 1.39	1.30	1.31	1.32
13 14	1.43	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53
15	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63
16	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73
17	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83
18	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94
19	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04
20	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14
21	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
22	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35
23	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45
24	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55
25	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65
26	2.66	2.67	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76
27	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86
28	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96
29	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06
30	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17
	2.46									0.05
31	3.18	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27
32	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37
33 34	3.38	3.39	3.40 3.51	3.41 3.52	3.42	3.43 3.54	3.44	3.45	3.46	3.47
35	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66	3.67	3.68
						<u> </u>			- <del></del>	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	640 <sup>mm</sup> .	(from 6	63 <b>7</b> .51 t	o 642.5	0).	
Centi- grade Degrees,					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	9.	9.
0	Millim.	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim, 0.07	Millim. 0.08	Millim.
1	0.10	0.11	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40
4	0.41	0.42	0.43	0.44	0.45	0.46	0.48	0.49	0.50	0.51
5	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61
6	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71
7	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.80	0.81	0.82
8	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92
9	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	1.02
10	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.11	1.12	1.13
11	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23
12	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33
13	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42	1.43	1.44
14	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54
15	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64
16	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.74	1.75
17	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85
18	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95
19	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.05	2.06
20	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16
21	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26
22	2.27	2.23	2.29	2.30	2.31	2.32	2.33	2.34	2.36	2.37
23	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47
24	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57
25	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.68
26	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78
27	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87	2.88
28	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.99
29	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09
30	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19
31	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.30
32	3.31	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40
33	3.41	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50
34 35	3.51 3.62	3.52 3.63	3.53	3.54	3.55 3.66	$3.56 \\ 3.67$	3.57	3.58 3.69	3.59	3.60
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		BA	AROME	ETER:	645 <sup>mm</sup> .	(from 6	342.51 t	o 647.5	0).	
Centigrade Degrees.					Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim. 0.01	Millim. 0.02	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09
1	0.10	0.11	0.12	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.39	0.40	0.41
4	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51
5	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61
6	0.62	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72
7	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82
8	0.83	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93
9	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03
10	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13
11	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24
12	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34
13	1.35	1.36	1.37	1.38	1.39	1.41	1.42	1.43	1.44	1.45
14	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55
15	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64	1.66
16	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76
17	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86
18	1.87	1.88	1.89	1.91	1.92	1.93	1.94	1.95	1.96	1.97
19	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07
20	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.17	2.18
21	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28
22	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38
23	2.39	2.40	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49
24	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59
25	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70
26	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80
27	2.51	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.90
28	2.92	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01
29	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11
30	3.12	3.13	3.14	3.15	3.16	3.18	3.19	3.20	3.21	3.22
31	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32
32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42
33	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53
34 35	3.54	3.55 3.65	3.56 3.66	3.57	3.58 3.68	3.59 3.69	3.60	3.61	3.62 3.72	3.63 3.73
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROM	ETER :	: 650 <sup>mm</sup>	(from	647.51	to 652.5	0).	
Centigrade Degrees.					Tenths of	of Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41
4	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51
5	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72
7	0.73	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.83
8	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93
9	0.94	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04
10	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14
11	1.15	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25
12	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35
13	1.36	1.37	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46
14	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56
15	1.57	1.58	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67
16	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77
17	1.78	1.79	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88
18	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98
19	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.07	2.08	2.09
20	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19
21	2.20	2.21	2.22	2.24	2.25	2.26	2.27	2.28	2.29	2.30
22	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40
23	2.41	2.42	2.43	2.44	2.46	2.47	2.48	2.49	2.50	2.51
24	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61
25	2.62	2.63	2.64	2.65	2.67	2.68	2.69	2.70	2.71	2.72
26	2.73	2.84	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
27	2.83	2.84	2.85	2.86	2.88	2.89	2.90	2.91	2.92	2.93
28	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3 03
29	3.04	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	3.14
30	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24
31	3.25	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34	3.35
32	3.36	3 37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45
33	3.46	3.47	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.56
34	3.57	3 58	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66
35	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROME	ETER:	655mm.	(from 6	652.51 t	o 657.50	0).	
Centigrade Degrees.					Tenths of	Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9,
0	Millim.	Millim.	Millim.	Mıllim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	. 0.02	0.03	0.04	0.05	0.06	0.07	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35 *	0.36	0.37	0.38	0.39	0.40	0.41
4	0.42	0.43	0.44	0.46	0.47	0.48	0.49	0.50	0.51	0.52
5	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.63	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73
7	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.83	0.84
8	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94
9	0.95	0.96	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05
10	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15
	1.10	1.16	1 10	1.00	1.01	1.00	1.00	1.04	1.05	1.00
11	$1.16 \\ 1.27$	1.17	1.18	1.20	1.21	1.22 1.32	1.23	1.24	1.25 1.35	1.26 1.36
12	1.37	1.28 1.39	1.29 1.40	1.30 1.41	1.31 1.42	1.43	1.33 1.44	1.34 1.45	1.46	1.47
13 14	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.57	1.58
15	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68
15	1.00	1.00	1.01	1.02	1.05	1.01	1.00	1.00	1.01	1.00
16	1.69	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79
17	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89
18	1.90	1.91	1.92	1.94	1.95	1.96	1.97	1.98	1.99	2.00
19	2.01	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10
20	2.11	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21
21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.31	2.32
22	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42
23	2.43	2.44	2.45	2.46	2.47	2.48	2.50	2.51	2.52	2.53
24	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63
25	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.74
26	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
27	2.15	2.76	2.88	2.78	2.79	2.91	2.92	2.93	2.94	2.95
28	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.05	3.06
29	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16
30	3.17	3.18	3.19	3.20	3.21	3.22	3.24	3.25	3.26	3.27
	0.55								0.00	0.00
31	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37
32	3.38	3.39	3.40	3.42	3.43	3.44	3.45	3.46	3.47	3.48 3.58
33 34	3.49 -3.59	3.50	$3.51 \\ 3.62$	3.52 3.63	3.53 3.64	3.54 3.65	3.55 3.66	3.56 3.67	3.57 3.68	3.69
35	3.70	3.71	3.72	3.73	3.74	3.75	3.76	3.77	3.79	3.80
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER :	660 <sup>mm</sup>	(from	657.51 t	o 662.5	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
•	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.41	0.42
4	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52
5	0.53	0.54 ,	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.63
6	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74
7	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.83	0.84
8	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.95
9	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.06
10	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16
11	1.17	1.18	1.19	1.20	1.21	1.23	1.24	1.0%	1.00	7.07
12	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.25 1.35	1.26 1.36	1.27 1.37
13	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48
14	1.49	1.50	1.51	1.52	1.53	1.55	1.56	1.57	1.58	1.59
15	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69
16	1.70	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80
17	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
18	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01
19	2.02	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12
20	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.23
21	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33
22	2.34	2.35	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44
23	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.53	2.54	2.55
24	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65
25	2.66	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.76
26	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.86	2.87
27	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97
28	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.06	3.07	3.08
29	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.19
30	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29
9.7	9.00	2.07	2.22		0.0"	0.00	0.07	0.00	0.60	2 (2
31	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40
32 33	$3.41 \\ 3.52$	3.42	3.43	3.44	$\frac{3.45}{3.56}$	3.46	3.47	3.48	3.49	3.51
34	3.62	3.63	3.64	3.65	3.66	3.68	3.69	3.59	3.60 3.71	3.72
35	3.73	3.74	3.75	3.76	3.77	3.78	3.79	3.80	3.81	3.82
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
C					93					

		В	AROMI	ETER :	665 <sup>mm</sup>	(from	662.51 t	o 667.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35	0.37	0.38	0.39	0.40	0.41	0.42
4	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.51	0.52	0.53
5	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63
6	0.64	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73	0.74
7	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83	0.84	0.85
8	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.95	0.96
9	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06
10	1.07	1.08	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17
11	1.18	1.19	1.20	1.21	1.22	1.23	1.25	1 96	1.27	1.00
12	1.29	1.19	1.31	1.32	1.33	1.23	1.25	1.26 1.36	1.37	1.28
13	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49
14	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59	1.60
15	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71
	ĺ									
16	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81
17	1.83	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92
18	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.02	2.03
19	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.13	2.14
20	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
21	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35
22	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44	2.45	2.46
23	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.56	2.57
24	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67
25	2.68	2.69	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78
26	2.79	2.80	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89
27	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00
28	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10
29	3.11	3.12	3.13	3.15	3.16	3.17	3.18	3.19	3.20	3.21
30	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.30	3.31	3.32
21	2 29	2.24	2.05	9.00	0.0**	2.00	0.00	0.40	9.47	0.40
31 32	3.33	3.34	3.35 3.46	3.36	3.37	3.38	3.39	3.40	3.41	3.42
33	3.54	3.55	3.56	3.47	$\frac{3.48}{3.59}$	3.49	3.50 3.61	3.51 3.62	3.52 3.63	3.53 $3.64$
34	3.65	3.66	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75
35	3.76	3.77	3.78	3.79	3.80	3.81	3.82	3.83	3.84	3.85
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	0.	1.					_	_	_	_

		В	AROME	TER ·	670 <sup>mm</sup>	(from	667.51 t	to 672.5	0.)	
Centigrade Degrees.					Tenths of	Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim.	Millim.	Millim. 0.05	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31
3	0.32	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42
4	0.43	0.44	0.45	0.47	0.48	0.49	0.50	0.51	0.52	0.53
5	0.54	0.55	0.56	0.57	0.58	0.60	0.61	0.62	0.63	0.64
6	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.73	0.74	0.75
7	0.76	0.77	0.78	0.79	0.80	0.70	0.82	0.73	0.74	0.75
8	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96
9	0.97	0.98	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07
10	1.08	1.09	1.10	1.11	1.13	1.14	1.15	1.16	1.17	1.18
	ł									
11	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.27	1.28	1.29
12	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.40
13	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50
14	1.51	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61
15	1.62	1.63	1.64	1.66	1.67	1.68	1.69	1.70	1.71	1.72
	1 70	7.74	1 ~~	1 50	1 ~~	7 70	1.00	101	1.00	1.00
16	1.73 1.84	1.74	1.75 1.86	1.76 1.87	1.77 1.88	1.78 1.89	1.80 1.90	1.81 1.91	1.82	1.83 1.94
17 18	1.95	1.96	1.50	1.98	1.99	2.00	2.01	2.02	2.03	2.04
19	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15
20	2.16	2.17	2.18	2.20	2.21	2.22	2.23	2.24	2.25	2.26
20										
21	2.27	2.28	2.29	2.30	2.31	2.33	2.34	2.35	2.36	2.37
22	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.46	2.47	2.48
23	2.49	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.59
24	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.68	2.69
25	2.70	2.71	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80
90	9.03	0.00	0.00	0.04	0.00	0.0~	9.00	2.89	9.00	9.07
26	2.81	2.82 2.93	2.83 2.94	2.84 $2.95$	2.86 2.96	2.87 $2.97$	2.88 2.99	3.00	2.90 3.01	2.91 3.02
27 28	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.13
29	3.14	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23
30	3.24	3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34
31	3.35	3.36	3.37	3.39	3.40	3.41	3.42	3.43	3.44	3.45
32	3.46	3.47	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.56
33	3.57	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.66	3.67
34	3.68	3.69	3.70	3.71	3.72	3.73	3.74	3.75	3.76	3 77
35	3.79	3.80	3.81	3.82	3.83	3.84	3.85	3.86	3.87	3.88
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROME	ETER:	675 <sup>mm</sup> ·	(from 6	672.51 t	o 677.5	0).	
Centigrade Degrees.					Tenths of	f Degrees.				
The Party	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.05	0.07	0.08	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.32
3	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53
5	0.54	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.64
6	0.65	0.66	0.68	0.69	0.70	0.71	0.72	0.73	0.74	0.75
7	0.76	0.77	0.03	0.80	0.70	0.71	0.72	0.73	0.74	0.75
8	0.87	0.88	0.89	0.90	0.92	0.93	0.94	0.95	0.96	0.97
9	0.98	0.99	1.00	1.01	1.02	1.03	1.05	1.06	1.07	1.08
10	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19
11	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.29	1.30
12	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.41
13	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51
14	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62
15	1.63	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73
16	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.82	1.83	1.84
17	1.85	1.86	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95
18	1.96	1.97	1.98	1.99	2.00	2.02	2.03	2.04	2.05	2.06
19	2.07	2.08	2.09	2.10	2.11	2.12	2.14	2.15	2.16	2.17
20	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.26	2.27	2.28
21	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.38	2.39
22	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49
23	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.60
24	2.61	2.63	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71
25	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
26	2.83	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92	2.93
27	2.94	2.95	2.96	2.97	2.99	3.00	3.01	3.02	3.03	3.04
28	3.05	3.06	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15
29	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.24	3.25	3.26
30	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.36	3.37
			٠							
31	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.48
32	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58
33	3.60	3.61	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69
34 35	3.70 3.81	3.72	3.73 3.83	3.74 $3.85$	3.75 3.86	3.76 3.87	3.77 3.88	3.78 3.89	3.79 3.90	3.80 3.91
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROMI	ETER :	680 <sup>mm.</sup>	(from	677.51 t	o 682.50	0).	
Centi- grade Degrees.					Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim, 0.02	Millim. 0.03	Millim. 0.04	Millim, 0.05	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim.
1	0.11	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.29	0.30	0.31	0.32
3	0.33	0.34	0.35	0.36	0.37	0.38	0.40	0.41	0.42	0.43
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54
5	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.63	0.64	0.65
6	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76
7	0.77	0.78	0.79	0.80	0.81	0.82	0.83	0.85	0.86	0.87
8	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.97	0.98
9	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.08	1.09
10	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.19	1.20
11	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.30	1.31
12	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42
13	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53
14	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.64
15	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.75
16	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85
17	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96
18	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07
19	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18
20	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29
21	2.30	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40
22	2.41	2.43	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51
23	2.52	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62
24	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.72	2.73
25	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
26	2.85	2.86	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95
27	2.96	2.97	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06
28	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17
29	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.26	3.27	3.28
30	3.29	3.30	3.31	3.33	3.34	3.35	3.36	3.37	3.38	3.39
31	3.40	3.41	3.42	3.44	3.45	3.46	3.47	3.48	3.49	3.50
32	3.51	3.52	3.53	3.54	3.56	3.57	3.58	3.59	3.60	3.61
33	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.70	3.71	3.72
34	3.73	3.74	3.75	3.76	3.78	3.79	3.80	3.81	3.82	3.83
35	3.84	3.85	3.86	3.87	3.89	3.90	3.91	3.92	3.93	3.94
-1	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROMI	ETER:	685 <sup>mm.</sup>	(from	682.51 t	o 687.50	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim, 0.03	Millim.	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim, 0.10
1	0.11	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.32
3	0.33	0.34	0.35	0.36	0.38	0.39	0.40	0.41	0.42	0.43
4	0.44	0.45	0.46	0.48	0.49	0.50	0.51	0.52	0.53	0.54
5	0.55	0.56	0.57	0.59	0.60	0.61	0.62	0.63	0.64	0.65
6	0.66	0.67	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76
7	0.77	0.78	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87
8	0.88	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98
9	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09
10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.21
11	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.32
12	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42	1.43
13	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53	1.54
14	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65
15	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.74	1.75	1.76
10	1.77	1 *0	1 70	1.00	101	1.82	104	105	1.00	10~
16	1.88	1.78 1.89	1.79 1.90	1.80 1.91	1.81 1.92	1.93	1.84	1.85 1.96	1.86	1.87 1.98
17 18	1.99	2.00	2.01	2.02	2.03	2.05	2.06	2.07	2.08	2.09
19	2.10	2.11	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20
20	2.21	2.22	2.23	2.24	2.26	2.27	2.28	2.29	2.30	2.31
0.1	2.32	2.33	2.34	2.35	2.37	2.38	2.39	2.40	2.41	2.42
21 22	2.32	2.44	2.45	2.35	2.48	2.35	2.50	2.40	2.41	2.42
23	2.54	2.55	2.56	2.58	2.59	2.60	2.61	2.62	2.63	2.64
24	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75
25	2.76	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86
26	2.87	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97
26	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08
28	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.20
29	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.31
30	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.41	3.42
31	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.52	3.53
32	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.62	3.63	3.64
33	3.65	3.66	3.67	3.68	3.69	3.70	3.71	3.73	3.74	3.75
34	3.76	3.77	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86
35	3.87	3.88	3.89	3.90	3.91	3.92	3.94	3.95	3.96	3.97
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER :	690 <sup>mm</sup>	(from	687.51	to 692.5	0).	
Centigrade Degrees.		· · · · · -			Tenths o	f Degrees.		-		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.21
2	0.22	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.31	0.32
3	0.33	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42	0.43
4	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55
5	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.65	0.66
6	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76	0.77
7	0.78	0.79	0.80	0.70	0.82	0.72	0.74	0.86	0.70	0.88
8	0.89	0.90	0.91	0.92	0.94	0.95	0.96	0.97	0.98	0.99
9	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10
10	1.11	1.12	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21
11	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1 00
12	1.34	1.35	1.36	1.20	1.38	1.39	1.40	1.41	1.43	1.33 1.44
13	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53	1.54	1.55
14	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.66
15	1.67	1.68	1.69	1.70	1.72	1.73	1.74	1.75	1.76	1.77
	3 =0	7	7.00	- 00			- 0-	- 00		
16	1.78	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.87	1.88
17	1.89 2.00	1.90 2.02	1.92 2.03	1.93	1.94	1.95	1.96	1.97	1.98	1.99
18 19	2.12	2.02	2.14	2.04 2.15	$2.05 \\ 2.16$	$2.06 \\ 2.17$	2.07 $2.18$	2.08 2.19	$2.09 \\ 2.21$	2.10 $2.22$
20	2.23	2.24	2.25	2.15	2.27	2.28	2.18	2.13	2.32	2.33
21	2.34	2.35	2.36	2.37	2.38	2.39	2.41	2.42	2.43	2.44
22	2.45	2.46	2.47	2.48	2.49	2.51	2.52	2.53	2.54	2.55
23	2.56	2.57	2.58	2.59	2.61	2.62	2.63	2.64	2.65	2.66
24 25	2.67 2.78	2.68 2.80	2.70 2.81	2.71 $2.82$	2.72 2.83	2.73 2.84	2.74 $2.85$	$2.75 \\ 2.86$	$2.76 \\ 2.87$	2.77 2.88
40	2.10	2.00	4.01	4.02	2.00	2.04	2.00	2.00	2.01	4.00
26	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00
27	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.10	3.11
28	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22
29	3.23	3.24	3.25	3.26	3.27	3.29	3.30	3.31	3.32	3.33
30	3.34	3.35	3.36	3.37	3.39	3.40	3.41	3.42	3.43	3.44
31	3.45	3.46	3.47	3.49	3.50	3.51	3.52	3.53	3.54	3.55
32	3.56	3.57	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66
33	3.68	3.69	3.70	3.71	3.72	3.73	3.74	3.75	3.76	3.78
34	3.79	3.80	3.81	3.82	3.83	3.84	3.85	3.86	3.88	3.89
35	3.90	3.91	3.92	3.93	3.94	3.95	3.96	3.98	3.99	4.00
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 695 <sup>mm.</sup> (from 692.51 to 697.50).										
Centigrade Degrees.					Tenths of	Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim,	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.03	0.04	0.06	0.07	0.08	0.09	0.10	
1	0.11	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.20	0.21	
2	0.22	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31	0.33	
3	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44	
4	0.45	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54	0.55	
5	0.56	0.57	0.58	0.59	0.61	0.62	0.63	0.64	0.65	0.66	
6	0.67	0.68	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	
7	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.89	
8	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.98	0.99	1.00	
9	1.01	1.02	1.03	1.04	1.05	1.07	1.08	1.09	1.10	1.11	
10	1.12	1.13	1.14	1.16	1.17	1.18	1.19	1.20	1.21	1.22	
11	1.23	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	
12	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.42	1.44	1.45	
13	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56	
14	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.66	1.67	
15	1.68	1.69	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78	
				i						}	
16	1.79	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.90	
17	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.99	2.00	2.01	
18	2.02	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.12	
19	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.21	2.22	2.23	
20	2.24	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	
21	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.45	2.46	
22	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.55	2.45	2.57	
23	2.58	2.59	2.60	2.61	2.62	2.64	2.65	2.66	2.67	2.68	
24	2.69	2.70	2.71	2.73	2.74	2.75	2.76	2.77	2.78	2.79	
25	2.80	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.91	
26	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00	3.01	3.02	
27	3.03	3.04	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	
28	3.14	3.15	3.16	3.17	3.19	3.20	3:21	3.22	3.23	3.24	
29	3.25	3.26	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	
30	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.47	
31	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.56	3.57	3.58	
32	3.59	3.60	3.61	3.62	3.63	3.65	3.66	3.67	3.68	3.69	
33	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.78	3.79	3.80	
34	3.81	3.83	3,84	3.85	3.86	3.87	3.88	3.89	3.90	3.91	
35	3.93	3.94	3.95	3.96	3.97	3.98	3.99	4.00	4.02	4.03	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

		В.	AROMI	ETER :	700 <sup>mm</sup> .	(from	69 <b>7</b> .51 t	o 702.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10
	0.11	0.10	0.14	0.15	0.10	0.17	0.18	0.10	0.20	0.01
$\begin{vmatrix} 1 \\ 2 \end{vmatrix}$	0.11	0.12	0.14	$0.15 \\ 0.26$	0.16	$0.17 \\ 0.28$	0.18	0.19 0.31	0.20	0.21 0.33
3	0.23	0.35	0.36	0.20	0.27	0.40	0.29	0.31	0.32	0.33
4	0.45	0.46	0.47	0.49	0.50	0.51	0.52	0.53	0.54	0.55
5	0.56	0.58	0.59	0.60	0.61	0.62	0.63	0.64	0.66	0.67
6	0.68	0.69	0.70	0.71	0.72	0.73	0.75	0.76	0.77	0.78
7	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87	0.88	0.89
8	0.90	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.01
9	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.10	1.11	1.12
10	1.13	1.14	1.15	1.16	1.17	1.19	1.20	1.21	1.22	1.23
	1.24	1.05	1.27	1 90	1 90	1.00	1 01	1.00	1.00	7.04
11 12	1.36	1.25 1.37	1.38	1.28 $1.39$	1.29 1.40	1.30 1.41	1.31 1.42	1.32 1.43	1.33	1.34
13	1.47	1.48	1.49	1.50	1.51	1.53	1.54	1.45	1.45 1.56	1.46 1.57
14	1.58	1.59	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68
15	1.69	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.79	1.80
10				2.10	200.2	2000	2000	2000	1	1.00
16	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
17	1.92	1.93	1.94	1.95	1.97	1.98	1.99	2.00	2.01	2.02
18	2.03	2.04	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.14
19	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.23	2.24	2.25
20	2.26	2.27	, 2.28	2.29	2.30	2.32	2.33	2.34	2.35	2.36
	0.07	9.90	0.40	0.47	0.40	0.40	0.44	2.47	2.40	
21	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47
22 23	2.49 2.60	$2.50 \\ 2.61$	$2.51 \\ 2.62$	$2.52 \\ 2.63$	2.53 $2.64$	2.54 2.66	2.55 $2.67$	2.56 $2.68$	2.58 2.69	2.59
23 24	2.71	2.72	2.73	2.75	2.76	2.77	2.78	$\frac{2.68}{2.79}$	2.89	2.70 $2.81$
25	2.82	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.93
				2.50	2.0,	2.30	2.50	2.00	1	21.00
26	2.94	2.95	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04
27	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15
28	3.16	3.17	3,19	3.20	3.21	3.22	3.23	3.24	3.25	3.27
29	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.36	3.37	3.38
30	3.39	3.40	3.41	3.42	3.43	3.45	3.46	3.47	3.48	3.49
0.7	2.50	0.51	9.50	2.54	0.75	0.50	0.7=	0.70	0.50	0.55
31	3.50	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.59	3.60
32	3.62 3.73	$\frac{3.63}{3.74}$	3.64 3.75	3.65 3.76	3.66 .3.77	3.67 3.78	3.68 3.80	3.69	3.71	3.72
34	3.84	3.85	3.86	3.88	3.89	3.90	3.91	$\frac{3.81}{3.92}$	$\frac{3.82}{3.93}$	3.83 3.94
35	3.95	3.97	3.98	3.99	4.00	4.01	4.02	4.03	4.04	4.06
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
C					101					

Centigrade Degrees.	0. Millim. 0.00	1.			Tenths o									
	Millim.	1.	Tenths of Degrees.											
0			2.	3.	4.	5.	6.	7.	8.	9.				
	0.00 1	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.				
0	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10				
1	0.11	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.22				
2	0.23	0.24	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0 33				
3	0.34	0.35	0.36	0.38	0.39	0.40	0.41	0.42	0.43	0.44				
4	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55	0.56				
5	0.57	0.58	0.59	0.60	0.61	0.63	0.64	0.65	0.66	0.67				
6	0.68	0.69	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.79				
7	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.88	0.89	0.90				
8	0.91	0.92	0.93	0.94	0.96	0.97	0.98	0.99	1.00	1.01				
9	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.12	1.13				
10	1.14	1.15	1.16	1.17	1.18	1.19	1.21	1.22	1.23	1.24				
	1.25	1.26	1.27	1.29	1.30	1.31	1.32	1.33	1.34	7 95				
11 12	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.45	1.46	1.35 $1.47$				
13	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.40	1.58				
14	1.59	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70				
15	1.71	1.72	1.73	1.74	1.75	1.76	1.78	1.79	1.80	1.81				
10		2.12	1000	2002	1.10	2000	1	1	1.00	1.01				
16	1.82	1.83	1.84	1.85	1.87	1.88	1.89	1.90	1.91	1.92				
17	1.93	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.03	2.04				
,18	2.05	2.06	2.07	2.08	2.09	2.11	2.12	2.13	2.14	2.15				
19	2.16	2.17	2.18	2.20	2.21	2.22	2.23	2.24	2.25	2.26				
20	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.36	2.37	2.38				
21	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.49				
22	2.50	2.51	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.61				
23	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70	2.71	2.72				
24	2.73	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.83				
25	2.84	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.94	2.95				
26	2.96	2.97	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.06				
27	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17				
28	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.27	3.28	3.29				
29	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40				
30	3.41	3.42	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.52				
21	3.53	9.54	9.55	3.56	0 5 7	9 50	2.60	9.61	2 69	2.62				
31 32	3.64	3.54	3.55		3.57	3.58	3.60	3.61 3.72	3.62	3.63				
33	3.75	3.65 3.77	3.66 3.78	3.68 3.79	3.69 3.80	3.70 3.81	$\frac{3.71}{3.82}$	3.83	3.73 3.85	3.74				
34	3.87	3.88	3.89	3.90	3.91	3.93	3.94	3.95	3.96	$3.86 \\ 3.97$				
35	3.98	3.99	4.01	4.02	4.03	4.04	4.05	4.06	4.07	4.08				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

	BAROMETER: 710 <sup>mm</sup> (from 707.51 to 712.50).										
Centi- grade Degrees.					Tenths o	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim. 0.00	Millim. 0.01	Millim.	Millim. 0.03	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim, 0.08	Millim. 0.09	Millim. 0.10	
1	0.11	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.21	0.22	
2	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.31	0.32	0.33	
3	0.34	0.36	0.37	0.38	0.39	0.40	0.41	0.42	0.44	0.45	
4	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54	0.55	0.56	
5	0.57	0.58	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.68	
6	0.69	0.70	0.71	0.72	0.73	0.74	0.76	0.77	0.78	0.79	
7	0.80	0.81	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.91	
8	0.92	0.93	0.94	0.95	0.96	0.97	0.99	1.00	1.01	1.02	
9	1.03	1.04	1.05	1.07	1.08	1.09	1.10	1.11	1.12	1.13	
10	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.23	1.24	1.25	
11	1.26	1.27	1.28	1.29	1.31	1.32	1.33	1.34	1.35	1.36	
12	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.46	1.47	1.48	
13	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59	
14	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70	1.71	
15	1.72	1.73	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.82	
16	1.83	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.93	1.94	
17	1.95	1.96	1.97	1.98	1.99	2.01	2.02	2.03	2.04	2.05	
18	2.06	2.07	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.17	
19	2.18	2.19	2.20	2.21	2.22	2.23	2.25	2.26	2.27	2.28	
20	2.29	2.30	2.31	2.33	2.34	2.35	2.36	2.37	2.38	2.40	
21	2.41	2.42	2.43	2.44	2.45	2.46	2.48	2.49	2.50	2.51	
22	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.60	2.61	2.62	
23	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.72	2.73	2.74	
24	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.83	2.84	2.85	
25	2.86	2.88	2.89	2.90	2.91	2.92	2.93	2.95	2.96	2.97	
26	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.07	3.08	
27	3.09	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20	
28	3.21	3.22	3.23	3.24	3.25	3.27	3.28	3.29	3.30	3.31	
29	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.43	
30	3.44	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53	3.54	
31	3.55	3.56	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.66	
32	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77	
33	3.78	3.79	3.80	3.82	3.83	3.84	3.85	3.86	3.87	3.88	
34	3.90	3.91	3.92	3.93	3.94	3.95	3.96	3.98	3.99	4.00	
35	4.01	4.02	4.03	4.05	4.06	4.07	4.08	4.09	4.10	4.11	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 715 <sup>mm.</sup> (from 712.51 to 717.50).										
Centigrade Degrees.					Tenths of	Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.10	
1	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.20	0.21	0.22	
2	0.23	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.32	0.33	
3	0.35	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	
4	0.46	0.47	0.48	0.50	0.51	0.52	0.53	0.54	0.55	0.57	
5	0.58	0.59	0.60	0.61	. 0.62	0.63	0.65	0.66	0.67	0.68	
6	0.69	0.70	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.80	
7	0.81	0.82	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91	
8	0.92	0.93	0.95	0.96	0.97	0.98	0.99	1.00	1.02	1.03	
9	1.04	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.13	1.14	
10	1.15	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.25	1.26	
	1.00	1.00	1.29	1.30	1.32	1.33	1.34	1.35	1.36	1.37	
11	1.27	1.28	1.41	1.42	1.43	1.44	1.45	1.35 $1.47$	1.48	1.49	
12	1.38	1.40		1.42	1.55	1.56	1.45	1.58	1.59	1.60	
13	1.50	1.51	1.52	1.65	1.66	1.67	1.68	1.70	1.71	1.72	
14	1.62	1.63	1.64 1.75	1.05	1.78	1.79	1.80	1.81	1.82	1.83	
15	1.73	1.74	1.19	1.77	1.10	1.13	1.00	1.01	1.02	1.00	
16	1.85	1.86	1.87	1.88	1.89	1.90	1.92	1.93	1.94	1.95	
17	1.96	1.97	1.98	2.00	2.01	2.02	2.03	2.04	2.05	2.07	
18	2.08	2.09	2.10	2.11	2.12	2.13	2.15	2.16	2.17	2.18	
19	2.19	2.20	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.30	
20	2.31	2.32	2.33	2.34	2.35	2.37	2.38	2.39	2.40	2.41	
21	2.42	2.43	2.45	2.46	2.47	2.48	2.49	2.50	2.52	2.53	
22	2.54	2.55	2.56	2.57	2.58	2.60	2.61	2.62	2.63	2.64	
23	2.65	2.67	2.68	2.69	2.70	2.71	2.72	2.74	2.75	2.76	
24	2.77	2.78	2.79	2.80	2.82	2.83	2.84	2.85	2.86	2.87	
25	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.97	2.98	2.99	
26	3.00	3.01	3.02	3.04	3.05	3.06	3.07	3.08	3.09	3.10	
27	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22	
28	3.23	3.24	3.25	3.27	3.28	3.29	3.30	3.31	3.32	3.34	
29	3.35	3.36	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45	
30	3.46	3.47	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.57	
31	3.58	3.59	3.60	3.61	3.62	3.64	3.65	3.66	3.67	3.68	
32	3.69	3.70	3.72	3.73	3.74	3.75	3.76	3.77	3.79	3.80	
33	3.81	3.82	3.83	3.84	3.85	3.87	3.88	3.89	3.90	3.91	
34	3.92	3.94	3.95	3.96	3.97	3.98	3.99	4.00	4.02	4.03	
35	4.04	4.05	4.06	4.07	4.09	4.10	4.11	4.12	4.13	4.14	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 720 <sup>mm.</sup> (from 717.51 to 722.50).										
Centigrade Degrees.					Tenths o	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10	
1	0.12	0.13	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	
2	0.23	0.24	0.26	0.27	0.28	0.29	0.30	0.31	0.33	0.34	
3	0.35	0.36	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.45	
4	0.46	0.48	0.49	0.50	0.51	0.52	0.53	0.55	0.56	0.57	
5	0.58	0.59	0.60	0.62	0.63	0.64	0.65	0.66	0.67	0.69	
C	0.70	0.71	0.72	0.73	0.74	0.76	0.77	0.78	0.79	0.80	
7	0.70	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.73	0.92	
8	0.93	0.94	0.95	0.96	0.98	0.99	1.00	1.01	1.02	1.03	
9	1.05	1.06	1.07	1.08	1.09	1.10	1.12	1.13	1.14	1.15	
10	1.16	1.17	1.19	1.20	1.21	1.22	1.23	1.24	1.26	1.27	
11	1.28	1.29	1.30	1.31	1.32	1.34	1.35	1.36	1.37	1.38	
12	1.39	1.41	1.42	1.43	1.44	1.45	1.46	1.48	1.49	1.50	
13	1.51	1.52	1.53	1.55	1.56	1.57	1.58	1.59	1.60	1.62	
14	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.73	
15	1.74	1.75	1.77	1.78	1.79	1.80	1.81	1.82	1.84	1.85	
7.0	1.00	1.0#	1 00	1.00	1.01	1.00	1.00	1.04	1.05	1.00	
16	1.86 1.98	1.87 1.99	1.88 2.00	1.89 2.01	1.91 2.02	1.92 $2.03$	1.93 2.05	1.94 2.06	1.95 2.07	1.96	
17 18	2.09	2.10	2.11	2.13	2.14	2.05	2.16	2.17	2.18	2.08 2.20	
19	2.21	2.22	2.23	2.24	2.25	2.27	2.28	2.29	2.30	2.31	
20	2.32	2.34	2.35	2.36	2.37	2.38	2.39	2.41	2.42	2.43	
				2.00						2.10	
21	2.44	2.45	2.46	2.48	2.49	2.50	2.51	2.52	2.53	2.54	
22	2.56	2.57	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66	
23	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.77	2.78	
24	2.79	2.80	2.81	2.82	2.84	2.85	2.86	2.87	2.88	2.89	
25	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.99	3.00	3.01	
90	2.00	2.02	204	2.00	2.07	2.00	2.00	2 10	9 11	9.10	
26	3.02 3.14	3.03 3.15	3.04 3.16	$\frac{3.06}{3.17}$	3.07 3.18	3.08	3.09 3.21	3.10 $3.22$	3.11	3.13	
27 28	3.14	3.27	3.16	3.17	3.30	3.31	3.32	3.34	3.23	3.24 3.36	
28	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45	3.46	3.36	
30	3.49	3.50	3.51	3.52	3.53	3.54	3.56	3.57	3.58	3.59	
00	3.10	0.50	0.01	J.02	0.00	V.0.2	3.00	0.01	0.00	0.00	
31	3.60	3.61	3.63	3.64	3.65	3.66	3.67	3.68	3.70	3.71	
32	3.72	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.81	3.82	
33	3.83	3.85	3.86	3.87	3.88	3.89	3.90	3.92	3.93	3.94	
34	3.95	3.96	3.97	3.99	4.00	4.01	4.02	4.03	4.04	4.06	
35	4.07	4.08	4.09	4.10	4.11	4.13	4.14	4.15	4.16	4.17	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 725 <sup>mm.</sup> (from 722.51 to 727.50).										
Centigrade Degrees.					Tenths o	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.11	
1	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.22	
2	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.32	0.33	0.34	
3	0.35	0.36	0.37	0.39	0.40	0.41	0.42	0.43	0.44	0.46	
4	0.47	0.48	0.49	0.50	0.51	0.53	0.54	0.55	0.56	0.57	
5	0.59	0.60	0.61	0.62	0.63	0.64	0.66	0.67	0.68	0.69	
								0.55			
6	0.70	0.71	0.73	0.74	0.75	0.76	0.77	0.78	0.80	0.81	
7	0.82	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.92	
8	0.94	0.95	0.96	0.97	0.98	0.99	1.01	1.02	1.03	1.04	
9	1.05	1.06	1.08	1.09	1.10	1.11	1.12	1.14	1.15	1.16	
10	1.17	1.18	1.19	1.21	1.22	1.23	1.24	1.25	1.26	1.28	
11	1.29	1.30	1.31	1.32	1.33	1.35	1.36	1.37	1.38	1.39	
12	1.40	1.42	1.43	1.44	1.45	1.46	1.47	1.49	1.50	1.51	
13	1.52	1.53	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.63	
14	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.74	
15	1.76	1.77	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86	
16	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95	1.97	1.98	
17	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.08	2.09	
18	2.11	2.12	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.21	
19	2.22	2.23	2.25	2.26	2.27	2.28	2.29	2.31	2.32	2.33	
20	2.34	2.35	2.36	2.38	2.39	2.40	2.41	2.42	2.43	2.45	
21	2.46	2.47	2.48	2.49	2.50	2.52	2.53	2.54	2.55	2.56	
22	2.57	2.59	2.60	2.61	2.62	2.63	2.64	2.66	2.67	2.68	
23	2.69	2.70	2.71	2.73	2.74	2.75	2.76	2.77	2.78	2.80	
24	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89	2.90	2.91	
25	2.93	2.94	2.95	2.96	2.97	2.98	3.00	3:01	3.02	3.03	
26	3.04	3.05	3.07	3.08	3.09	3.10	3.11	3.12	3.14	3.15	
27	3.16	3.17	3.18	3.19	3.21	3.22	3.23	3.24	3.25	3.26	
28	3.28	3.29	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	
29	3.39	3.41	3.42	3.43	3.44	3.45	3.46	3.48	3.49	3.50	
30	3.51	3.52	3.53	3.55	3.56	3.57	3.58	3.59	3.60	3.62	
31	3.63	3.64	3.65	3.66	3.67	3.69	3.70	3.71	3.72	3.73	
32	3.74	3.76	3.77	3.78	3.79	3.80	3.81	3.83	3.84	3.85	
33	3.86	3.87	3.88	3.90	3.91	3.92	3.93	3.94	3.96	3.97	
34	3.98	3.99	4.00	4.01	4.03	4.04	4.05	4.06	4.07	4.08	
35	4.10	4.11	4.12	4.13	. 4.14	4.15	4.17	4.18	4.19	4.20	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 730 <sup>mm.</sup> (from 727.51 to 732.50).										
Centigrade Degrees.					Tenths o	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
	0.70	0.70	0.7.			0.10					
1	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.22	
2	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34	
3	0.35	0.37	0.38	0.39	0.40	0.41	0.42	0.44	0.45	0.46	
4	0.47	0.48		0.51	0.52	0.53	0.54	0.55	0.57	0.58	
5	0.59	0.60	0.61	0.62	0.64	0.65	0.66	0.67	0.68	0.70	
6	0.71	0.72	0.73	0.74	0.75	0.77	0.78	0.79	0.80	0.81	
7	0.82	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	
8	0.94	0.95	0.97	0.98	0.99	1.00	1.01	1.03	1.04	1.05	
9	1.06	1.07	1.08	1.10	1.11	1.12	1.13	1.14	1.15	1.17	
10	1.18	1.19	1.20	1.21	1.23	1.24	1.25	1.26	1.27	1.28	
11	1.30	1.31	1.32	1.33	1.34	1.35	1.37	1.38	1.39	1.40	
12	1.41	1.43	1.44	1.45	1.46	1.47	1.48	1.50	1.51	1.52	
13	1.53	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	
14	1.65	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.74	1.76	
15	1.77	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86	1.87	
16	1.89	1.90	1.91	1.92	1.93	1.94	1.96	1.97	1.98	1.99	
17	2.00	2 01	2.03	2.04	2.05	2.06	2.07	2.09	2.10	2.11	
18	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20	2.22	2.23	
19	2.24	2.25	2.26	2.27	2.29	2.30	2.31	2.32	2.33	2.34	
20	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44	2.45	2.46	
21	2.47	2.49	2.50	2.51	2.52	2.53	2.54	2.56	2.57	2.58	
22	2.59	2.60	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70	
23	2.71	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.82	
24	2.83	2.84	2.85	2.86	2.87	2.89	2.90	2.91	2.92	2.93	
25	2.95	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04	3.05	
26	3.06	3.08	3.09	3.10	3.11	3.12	3.13	3.15	3.16	3.17	
27	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.26	3.28	3.29	
28	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.41	
29	3.42	3.43	3.44	3.45	3.46	3.48	3.49	3.50	3.51	3.52	
30	3.53	3.55	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64	
31	3.65	3.66	3.68	3.69	3.70	3.71	3 72	3.73	3.75	3.76	
32	3.77	3.78	3.79	3.81	3.82	3.83	3.84	3.85	3.86	3.88	
33	3.89	3.90	3.91	3.92	3.94	3.95	3.96	3.97	3.98	3.99	
34	4.01	4.02	4.03	4.04	4.05	4.06	4.07	4.09	4.10	4.11	
35	4.12	4.14	4.15	4.16	4.17	4.18	4.19	4.21	4.22	4.23	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 735 <sup>mm.</sup> (from 732.51 to 737.50).										
Centi- grade Degrees.					Tenths o	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.11	
1	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.21	0.23	
2	0.24	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.34	
3	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.46	
4	0.47	0.49	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58	
5	0.59	0.61	0.62	0.63	0.64	0.65	0.66	0.68	0.69	0.70	
6	0.71	0.72	0.74	0.75	0.76	0.77	0.78	0.79	0.81	0.82	
7	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.93	0.94	
8	0 95	0.96	0.97	0.98	1.00	1.01	1.02	1.03	1.04	1.06	
9	1.07	1.08	1.09	1.10	1.12	1.13	1.14	1.15	1.16	1.17	
10	1.19	1.20	1.21	1.22	1.23	1.25	1.26	1.27	1.28	1.29	
11	1.30	1.32	1.33	1.34	1.35	1.36	1.37	1.39	1.40	1.41	
12	1.42	1.44	1.45	1.46	1.47	1.48	1.49	1.51	1.52	1.53	
13	1.54	1.55	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65	
14	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.74	1.76	1.77	
15	1.78	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.87	1.89	
	- 00										
16	1.90	1.91	1.92	1.93	1.95	1.96	1.97	1.98	1.99	2.00	
17	2.02	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.12	
18	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.23	2.24	
19	2.25	2.27	2.28	2.29	2.30	2.31	2.33	2.34	2.35	2.36	
20	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.46	2.47	2.48	
21	2.49	2.50	2.51	2.53	2.54	2.55	2.56	2.57	2.59	2.60	
22	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.72	
23	2.73	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.82	2.84	
24	2.85	2.86	2.87	2.88	2.89	2.91	2.92	2.93	2.94	2.95	
25	2.97	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.07	
26	3.08	3.10	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.19	
27	3.20	3.21	3.23	3.24	3.25	3.26	3.27	3.29	3.30	3.31	
28	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40	3.42	3.43	
29	3.44	3.45	3.46	3.48	3.49	3.50	3.51	3.52	3.54	3.55	
30	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64	3.65	3.67	
								0.70		0.55	
31	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.78	
32	3.80	3.81	3.82	3.83	3.84	3.86	3.87	3.88	3.89	3.90	
33	3.91	3.93	3.94	3.95	3.96	3.97	3.99	4.00	4.01	4.02	
34	4.03	3.05	4.06	4.07	4.08	4.09	4.10	4.12	4.13	4.14	
35	4.15	4.16	4.18	4.19	4.20	4.21	4.22	4.24	4.25	4.26	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 740 <sup>mm</sup> (from 737.51 to 742.50).										
Centi- grade Degrees.					Tenths of	Degrees.					
	0.	L	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim.	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim.	Millim. 0.11	
1	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.21	0.23	
2	0.24	0.25	0.26	0.27	0.29	0.30	0.31	0.32	0.33	0.35	
3	0.36	0.37	0.38	0.39	0.41	0.42	0.43	0.44	0.45	0.47	
4	0.48	0.49	0.50	0.51	0.53	0.54	0.55	0.56	0.57	0.59	
5	0.60	0.61	0.62	0.63	0.64	0.66	0.67	0.68	0.69	0.70	
6	0.72	0.73	0.74	0.75	0.76	0.78	0.79	0.80	0.81	0.82	
7	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	
8	0.96	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.06	
9	1.07	1.09	1.10	1.11	1.12	1.13	1.15	1.16	1.17	1.18	
10	1.19	1.21	1.22	1.23	1.24	1.25	1.27	1.28	1.29	1.30	
11	1.31	1.33	1.34	1.35	1.36	1.37	1.39	1.40	1.41	1.42	
12	1.43	1.45	1.46	1.47	1.48	1.49	1.50	1.52	1.53	1.54	
13	1.55	1.56	1.58	1.59	1.60	1.61	1.62	1.64	1.65	1.66	
14	1.67	1.68	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78	
15	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	
16	1.91	1.92	1.93	1.95	1.96	1.97	1.98	1.99	2.01	2.02	
17	2.03	2.04	2.05	2.07	2.08	2.09	2.10	2.11	2.13	2.14	
18	2.15	2.16	2.17	2.19	2.20	2.21	2.22	2.23	2.25	2.26	
19	2.27	2.28	2.29	2.31	2.32	2.33	2.34	2.35	2.36	2.38	
20	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.50	
21	2.51	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.60	2.62	
22	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.74	
23	2.75	2.76	2.77	2.78	2.79	2.81	2.82	2.83	2.84	2.85	
24	2.87	2.88	2.89	2.90	2.91	2.93	2.94	2.95	2.96	2.97	
25	2.99	3.00	3.01	3.02	3.03	3.05	3.06	3.07	3.08	3.09	
26	3.11	3.12	3.13	3.14	3.15	3.17	3.18	3.19	3.20	3.21	
27	3.22	3.24	3.25	3.26	3.27	3.28	3.30	3.31	3.32	3.33	
28	3.34	3.36	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45	
29	3.46	3.48	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.57	
30	3.58	3.60	3.61	3.62	3.63	3.64	3.65	3.67	3.68	3.69	
31	3.70	3.71	3.73	3.74	3.75	3.76	3.77	3.79	3.80	3.81	
32	3.82	3.83	3.85	3.86	3.87	3.88	3.89	3.91	3.92	3.93	
33	3.94	3.95	3.97	3.98	3.99	4.00	4.01	4.02	4.04	4.05	
34	4.06	4.07	4.08	4.10	4.11	4.12	4.13	4.14	4.16	4.17	
35	4.18	4.19	4.20	4.22	4.23	4.24	4.25	4.26	4.28	4.29	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 745 <sup>mm</sup> (from 742.51 to 747.50).													
Centi- grade Degrees.		Tenths of Degrees.												
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim. 0.00	Millim. 0.01	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.10	Millim. 0.11				
1	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.22	0.23				
2	0.24	0.25	0.26	0.28	0.29	0.30	0.31	0.32	0.34	0.35				
3	0.36	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.46	0.47				
4	0.48	0.49	0.51	0.52	0.53	0.54	0.55	0.57	0.58	0.59				
5	0.60	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71				
6	0.72	0.73	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83				
7	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.93	0.94	0.95				
8	0.96	0.97	0.99	1.00	1.01	1.02	1.03	1.05	1.06	1.07				
9	1.08	1.09	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19				
10	1.20	1.21	1.23	1.24	1.25	1.26	1.27	1.29	1.30	1.31				
11	1.32	1.33	1.35	1.36	1.37	1.38	1.39	1.41	1.42	1.43				
12	1.44	1.45	1.47	1.48	1.49	1.50	1.52	1.53	1.54	1.55				
13	1.56	1.58	1.59	1.60	1.61	1.62	1.64	1.65	1.66	1.67				
14	1.68	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79				
15	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91				
16	1.92	1.94	1.95	1.96	1.97	1.98	2.00	2.01	2.02	2.03				
17	2.04	2.06	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.15				
18	2.16	2.18	2.19	2.20	2.21	2.22	2.24	2.25	2.26	2.27				
19	2.28	2.30	2.31	2.32	2.33	2.34	2.36	2.37	2.38	2.39				
20	2.40	2.42	2.43	2.44	2.45	2.46	2.48	2.49	2.50	2.51				
21	2.53	2.54	2.55	2.56	2.57	2.59	2.60	2.61	2.62	2.63				
22	2.65	2.66	2.67	2.68	2.69	2.71	2.72	2.73	2.74	2.75				
23	2.77	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.87				
2.4	2.89	2.90	2.91	2.92	2.93	2.95	2.96	2.97	2.98	2.99				
25	3.01	3.02	3.03	3.04	3.05	3.07	3.08	3.09	3.10	3.11				
26	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.23				
27	3.25	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34	3.35				
28	3.37	3.38	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.48				
29	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.60				
30	3.61	3.62	3.63	3.64	3.66	3.67	3.68	3.69	3.70	3.72				
31	3.73	3.74	3.75	3.76	3.78	3.79	3.80	3.81	3.82	3.84				
32	3.85	3.86	3.87	3.88	3.90	3.91	3.92	3.93	3.94	3.96				
33	3.97	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.06	4.08				
34	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.18	4.20				
35	4.21	4.22	4.23	4.24	4.26	4.27	4.28	4.29	4.30	4.32				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

	BAROMETER: 750 <sup>mm</sup> (from 747.51 to 752.50).												
Centi- grade Degrees.		Tenths of Degrees.  0. 1. 2. 3. 4. 5. 6. 7. 8. 9.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.			
	0.00	0.01	0.02	0.01	0,00	0.00	0.01	0.03	0.10				
1	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.21	0.22	0.23			
2	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.33	0.34	0.35			
3	0.36	0.38	0.39	0.40	0.41	0.42	0.44	0.45	0.46	0.47			
4	0.48	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58	0.59			
5	0.61	0.62	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.71			
6	0.73	0.74	0.75	0.76	0.77	0.79	0.80	0.81	0.82	0.84			
7	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.96			
8	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.07	1.08			
9	1.09	1.10	1.11	1.13	1.14	1.15	1.16	1.17	1.19	1.20			
10	1.21	1.22	1.23	1.25	1.26	1.27	1.28	1.30	1.31	1.32			
11	1.33	1.34	1.36	1.37	1.38	1.39	1.40	1.42	1.43	1.44			
12	1.45	1.46	1.48	1.49	1.50	1.51	1.53	1.54	1.55	1.56			
13	1.57	1.59	1.60	1.61	1.62	1.63	1.65	1.66	1.67	1.68			
14	1.69	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79	1.80			
15	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.92			
	7.04				7.00	2.00				0.0			
16	1.94	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.03	2.05			
17	2.06	2.07	2.08	2.09 2.21	2.11	2.12	2.13	2.14	2.15	2.17			
18	2.30	2.19 2.31	2.32	2.34	$2.23 \\ 2.35$	2.24 $2.36$	2.25	2.26 2.38	2.28 2.40	2.29 $2.41$			
20	2.42	2.43	2.45	2.46	2.47	2.48	2.49	2.51	2.40	$\frac{2.41}{2.53}$			
		2.10		2.10	2011	2.10	2.40	2.01	2.02	2.55			
21	2.54	2.55	2.57	2.58	2.59	2.60	2.61	2.63	2.64	2.65			
22	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.75	2.76	2.77			
23	2.78	2.80	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89			
24	2.91	2.92	2.93	2.94	2.95	2.97	2.98	2.99	3.00	3.01			
25	3.03	3.04	3.05	3.06	3.07	3.09	3.10	3.11	3.12	3.14			
26	3.15	3.16	3.17	3.18	3.20	3.21	3.22	3,23	3.24	3.26			
27	3.27	3.28	3.29	3.30	3.32	3.33	3.34	3.35	3.37	3.38			
28	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.47	3.49	3.50			
29	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.60	3.61	3.62			
30	3.63	3.64	3.66	3.67	3.68	3.69	3.70	3.72	3.73	3.74			
31	3.75	3.76	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86			
32	3.87	3.89	3.90	3.91	3.92	3.93	3.95	3.96	3.97	3.98			
33	3.99	4.01	4.02	4.03	4.04	4.06	4.07	4.08	4.09	4.10			
34	4.12	4.13	4.14	4.15	4.16	4.18	4.19	4.20	4.21	4.22			
35	4.24	4.25	4.26	4.27	4.29	4.30	4.31	4.32	4.33	4.35			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

		BAROMETER: 755 <sup>tnm.</sup> (from 752.51 to 757.50).										
Centi- grade Degrees.	O.         1.         2.         3.         4.         5.         6.         7.         8.         9.           Millim.         Mill											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0					1	4			1			
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.09	0.10	0.11		
1	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.21	0.22	0.23		
2	0.24	0.26	0.27	0.28	0.29	0.30	0.32	0.33	0.34	0.35		
3	0.37	0.38	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.48		
4	0.49	0.50	0.51	0.52	0.54	0.55	0.56	0.57	0.58	0.60		
5	0.61	0.62	0.63	0.65	0.66	0.67	0.68	0.69	0.71	0.72		
6	0.73	0.74	0.76	0.77	0.78	0.79	0.80	0.82	0.83	0.84		
7	0.85	0.87	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.96		
8	0.97	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.08		
9	1.10	1.11	1.12	1.13	1.15	1.16	1.17	1.18	1.19	1.21		
10	1.22	1.23	1.24	1.26	1.27	1.28	1.29	1.30	1.32	1.33		
11	1.34	1.35	1.36	1.38	1.39	1.40	1.41	1.43	1.44	1.45		
11 12	1.46	1.35	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57		
13	1.58	1.60	1.43	1.62	1.63	1.65	1.66	1.67	1.68	1.69		
14	1.71	1.72	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82		
15	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94		
10	1100	2.01	2.00				1.00		2.00			
16	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.06		
17	2.07	2.08	2.10	2.11	2.12	2.13	2.14	2.16	2.17	2.18		
18	2.19	2.21	2.22	2.23	2.24	2.25	2.27	2.28	2.29	2.30		
19	2.32	2.33	2.34	2.35	2.36	.2.38	2.39	2.40	2.41	2.42		
20	2.44	2.45	2.46	2.47	2.49	2.50	2.51	2.52	2.53	2.55		
21	2.56	2.57	2.58	2.60	2.61	2.62	2.63	2.64	2.66	2.67		
22	2.68	2.69	2.71	2.72	2.73	2.74	2.75	2.77	2.78	2.79		
23	2.80	2.81	2.83	2.84 2.96	2.85 2.97	2.86 2.99	2.88 3.00	2.89 3.01	2.90 3.02	2.91 3.03		
24 25	$\frac{2.92}{3.05}$	2.94 3.06	$\frac{2.95}{3.07}$	3.08	3.10	3.11	3.12	3.13	3.14	3.16		
6.5	5.05	5.00	0.07	0.00	0.10	0.11	0.12	0.10	0.14	0.10		
26	3.17	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.27	3.28		
27	3.29	3.30	3.31	3.33	3.34	3.35	3.36	3.38	3.39	3.40		
28	3.41	3.42	3.44	3.45	3.46	3.47	3.49	3.50	3.51	3.52		
29	3.53	3.55	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64		
30	3.66	3.67	3.68	3.69	3.70	3.72	3.73	3.74	3.75	3.77		
21	2 170	2 70	2 60	2 21	3.83	3.84	2 25	2 86	3.88	3.89		
31 32	3.78 3.90	3.79 3.91	$\frac{3.80}{3.92}$	3.81 3.94	3.95	3.96	3.85 3.97	3.86 3.98	4.00	4.01		
33	4.02	4.03	4.05	4.06	4.07	4.08	4.09	4.11	4.12	4.13		
84	4.14	4.16	4.17	4.18	4.19	4.20	4.22	4.23	4.24	4.25		
35	4.26	4.28	4.29	4.30	4.31	4.33	4.34	4.35	4.36	4.37		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

		BAROMETER: 760 <sup>mm.</sup> (from 757.51 to 762.50).											
Centi- grade Degrees.					Tenths o	f Degrees.							
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim. 0.10	Millim. 0.11			
1	0.12	0.13	0.15	0.16	0.17	0.18	0.20	0.21	0.22	0.23			
2	0.25	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34	0.36			
3	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.47	0.48			
4	0.49	0.50	0.52	0.53	0.54	0.55	0.56	0.58	0.59	0.60			
5	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71	0.72			
6	0.74	0.75	0.76	0.77	0.79	0.80	0.81	0.82	0.83	0.85			
7	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.96	0.97			
8	0.98	0.99	1.01	1.02	1.03	1.04	1.05	1.07	1.08	1.09			
9	1.10	1.12	1.13	1.14	1.15	1.17	1.18	1.19	1.20	1.21			
10	1.23	1.24	1.25	1.26	1.28	1.29	1.30	1.31	1.32	1.34			
11	1.35	1.36	1.37	1.39	1.40	1.41	1.42	1.44	1.45	1.46			
12	1.47	1.48	1.50	1.51	1.52	1.53	1.55	1.56	1.57	1.58			
13	1.59	1.61	1.62	1.63	1.64	1.66	1.67	1.68	1.69	1.71			
14	1.72	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.83			
15	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95			
16	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07			
17	2.09	2.10	2.11	2.12	2.13	2.15	2.16	2.17	2.18	2.20			
18	2.21	2.22	2.23	2.24	2.26	2.27	2.28	2.29	2.31	2.32			
19	2.33	2.34	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44			
20	2.45	2.47	2.48	2.49	2.50	2.51	2.53	2.54	2.55	2.56			
21	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66	2.67	2.69			
22	2.70	2.71	2.72	2.74	2.75	2.76	2.77	2.78	2.80	2.81			
23	2.82	2.83	2.85	2.86	2.87	2.88	2.89	2.91	2.92	2.93			
24	2.94	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04	3.05			
25	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15	3.16	3.18			
26	3.19	3.20	3.21	3.23	3.24	3.25	3.26	3.28	3.29	3.30			
27	3.31	3.32	3.34	3.35	3.36	3.37	3.39	3.40	3.41	3.42			
28	3.43	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53	3.54			
29	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64	3.66	3.67			
30	3.68	3.69	3.70	3.72	3.73	3.74	3.75	3.77	3.78	3.79			
31	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91			
32	3.93	3.94	3.95	3.96	- 3.97	3.99	4.00	4.01	4.02	4.04			
33	4.05	4.06	4.07	4.08	4.10	4.11	4.12	4.13	4.15	4.16			
34	4.17	4.18	4.20	4.21	4.22	4.23	4.24	4.26	4.27	4.28			
35	4.29	4.31	4.32	4.33	4.34	4.35	4.37	4.38	4.39	4.40			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

	BAROMETER: 765 <sup>mm</sup> . (from 762.51 to 767.50).														
Centi- grade Degrees		٠			Tenths o	f Degrees.									
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.					
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.09	0.10	0.11					
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.23					
2	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.35	0.36					
3	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.46	0.47	0.48					
4	0.49	0.51	0.52	0.53	0.54	0.56	0.57	0.58	0.59	0.61					
5	0.62	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.73					
6	0.74	0.75	0.77	0.78	0.79	0.80	0.82	0.83	0.84	0.85					
7	0.86	0.88	0.89	0.90	0.91	0.93	0-94	0.95	0.96	0.98					
8	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.09	1.10					
9	1.11	1.12 1.14 1.15 1.16 1.17 1.19 1.20 1.21 1.22													
10	1.23														
11	1.36	1.37	1.38	1.40	1.41	1.42	1.43	1.44	1.46	1.47					
12	1.48	1.49	1.51	1.52	1.53	1.54	1.56	1.57	1.58	1.59					
13	1.61	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72					
14	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.83	1.84					
15	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96					
16	1.98	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.09					
17	2.10	2.11	2.12	2.14	2.15	2.16	2.17	2.19	2.20	2.21					
18	2.22	2.23	2.25	2.26	2.27	2.28	2.30	2.31	2.32	2.33					
19	2.35	2.36	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.46					
20	2.47	2.48	2.49	2.51	2.52	2.53	2.54	2.56	2.57	2.58					
21	2.59	2.61	2.62	2.63	2.64	2.65	2.67	2.68	2.69	2.70					
21 22	2.72	2.73	2.74	2.75	2.77	2.78	2.79	2.80	2.82	2.83					
23	2.84	2.85	2.86	2.88	2.89	2.90	2.91	2.93	2.94	2.95					
24	2.96	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.07					
25	3.09	3.10	3.11	3.12	3.14	3.15	3.16	3.17	3.19	3.20					
20	0.00	0.10													
26	3.21	3.22	3.23	3.25	3.26	3.27	3.28	3.30	3.31	3.32					
.27	3.33	3.35	3.36	3.37	3.38	3.40	3.41	3.42	3.43	3.44					
:28	3.46	3.47	3.48	3.49	3.51	3.52	3.53	3.54	3.56	3.57					
29	3.58	3.59	3.61	3.62	3.63	3.64	3.65	3.67	3.68	3.69					
.30	3.70	3.72	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.82					
31	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94					
32	3.95	3.96	3.98	3.99	4.00	4.01	4.03	4.04	4.05	4.06					
33	4.07	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.19					
34	4.20	4.21	4.22	4.24	4.25	4.26	4.27	4.28	4.30	4.31					
35	4.32	4.33	4.35	4.36	4.37	4.38	4.40	4.41	4.42	4.43					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					

	BAROMETER: 770 <sup>mm</sup> (from 767.51 to 772.50).														
Centi- grade Degrees.	Tenths of Degrees.  0. 1. 2. 3. 4. 5. 6. 7. 8. 9.														
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.					
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.09	0.10	0.11					
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.24					
2	0.25	0.26	0.27	0.29	0.30	0.31	0.32	0.34	0.35	0.36					
3	0.37	0.39	0.40	0.41	0.42	0.43	0.45	0.46	0.47	0.48					
4	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58	0.60	0.61					
5	0.62	0.63	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.73					
	0 ~~	0.70	0	0.50	0.00	0.07	0.00	0.60	0.07	0.00					
6	0.75	0.76	0.77	0.78	0.80	0.81	0.82	0.83	0.85	0.86					
7 8	0.87 $0.99$	0.88 1.01	$0.89 \\ 1.02$	0.91 1.03	0.92 1.04	0.93 1.06	0.94	0.96	0.97	0.98					
9	1.12	1.13	1.14	1.16	1.17	1.18	1.07 1.19	1.08	1.09 1.22	1.11 1.23					
10															
	1.21	1.24   1.26   1.27   1.28   1.29   1.30   1.32   1.33   1.34   1.35													
11	1.37	1.38	1.39	1.40	1.42	1.43	1.44	1.45	1.47	1.48					
12	1.49	1.50	1.52	1.53	1.54	1.55	1.57	1.58	1.59	1.60					
13	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72	1.73					
14	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85					
15	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98					
16	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10					
17	2.11	2.13	2.14	2.15	2.16	2.17	2.19	2.20	2.21	2.22					
18	2.24	2.25	2.26	2.27	2.29	2.30	2.31	2.32	2.34	2.35					
19	2.36	2.37	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47					
20	2.49	2.50	2.51	2.52	2.54	2.55	2.56	2.57	2.58	2.60					
21	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.70	2.71	2.72					
22	2.73	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.83	2.85					
23	2.86	2.87	2.88	2.90	2.91	2.92	2.93	2.95	2.96	2.97					
24	2.98	3.00	3.01	3.02	3.03	3.04	3.06	3.07	3.08	3.09					
25	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.19	3.21	3.22					
26	3.23	3.24	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34					
27	3.36	3.37	3.38	3.39	3.41	3.42	3.43	3.44	3.45	3.47					
28	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.57	3.58	3.59					
29	3.60	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.70	3.72					
30	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.82	3.83	3.84					
91	3.85	3.87	3.88	3.89	3.90	3.91	3.93	3.94	9.05	2.00					
31 32	3.98	3.99	4.00	4.01	4.03	4.04	4:05	4.06	3.95 4.08	3.96 4.09					
33	4.10	4.11	4.13	4.14	4.15	4.16	4.03	4.19	4.03	4.09					
34	4.23	4.24	4.25	4.26	4.28	4.29	4.30	4.31	4.32	4.34					
35	4.35	4.36	4.37	4.39	4.40	4.41	4.42	4.44	4.45	4.46					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					

		BAROMETER: 775 <sup>mrn.</sup> (from 772.51 to 777.50).												
Centigrade Degrees.		Tenths of Degrees.  0. 1. 2. 3. 4. 5. 6. 7. 8. 9.												
4	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim.				
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.11				
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.23	0.24				
2	0.25	0.26	0.28	0.29	0.30	0.31	0.33	0.34	0.35	0.36				
3	0.38	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.48	0.49				
4	0.50	0.51	0.53	0.54	0.55	0.56	0.58	0.59	0.60	0.61				
5	0.63	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.73	0.74				
6	0.75	0.76	0.78	0.79	0.80	0.81	0.83	0.84	0.85	0.86				
7	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.96	0.98	0.99				
8 9	1.00 1.13	3   1.14   1.15   1.16   1.18   1.19   1.20   1.21   1.23   1.24												
10	1.25	1.14	1.28	1.29	1.30	1.31	1.33	1.34	1.35	1.36				
	1.20	1.20	1120	1.20	1.00	1.01	1.00	1.01	1.00	1.00				
11	1.38	1.39	1.40	1.41	1.43	1.44	1.45	1.46	1.48	1.49				
12	1.50	1.51	1.53	1.54	1.55	1.56	1.58	1.59	1.60	1.61				
13	1.63	1.64	1.65	1.66	1.68	1.69	1.70	1.71	1.73	1.74				
14	1.75	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86				
15	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99				
	2.00	0.07	2.00	2.01	0.05	0.00	2.00	2.00	2.0					
16	2.00	2.01	2.03	$\frac{2.04}{2.16}$	$2.05 \\ 2.18$	2.06	2.08	2.09	2.10	2.11				
17	2.13 $2.25$	2.14 $2.26$	2.15 2.28	2.10	2.10	2.19 2.31	2.20 2.33	2.21 2.34	2.23 2.35	2.24 2.36				
19	2.38	2.39	2.40	2.41	2.43	2.44	2.45	2.46	2.48	2.49				
20	2.50	2.51	2.53	2.54	2.55	2.56	2.58	2.59	2.60	2.61				
21	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.73	2.74				
22	2.75	2.76	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86				
23	2.88	2.89	2.90	2.91	2.93	2.94	2.95	2.96	2.98	2.99				
24	3.00	3.01	3.03	3.04	3.05	3.06	3.08	3.09	3.10	3.11				
25	3.13	3.14	3.15	3.16	3.18	3.19	3.20	3.21	3.23	3.24				
26	3.25	3.26	3.28	3.29	3.30	3.31	3.33	3.34	3.35	3.36				
27	3.38	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.48	3.49				
28	3.50	3.51	3.53	3.54	3.55	3.56	3.58	3.59	3.60	3.61				
29	3.63	3.64	3.65	3.66	3.68	3.69	3.70	3.72	3.73	3.74				
30	3.75	3.77	3.78	3.79	3.80	3.82	3.83	3.84	3.85	3.87				
31	3.88	3.89	3.90	3.92	3.93	3.94	3.95	3.97	3.98	3.99				
32	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09	4.10	4.12				
33	4.13	4.14	4.15	4.17	4.18	4.19	4.20	4.22	4.23	4.24				
34 35	4.25 4.38	4.27	4.2S 4.40	4.29 4.42	4.30 4.43	4.32 4.44	4.33 4.45	4.34	4.35 4.48	4.37				
			7.40				7.40							
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

		BAROMETER: 780 <sup>mm.</sup> (from 777.51 to 782.50).													
Centigrade Degrees.			*		Tenths o	f Degrees.									
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
0	Millim.	Millim.	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim. 0.10	Millim.					
	0.00	0.01	0.03	0.04	0.03	0.00	0.03	0.03	0.10	0.11					
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.23	0.24					
2	0.25	0.26	0.28	0.29	0.30	0.31	0.33	0.34	0.35	0.37					
3	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.47	0.48	0.49					
4	0.50	0.52	0.53	0.54	0.55	0.57	0.58	0.59	0.60	0.62					
5	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.73	0.74					
6	0.76	0.77	0.78	0.79	0.81	0.82	0.83	0.84	0.86	0.87					
7	0.76	0.77	0.73	0.79	0.93	0.84	0.96	0.97	0.98	0.99					
8	1.01	1.02	1.03	1.04	1.06	1.07	1.08	1.10	1.11	1.12					
9	1.13	1.15	1.16	1.17	1.18	1.20	1.21	1.22	1.23	1.25					
10	1.26	1.27	1.16												
11	1.38	1.40	1.41	1.42	1.44	1.45	1.46	1.47	1.49	1.50					
12	1.51	1.52	1.54	1.55	1.56	1.57	1.59	1.60	1.61	1.62					
13	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75					
14	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86	1.88					
15	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00					
16	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.13					
17	2.14	2.05	2.17	2.03	2.19	2.20	2.09	2.10	2.11	2.15					
18	2.27	2.28	2.29	2.30	2.13	2.33	2.34	2.35	2.37	2.23					
19	2.39	2.40	2.42	2.43	2.44	2.45	2.47	2.48	2.49	2.51					
20	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.61	2.62	2.63					
21	2.64	2.66	2.67	2.68	2.69	2.71	2.72	2.73	2.74	2.76					
22	2.77	2.78	2.79	2.81	2.82	2.83	2.85	2.86	2.87	2.88					
23	2.90	2.91	2.92	2.93	2.95	2.96	2.97	2.98	3.00	3.01					
24	3.02	3.03	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.14					
25	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.24	3.25	3.26					
90	3.27	3.29	9 90	3.31	9 90	224	3.35	9.96	3.37	2 20					
26 27	3.40	3.29	3.30	3.44	3.32 3.45	3.34 3.46	3.47	3.36 3.49	3.50	3.39 3.51					
28	3.52	3.54	3.55	3.56	3.58	3.59	3.60	3.49	3.63	3.64					
29	3.65	3.66	3.68	3.69	3.70	3.71	3.73	3.74	3.75	3.76					
30	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89					
31	3.90	3.92	3.93	3.94	3.95	3.97	3.98	3.99	4.00	4.02					
32	4.03	4.04	4.05	4.07	4.08	4.09	4.10	4.12	4.13	4.14					
33	4.15	4.17	4.18	4.19	4.20	4.22	4.23	4.24	4.26	4.27					
34	4.28	4.29	4.31	4.32	4.33	4.34	4.36	4.37	4.38	4.39					
35	4.41	4.42	4.43	4.44	4.46	4.47	4.48	4.49	4.51	4.52					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					

		BAROMETER: 785 <sup>mm.</sup> (from 782.51 to 787.50).												
Centi- grade Degrees.					Tenths o	f Degrees.								
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim. 0.08	Millim.	Millim.	Millim.				
	0.00	0.02	0100											
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.22	0.23	0.24				
2	0.25	0.27	0.28	0.29	0.30	0.32	0.33	0.34	0.35	0.37				
3	0.38	0.39	0.41	0.42	0.43	0.44	0.46	0.47	0.48	0.49				
4	0.51	0.52	0.53	0.54	0.56	0.57	0.58	0.60	0.61	0.62				
5	0.63	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.73	0.75				
6	0.76	0.77	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87				
6 7	0.76	0.90	0.79	0.92	0.94	0.82	0.96	0.98	0.99	1.00				
8	1.01	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.11	1.13				
9	1.14	1.15	1.17	1.18	1.19	1.20	1.22	1.23	1.24	1.25				
10	1.27	1.28	1.29	1.30	1.32	1.33	1.34	1.36	1.37	1.38				
										ļ				
11	1.39	.39   1.41   1.42   1.43   1.44   1.46   1.47   1.48   1.50   1.51												
12	1.52	1.53	1.55	1.56	1.57	1.58	1.60	1.61	1.62	1.63				
13	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75	1.76				
14	1.77	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.88	1.89				
15	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01				
						0.00	0.10	0.10	0.10	0.74				
16	2.03	2.04	2.05	2.07	2.08	2.09	2.10 $2.23$	2.12 $2.24$	2.13 2.26	2.14 2.27				
17	2.15	2.17	2.18	2.19	2.20	2.22 2.34	2.36	2.24	2.38	2.39				
18	2.28	2.29	2.31 2.43	2.32 $2.45$	2.46	2.47	2.48	2.50	2.51	2.52				
19	2.41	2.42	2.43	2.45	2.58	2.60	2.61	2.62	2.64	2.65				
20	4.95	2.00	2.90	2.51	2.00	2.00	2.01	2.02	2.01	2.00				
21	2.66	2.67	2.69	2.70	2.71	2.72	2.74	2.75	2.76	2.77				
22	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.88	2.89	2.90				
23	2.91	2.93	2.94	2.95	2.96	2.98	2.99	3.00	3.02	3.03				
24	3.04	3.05	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15				
25	3.17	3.18	3.19	3.21	3.22	3.23	3.24	3.26	3.27	3.28				
26	3.29	3.31	3.32	3.33	3.34	3.36	3.37	3.38	3.40	3.41				
27	3.42	3.43	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53				
28	3.55	3.56	3.57	3.59	3.60	3.61	3.62	3.64	3.65	3.66				
29	3.67	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.78	3.79				
30	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91				
31	3.93	3.94	3.95	3.97	3.98	3.99	4.00	4.02	4.03	4.04				
32	4.05	4.07	4.08	4.09	4.11	4.12	4.13	4.14	4.16	4.17				
33	4.18	4.19	4.21	4.22	4.23	4.24	4.26	4.27	4.28	4.30				
34	4.31	4.32	4.33	4.35	4.36	4.37	4.38	4.40	4.41	4.42				
35	4.43	4.45	4.46	4.47	4.49	4.50	4.51	4.52	4.54	4.55				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

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		BAROMETER: 790 <sup>mm.</sup> (from 787.51 to 792.50).											
Centi- grade Degrees.					Tenths o	f Degrees.							
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
0	Millim. 0.00	Millim. 0.01	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10	Millim. 0.11			
1	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.22	0.23	0.24			
2	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34	0.36	0.37			
3	0.38	0.40	0.41	0.42	0.43	0.45	0.46	0.47	0.48	0.50			
4	0.51	0.52	0.54	0.55	0.56	0.57	0.59	0.60	0.61	0.62			
5	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.73	0.74	0.75			
6	0.77	0.78	0.79	0.80	0.82	0.83	0.84	0.85	0.87	0.88			
7	0.89	0.91	0.92	0.93	0.94	0.96	0.97	0.98	0.99	1.01			
8	1.02	1.03	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.13			
9	1.15	1.16	1.17	1.19	1.20	1.21	1.22	1.24	1.25	1.26			
10	1.28	1.29	1.30	1.31	1.33	1.34	1.35	1.36	1.38	1.39			
11	1.40	1.42	1.43	1.44	1.45	1.47	1.48	1.49	1.50	1.52			
12	1.53	1.54	1.56	1.57	1.58	1.59	1.61	1.62	1.63	1.64			
13	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.75	1.76	1.77			
14	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.87	1.89	1.90			
15	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03			
16	2.04	2.05	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.15			
17	2.17	2.18	2.19	2.21	2.22	2.23	2.24	2.26	2.27	2.28			
18	2.30	2.31	2.32	2.33	2.35	2.36	2.37	2.38	2.40	2.41			
19	2.42	2.44	2.45	2.46	2.47	2.49	2.50	2.51	2.52	2.54			
20	2.55	2.56	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66			
21	2.68	2.69	2.70	2.72	2.73	2.74	2.75	2.77	2.78	2.79			
22	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89	2.91	2.92			
23	2.93	2.95	2.96	2.97	2.98	3.00	3.01	3.02	3.03	3.05			
24	3.06	3.07	3.09	3.10	3.11	3.12	3.14	3.15	3.16	3.17			
25	3.19	3.20	3.21	3.23	3.24	3.25	3.26	3.28	3.29	3.30			
26	3.32	3.33	3.34	3.35	3.37	3.38	3.39	3.40	3.42	3.43			
27	3.44	3.46	3.47	3.48	3.49	3.51	3.52	3.53	3.54	3.56			
28	3.57	3.58	3.60	3.61	3.62	3.63	3.65	3.66	3.67	3.68			
29	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.79	3.80	3.81			
30	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94			
31	3.95	3.97	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.07			
32	4.08	4.09	4.11	4.12	4.13	4.14	4.16	4.17	4.18	4.19			
33	4.21	4.22	4.23	4.25	4.26	4.27	4.28	4.30	4.31	4.32			
34	4.34	4.35	4.36	4.37	4.39	4.40	4.41	4.42	4.44	4.45			
35	4.46	4.48	4.49	4.50	4.51	4.53	4.54	4.55	4.56	4.58			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

		BAROMETER: 795 <sup>mm.</sup> (from 792.51 to 797.50).  Tenths of Degrees.												
Centigrade Degrees.					Tenths o	f Degrees.								
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim.	Mıllim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.				
0	0.00	0.01	0.05	0.04	0.05	0.00	0.03	0.09	0.10	0.12				
1	0.13	0.14	0.15	0.17	0.18	0.19	0.21	0.22	0.23	0.24				
2	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.35	0.36	0.37				
3	0.38	0.40	0.41	0.42	0.44	0.45	0.46	0.47	0.49	0.50				
4	0.51	0.53	0.54	0.55	0.56	0.58	0.59	0.60	0.62	0.63				
5	0.64	0.65	0.67	0.68	0.69	0.71	0.72	0.73	0.74	0.76				
6	0.77	0.78	0.80	0.81	0.82	0.83	0.85	0.86	0.87	0.89				
7	0.90	0.91	0.92	0.94	0.95	0.96	0.98	0.99	1.00	1.01				
8	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.12	1.13	1.14				
9	1.15	1.17	1.18	1.19	1.21	1.22	1.23	1.24	1.26	1.27				
10	1.28													
11	1.41	1.42	1.44	1.45	1.46	1.48	1.49	1.50	1.51	1.53				
12	1.54	1.55	1.57	1.58	1.59	1.60	1.62	1.63	1.64	1.66				
13	1.67	1.68	1.69	1.71	1.72	1.73	1.75	1.76	1.77	1.78				
14	1.80	1.81	1.82	1.83	1.85	1.86	1.87	1.89	1.90	1.91				
15	1.92	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03	2.04				
16	2.05	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.16	2.17				
17	2.18	2.19	2.21	2.22	2.23	2.25	2.26	2.27	2.28	2.30				
18	2.31	2.32	2.34	2.35	2.36	2.37	2.39	2.40	2.41	2.43				
19	2.44	2.45	2.46	2.48	2.49	2.50	2.51	2.53	2.54	2.55				
20	2.57	2.58	2.59	2.60	2.62	2.63	2.64	2.66	2.67	2.68				
21	2.69	2.71	2.72	2.73	2.75	2.76	2.77	2.78	2.80	2.81				
22	2.82	2.84	2.85	2.86	2.87	2.89	2.90	2.91	2.93	2.94				
23	2.95	2.96	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.07				
24	3.08	3.09	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.19				
25	3.21	3.22	3.23	3.25	3.26	3.27	3.28	3.30	3.31	3.32				
26	3.34	3.35	3.36	3.37	3.39	3.40	3.41	3.43	3.44	3.45				
27	3.46	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.57	3.58				
28	3.59	3.61	3.62	3.63	3.64	3.66	3.67	3.68	3.70	3.71				
29	3.72	3.73	3.75	3.76	3.77	3.79	3.80	3.81	3.82	3.84				
30	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94	3.95	3.96				
31	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09				
32	4.11	4.12	4.13	4.14	4.16	4.17	4.18	4.20	4.21	4.22				
33	4.23	4.25	4.26	4.27	4.29	4.30	4.31	4.32	4.34	4.35				
34	4.36	4.38	4.39	4.40	4.41	4.43	4.44	4.45	4.47	4.48				
35	4.49	4.50	4.52	4.53	4.54	4.56	4.57	4.58	4.59	4.61				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

		BAROMETER: 800 <sup>mm.</sup> (from 797.51 to 802.50).												
Centi- grade Degrees.					Tenths o	f Degrees.								
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim. 0.00	Millim. 0.01	Millim, 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10	Millim. 0.12				
1	0.13	0.14	0.15	0.17	0.18	0.19	0.21	0.22	0.23	0.25				
2	0.26	0.27	0.28	0.30	0.31	0.32	0.34	0.35	0.36	0.37				
3	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.48	0.49	0.50				
4	0.52	0.53	0.54	0.56	0.57	0.58	0.59	0.61	0.62	0.63				
5	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.74	0.75	0.76				
6	0.77	0.79	0.80	0.81	0.83	0.84	0.85	0.87	0.88	0.89				
7	0.90	0.92	0.93	0.94	0.96	0.97	0.98	0.99	1.01	1.02				
8	1.03	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.14	1.15				
9	1.16	1.17	1.19	1.20	1.21	1.23	1.24	1.25	1.27	1.28				
10	1.29	1.30												
11	1.42	1.43	1.45	1.46	1.47	1.48	1.50	1.51	1.52	1.54				
12	1.55	1.56	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.67				
13	1.68	1.69	1.70	1.72	1.73	1.74	1.76	1.77	1.78	1.79				
14	1.81	1.82	1.83	1.85	1.86	1.87	1.89	1.90	1.91	1.92				
15	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03	2.04	2.05				
16	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.16	2.17	2.18				
17	2.20	2.21	2.22	2.23	2.25	2.26	2.27	2.29	2.30	2.31				
18	2.32	2.34	2.35	2.36	2.38	2.39	2.40	2.41	2.43	2.44				
19	2.45	2.47	2.48	2.49	2.50	2.52	2.53	2.54	2.56	2.57				
20	2.58	2.60	2.61	2.62	2.63	2.65	2.66	2.67	2.69	2.70				
21	2.71	2.72	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.83				
22	2.84	2.85	2.87	2.88	2.89	2.91	2.92	2.93	2.94	2.96				
23	2.97	2.98	3.00	3.01	3.02	• 3.03	3.05	3.06	3.07	3.09				
24	3.10	3.11	3.12	3.14	3.15	3.16	3.18	3.19	3.20	3.22				
25	3.23	3.24	3.25	3.27	3.28	3.29	3.31	3.32	3.33	3.34				
26	3.36	3.37	3.38	3.40	3.41	3.42	3.43	3.45	3.46	3.47				
27	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.58	3.59	3.60				
28	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.71	3.72	3.73				
29	3.74	3.76	3.77	3.78	3.80	3.81	3.82	3.83	3.85	3.86				
30	3.87	3.89	3.90	3.91	3.93	3.94	3.95	3.96	3.98	3.99				
31	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09	4.11	4.12				
32	4.13	4.14	4.16	4.17	4.18	4.20	4.21	4.22	4.24	4.25				
33	4.26	4.27	4.29	4.30	4.31	4.33	4.34	4.35	4.36	4.38				
34	4.39	4.40	4.42	4.43	4.44	4.45	4.47	4.48	4.49	4.51				
35	4.52	4.53	4.55	4.56	4.57	4.58	4.60	4.61	4.62	4.64				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				



### XXI.

### OLD FRENCH BAROMETER.

### TABLE

FOR

# REDUCING TO THE FREEZING POINT THE OBSERVATIONS TAKEN WITH OLD FRENCH BAROMETERS,

PROVIDED WITH BRASS SCALES, EXTENDING FROM THE CISTERN TO THE

TOP OF THE MERCURIAL COLUMN; CALCULATED FROM 240 TO 345

LINES, OR FROM 23 INCHES 4 LINES TO 28 INCHES 9 LINES.

By Kaemtz.

### TABLE XXI.

This table is taken from Kaemtz's Lehrbuch der Meteorologie, Vol. II. p. 236. To render it more useful, the first page, giving the corrections for Barometrical Heights between 240 and 280 Paris lines, has been added.

The values adopted by Kaemtz for reducing the Old French Barometer are the following: —

Let h =observed height in French lines.

- " t = temperature of attached thermometer in degrees of Reaumur.
- "  $m = \text{expansion of mercury between 0 and } 80^{\circ} \text{ Reaumur} = 0.018018.$
- "  $l = \text{linear expansion of brass between 0 and 80}^{\circ}$  Reaumur = 0.0018782.

The normal temperature of standard being  $= 13^{\circ}$  Reaumur.

And the formula becomes, -

$$-h \cdot \frac{m \times t - l \cdot (t - 13)}{1 + m \times t}$$

The Table gives the corrections only for full degrees and for every fifth line; but the intermediate values can easily be found by an interpolation at sight.

### Example of Reduction.

Observed height	•		•	•		•	=	325.32 lines.	
Attached thermome	eter					•	=	12.5 Reaumui	r.
In the line beginning wi	th 12	°, and	l in th	e ver	tical	colum	n he	aded 325 lines	,
we find,	Cori	ection	n for	12°	=	=0.	89 li	nes.	
	Inte	rpolat	ion fo	or 0°.	.5 =	<del></del> 0.	03	66	
	Cor	rection	n for	12°	- 5 -		92	66	
	001	i COLIO	101	1~ .		0.	U~3		

And we have,

Observed height, 325.32 "Correction for 12°.5, —0.92 "

Height at the freezing point = 324.40 lines.

Normal Temperature of the Scale = 13° Reaumur.

Attached Thermom- eter.			F	Sarometer in	n Paris Line	s.			Attached Thermometer.
Degrees of Reaumur.	240	245	250	255	260	265	270	275	Degrees of Reaumur.
-15	Par. Lines. +0.65	Par Lines. +0.66	Par. Lines. +0.68	Par. Lines. +0.69	Par. Lines. +0.70	Par Lines	Par. Lines. +0.73	Par. Lines. +0.75	° -15
-14	0.60	0.61	0.63	0.64	0.65	0.67	0.68	0.69	-13
-13	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.64	-13
-12	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	-13
-11	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.52	-11
-10	0.41	0.42	0.43	0.44	0.44	0.45	0.46	0.47	-10
- 9	+0.36	+0.37	+0.38	+0.38	+0.39	+0.40	+0.41	+0.41	- 9
- 8	0.31	0.32	0.33	0.33	0.34	0.35	0.35	0.36	- 8
- 7	0.27	0.27	0.28	0.28	0.29	0.29	0.30	0.30	- 7
- 6	0.22	0.22	0.23	0.23	0.24	0.24	0.24	0.25	- 6
- 5	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	- 5
- 4	+0.12	+0.12	+0.13	+0.13	+0.13	+0.13	+0.14	+0.14	- 4
- 3	0.07	0.07	0.08	0.08	0.08	0.08	0.08	0.08	- 3
- 2	+0.02	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	- 2
- 1	-0.02	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1
0	-0.07	-0.07	-0.08	-0.03	-0.08	-0.08	-0.08	-0.08	0
+ 1	-0.12	-0.12	-0.13	-0.13	-0.13	-0.13	-0.14	-0.14	+ 1
2	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	2
3	0.22	0.22	0.23	0.23	0.24	0.24	0.24	0.25	3
4	0.27	0.27	0.28	0.28	0.29	0.29	0.30	0.30	4
5	0.31	0.32	0.33	0.33	0.34	0.35	0.35	0.36	5
+ 6	-0.36	-0.37	-0.38	-0.38	-0.39	-0.40	-0.41	-0.41	+ 6
7	0.41	0.42	0.43	0.44	0.44	0.45	0.46	0.47	7
8	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.52	8
9	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	9
10	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.64	10
+11	-0.60	-0.61	-0.63	-0.64	-0.65	-0.67	-0.68	-0.69	+11
12	0.65	0.66	0.68	0.69	0.70	0.72	0.73	0.75	12
13	0.70	0.71	0.73	0.74	0.76	0.77	0.79	0.80	13
14	0.75	0.76	0.78	0.79	0.81	0.82	0.84	0.86	14
15	0.80	0.81	0.83	0.84	0.86	0.88	0.89	0.91	15
+16	-0.84	-0.86	-0.88	-0.90	-0.91	-0.93	-0.95	-0.97	+16
17	0.89	0.91	0.93	0.95	0.97	0.98	1.00	1.02	17
18	0.94	0.96	0.98	1.00	1.02	1.04	1.06	1.08	18
19 20	0.99 1.04	1.01 1.06	1.03 1.08	1.05 1.10	1.07 1.12	1.09 1.14	1.11 1.17	1.13 1.19	19 20
+21	-1.08	-1.11	-1.13	-1.15	-1.17	-1.20	-1.22	-1.24	+21
22	1.13	1.16	1.18	1.20	1.23	1.25	1.27	1.30	22
23	1.18	1.20	1.23	1.25	1.28	1.30	1.33	1.35	23
24	1.23	1.25	1.28	1.31	1.33	1.36	1.38	1.41	$\begin{array}{c} 24 \\ 25 \end{array}$
25	1.28	1.30	1.33	1.36	1.38	1.41	1.44	1.46	40

Normal Temperature of the Scale  $\Longrightarrow$  13° Reaumur.

Attached Thermom- eter.		Barometer in Paris Lines.											
Degrees of Reaumur.	280	285	290	295	300	305	310	Degrees of Reaumur.					
0	Par. Lines.	Par. Lines.	Par. Lines.		Par. Lines.	Par. Lines.	Par. Lines.	0					
-15	+0.77	+0.78	+0.79	+0.81	+0.82	+0.84	+0.85	-15					
-14	0.71	0.73	0.74	0.75	0.76	0.77	0.79	-14					
-13	0.65	0.67	0.68	0.69	0.70	0.71	0.72	-13					
-12	0.60	0.61	0.62 0.56	0.63	0.64	0.65	0.66 0.60	-12 -11					
-11	0.54	0.55	0.50	0.57	$0.58 \\ 0.52$	0.59	0.54	-11 -10					
-10	0.48	0.49	0.50	0.51	0.32	0.53	0.94	-10					
- 9	+0.43	+0.44	+0.44	+0.45	+0.46	+0.46	+0.47	- 9					
-8	0.37	0.38	0.38	0.39	0.40	0.40	0.41	-8					
- 7	0.31	0.32	0.32	0.33	0.34	0.34	0.35	- 7					
- 6	0.26	0.26	0.26	0.27	0.27	0.28	0.28	- 6					
- 5	0.20	0.20	0.21	0.21	0.21	0.22	0.22	- 5					
	0.20	0.20	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.21	0.21	0.22	0.22						
- 4	+0.14	+0.15	+0.15	+0.15	+0.15	+0.16	+0.16	- 4					
- 3	0.09	0.09	0.09	0.09	0.09	0.09	0.09	- 3					
- 2	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	- 2					
- 1	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1					
0	-0.08	-0.09	-0.09	-0.09	-0.09	-0.09	-0.09	0					
+ 1	-0.14	-0.14	-0.15	-0.15	-0.15	-0.15	-0.16	+ 1					
2	0.20	0.20	0.21	0.21	0.21	0.22	0.22	2					
3	0.26	0.26	0.27	0.27	0.27	0.28	0.28	3					
4	0.31	0.32	0.32	0.33	0.33	0.34	0.35	4					
5	0.37	0.37	0.38	0.39	0.40	0.40	0.41	5					
+ 6	-0.43	-0.43	-0.44	-0.45	-0.46	-0.46	-0.47	+ 6					
7	0.48	0.49	0.50	0.51	0.52	0.53	0.53	7					
8	0.54	0.55	0.56	0.57	0.58	0.59	0.60	8					
9	0.60	0.61	0.62	0.63	0.64	0.65	0.66	9					
10	0.65	0.66	0.68	0.69	0.70	0.71	0.72	10					
+11	-0.71	-0.72	-0.74	-0.75	_0.76	-0.77	-0.79	+11					
12	0.77	0.78	0.80	0.81	0.82	0.84	0.85	12					
13	0.82	0.84	0.85	0.87	0.88	0.90	0.91	13					
14	0.88	0.90	0.91	0.93	0.94	0.96	0.98	14					
15	0.94	0.95	0.97	0.99	1.00	1.02	1.04	15					
1 1													
+16	-0.99	-1.01	-1.03	-1.05	-1.07	-1.08	-1.10	+16					
17	1.05	1.07	1.09	1.11	1.13	1.15	1.16	17					
18	1.11	1.13	1.15	1.17	1.19	1.21	1.23	18					
19	1.16	1.18	1.21	1.23	1.25	1.27	1.29	19					
20	1.22	1.24	1.27	1.29	1.31	1.33	1.35	20					
+21	-1.28	-1.30	-1.33	-1.35	-1.37	-1.39	-1.42	+21					
22	1.34	1.36	1.38	1.41	1.43	1.45	1.48	22					
23	1.39	1.41	1.44	1.47	1.49	1.52	1.54	23					
24	1.45	1.47	1.50	1.53	1.55	1.58	1.60	24					
25	1.50	1.53	1.56	1.59	1.61	1.64	1.67	25					

Normal Temperature of the Scale = 13° Reaumur.

Attached	Barometer in Paris Lines,										
Thermom- eter.		1	Baron	eter in Paris	Lines.	1		Attached Thermometer.			
Degrees of Reaumur.	315	320	325	330	335	340	345	Degrees of Reaumur			
° -15	Par. Lines. +0.86	Par. Lines. +0.88	Par. Lines. +0.89	Par. Lines.	Par. Lines. +0.92	Par. Lines. +0.93	Par. Lines. +0.95	° -15			
-14	0.80	0.81	0.83	0.84	0.85	0.86	0.88	-14			
-13	0.74	0.75	0.76	0.78	0.78	0.79	0.81	-13			
-12	0.67	0.68	0.69	0.70	0.71	0.73	0.74	-12			
-11	0.61	0.62	0.63	0.64	0.65	0.66	0.67	-11			
-10	0.54	0.55	0.56	0.57	0.58	0.59	0.60	-10			
- 9	+0.48	+0.49	+0.50	+0.50	+0.51	+0.52	+0.53	- 9			
- 8	0.42	0.42	0.43	0.44	0.44	0.45	0.46	- 8			
- 7	0.35	0.36	0.36	0.37	0.37	0.38	0.39	- 7			
- 6	0.29	0.29	0.30	0.30	0.31	0.31	0.32	- 6			
- 5	0.22	0.23	0.23	0.24	0.24	0.24	0.25	- 5			
- 4	+0.16	+0.16	+0.17	+0.17	+0.17	+0.17	+0.18	- 4			
- 3	0.10	0.10	0.10	0.10	0.10	0.10	0.11	- 3			
- 2	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.04	- 2			
- 1	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1			
0	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10	0			
+ 1	-0.16	-0.16	-0.16	-0.17	-0.17	-0.17	-0.17	+ 1			
2	0.22	0.23	0.23	0.23	0.24	0.24	0.24	2			
3	0.29	0.29	0.30	0.30	0.31	0.31	0.31	3			
4	0.35	0.36	0.36	0.37	0.37	0.38	0.38	4			
5	0.42	0.42	0.43	0.44	0.44	0.45	0.45	5			
+ 6	-0.48	-0.49	-0.49	-0.50	-0.51	-0.52	-0.53	+ 6			
7	0.54	0.55	0.56	0.57	0.58	0.59	0.60	7			
8	0.61	0.62	0.63	0.64	0.65	0.66	0.67	8			
9	0.67	0.68	0.69	0.70	0.71	0.72	0.74	9			
10	0.74	0.75	0.76	0.77	0.78	0.79	0.81	10			
+11	-0.80	-0.81	-0.82	-0.84	-0.85	-0.86	-0.88	+11			
12	0.86	0.88	0.89	0.90	0.92	0.93	0.95	12			
13	0.93	0.94	0.96	0.97	0.99	1.00	1.02	13			
14 15	0.99	1.01	1.02 1.09	1.04	1.05	1.07	1.09	14 15			
15	1.05	1.07	1.05	1.10	1.12	1.14	1.16	19			
+16	-1.12	-1.14	-1.15	-1.17	-1.19	-1.21	-1.23	+16			
17	1.18	1.20	1.22	1.24	1.26	1.28	1.30	17			
18	1.25	1.27	1.29	1.31	1.33	1.35	1.37	18			
19	1.31	1.33	1.35	1.37	1.39	1.41	1.44	19			
20	1.37	1.40	1.42	1.44	1.46	1.48	1.51	20			
+21	-1.44	-1.46	-1.48	-1.51	-1.53	-1.55	-1.58	+21			
22	1.50	1.53	1.55	1.57	1.60	1.62	1.65	22			
23	1.57	1.59	1.62	1.64	1.67	1.69	1.72	23			
24	1.63	1.66	1.68	1.71	1.73	1.76	1.79	24			
25	1.69	1.72	1.75	1.78	1.80	1.83	1.86	25			



### TABLES

FOR CORRECTING THE

DEPRESSION OF THE BAROMETRICAL COLUMN

DUE TO CAPILLARY ACTION.

#### CORRECTION FOR CAPILLARY ACTION.

It is known that the effects of capillary action are not the same in different liquids. In a tube plunged in water, the liquid in the tube rises higher than the level of the water in the vessel, and terminates by a concave surface, which is called a concave meniscus. In a tube plunged in mercury the liquid in the tube stands lower than the mercury in the vessel, and terminates by a convex surface, or a convex meniscus. It is thus evident that the mercurial column in the tube of a Barometer does not rise to its true height, and that it needs to be corrected for the depression due to capillarity, before it indicates the real pressure of the atmosphere.

La Place, in the *Mécanique Céleste*, Tom. IV., has shown that the value of that correction depends upon the form of the meniscus, and gave a formula to compute it. As this form varies in tubes of different bores, so does the depression, which diminishes as the diameter of the tube increases. The form of the meniscus, however, was supposed to be the same in tubes of the same diameter, and constant in the same tube; and on this supposition the tables generally used for correcting the capillary action have been computed. But more accurate observations have proved that, owing to various causes not yet all well understood, the form of the meniscus is often different in tubes of the same diameter, and that it is even variable in the tube of the same instrument.

It thus became necessary to construct new tables, taking into consideration, in a given case, both the diameter of the tube and the form of the meniscus. Such tables, with a double entry, have been given by Schleiermacher, in the Bibliothèque Universelle de Genève, Tom. VIII.; by Bravais, in the Anuales de Physique et de Chimie, Tom. V. p. 508; and by Delcros. The numbers in these tables agree very closely; but as Delcros's table is more extended than that of Schleiermacher, and in a more convenient form than that of Bravais, it is given below, together with a reduction of it to English measures, for the ordinary use.

The other tables may serve for comparison.

Table XXII., from the Report of the Committee of Physics and Meteorology of the Royal Society of London, 1840, gives the correction to be applied to English barometers for capillary action in boiled and unboiled tubes. It takes into account the diameter of the tube, but not the variations of the height of the meniscus, or of the convexity which terminates the barometrical column. This last element is supposed to be in its normal state, and constant.

Tables XXIII. and XXIV., by Delcros, in the Annuaire Météorologique de France, for 1849, give the means of finding the true correction to be applied to metrical barometers for capillary action.

The first shows the normal height of the meniscus when in contact with the air (as is the case in the inferior branch of a siphon barometer), and in the barometric vacuum at the top of the column, in tubes of different bores. It enables the observer to judge better of its variations.

Table XXIV. has been calculated by Delcros after the formulas of Schleiermacher, making the constant x equal to  $6^{\text{mm}}.5278$ , being the mean value between that of Gay-Lussac =  $6^{\text{mm}}.5262$ , and that of Schleiermacher =  $6^{\text{mm}}.5295$ . It gives the amount of the capillary action in millimetres of mercury, taking into account both the size of the bore, or the internal radius of the tube, which will be found in the vertical argument, and the height of the meniscus, given in the horizontal argument. The internal radius of the tube is supposed to be known; the height of the meniscus, or the vertical distance from the base, that is, from the sharp line where the mercury ceases to be in contact with the walls of the tube, to the very top of the convexity, can be ascertained by measuring it several times by means of the vernier.

Example: — Suppose the internal radius of the tube to be  $3^{mm}.2$ , and the height of the meniscus to be  $0^{mm}.8$ ; seek in the first vertical column the number  $3^{mm}.2$ ; follow then the horizontal line as far as the vertical column headed  $0^{mm}.8$ , you find there the number  $0^{mm}.776$ , which is the amount of the depression due to capillary action, or the value of the correction to be added to the observation.

Table XXV. is taken from Pouillet's Eléments de Physique, Vol. II. p. 698 (1853). Table XXVI. is found in Gehler's Physicalisches Wörterbuch, and in Schubarth, Physicalische Tabellen, p. 21.

Table XXVII., which is Delcros's table reduced into English measures, gives the means of correcting with more accuracy the indications of the English barometers. For its use, see, above, the explanation to Table XXIV.

Table XXVIII. is from Baily's Astronomical Tables.

XXII. TABLE FOR THE CORRECTION TO BE ADDED TO ENGLISH BAROMETERS FOR CAPILLARY ACTION.

Diameter	Correct	tion for
of Tube.	Unboiled Tubes.	Boiled Tubes.
Inch.	Inch.	Inch.
0.60	0.004	0.002
0.50	0.007	0.003
0.45	0.010	0.005
0.40	0.014	0.007
0.35	0.020	0.010
0.30	0.028	0.014
0.25	0.040	0.020
0.20	0.060	0.029
0.15	0.088	0.044
0.10	0.142	0.070

XXIII. TABLE OF THE HEIGHT OF THE MENISCUS OF THE BAROMETRICAL COLUMN.

Internal Radius of the Tube in	Normal Heig niscus in I	ht of the Me- Iillimetres.
Millimetres.	In the Air.	In the Vacuum.
1 2	0.427 0.795	0.34
3	1.079	0.86
5	1.413 1.488	1.13
7	1.524	1.13
<u> </u>		

Vertical Argument = Internal Radius of Tube. Horizontal Argument = Height of Menisous in Millimetres.

Jo.	e		_	_	-		_	=	_			_						=	=	_		==	_	_	_	=		-	_				
Radius of	the Tube in Milli- metres.	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2, 2, 2, 2, 2, 3		9 6	7	* 9°	3.8		4.0	2.4	4.	4.0	4. 8.	5.0	5.5	5.4	5.6	5.8	ų ų	2 0	7.0	4.0	0.8	1	7.0
	1.8	Millim.	33	39	3	3	3	3	3 3	: 3	3	33	33	3	"	*	: 3	: :	: 3	: 3	\$	2	0.418	0.376	0.338	0.304	0.079	900	0.62.0	0.221	0.180		0.163
	1.7	Millim.	39	39	3	3	3	3	3 3	: 3	3	3	33	ä	0.887	i	0.790	007.0	0.630	0.003	0.504	0.452	0.405	0.364	0.327	0.294	0.964	0000	0.200	0.214	0.174		0.158
	1.6	Millim.	3	3	3	3	3	3	3 3	: 3	z	1.238	1 005	0.970	0.861	1	0.700	0.002	0.609	0.044 0.044	0.486	0.436	0.390	0.350	0.315	0.283	0.954	+62	0.223	0.200	0.168		0.152
	1.5	Millim.	3	3	3	3	2	3	3 3	: 3	388	1.203	1001	0.938	0.831	1	0.733	100.0	0.080	2270	0.467	0.418	0.374	0.336	0.301	0.271	0.943	0100	0.213	0.137	0.160		0.145
	1.4	Millim.	3	3	33	3	3	3	3 :	1.511	1 200	1.161	1001	0.901	0.797	t	101.0	0.020	0.009	0.433	0.445	0.398	0.356	0.319	0.287	0.257	0 931	0000	0.500	0.107	0.153		0.138
	1.3	Millim.	"	33	¥	3	×	3	3 .	1.676	1 970	1.112	0.076	0.860	092.0	2	0.6/3	160.0	155.0	0.470	0.422	0.377	0.337	0.302	0.271	0.243	016.0	2010	0.137	771.0	0.144		0.130
7%	1.2	Millim.	3	33	3	z	z	39	1.866	1.508	0101	1.057	9600	0.814	0.718	1	0.639	0.500	0.000	0.440	0.397	0.354	0.317	0.284	0.255	0.228	0 905	100	0.100	0.100	0.135		0.122
Height of the Meniscus in Millimetres.	1.1	Millim.	3	×	3	3	3	2.087	1.780	1.318	1 1 1 9	0.995	0.871	0.764	0.673	2	1.034	0.020	0.407	0.410	0.370	0.330	0.295	0.264	0.237	0.213	1010	0.170	271.0	401.0	0.126		0.114
iscus in I	1.0	Millim.	"	33	3	3	2.348	1.978	1.680	1.235	1 060	0.958	0180	0.710	0.624	1	1000	0.487	0.432	0.004	0.342	0.305	0.272	0.244	0.518	0.196	9410	0 11 0	0.1.0	247	0.116		0.105
the Men	6.0	Millim.	3	3	3	2.662	2.209	1.851	1.565	1.142	200	0.855	0.745	0.652	0.572	0	0.504	0.440	0.395	0.001	0.312	0.278	0.248	0.222	0.199	0.178	0.160	201.0	0 1 4 4	0.100	0.105		0.095
Height of	0.8	Millim.	ij	×	3.050	2.483	2.046	1.705	1.436	1.218	2020	0.776	0.675	0.590	0.517	h h	0.400	0.402	0.336	0.010	0.281	0.250	0.254	0.500	0.179	0.160	0 144	100	0.1.0	0.110	0.095		0.085
	0.7	Millim.	33	3.542	2.812	2.270	1.859	1.541	1.292	0.932	008	0.691	0.601	0.524	0.459		0.404	0.000	0.315	0.200	0.249	0.221	0.198	0.177	0.158	0.142	7610		100	0.100	0.084	1	0.075
	9.0	Millim.	4.190	3.218	2.528	2.054	1.648	1.360	1.135	0.815	8090	0.602	0.593	0.455	0.399	2	0.300	0.009	0.273	0.242	0.215	0.192	0 171	0.153	0.137	0.122	0110	017.0	0000	0.003	0.050		0.065
	0.5	Millim. 5.085	3.728	2.825	2.196	1.746	1.413	1.161	996.0	0.691	0 501	0.509	0.441	0.384	0.336	ç	0.230	0.200	0.230	107.0	0.181	0.161	0.144	0.128	0.115	0.103	6600	0.00	0.000	#10.0	0.061	1	0.055
	0.4	Millim. 4.396	3.162	2.363	1.820	1.437	1.158	0.948	0.787	0.560	0.77	0.412	0.356	0.310	0.271	0	0.238	0.210	0.100	0.104	0.146	0.130	0.116	0.103	0.095	0.083	0.074	0.00	0000	0.000	0.049		0.044
	0.3	Millim. 3.516	2.484		_	1.103				0.502	0 369	0.312	0 96 0	0.234	0.502		0.130	_	0.140	_	0.110	0.098	0.087	0.078	0.00	0.062	0.056			_	0.037	4	0.033
	€.0	Millim. 2.460			_		_			0.337	0 943		_	0.157	-	00.0	0.120	_			0.074			_		0.045	0.037					6	0.025
	0.1	Millim. 1.268	0.876	0.638	0.484	0.378	0.305	0.245	0.203	0.170	0 199	0.105	0.091	0.079	0.069	0	0.000	0.000	0.047	240.0	0.037	0.033	0.059	0 0 0 2 6	0.053	0.021	0.019	7100	0.01		0.014		0.011
Radius of	in Milli- metres,	1.0	1.2	1.4	1.6	1.8	2.0	2.5	4:0	ν οι c ∞	G	3.5	3.4	3.6	3.8		0.4	7:4:	4.4	0.4	8:4	5.0	5.2	5.4	5.6	5.8	0 9	0.9	1 7	# Y	8.9	1	7.0
C					_		-			,		-	==	1:	32	-		_	-	_				_		_	_		-	-			!

FROM POUILLET.

Internal Diameter of Tube.	Depression.	Differences.	Internal Diameter of Tube.	Depression.	Differences.	Internal Diameter of Tube.	Depression.	Differences
Millimetres.	Millimetres.	Millimet.	Millimetres.	Millimetres.	Millimet.	Millimetres.	Millimetres.	Millimet.
2.00 2.50 3.00 3.50 4.00	4.579 3.595 2.902 2.415 2.053	0.985 0.692 0.487 0.362 0.301	8.50 9.00 9.50 10.00 10.50	0.604 0.534 0.473 0.419 0.372	0.070 0.061 0.054 0.047 0.042	15.00 15.50 16.00 16.50 17.00	0.127 0.112 0.099 0.087 0.077	0.015 0.013 0.012 0.010 ·
4.50 5.00 5.50 6.00 6.50	1.752 1.507 1.306 1.136 0.995	0.245 0.201 0.170 0.141 0.118	11.00 11.50 12.00 12.50 13.00	0.330 0.293 0.260 0.230 0.204	0.037 0.033 0.030 0.026 0.023	17.50 18.00 18.50 19.00 19.50	0.068 0.060 0.053 0.047 0.041	0.008 0.007 0.006 0.006 0.005
7.00 7.50 8.00	0.877 0.775 0.684	0.102 0.091 0.080	13.50 14.00 14.50	0.181 0.161 0.143	0.020 0.018 0.016	20.00 20.50 21.00	0.036 0.032 0.028	0.004

#### XXVI. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION.

Internal		Depression	according t	0	Internal		Depression :	according t	0
Diameter of Tube.	La Place.	Young.	Ivory.	Cavendish.	Diameter of Tube.	La Place.	Young	Ivory.	Cavendish
Millimetres.	Millim.	Millim.	Millim.	Millim.	Millimetres.	Millim.	Millim.	Millim.	Millim.
2.00	4.454	4.887	4.888	4.472	11.50	0.315			
2.50	3.568				12.00	0.281	0.242	0.253	0.200
3.00	2.918	2.986	2.988	3.054	12.50	0.250			
3.50	2.442				13.00	0.223	0.188	0.196	0.170
4.00	2.068	2.063	2.066	2.187	13.50	0.198	!		
4.50	1.774				14.00	0.176	0.144	0.152	0.150
5.00	1.534	1.510	1.513	1.735	14.50	0.156			
5.50	1.337				15.00	0.137	0.111	0.118	0.131
6.00	1.171	1.139	1.134	1.377	15.50	0.121			
6.50	1.030				16.00	0.107	0.088	0.087	
7.00	0.909	0.869	0.868	1.073	16.50	0.094			
7.50	0.803				17.00	0.083	0.068	0.071	
8.00	0.712	0.669	0.673	0.820	17.50	0.073			
8.50	0.632				18.00	0.064	0.053	0.054	
9.00	0.562	0.517	0.521	0.608	18.50	0.056			
9.50	0.500				19.00	0.049	0.041	0.042	
10.00	0.445	0.402	0.406	0.406	19.50	0.043			
10.50	0.397				20.00	0.038	0.031	0.031	
11.00	0.354	0.311	0.316	0.270	20.50	0.034			
11.50	0.315				21.00	0.030	0.024	0.024	

XXVII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, REDUCED INTO ENGLISH INCHES FROM DELCROS'S TABLE.

Internal Diam- eter		·		Heigl	at of Me	niscus i	n Thou	saudths	of an I	Inglish	Inch.		-	
of Tube.	5	10	15	20	25	30	35	40	45	50	55	60	65	70
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0.10	0.040			0.136	0.155									
0.12	.027	.053	.076	.097	.114	0.00=								
0.14	.019	.038	.056	.071		0.097	0.004							
0.16	.015	.029	.042	.055	.066		0.084	0.0**						
0.18	.011	.022	.033	.043	.052	.060	.067	0.073						
0.20	.009	.018	.026	.034	.042	.049	.055	.060	0.064					
0.22	.007	.014	.021	.028	.034	.040	.045	.049		0.057				
0.24	.006	.012	.017	.023	.028	.033	.037	.041	.045		0.050			
0.26	.005	.010	.014	.019	.023	.027	.031	.035	.038	.040	.043	0.045		
0.28	.004	.008	.012	.016	.019	.023	.026	.029	.032	.034	.036	.038		
0.30	.003	.007	.010	.013	.016	.019	.022	.025	.027	.029	.031	.033	0.034	
0.32	.003	.006	.009	.011	.014	.016	.019	.021	.023	.025	.027	.028	.030	
0.34	.002	.005	.007	.010	.012	.014	.016	.018	.020	.022	.023	.024	.026	
0.36	.002	.004	.006	.008	.010	.012	.014	.016	.017	.019	.020	.021	.022	
0.38	.002	.004	.005	.007	.009	.010	.012	.013	.015	.016	.017	.018	.019	
0.40	.002	.003	.005	.006	.008	.009	.010	.012	.013	.014	.015	.016	.017	
0.42	.001	.003	.004	.005	.007	.008	.009	.010	.011	.012	.013	.014	.015	0.015
0.44	.001	.002	.004	.005	.006	.007	.008	.009	.010	.011	.011	.012	.013	.013
0.46	.001	.002	.003	.004	.005	.006	.007	.008	.008	.009	.010	.011	.011	.012
0.48	.001	.002	.003	.004	.004	.005	.006	.007	.007	.008	.009	.009	.010	.010
0.50	.001	.002	.002	.003	.004	.004	.005	.006	.006	.007	.008	.008	.008	.009
0.52	.001	.001	.002	.003	.003	.004	.005	.005	.006	.006	.007	.007	.007	.008
0.54	.001	.001	.002	.002	.003	-003	.004	.004	.005	.005	.006	.006	.006	.007
	5	10	15	20	25	30	35	40	45	50	55	60	65	70

XXVIII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, EXPRESSED IN ENGLISH INCHES. — BAILY.

Diameter	Depr	ession accordin	ng to	Diameter	Depr	ession accordi	ng to	
of Tube.	Ivory.	Young.	La Place.	of Tube.	Ivory.	Young.	La Place.	
Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch.	Eug. Inch.	Eng Inch.	Eng. Inch.	Eng. Inch.	
0.05	0.2949	0.2964	0	0.35	0.0212	0.0196	0.0216	
0.10	.1404	.1424	.1394	0.40	.0154	.0139	.0159	
0.15	.0865	.0880	.0854	0.45	.0112	.0100	.0117	
0.20	.0583	.0589	.0580	0.50	.0082	.0074	.0087	
0.25	•0409	.0404	.0412	0.60	.0043	.0045	.0046	
0.30	.0293	.0280	.0296	0.70	.0023		.0024	
0.35	0.0212	0.0196	0.0216	0.80	0.0012	0	0.0013	

# METEOROLOGICAL TABLES

IV.

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### BAROMETRICAL

### MEASUREMENT OF HEIGHTS,

OR

### TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

D



### HYPSOMETRICAL TABLES

FOR

COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

Numerous determinations of altitude are one of the great desiderata of physical science, and no more ready means for obtaining them is at the disposal of the scientific man than the Barometer. A traveller, furnished with the improved and convenient instruments we can now command, and with some experience in using them, can take a large number of barometric observations for determining heights, at the cost of little trouble or time. It is, however, quite otherwise with the computations by which the results are obtained. The prospect of that tedious and time-robbing labor not only too often cools the zeal of the observer, but a vast amount of data actually collected remain of no avail from the want of having been computed.

The object of this much enlarged set of Hypsometrical Tables is to facilitate the task of the computer. It contains practical tables adapted to the three usual barometrical scales, and, among them, No. I., II., and V. are so disposed as to dispense with the use of logarithms, and to reduce the computation to the simplest arithmetical operations. The others suppose the use of logarithms, a method which may still be preferred by some observers.

As these various tables represent the development of the principal formulæ which have been proposed, the computer is enabled to compare the results obtained by each of them, and to select that which he most approves.

These formulæ may be referred to two classes, the respective types of which are Laplace's and Bessel's formulæ.

Laplace, in the Mécanique Céleste, Tom. IV. p. 292, gave a complete solution of the problem, and proposed a formula which soon superseded the older and less accurate formulæ of De Luc, Shuckburgh, and others. The coefficients which enter in it were derived from the best determinations of the needed physical constants which science could then furnish, the most important of which are the relative weight of the air and of the mercury, and the rate of expansion of air by heat. The first was assumed to be 10457, according to the experiments of Biot and Arago; and the barometrical coefficient deduced from it, 18317 metres. This coefficient was, however, empirically increased to 18336 metres, in order to adjust the results of the formula to those furnished by the careful trigonometrical measurements made by Ramond for the purpose of testing its correctness. It becomes 18393 metres when including the correction due to the effect of the decrease of gravity with the height on the density of the mercurial column and of the air. The coefficient expressing the expansion of the air by heat, as determined by Gay-Lussac, viz. 0.00375 of its bulk for one Centigrade degree, was adopted, but Laplace increased it to 0.004, in order to take into the account the effect of the greater expansive power of the vapors contained in the atmosphere.

D

These values have been retained in the different formulæ proposed later by Gauss, in Schumacher's Jahrbuch for 1840, by Schmidt, Mathem. und Physische Geographie, II. p. 205, and by Baily, Astronomical Tables, p. 183, which, therefore, only change the form without changing the results. D'Aubuisson, in his formula and tables, Traité de Géognosie, p. 488, only reduced the barometrical coefficient to its theoretical value, which he determined to be 18365 metres, leaving unchanged the other coefficients of Laplace's formula.

Bessel first introduced, in his formula, Astronomische Nachrichten, No. 356, a separate correction for the effect of moisture. The correction for the temperature of the air is computed in his tables for two values of the coefficient, that of Gay-Lussac, 0.00375, and that of Rudberg, 0.00365. Laplace's barometrical coefficient is retained, but the correction for the decrease of gravity is considerably modified.

In Elie Ritter's formula, in the Mémoires de la Societé de Physique de Genève, Tom. XIII. p. 343, the corrections for temperature and moisture are also separated; but other values of the barometrical and thermometrical coefficients, derived from Regnault's determinations, are used, and a new method is proposed for applying the correction due to the expansion of air, which is made proportional to the square of the difference between the observed temperatures at each station.

Baeyer's formula, recently published in Poggendorf's Annalen der Physik und Chemie, Tom. XCVIII. p. 371, does not belong to either of the two classes just mentioned; for while it keeps Laplace's barometrical and thermometrical coefficients, it corrects the effect of temperature by a method analogous to that of Ritter, and it entirely neglects the effect of aqueous vapor.

In the following set the tables of Delcros, Guyot, and Loomis develop the formula of Laplace. The much larger tables of Delcros render unnecessary those of Oltmanns, which are yearly reprinted in the Annuaire du Bureau des Longitudes. Instead of Gauss's tables will be found the tables of Dippe, which are computed from the same formula, but are more extended. Baily's tables close the first series. The tables of Plantamour, computed from Bessel's formula, are given here in preference to Bessel's tables, because Plantamour substituted for Laplace's barometrical coefficient that derived from the probably more accurate determination of the relative weight of the air and mercury by Regnault, viz. 18404.8 metres. E. Ritter's tables, computed from his own formula, give perhaps, in extreme cases, better results; but as, in ordinary circumstances, the altitudes obtained do not much differ from those furnished by the less complicated tables of Plantamour, they were not reprinted here.

The miscellaneous tables which follow furnish useful materials for solving several questions connected with the barometrical measurements.

Regnault's table of Barometric Pressures corresponding to Temperatures of the Boiling Point of Water, revised by Moritz, and its reduction to English measures, will be found a valuable addition for thermometrical measurements of heights.

The Appendix to the Hypsometrical Tables now offers, in a new form, a complete series of tables for the comparison of the different measures of length generally used for indicating altitudes, the convenience of which will be fully appreciated by those who have attempted to collect and to use the abundant contributions furnished by all civilized nations to that branch of geographical science.

#### TABLES

FOR

# DETERMINING DIFFERENCES OF LEVEL BY MEANS OF BAROMETRICAL OBSERVATIONS,

COMPUTED FROM THE COMPLETE FORMULA OF LAPLACE,

By M. T. DELCROS.

### Construction of the Tables.

If we take z = difference of level of the two barometers, a = earth's mean radius = 6366200 metres, L = mean latitude between the two stations.

and further: -

At Station. 
$$\begin{cases} h = \text{observed height of the barometer,} \\ T = \text{temperature of the barometer,} \\ t = \text{temperature of the air,} \\ t' = \text{observed height of the barometer,} \\ t' = \text{temperature of the barometer,} \\ t' = \text{temperature of the air,} \end{cases}$$

and if we make finally H = h + h'.  $\left(\frac{T - T'}{6196}\right)$ ,

we shall have, according to Laplace, the following general and complete equation: -

$$z=18336 ext{ metres} imes \left\{ egin{array}{ll} (1+rac{2.\left(\ell+rac{p'}{1000}
ight)}{1000}) \\ (1+0.0028371 ext{ cos. 2. L)} \\ ((1+rac{z}{a}). & ext{Log. } (rac{h}{H})+rac{z}{a} \ 0.868589) \end{array} 
ight\}$$

after the proper transformations this equation becomes: -

$$z = \text{Log.} \left( \frac{h}{H} \right) \text{ 18336 metres} \times \left\{ \begin{cases} \left( 1 + \frac{2. \ (l + l')}{1000} \right) \\ \left( 1 + 0.0028371 \text{ cos. 2. L} \right) \\ \left( 1 + \frac{\left( \log. \left( \frac{h}{H} \right) + 0.868589 \right). \frac{z}{a}}{\text{Log.} \left( \frac{h}{H} \right)} \right) \right\}$$
D

introducing into this expression the value in metres of a, the earth's mean radius, making  $z=\text{Log.}\left(\frac{\hbar}{H}\right)$  18336 and Log.  $\left(\frac{\hbar}{H}\right)=\left(\frac{z}{18336}\right)$ , which can be done without sensible error, the above formula takes the following form, sufficiently accurate for practical purposes:—

$$z = \text{Log.}\left(\frac{h}{H}\right)$$
. 18336 metres  $\times \left\{ \begin{array}{l} \left(1 + \frac{(2.\ (t+t')}{1000}\right) \\ \left(1 + 0.0028371 \text{ cos. 2. L}\right) \\ \left(1 + \frac{z+15926}{6366200}\right) \end{array} \right\}$ 

the four factors of which can easily be developed in tables, as has been done by Mr. Oltmanns. But though this savant chose to develop also the second factor, I found it better not to do so, partly because the calculation of it is very easy, and also or account of the great extent it would have been necessary to give to this table, in order to avoid troublesome interpolations.

In the calculation of h'.  $\left(\frac{T-T'}{6196}\right)$ , Mr. Oltmanns used the constant coefficient of the absolute expansion of the mercurial column; I took that of the relative expansion of the mercury and of the brass scale. It is obvious, therefore, that if the scale of the barometer employed was of wood, glass, iron, or of another substance, it would be necessary to make use of as many different coefficients, and the Table II. could not be used. Moreover, Oltmanns combined the last two factors of the general formula in one single table with double entry. This table I have calculated, extending it sufficiently to avoid a double interpolation; but as it seemed to me much too extensive, I substituted for it Tables III. and IV., which are more condensed, without rendering any troublesome interpolation necessary.

I carried the calculation of these tables beyond the limits at which Oltmanns chose to stop, in order that they may answer for the most extreme cases.

At the head of each table will be found the factor of which it is the development; this makes any other explanation superfluous.

All these tables give, at sight, the numbers wanted; only when very great precision is desired, a slight interpolation, at sight, and very easy to apply, may be required. My principal object was to relieve the computer of the troublesome and annoying labor of interpolations.

I added to these four tables the small Table V., taken from the *Annuaire du Bureau des Longitudes* of Paris. It will be seldom used.

When calculating differences of level, in the same order, with the tables, and by the complete formula of Laplace, the results thus obtained never differ by more than one decimetre in the most extreme cases. The following example will illustrate this statement. I take the observation made in a balloon, by Gay-Lussac, at Paris, as an extreme case, which is very well adapted to manifest the errors of the tables, if there were any, by comparing the results obtained by means of them with those of the direct calculation according to the complete formula of Laplace, from which they are derived.

D

Example of Calculation by the complete Formula of Laplace and by the Tables Height of the Balloon of Gay-Lussac.

The observation gave: -

Balloon 
$$h' = 328.80$$
  $T' = -9.5$   $t' = -9.5$   
Paris  $h = 765.68$   $T = +30.8$   $t = +30.8$ 

$$T - T' = +40.3$$
  $(t + t') = +21.3$  et  $2(t + t') = 42^{\circ}.6$ 

With these data the formula of Laplace gives the following calculation: -

Log. 
$$h'$$
. = 328.80 = 2.5169318

Log. 
$$(T - T') = +40.3$$
 = 1.6053050

Log. dilat. coefficient = 
$$0.0001614 = 6.2079035$$

Corr. 
$$a = +$$
 $h' =$ 

$$\begin{array}{c}
Milli. \\
2.14 \text{ log.} = 0.3301403 \\
328.80
\end{array}$$

$$H = 330.94 \log. = 2.5197480$$
 $\log. h = 765.68 = 2.8840473$ 

$$(\text{Log. } h - \text{Log. H}) = \text{Difference of Log.} = 0.3642993$$

Log. of (Log. 
$$h - \log H$$
) = 9.5614583

Log. general coefficient 
$$= 18336 = 4.2633046$$

Log. 
$$\left(\frac{h}{H}\right)$$
 18336  $= (A + a) = 3.8247629$   
Corresponding number  $= 6679.79 = (A + a)$ 

Log. cos. 
$$2 L = 97^{\circ} 40' = -$$
 9.1251872

Log. constant = 
$$0.0028371 = +$$
 7.4528746

$$Log. (A + a) = 6679.79. = +$$
 3.8247629

Log. ( 
$$(0.0028371. \text{ Cos. } 2 \text{ L}) \times (A + a)$$
 ) =  $-0.4028247$ 

Corresponding number 
$$=$$
  $-2.53$ 

$$(\Lambda + a + \beta) = \frac{-}{6677.26}$$

Corr. temp. air = 
$$v$$
 = 284.45 =  $(6.677 \times 42.6)$ 

$$(A + a + \beta + v) = 6961.71$$
  
Constant = . + 15926

$$22887.71 \dots \text{Log.} \dots = 4.3596022$$

Comp<sup>t</sup>. log. 
$$a = 6366200 \dots \text{Log.} \dots = 3.1961197$$

$$(A + a + \beta + v) = 6961.71 \dots \text{Log.} \dots = 3.8427153$$

$$\delta = +$$
 25.03 Log. =  $+$  1.3984372

$$(A + a + \beta + v + \delta) = 6986.74$$

Altitude of balloon = 7035.44 by the formula of Laplace.

Now let us calculate by the tables, placing side by side the corresponding results given by the formula of Laplace.

Balloon 
$$h' = 328.80$$
  $T' = -9.5$   $t' = -9.5$ 
Paris  $h = 765.68$   $T = +30.8$   $t = +30.8$ 

with  $\begin{cases} h' = 328.80 \\ h = 765.68 \end{cases}$  Table I. gives  $\begin{cases} 1478.4 \\ 8209.8 \end{cases}$  By the formula of Eaplace we found:

$$A = 6731.4$$
with  $(T' - T) = -40^{\circ}.3$ , Table II. gives  $a = -52.0$ 

$$(A + a) = 6679.4$$

$$(A + a) = 6679.4$$
with  $A = 6679.79$ 
with  $A = 6679.79$ 

$$A = 6677.1$$
with  $A = 6677.1$ 

$$A = 6677.26$$
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Two results which are sensibly identical. This ought not to astonish us; the tables being the exact development of the formula, they ought to give the same results, provided in both cases nothing has been neglected, and the four factors have been calculated in the same relative order.

DELCROS.

# Disposition and Use of the Tables.

The disposition of the tables is the following:—

In Table I., the first column on the left contains the height of the barometer in millimetres, corrected for the error of the instrument.

The second column headed N (number), gives in metres the first two figures of the number corresponding to each height of the barometer in the first column; the third column, headed 0.0, gives the remaining figures for the full number of millimetres; the following columns give the remaining figures for the same number of millimetres and each decimal fraction of a millimetre which may follow it. The value of the hundredths is to be found in the last column.

Example: — Height of Barometer = 761.00.

We look out in the first column for the number 761, and we find on the same line in the second column, 81; in the third column, headed 0.0, or full number, 61.1. The corresponding number is thus 8161.1 metres.

Height of barometer = 761.35.

The second column gives 81; the column headed 0.3 gives, on the same line, 64.2. The corresponding number is then 8164.2. Adding the value of five hundredths of millim., being 0<sup>m</sup>.5, as indicated in the last column, we have 8164.7 metres, corresponding to 761.35 millim.

The other four tables need no further explanation.

To calculate, by means of the tables, a difference of level from two barometrical observations, proceed in the following manner:—

- 1. Take the height of the barometer at the lower station, or h, and seek in Table I. the number corresponding to this height. Seek likewise the number corresponding to the height of the barometer at the upper station. Subtract the second from the first. The remainder is the approximate difference of level between the two stations. Then apply the following corrections.
  - 2. Correction to be applied for the temperature of the barometers.

If T' be the temperature of the attached thermometer at the upper station, and T that of the attached thermometer at the lower station, take the difference, or T' - T, and seek in Table II. the number corresponding to this difference.

When T' is smaller than T, that is, when the temperature of the attached thermometer of the upper station is lower than that of the lower station, the correction is to be *subtracted* from the approximate height; when T' is greater than T, it is to be *added*.

3. Correction for the temperature of the air.

The first correction having been applied, multiply the number obtained, or N, by the double sum of the temperatures of the air at both stations, and divide the product by 1000; the number thus found, or the quantity expressed by  $\frac{N}{1000}$ . 2 (t + t) is the correction in metres which is to be *added* to the preceding number N.

- 4. Tables III. and IV. give two corrections; the first due to the decrease of gravitation in latitude, which is to be added when the mean latitude of the places of observation is between the 45th parallel and the equator; and to be subtracted when it is between the same parallel and the poles, as indicated at the head of the columns. The second correction, due to the decrease of gravitation on the vertical line, is always additive.
- 5. Table V. gives another small correction to be added in the case of the lower station being very elevated above the level of the ocean.

## Examples of Calculation.

Measurement of the Height of Guanaxuato. By M. de Humboldt.

Barometer at the upper station, Barometer at the level of the sea, h' = 600.95 T' = 21.3 t' = 21.3h = 763.15 T = 25.3 t = 25.3

## BAROMETRICAL MEASUREMENT OF HEIGHTS.

Table I. gives the corresponding numbers,	{	h = 8 $h' = 9$	8183.5 6280.8	
Table II. gives for T' — T,	Difference,	_	$\frac{1902.7}{5.2}$	
Table II. gives for 1 — 1,	Difference,		1897.5	= N
$\frac{N}{1000}$ . 2 $(t+t') = 1.897 \times 93.2$ ,		+	176.8	
	Sum,	9	2074.3	
Table III. gives for mean latitude of 21°,		+	4.3	
Table IV. gives for decrease of gravitation	in the vertical line,	+	6.0	
Hence altitude of Guanaxuato above the o	cean,		2084.6	

Measurement of the height of Mont Blanc, August 29, 1844. By MM. Bravais and Martins.

Barometer at one metre below the summit,	h' = 424.05	T' = -	$4.2 \ t' = -$	$\mathring{7}.6$
Barometer of the Observatory of Geneva,	h = 729.65	T =	$18.6 \ t =$	19.3

Table I. gives for numbers corresponding	to	$\begin{cases} h = 7826.0 \\ h' = 3504.4 \end{cases}$
	Difference,	4321.6
Table II. gives for T' — T,		<b>—</b> 29.3
•	Difference,	$\overline{4292.3} = N$
$\frac{N}{1000}$ . 2 $(t + t') = 4292 \times 23.4 =$		+ 100.4
	Sum,	4392.7
Table III. gives for the mean latitude of 4	6°,	- 0.4
	Difference,	4392.3
Table IV. for decrease of gravitation in th	e vertical line	+ 13.7
Table V. for the elevation of the lower sta	tion,	+ 0.5
	Sum,	4406.5
Elevation of the lower barometer above the	e ocean,	407.0
Hence elevation of upper barometer above	e the ocean,	4813.5
Finally, height of the summit of Mont Bla	nc above the ocea	n, 4814.5

TABLE I. — Giving A = 18336  $\times$  log. H or h..., argument H or h in Millimetres.

r=====		IABLI	3 1. — UI	ving A =	- 100000 X	10g. 11 01	76, alg	unient 11	01 76 111 14	fillimetre		
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres,	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
288	4	23.4	26.2	28.9	31.7	34.4	37.2	40.0	42.7	45.5	48.2	1   0.3
289	4	51.0	53.8	56.5	59.3	62.0	64.8	67.5	70.3	73.0	75.8	2 0.5
290	4	78.5	81.3	84.0	86.7	89.5	92.2	95.0	97.7			3 0.8
290	5									00.4	03.2	4 1.1
291	5	05.9	08.7	11.4	14.1	16.8	19.6	22.3	25.0	27.8	30.5	5 1.4
292	5	33.2	36.0	38.7	41.4	44.1	46.8	49.6	52.3	55.0	57.7	6 1.6
293	5	60.5	63.2	65.9	68.6	71.3	74.0	76.7	79.5	82.2	84.9	7 1.9
294	5	87.6	90.3	93.0	95.7	98.4						8 2.2
294	6						01.1	03.8	06.5	09.2	11.9	9 2.4
295	6	14.6	17.3	20.0	22.7	25.4	28.1	30.8	33.5	36.2	38.9	
296	6	41.6	44.3	47.0	49.6	52.3	55.0	57.7	60.4	63.1	65.8	1
297	6	68.4	71.1	73.8	76.5	79.1	81.8	84.5	87.2	89.9	92.5	
298	6	95.2	97.9									
298	7			00.5	03.2	05.9	08.6	11.2	13.9	16.6	19.2	
299	7	21.9	24.5	27.2	29.9	32.5	35.2	37.8	40.5	43.2	45.8	
300	7	48.5	51.1	53.8	56.4	59.1	61.7	64.4	67.0	69.7	72.3	
301	7	75.0	77.6	80.3	82.9	85.5	88.2	90.8	93.5	96.1	98.7	
302	8	01.4	04.0	06.6	09.3	11.9	14.5	17.2	19.8	22.4	25.1	
303	8	27.7	30.3	33.0	35.6	38.2	40.8	43.5	46.1	48.6	51.3	
304	8	54.0	56.6	59.2	61.8	64.4	67.0	69.6	72.3	74.9	77.5	
305	8	80.1	82.7	85.3	87.9	90.5	93.1	95.7	98.3			
305	9									01.0	03.6	
306	9	06.2	08.8	11.4	14.0	16.6	19.2	21.8	24.4	27.0	29.6	1   0.3
307	9	32.1	34.7	37.3	39.9	42.5	45.1	47.7	50.3	52.9	55.5	2 0.5
308	9	58.0	60.6	63.2	65.8	68.4	70.9	73.5	76.1	78.7	81.3	3 0.8
309	9	83.9	86.4	89.0	91.6	94.1	96.7	99.3				4 1.0
309	10								01.9	04.4	07.0	5 1.3
310	10	09.6	12.1	14.7	17.3	19.8	22.4	25.0	27.5	30.1	32.7	6 1.5
311	10	35.2	37.8	40.3	42.9	45.5	48.0	50.6	53.1	55.7	58.2	7 1.8
312	10	60.8	63.3	65.9	68.4	71.0	73.5	76.1	78.6	81.2	83.7	8 2.1
313	10	86.3	88.8	91.4	93.9	96.4	99.0					9 2.3
313	11							01.5	04.1	06.6	09.1	
314	11	11.7	14.2	16.7	19.3	21.8	24.3	26.9	29.4	31.9	34.5	
315	11	37.0	39.5	42.0	44.6	47.1	49.6	52.1	54.7	57.2	59.7	
316	11	62.2	64.8	67.3	69.8	72.3	74.8	77.3	79.9	82.4	84.9	
317	11	87.4	89.9	92.4	94.9	97.4	99.9					
317	12							02.4	05.0	07.5	10.0	
318	12	12.5	15.0	17.5	20.0	22.5	25.0	27.5	30.0	32.5	35.0	
319	12	37.5	40.0	42.5	45.0	47.5	50.0	52.4	54.9	57.4	59.9	
320	12	62.4	64.9	67.4	69.9	72.3	74.8	77.3	79.8	82.3	84.8	
321	12	87.2	89.7	92.2	94.7	92.1	99.6	00.7	0.4.0	0===	00 =	
321	13	-0.0	7.4.7		70	0	24	02.1	04.6	07.1	09.5	
322	13	12.0	14.5	17.0	19.4	21.9	24.4	26.8	29.3	31.8	34.2	
323	13	36.7	39.2	41.6	44.1	46.6	49.0	51.5	53.9	56.4	58.9	
324	13	61.3	63.8	66.2	68.7	71.1	73.6	76.1	78.5	81.0	83.4	
325	13	85.9	88.3	90.8	93.2	95.7	98.1	00 -	00.0	0	0 == 0	
325	14							00.5	03.0	05.4	07.9	
Barom- eter Hor h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
						17						

326 to 364mm.

					9.4	0 10 0	64 <sup>mm</sup> .						
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for	Parts r each
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.		Metr.
326	14	10.3	12.8	15.2	17.6	20.1	22.5	25.0	27.4	29.8	32.3	1	10.2
327	14	34.7	37.2	39.6	42.0	44.5	46.9	49.3	51.7	54.2	56.6	2	0.5
328	14	59.0	61.5	63.9	66.3	68.7	71.2	73.6	76.0	78.4	80.9	3	0.7
329	14	83.3	85.7	88.1	90.5	92.9	95.4	97.8				4	1.0
329	15					•			00.2	02.6	05.0	5	1.2
330	15	07.4	09.9	12.3	14.7	17.1	19.5	21.9	24.3	26.7	29.1	6	1.5
331	15	31.5	33.9	36.3	38.7	41.2	43.6	46.0	48.4	50.8	53.2	7	1.7
332	15	55.6	58.0	60.4	62.8	65.1	67.5	69.9	72.3	74.7	77.1	8	2.0
333	15	79.5	81.9	84.3	86.7	89.1	91.4	93.8	96.2	98.6		9	2.2
333	16										01.0		
334	16	03.4	05.8	08.1	10.5	12.9	15.3	17.7	20.0	22.4	24.8		
335	16	27.2	29.6	31.9	34.3	36.7	39.1	41.4	43.8	46.2	48.8		
336	16	50.9	53.3	55.7	58.0	60.4	62.8	65.1	67.5	69.9	72.2	1	0.2
337	16	74.6	77.0	79.3	81.7	84.0	86.4	88.8	91.1	93.5	95.8	2	0.4
338	16	98.2										3	0.7
338	17		00.5	02.9	05.2	07.6	10.0	12.3	14.7	17.0	19.4	4	1.0
339	17	21.7	24.1	26.4	28.8	31.1	33.4	35.8	38.1	40.5	42.8	5	1.2
340	17	45.2	47.5	49.8	52.2	54.5	56.9	59.2	61.5	63.9	66.2	6	1.5
341	17	68.6	70.9	73.2	75.6	77.9	80.2	82.6	84.9	87.2	89.5	7	1.7
342	17	91.9	94.2	96.5	98.9							8	1.9
342	18					01.2	03.5	05.8	08.2	10.5	12.8	9	2.2
343	18	15.1	17.4	19.8	22.1	24.4	26.7	29.0	31.4	33.7	36.0		
344	18	38.3	40.6	42.9	45.2	47.6	49.9	52.2	54.5	56.8	59.1		
345	18	61.4	63.7	66.0	68.3	70.6	73.0	75.3	77.6	79.9	82.2		
346	18	84.5	86.8	89.1	91.4	93.7	96.0	98.3					
346	19								00.6	02.9	05.2		
347	19	07.5	09.6	12.0	14.3	16.6	18.9	21.2	23.5	25.8	28.1		
348	19	30.4	32.7	34.9	37.2	39.5	41.8	44.1	46.4	48.6	50.9		
349	19	53.2	55.5	57.8	60.1	62.3	64.6	66.9	69.2	71.5	73.7		
350	19	76.0	78.3	80.6	82.8	85.1	87.4	89.6	91.9	94.2	96.5	1	0.2
351	19	98.7										2	0.4
351	20		01.0	03.3	05.5	07.8	10.1	12.3	14.6	16.8	19.1	3	0.7
352	20	21.4	23.6	25.9	28.2	30.4	32.7	34.9	37.2	39.5	41.7	4	0.9
353	20	44.0	46.2	48.5	50.7	53.0	55.2	57.5	59.7	62.0	64.2	5	1.1
354	20	66.5	68.7	71.0	73.2	75.5	77.7	80.0	82.2	84.5	86.7	6	1.3
355	20	89.0	91.2	93.4	95.7	97.9	00.2	00.4	04.2	00.0	00.7	7	1.6
355 356	21	11.4	19.6	15.0	10 1	90.9	00.2	02.4	04.6	06.9	09.1	8	1.8
357	21	11.4	13.6	15.8	18.1	20.3	22.5	24.8	27.0	29.2	31.5	9	2.1
358	21	33.7	35.9	38.2	40.4	42.6	44.8	47.1	49.3	51.5	53.7		
359	21	56.0	58.2	60.4	62.6	64.9	67.1	69.3	71.5	73.7	76.0		
360	21	78.2	80.4	82.6	84.8	87.0	89.3	91.5	93.7	95.9	98.1		
361	22	i	02.5	04.8	07.0	09.2	11.4	13.6	15.8	18.0	20.2		
362	$\begin{bmatrix} 22 \\ 22 \end{bmatrix}$	22.4 44.5	24.6	26.8	29.0	31.2	33.4	35.6	37.9	40.1	42.3		
363	22 22	66.4	46.7 68.6	48.9	51.0	53.2	55.4	57.6	59.8	62.0	64.2		
364	22 2	88.3	90.5	70.8	73.0	75.2	77.4	79.6	81.8	83.9	86.1		
364	23	00.0	30.0	92.7	94.9	97.1	99.3	01.4	03.6	05.8	08.0		
Barom- eter Hor h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for	rts each mm.

365 to 403mm.

					365	to 4	03mm.	,					
Barometer H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm	h
Milli.	Metr.	Metres.	Metres,	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Met	r.
365	23	10.2	12.4	14.5	16.7	18.9	21.1	23.2	25.4	27.6	29.8	1 0.2	2
366	23	32.0	34.1	36.3	38.5	40.7	42.8	45.0	47.2	49.3	51.5	2 0.4	- }
367	23	53.7	55.9	58.0	60.2	62.4	64.5	66.7	68.9	71.0	73.2	3 0.6	
368	23	75.4	77.5	79.7	81.8	84.0	86.2	88.3	90.5	92.6	94.8	4 0.9	
369	23	97.0	99.1									5 1.1	- 1
369	24			01.3	03.4	05.6	07.7	09.9	12.1	14.2	16.4	6 1.3	- 1
370	24	18.5	20.6	22.8	24.9	27.1	29.2	31.4	33.5	35.7	37.8	7 1.5	- 1
371	24	40.0	42.1	44.3	46.4	48.6	50.7	52.9	55.0	57.2	59.3	8 1.7	
372	24	61.5	63.6	65.8	67.9	70.1	72.2	74.3	76.5	78.6	80.8	9 1.9	
373	24	82.9	85.0	87.2	89.3	91.4	93.6	95.7	97.8	99.9			
373	25	040	00.0	00.4							02.1		1
374	25	04.2	06.3	08.4	10.6	12.7	14.8	16.9	19.0	21.2	23.3		
375	25	25.4	27.5	29.6	31.8	33.9	36.0	38.1	40.2	42.4	44.5		
376	25	46.6	48.7	50.8	53.0	55.1	57.2	59.3	61.4	63.6	65.7		-
377	25	67.8	69.9	72.0	74.1	76.2	78.3	80.5	82.6	84.7	86.8		
378	25	88.9	91.0	93.1	95.2	97.3	99.4						ı
378	26							01.5	03.6	05.7	07.8	1	
379	26	09.9	12.0	14.1	16.2	18.3	20.4	22.5	24.6	26.7	28.8		
380	26	30.9	33.0	35.1	37.2	39.3	41.3	43.4	45.5	47.6	49.7		l
381	26	51.8	53.9	56.0	58.1	60.2	62.2	64.3	66.4	68.5	70.6		
382	26	72.7	74.8	76.9	78.9	81.0	83.1	85.2	87.3	89.3	91.4		
383	26	93.5	95.6	97.7	99.7								
383	27					01.8	03.9	06.0	08.1	10.1	12.2	1   0.2	I
384	27	14.3	16.4	18.4	20.5	22.6	24.6	26.7	28.8	30.9	32.9	2 0.4	
385	27	35.0	37.1	39.1	41.2	43.2	45.3	47.4	49.4	51.5	53.5	3 0.6	
386	27	55.6	57.7	59.7	61.8	63.8	65.9	68.0	70.0	72.1	74.1	4 0.9	-
387	27	76.2	78.3	80.3	82.4	84.4	86.5	88.6	90.6	92.7	94.7	5 1.1	ii
388	27	96.8	98.8									6 1.3	il
388	28			00.9	02.9	05.0	07.0	09.1	11.1	13.2	15.2	7 1.5	
389	28	17.3	19.3	21.4	23.4	25.5	27.5	29.6	31.6	33.7	35.7	8 1.7	
390	28	37.8	39.8	41.9	43.9	46.0	48.0	50.0	52.1	54.1	56.2	9 1.9	
391	28	58.2	60.2	62.3	64.3	66.3	68.3	70.4	72.4	74.4	76.5		-
392	28	78.5	80.5	82.6	84.6	86.6	88.6	90.7	92.7	94.7	96.8		
393	28	98.8	00.0	00.0	040	00.0	00.0	70.0	70.0	750	1.00		
393	29	10.0	00.8	02.8	04.9	06.9	08.9	10.9	12.9	15.0	17.0		
394	29	19.0	21.0	23.0	25.1	27.1	29.1	31.1	33.1	35.2	37.2		
395	29	39.2 59.3	41.2	43.2	45.2	47.2	49.2	51.3	53.3	55.3	57.3		1
396	29	79.4	61.3 81.4	63.3	65.3	67.3	69.3	71.4	73.4	75.4	77.4		1
397	29 29	99.5	01.4	83.4	85.4	87.4	89.4	91.5	93.5	95.5	97.5		1
398 398	30	99.9	01.5	03.5	05.5	07.5	09.5	11.5	13.5	15.5	17.5		1
399	30	19.5	21.5	23.5	25.5	27.5	29.4	31.4	33.4	35.4	37.4		-
000	90	20.0	22.0	20.0	20.0	21.0	20.4	31.4	30.4	5014	911.4		
400	30	39.4	41.4	43.4	45.4	47.4	49.4	51.3	53.3	55.3	57.3		
401	30	59.3	61.3	63.3	65.2	67.2	69.2	71.2	73.2	75.1	77.1		-
402	30	79.1	81.1	83.1	85.0	87.0	89.0	91.0	93.0	94.9	96.9		1
403	30	98.9											
Barom- eter or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.	
D						19							4

403 to 442mm.

					400	3 to 4	42.					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
403	31		00.9	02.8	04.8	06.8	08.7	10.7	12.7	14.7	16.6	1   0.2
404	31	18.6	20.6	22.5	24.5	26.5	28.4	30.4	32.4	34.4	36.3	2 0.4
405	31	38.3	40.3	42.2	44.2	46.1	48.1	50.1	52.0	54.0	55.9	3 0.6
406	31	57.9	59.9	61.8	63.8	65.7	67.7	69.7	71.6	73.6	75.5	4 0.8
407	31	77.5	79.5	81.4	83.4	85.3	87.3	89.3	91.2	93.2	95.1	5 1.0
408	31	97.1	99.0									6 1.2
408	32			01.0	02.9	04.9	06.8	08.8	10.7	12.7	14.6	7 1.4
409	32	16.6	18.5	20.5	22.4	24.4	26.3	28.2	30.2	32.1	34.1	8 1.6
410	32	36.0	37.9	39.9	41.8	43.8	45.7	47.6	49.6	51.5	53.5	9 1.8
411	32	55.4	57.3	59.3	61.2	63.2	65.1	67.0	69.0	70.9	72.9	
412	32	74.8	76.7	78.7	80.6	82.5	84.4	86.4	88.3	90.2	92.2	
413	32	94.1	96.0	97.9	99.9							
413	33					01.8	03.7	05.6	07.5	09.5	11.4	
414	33	13.3	15.2	17.1	19.1	21.0	22.9	24.8	26.7	28.7	30.6	
415	33	32.5	34.4	36.3	38.3	40.2	42.1	44.0	45.9	47.9	49.8	
416	33	51.7	53.6	55.5	57.4	59.3	61.2	63.2	65.1	67.0	68.9	
417	33	70.8	72.7	74.6	76.5	78.4	80.3	82.3	84.2	86.1	88.0	
418	33	89.9	91.8	93.7	95.6	97.5	99.4					
418	34							01.3	03.2	05.1	07.0	
419	34	08.9	10.8	12.7	14.6	16.5	18.4	20.3	22.2	24.1	26.0	
420	34	27.9	29.8	31.7	33.6	35.5	37.3	39.2	41.1	43.0	44.9	
421	34	46.8	48.7	50.6	52.5	54.4	56.2	58.1	60.0	61.9	63.8	
422	34	65.7	67.6	69.5	71.4	73.3	75.1	77.0	78.9	80.8	82.7	1   0.2
423	34	84.6	86.5	88.4	90.2	92.1	94.0	95.9	97.8	99.6		2 0.4
423	35										01.5	3 0.6
424	35	03.4	05.3	07.2	09.0	10.9	12.8	14.7	16.6	18.4	20.3	4 0.8 5 1.0
425	35	22.2	24.1	25.9	27.8	29.6	31.5	33.4	35.2	37.1	38.9	6 1.2
426	35	40.8	42.7	44.5	46.4	48.3	50.1	52.0	53.9	55.8	57.6	7 1.4
427	35	59.5	61.4	63.2	65.1	67.0	68.8	70.7	72.6	74.5	76.3	8 1.6
428	35	78.2	80.1	81.9	83.8	85.6	87.5	89.4	91.2	93.1	94.9	9 1.8
429	35	96.8	98.6									
429	36			00.5	02.3	04.2	06.0	07.9	09.7	11.6	13.4	
430	36	15.3	17.1	19.0	20.8	22.7	24.6	26.4	28.2	30.1	31.9	
431	36	33.8	35.6	37.5	39.3	41.2	43.0	44.8	46.7	48.5	50.4	
432	36	52.2	54.0	55.9	57.7	59.6	61.4	63.2	65.1	66.9	68.8	
433	36	70.6	72.4	74.3	76.1	78.0	79.8	81.6	83.5	85.3	87.2	
434	36	89.0	90.8	92.7	94.5	96.3	98.1					
434	37							00.0	01.8	03.6	05.5	
435	37	07.3	09.1	11.0	12.8	14.6	16.4	18.3	20.1	21.9	23.8	
436	37	25.6	27.4	29.2	31.1	32.9	34.7	36.5	38.3	40.2	42.0	
437	37	43.8	45.6	47.5	49.3	51.1	52.9	54.8	56.6	58.4	60.3	
438	37	62.1	63.9	65.7	67.6	69.4	71.2	73.0	74.8	76.7	78.5	
439	37	80.3	82.1	83.9	85.7	87.5	89.3	91.2	93.0	94.8	96.6	
440	37	98.4										
440	38		00.2	02.0	03.8	05.6	07.5	09.3	11.1	12.9	14.7	
441	38	16.5	18.3	20.1	21.9	23.7	25.5	27.3	29.1	30.9	32.7	
442	38	34.5	36.3	38.1	39.9	41.7	43.5	45.3	47.1	48.9	50.7	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

443 to 482mm.

Barom-						enth of			,			Parts
eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for each 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres,	Metres.	Metr
443	38	52.5	54.3	56.1	57.9	59.7	61.4	63.2	65.0	66.8	68.6	
444	38	70.4	72.2	74.0	75.8	77.6	79.3	81.1	82.9	84.7	86.5	
445	38	88.3	90.1	91.9	93.7	95.5	97.2	99.0				}
445	39								00.8	02.6	04.4	
446	39	06.2	08.0	09.8	11.5	13.3	15.1	16.9	18.7	20.4	22.2	
447	39	24.0	25.8	27.6	29.3	31.1	32.9	34.7	36.5	38.2	40.0	
448	39	41.8	43.6	45.4	47.1	48.9	50.7	52.5	54.3	56.0	57.8	
449	39	59.6	61.4	63.1	64.9	66.7	68.4	70.2	72.0	73.8	75.5	
450	39	77.3	79.1	80.8	82.6	84.3	86.1	87.9	89.6	91.4	93.1	
451	39	94.9	96.7	98.4								
451	40				00.2	02.0	03.7	05.5	07.3	09.1	10.8	
452	40	12.6	14.4	16.1	17.9	19.6	21.4	23.2	24.9	26.7	28.4	
453	40	30.2	32.0	33.7	35.5	37.2	39.0	40.8	42.5	44.3	46.0	
454	40	47.8	49.5	51.3	53.0	54.8	56.5	58.3	60.0	61.8	63.5	
455	40	65.3	67.0	68.8	70.5	72.3	74.0	75.8	77.5	79.3	81.0	1   0.2
456	40	82.8	84.5	86.3	88.0	89.8	91.5	93.2	95.0	96.7	98.5	2 0.3
457	41	00.2	01.9	03.7	05.4	07.2	08.9	10.6	12.4	14.1	15.9	3 0.5
458	41	17.6	19.3	21.1	22.8	24.6	26.3	28.0	29.8	31.5	33.3	4 0.7
459	41	35.0	36.7	38.5	40.2	41.9	43.6	45.4	47.1	48.8	50.6	5 0.9
460	41	52.3	54.0	55.8	57.5	59.2	60.9	62.7	64.4	66.1	67.9	6 1.0
461	41	69.6	71.3	73.1	74.8	76.5	78.2	80.0	81.7	83.4	85.2	7 1.2
462	41	86.9	88.6	90.3	92.1	93.8	95.5	97.2	98.9	00.1	0512	8 1.4
462	42		00.0	00.0	02.1		00.0	02	00.0	00.7	02.3	9 1.6
463	42	04.1	05.8	07.5	09.3	11.0	12.7	14.4	16.1	17.9	19.6	. ,
464	42	21.3	23.0	24.7	26.4	28.1	29.8	31.6	33.3	35.0	36.7	
465	42	38.4	40.1	41.8	43.5	45.2	46.9	48.7	50.4	52.1	53.8	
	42	55.5	57.2	58.9	60.6	62.3	64.0	65.8	67.5	69.2	70.9	
466	42	72.6	74.3	76.0	77.7	79.4	81.1	82.8	84.5	86.2	87.9	
467	42	89.6	91.3	93.0	94.7	96.4	98.1	99.8	0.4.0	00.2	01.0	
468	[	33.0	31.3	30.0	34.1	30.4	33.1	23.0	01.5	03.2	04.9	
468	43	00.6	08.3	10.0	11 ~	13.4	15.1	16.8	18.5	20.2	21.9	
469	43	06.6		27.0	11.7 28.7	30.4	15.1 32.0	33.7	35.4	37.1	38.8	
470	43	23.6	25.3	43.9		47.3	48.9	50.6	52.3	54.0	55.7	
471	43	40.5	42.2		45.6	1				70.9	72.6	
472	43	57.4	59.1	60.8	62.5	64.2	65.8	67.5	69.2			
473	43	74.3	76.0	77.7	79.3	81.0	82.7	84.4	86.1	87.7	89.4	
474 474	43 44	91.1	92.8	94.5	96.1	97.8	99.5	01.2	02.9	04.5	06.2	
		07.9	09.6	11.2	12.9	14.6	16.2	17.9	19.6	21.3	22.9	
475	44	1		27.9		31.3		35.6	37.3	39.0	40.6	
476	44	24.6	26.3	ſ	29.6		33.9	51.3	53.0	54.7	56.3	
477	44	41.3	43.0	44.6	46.3	48.0 64.7	49.6					
478	44	58.0	59.7	61.3	63.0		66.3	68.0	69.7	71.4	73.0	
479	44	74.7	76.4	78.0	79.7	81.3 97.9	83.0	84.7	86.3	88.0	89.6	
480	44	91.3	93.0	94.6	96.3	97.9	99.6	01.9	02.0	01.0	06.9	
480	45	0= 0	00 -	11.0	100	7,-	70.1	01.3	02.9	04.6	06.2	
481 482	45 45	07.9 24.3	09.5 25.9	11.2 27.6	12.8 29.2	14.5 30.9	16.1 32.5	17.7 34.2	19.4 35.8	21.0 37.5	22.7 39.1	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac

483 to 524<sup>mm</sup>.

						10 3				1		
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
483	4.5	40.8	42.4	44.1	45.7	47.4	49.0	50.7	52.3	54.0	55.6	1   0.2
484	45	57.3	58.9	60.6	62.2	63.9	65 5	67.1	68.8	70.4	72.1	2 0.3
485	45	73.7	75.3	77.0	78.6	80.3	81.9	83.6	85.2	86.9	88.5	3 0.5
486	45	90.2	91.8	93.5	95.1	96.8	98.4					4 0.6
486	46							0.00	01.7	03.3	05.0	5 0.8
487	46	06.6	08.2	09.9	11.5	13.1	14.7	16.4	18.0	19.6	21.3	6 1.0
488	46	22.9	24.5	26.2	27.8	29.4	31.0	32.7	34.3	35.9	37.6	7 1.1
489	46	39.2	40.8	42.4	44.1	45.7	47.3	48.9	50.5	52.2	53.8	8 1.3
490	46	55.4	57.0	58.6	60.3	61.9	63.5	65.1	66.7	68.4	70.0	9 1.4
491	46	71.6	73.2	74.9	76.5	78.1	79.7	81.4	83.0	84.6	86.3	
492	46	87.9	89.5	91.1	92.8	94.4	96.0	97.6	99.2			
492	47									00.9	02.5	
493	47	04.1	05.7	07.3	08.9	10.5	12.1	13.8	15.4	17.0	18.6	
494	47	20.2	21.8	23.4	25.0	26.6	28.2	29.9	31.5	33.1	34.7	
495	47	36.3	37.9	39.5	41.1	42.7	44.3	45.9	47.5	49.1	50.7	
496	47	52.3	53.9	55.5	57.1	58.7	60.3	61.9	63.5	65.1	66.7	
497	47	68.3	69.9	71.5	73.1	74.7	76.3	78.0	79.6	81.2	82.8	
498	47	84.4	86.0	87.6	89.2	90.8	92.4	94.0	95.6	97.2	98.8	
499	48	00.4	02.0	03.6	05.2	06.8	08.3	09.9	11.5	13.1	14.7	
500	48	16.3	17.9	19.5	21.1	22.7	24.2	25.8	27.4	89.0	30.6	
501	48	32.2	33.8	35.4	37.0	38.6	40.1	41.7	43.3	44.9	46.5	
502	48	48.1	49.7	51.3	52.9	54.5	56.0	57.6	59.2	60.8	62.4	
503	48	64.0	65.6	67.2	68.7	70.3	71.9	73.5	75.1	76.6	78.2	
504	48	79.8	81.4	83.0	84.5	86.1	87.7	89.3	90.9	92.4	94.0	
505	48	95.6	97.2	98.7								
505	49				00.3	01.9	03.4	05.0	06.6	08.2	09.7	
506	49	11.3	12.9	14.4	16.0	17.6	19.1	20.7	22.3	23.9	25.4	
507	49	27.0	28.6	30.1	31.7	33.3	34.8	36.4	38.0	39.6	41.1	
508	49	42.7	44.3	45.8	47.4	49.0	50.5	52.1	53.7	55.3	56.8	
509	49	58.4	60.0	61.5	63.1	64.6	66.2	67.8	69.3	70.9	72.4	
510	49	74.0	75.6	77.1	78.7	80.2	81.8	83.4	84.9	86.5	88.0	
511	49	89.6	91.2	92.7	94.3	95.8	97.4	99.0				
511	50				000				00.5	02.1	03.6	
512	50	05.2	06.7	08.3	09.8	11.4	12.9	14.5	16.0	17.6	19.1	
513	50	20.7	22.2	23.8	25.3	26.9	28.4	30.0	31.5	33.1	34.6	
514	50	36.2	37.7	39.3	40.8	42.4	43.9	45.5	46.0	48.6	50.1	
515	50	51.7	53.2	54.8	56.3	57.9	59.4	61.0	62.5	64.1	65.6	
516	50	67.2	68.7	70.3	71.8	73.4	74.9	76.4	78.0	79.5	81.1	
517	50	82.6	84.1	85.7	87.2	88.7	90.2	91.8	93.3	94.8	96.4	
518	50	97.9	99.4	01.0	02.7	04.7	05.0	07.7	00 ~	10.0	11.0	
518	51	12.0	14.9	01.0	02.5	04.1	05.6	07.1	08.7	10.2	11.8	
519	51	13.3	14.8	16.4	17.9	19.4	20.9	22.5	24.0	25.5	27.1	
520	51	28.6	30.1	31.7	33.2	34.7	36.2	37.8	39.3	40.8	42.4	
521 522	51	43.9	45.4	47.0	48.5	50.0	51.5	53.1	54.6	56.1	57.7 72.9	
523	51	59.2	60.7	62.2	63.8	65.3	66.8	68.3	69.8	71.4	88.2	
524	51 51	74.4 89.7	75.9 91.2	77.5 92.7	79.0 94.3	80.5 95.8	82.0 97.3	83.6 98.8	85.1	86.6	00.2	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

524 to 565mm.

1	1								1	1	ĭ	T _
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
524	52								00.3	01.9	03.4	
525	52	04.9	06.4	07.9	09.4	10.9	12.4	14.0	15.5	17.0	18.5	
526	52	20.0	21.5	23.0	24.5	26.0	27.5	29.1	30.6	32.1	33.6	
527	52	35.1	36.6	38.1	39.6	41.1	42.6	44.2	45.7	47.2	48.7	
528	52	50.2	51.7	53.2	54.7	56.2	57.7	59.3	60.8	62.3	63.8	
529	52	65.3	66.8	68.3	69.8	71.3	72.8	74.3	75.8	77.3	78.8	1 0.1
530	52	80.3	81.8	83.3	84.8	86.3	87.8	89.3	90.8	92.3	93.8	2 0.3
531	52	95.3	96.8	98.3	99.8							3 0.4
531	53					01.3	02.8	04.3	05.8	07.3	08.8	4 0.6
532	53	10.3	11.8	13.3	14.8	16.3	17.8	19.3	20.8	22.3	23.8	5 0.7
533	53	25.3	26.8	28.3	29.8	31.3	32.7	34.2	35.7	37.2	38.7	6 0.9
534	53	40.2	41.7	43.2	44.7	46.2	47.6	49.1	50.6	52.1	53.6	7 1.0
535	53	55.1	56.5	58.1	59.6	61.1	62.5	64.0	65.5	67.0	68.5	8 1.2
536	53	70.0	71.5	73.0	74.4	75.9	77.4	78.9	80.4	81.8	83.3	9   1.3
537	53	84.8	86.3	87.8	89.2	90.7	92.2	93.7	95.2	96.6	98.1	
538	53	99.6										
538	54		01.1	02.6	04.0	05.5	07.0	08.5	10.0	11.4	12.9	
539	54	14.4	15.9	17.4	18.8	20.3	21.8	23.3	24.8	26.2	27.7	
540	54	29.2	30.7	32.1	33.6	35.1	36.5	38.0	39.5	41.0	42.4	
541	54	43.9	45.4	46.8	48.3	49.8	51.2	52.7	54.2	55.7	57.1	
542	54	58.6	60.1	61.5	63.0	64.5	66.0	67.4	68.9	70.4	71.8	
543	54	73.3	74.8	76.2	77.7	79.1	80.6	82.1	83.5	85.0	86.4	
544	54	87.9	89.4	90.8	92.3	93.7	95.2	96.7	98.1	99.6		
544	55	]									01.0	
545	55	02.5	04.0	05.4	06.9	08.4	09.8	11.3	12.8	14.3	15.7	
546	55	17.2	18.7	20.1	21.6	23.0	24.5	26.0	27.4	28.9	30.3	
547	55	31.8	33.3	34.7	36.1	37.6	39.0	40.5	41.9	43.4	41.8	
548	55	46.3	47.7	49.2	50.6	52.1	53.5	55.0	56.4	57.9	59.3	
549	55	60.8	62.2	63.7	65.1	66.6	68.0	69.5	70.9	72.4	73.8	
550	55	75.3	76.7	78.2	79.6	81.1	82.5	84.0	85.4	86.9	88.3	
551	55	89.8	91.2	92.7	94.1	95.6	97.0	98.4	99.9			
551	56	1								01.3	02.8	1 0.1
552	56	04.2	05.6	07.1	08.5	10.0	11.4	12.8	14.3	15.7	17.2	2 0.3
553	56	18.6	20.0	21.5	22.9	24.4	25.8	27.2	28.7	30.1	31.6	3 0.4
554	56	33.0	34.4	35.9	37.3	38.8	40.2	41.6	43.1	44.5	46.0	4 0.6
555	56	47.4	48.8	50.3	51.7	53.1	54.5	56.0	57.4	58.8	60.3	5 0.7
556	56	61.7	63.1	64.6	66.0	67.4	68.8	70.3	71.7	73.1	74.6	6 0.9
557	56	76.0	77.4	78.9	80.3	81.7	83.1	84.6	86.0	87.4	88.9	7 1.0
558	57	90.3	91.7	93.2	94.6	96.0	97.4	98.9				8 1.2
558	57								00.3	01.7	03.2	9 1.3
559	57	04.6	06.0	07.4	08.9	10.3	11.7	13.1	14.5	16.0	17.4	
560	57	13.8	20.2	21.6	23.1	24.5	25.9	27.3	28.7	30.2	31.6	
561	57	33.0	34.4	35.8	37.3	38.7	40.1	41.5	42.9	44.4	45.8	
562	57	47.2	48.6	50.0	51.4	52.8	54.2	55.7	57.1	58.5	59.9	
563	57	61.3	62.7	61.1	65.5	66.9	68.3	69.8	71.2	72.6	74.0	
564	57	75.4	76.8	78.2	79.6	81.0	82.4	83.9	85.3	86.7	88.1	
565	57	89.5	90.9	92.4	93.8	95.2	96.6	98.0	99.4			
Barom- eter H or h	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

**565** to **605**<sup>mm</sup>.

							- 10 0	U3					
565   58	eter	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
566	Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
567	565	58									00.8	02.2	
568	566	58	03.6	05.0	06.4	07.8	09.2	10.6	12.1	13.5	14.9	16.3	
569	567	58	17.7	19.1	20.5	21.9	23.3	24.7	26.1	27.5	28.9	30.3	
570	568	58	31.7	33.1	34.5	35.9	37.3	38.7	40.1	41.5	42.9	44.3	
571	569	58		1	48.5	49.9	51.3	1		55.5			
572   58	570	l .						£		1			
572   59	1	i				1		į.	1			86.2	
573		l .	87.6	89.0	90.4	91.8	93.2	94.5	95.9	97.3	98.7		
574   59		1				_							
Second Color	1 1	1						1	}				
576	574	59	15.4	16.8	18.2	19.6	21.0	22.3	23.7	25.1	26.5	27.9	
577	575	59	29.3	30.7	32.1	33.4	34.8	36.2	37.6	39.0	40.3	41.7	
578	576	1		1									1 1 !
579		1				ł							
S80	578	59		1		74.8	1	77.6		80.4	81.7	83.1	1 1 1
580					87.2	88.6	90.0	91.3	92.7	94.1	95.5	96.8	
SS1	1	1	98.2	99.6									1 1
S82		1				1							1 1 1
583		1 1					1						
584         60         52.9         54.3         55.6         57.0         58.4         59.7         61.1         62.5         63.9         65.2           585         60         66.6         68.0         69.3         70.7         72.0         73.4         74.8         76.1         77.5         78.8           586         60         80.2         81.6         82.9         84.3         85.6         87.0         88.4         89.7         91.1         92.4           587         60         93.8         95.1         96.5         97.8         99.2           587         61         07.3         08.6         10.0         11.3         12.7         14.0         15.4         16.7         18.1         19.4           589         61         20.8         22.1         23.5         24.8         26.2         27.5         28.9         30.2         31.6         32.9           590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5				ì		ž.							1 1
585         60         66.6         68.0         69.3         70.7         72.0         73.4         74.8         76.1         77.5         78.8           586         60         80.2         81.6         82.9         84.3         85.6         87.0         88.4         89.7         91.1         92.4           587         60         93.8         95.1         96.5         97.8         99.2         00.5         01.9         03.2         04.6         05.9           587         61         07.3         08.6         10.0         11.3         12.7         14.0         15.4         16.7         18.1         19.4           589         61         20.8         22.1         23.5         24.8         26.2         27.5         28.9         30.2         31.6         32.9           590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3		1			1								9 1.2
586         60         SO.2         81.6         82.9         84.3         85.6         87.0         88.4         89.7         91.1         92.4           587         60         93.8         95.1         96.5         97.8         99.2         00.5         01.9         03.2         04.6         05.9           587         61         07.3         08.6         10.0         11.3         12.7         14.0         15.4         16.7         18.1         19.4           589         61         20.8         22.1         23.5         24.8         26.2         27.5         28.9         30.2         31.6         32.9           590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7				ł		1	l i						
587         60         93.8         95.1         96.5         97.8         99.2         00.5         01.9         03.2         04.6         05.9           588         61         07.3         08.6         10.0         11.3         12.7         14.0         15.4         16.7         18.1         19.4           589         61         20.8         22.1         23.5         24.8         26.2         27.5         28.9         30.2         31.6         32.9           590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7         76.0         77.4         78.7         80.1         81.4         82.7         84.1         85.4         86.8           594         61         201.5 <td< td=""><td></td><td>   </td><td></td><td></td><td></td><td>ł.</td><td>}</td><td></td><td></td><td></td><td></td><td></td><td></td></td<>						ł.	}						
587         61         07.3         08.6         10.0         11.3         12.7         14.0         15.4         16.7         18.1         19.4           588         61         20.8         22.1         23.5         24.8         26.2         27.5         28.9         30.2         31.6         32.9           590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7         76.0         77.4         78.7         80.1         81.4         82.7         84.1         85.4         86.8           594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8           594         62         01.5         02.8					1			87.0	88.4	89.7	91.1	92.4	
588         61         07.3         08.6         10.0         11.3         12.7         14.0         15.4         16.7         18.1         19.4           589         61         20.8         22.1         23.5         24.8         26.2         27.5         28.9         30.2         31.6         32.9           590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7         76.0         77.4         78.7         80.1         81.4         82.7         84.1         85.4         86.8           594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8           594         62         01.5         02.8			93.8	95.1	96.5	97.8	99.2	00 =	04.0	00.0	0.1.0	05.0	
589         61         20.8         22.1         23.5         24.8         26.2         27.5         28.9         30.2         31.6         32.9           590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7         76.0         77.4         78.7         80.1         81.4         82.7         84.1         85.4         86.8           594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8           594         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           595         62         01.4.9         16.2 <t< td=""><td></td><td></td><td>0** 0</td><td>00.0</td><td>100</td><td>11.0</td><td>10.5</td><td></td><td></td><td></td><td></td><td></td><td></td></t<>			0** 0	00.0	100	11.0	10.5						
590         61         34.3         35.6         37.0         38.3         39.7         41.0         42.4         43.7         45.1         46.4           591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7         76.0         77.4         78.7         80.1         81.4         82.7         84.1         85.4         86.8           594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8           594         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           595         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           596         62         14.9         16.2											1		
591         61         47.8         49.1         50.5         51.8         53.2         54.5         55.9         57.2         58.6         59.9           592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7         76.0         77.4         78.7         80.1         81.4         82.7         84.1         85.4         86.8           594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8           594         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           596         62         14.9         16.2         17.6         18.9         20.2         21.5         22.9         24.2         25.5         26.9           597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9							1				1		1
592         61         61.3         62.6         64.0         65.3         66.7         68.0         69.3         70.7         72.0         73.4           593         61         74.7         76.0         77.4         78.7         80.1         81.4         82.7         84.1         85.4         86.8           594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8           594         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           596         62         14.9         16.2         17.6         18.9         20.2         21.5         22.9         24.2         25.5         26.9           597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2													
593         61         74.7         76.0         77.4         78.7         80.1-         81.4         82.7         84.1         85.4         86.8           594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8         00.2           594         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           596         62         14.9         16.2         17.6         18.9         20.2         21.5         22.9         24.2         25.5         26.9           597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2 <td< td=""><td>11</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	11												
594         61         88.1         89.4         90.8         92.1         93.5         94.8         96.1         97.5         98.8         00.2           594         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           596         62         14.9         16.2         17.6         18.9         20.2         21.5         22.9         24.2         25.5         26.9           597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2         69.5         70.8         72.2         73.5         74.8         76.1         77.4         78.8         80.1           601         62         81.4	11										1		
594         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           596         62         14.9         16.2         17.6         18.9         20.2         21.5         22.9         24.2         25.5         26.9           597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2         69.5         70.8         72.2         73.5         74.8         76.1         77.4         78.8         80.1           601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         63         04.7	1											00.0	
595         62         01.5         02.8         04.2         05.5         06.9         08.2         09.5         10.9         12.2         13.6           596         62         14.9         16.2         17.6         18.9         20.2         21.5         22.9         24.2         25.5         26.9           597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2         69.5         70.8         72.2         73.5         74.8         76.1         77.4         78.8         80.1           601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         63         04.7	11		00.1	00.1	20.0	02.1	00.0	0		00	00.0	00.2	
596         62         14.9         16.2         17.6         18.9         20.2         21.5         22.9         24.2         25.5         26.9           597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2         69.5         70.8         72.2         73.5         74.8         76.1         77.4         78.8         80.1           601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         63         94.7         96.0         97.3         98.7         98.7         90.0         01.3         02.6         03.9         05.3         06.6           603         63			01.5	02-8	04.2	05.5	06.9	08.2	09.5	10.9	12.2		
597         62         28.2         29.5         30.9         32.2         33.6         34.9         36.2         37.6         38.9         40.3           598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2         69.5         70.8         72.2         73.5         74.8         76.1         77.4         78.8         80.1           601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         62         94.7         96.0         97.3         98.7         98.7         90.0         01.3         02.6         03.9         05.3         06.6           603         63         07.9         09.2         10.5         11.9         13.2         14.5         15.8         17.1         18.5         19.8           604         63	11												
598         62         41.6         42.9         44.3         45.6         46.9         48.2         49.6         50.9         52.2         53.6           599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2         69.5         70.8         72.2         73.5         74.8         76.1         77.4         78.8         80.1           601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         62         94.7         96.0         97.3         98.7         98.7         99.4         90.7         92.0         93.4           602         63         07.9         09.2         10.5         11.9         13.2         14.5         15.8         17.1         18.5         19.8           604         63         21.1         22.4         23.7         25.1         26.4         27.7         29.0         30.3         31.7         33.0           605         63         34.3         35.6	- 11												
599         62         54.9         56.2         57.6         58.9         60.2         61.5         62.9         64.2         65.5         66.9           600         62         68.2         69.5         70.8         72.2         73.5         74.8         76.1         77.4         78.8         80.1           601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         62         94.7         96.0         97.3         98.7         00.0         01.3         02.6         03.9         05.3         06.6           603         63         07.9         09.2         10.5         11.9         13.2         14.5         15.8         17.1         18.5         19.8           604         63         21.1         22.4         23.7         25.1         26.4         27.7         29.0         30.3         31.7         33.0           605         63         34.3         35.6         36.9         38.2         39.5         40.8         42.2         43.5         44.8         46.1     Parts  for each	- 11		1							- 1			
601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         62         94.7         96.0         97.3         98.7         00.0         01.3         02.6         03.9         05.3         06.6           603         63         07.9         09.2         10.5         11.9         13.2         14.5         15.8         17.1         18.5         19.8           604         63         21.1         22.4         23.7         25.1         26.4         27.7         29.0         30.3         31.7         33.0           605         63         34.3         35.6         36.9         38.2         39.5         40.8         42.2         43.5         44.8         46.1    Barone eter	19									- 1			
601         62         81.4         82.7         84.1         85.4         86.7         88.0         89.4         90.7         92.0         93.4           602         62         94.7         96.0         97.3         98.7         00.0         01.3         02.6         03.9         05.3         06.6           603         63         07.9         09.2         10.5         11.9         13.2         14.5         15.8         17.1         18.5         19.8           604         63         21.1         22.4         23.7         25.1         26.4         27.7         29.0         30.3         31.7         33.0           605         63         34.3         35.6         36.9         38.2         39.5         40.8         42.2         43.5         44.8         46.1    Barone eter	600	62	68.2	69.5	70.8	72.2	73.5	74.8	76.1	77.4	78.8	80.1	
602         62         94.7         96.0         97.3         98.7         00.0         01.3         02.6         03.9         05.3         06.6           603         63         07.9         09.2         10.5         11.9         13.2         14.5         15.8         17.1         18.5         19.8           604         63         21.1         22.4         23.7         25.1         26.4         27.7         29.0         30.3         31.7         33.0           605         63         34.3         35.6         36.9         38.2         39.5         40.8         42.2         43.5         44.8         46.1           Barometer eter         N.         0.0         0.1         0.2         0.3         0.4         0.5         0.6         0.7         0.8         0.9         Parts for each	00-	1			0.4		00.0				1		
602         63         07.9         09.2         10.5         11.9         13.2         14.5         15.8         17.1         18.5         19.8           604         63         21.1         22.4         23.7         25.1         26.4         27.7         29.0         30.3         31.7         33.0           605         63         34.3         35.6         36.9         38.2         39.5         40.8         42.2         43.5         44.8         46.1		1 1											
CO3   63   07.9   09.2   10.5   11.9   13.2   14.5   15.8   17.1   18.5   19.8   604   63   21.1   22.4   23.7   25.1   26.4   27.7   29.0   30.3   31.7   33.0   605   63   34.3   35.6   36.9   38.2   39.5   40.8   42.2   43.5   44.8   46.1     Barometer   N.   O.O   O.1   O.2   O.3   O.4   O.5   O.6   O.7   O.8   O.9   Parts for each							00.0	01.3	02.6	03.9	05.3	06.6	
604     63     21.1     22.4     23.7     25.1     26.4     27.7     29.0     30.3     31.7     33.0       605     63     34.3     35.6     36.9     38.2     39.5     40.8     42.2     43.5     44.8     46.1       Barom: eter       N.     0.0     0.1     0.2     0.3     0.4     0.5     0.6     0.7     0.8     0.9     Parts for each for ea	11		07.9	09.2	10.5	11.9							
605         63         34.3         35.6         36.9         38.2         39.5         40.8         42.2         43.5         44.8         46.1           Barom- eter         N.         0.0         0.1         0.2         0.3         0.4         0.5         0.6         0.7         0.8         0.9         Parts for each fo				1							1		
eter N. 0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 for each						1			1	i			
O.UIMM			0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

606 to 647mm.

Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli. 606	Metr. 63	Metres.	Metres, 48.7	Metres. 50.0	Metres, 51.3	Metres. 52.6	Metres.	Metres. 55.3	Metres. 56.6	Metres. 57.9	Metres. 59.2	Metr.
607	63	60.5	61.8	63.1	64.5	65.8	53.9 67.1	68.4	69.7	71.1	72.4	
608	63	73.7	75.0	,	77.6		ŧ.		82.8	84.1	85.4	
609	63	86.7	88.0	76.3		78.9	80.2	81.5	95.9	97.2	98.5	
610		99.8	88.0	89.3	90.6	91.9	93.2	94.6	99.9	91.4	30.9	
610	63	99.5	01.1	09.4	09.7	05.0	06.9	07.6	08.9	10.2	11.5	
611	64	12.8	14.1	02.4	03.7	05.0	06 3	07.6 20.7	22.0	23.3	24.6	
612	64	25.9	27.2	$15.4 \\ 28.5$	16.7 29.8	31.1	19.3 32.4	33.7	35.0	36.3	37.6	
613		38.9	40.2	41.5	42.8		1		48.0	49.3	50.6	
614	64	51.9	53.2			44.1	45.4	46.7	60.9	62.2	63.5	
	64	1	66.1	54.5	55.8	57.1	58.3	59.6 72.5	73.8	75.1	76.4	
615	64	64.8	79.0	67.4	68.7	70.0	71.2		86.8	88.1	89.4	
616	64	77.7	i .	80.3	81.6	82.9	84.2	85.5		55.1	39.4	
617	64	90.7	92.0	93.3	94.6	95.9	97.1	98.4	99.7	01.0	00.0	
617	65	02.0	010	00.0	07.4	00 ~	10.0	11.0	19.6	01.0	02.3 15.1	
618	65	03.6	04.9	06.2	07.4	08.7	10.0	11.3	12.6	13.8		
619	65	16.4	17.7	19.0	20.3	21.6	22.8	24.1	25.4	26.7	28.0 40.8	
620	65	29.3	30.6	31.9	33.1	34.4	35.7	37.0	38.3	39.5		1   0.1
621	65	42.1	43.4	44.7	45.9	47.2	48.5	49.8	51.1	52.3	53.6	$\begin{bmatrix} 1 & 0.1 \\ 2 & 0.2 \end{bmatrix}$
622	65	54.9	56.2	57.5	58.7	60.0	61.3	62.6	63.9	65.1	66.4	
623	65	67.7	69.0	70.3	71.5	72.8	74.1	75.4	76.7	77.9	79.2	3 0.4
624	65	80.5	81.8	83.0	84.3	85.6	86.8	88.1	89.4	90.7	91.9	4 0.5
-2.5					2 2							$\begin{bmatrix} 5 & 0.6 \\ c & 0.6 \end{bmatrix}$
625	65	93.2	94.5	95.8	97.0	98.3	99.6		00.0	00.		6 0.8
625	66		0	00.4	00.0			00.9	02.2	03.4	04.7	7 0.9
626	66	06.0	07.3	08.5	09.8	11.1	12.3	13.6	14.9	16.2	17.4	8 1.0
627	66	18.7	20.0	21.2	22.5	23.8	25.0	26.3	27.6	28.9	30.1	9 1.1
628	66	31.4	32.7	33.9	36.2	56.4	37.7	39.0	40.2	41.5	42.7	
629	66	44.0	45.3	46.5	47.8	49.1	50.3	51.6	52.9	54.2	55.4	
630	66	56.7	58.0	59.2	60.5	61.7	63.0	64.3	65.5	66.8	68.0	
631	66	69.3	70.6	71.8	73.1	74.4	75.6	76.9	78.2	79.5	80.7	
632	66	82.0	83.2	84.5	85.7	87.0	88.2	89.5	90.7	92.0	93.2	
633	66	94.5	95.8	97.0	98.3	99.5						
633	67						00.8	02.1	03.3	04.6	05.8	
634	67	07.1	08.4	09.6	10.9	12.1	13.4	14.7	15.9	17.2	18.4	
635	67	19.7	20.9	22.2	23.4	24.7	25.9	27.2	28.4	29.7	30.9	
636	67	32.2	33.4	34.7	35.9	37.2	38.4	39.7	40.9	42.2	43.4	
637	67	44.7	45.9	47.2	48.4	49.7	50.9	52.2	53.4	54.7	55.9	
638	67	57.2	58.4	59.7	60.9	62.2	63.4	64.7	65.9	67.2	68.4	
639	67	69.7	70.9	72.2	73.4	74.7	75.9	77.1	78.4	79.6	80.9	
640	67	82.1	83.3	84.6	85.8	87.1	88.3	89.6	90.8	92.1	93.3	
641	67	94.6	95.8	97.1	98.3	99.6						
641	68						00.8	02.0	03.3	04.5	05.8	
642	68	07.0		09.5	10.7	1	13.2	14.4	15.7	16.9	18.2	
643	68	19.4	20.6	21.9	23.1	24.3	25.5	26.8	28.0	29.2	30.5	
644	68	31.7	32.9	34.2	35.4	36.7	37.9	39.1	40.4	41.6	42.9	
645	68	44.1	45.3	46.6	47.8	49.0	50.2	51.5	52.7	53.9	55.2	
646	68	56.4	57.6	58.9	60.1	61.3	62.5	63.8	65.0	66.2	67.5	
647	68	68.7	69.9	71.2	72.4	73.6	74.8	76.1	77.3	78.5	79.8	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm

648 to 689mm.

Here   N.   O.O   O.1   O.2   O.3   O.4   O.5   O.6   O.7   O.S   O.9   O.6   O.7	-	1			1	,	10 0			· · · · · · · · · · · · · · · · · · ·	1		1
649	eter	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
649   68   93.3   94.5   95.8   97.0   98.2   99.4   00.7   01.9   03.1   04.4     659   69   69   69   69   69   69   69	Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
649   69	648	68	81.0	82.2	83.5	84.7	85.9	87.1	88.4	89.6	90.8	92.1	
650	649	68	93.3	94.5	95.8	97.0	98.2	99.4					
651	649	69							00.7	01.9	03.1	04.4	
652	650	69	05.6	06.8	08.0	09.3	10.5	11.7	12.9	14.1	15.4	16.6	
653	651	69	1	19.0	20.2	21.5	22.7	23.9	25.1	26.3	27.6	28.8	
654   69						1		ı	1		1		
655	1	1					1		i				
656			1			1							
657					1			ı	i				
657   70		)	Į.			1					88.5	89.7	
658	1		90.9	92.1	93.3	94.5	95.7	96.9	98.2	99.4	00.0		
659			000 0	0.00	05.	00.0	0=0	00.0	70.0	,,, -			
660		1	l .			i	1						
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665		1			1	1	1		1				
666         70         99.2         00.4         01.6         02.8         04.0         05.2         06.4         07.6         08.8         10.0         8         1.         7         0.6         667         71         11.2         12.4         13.6         14.8         16.0         17.1         18.3         19.5         20.7         21.9         9         1.           668         71         23.1         24.3         25.5         26.7         27.9         29.0         30.2         31.4         32.6         33.8         36.9         40.9         42.1         43.3         44.5         45.7         66.0         67.0         71         46.9         48.1         49.3         50.5         51.7         52.8         54.0         55.2         56.4         57.6         671         71         58.8         60.0         61.2         62.3         63.5         64.7         65.9         67.1         68.2         69.4           672         71         70.6         71.8         73.0         74.2         75.4         76.5         77.7         78.9         80.1         81.3           673         71         94.3         95.5         96.7         97.8 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>													
666         71         0.0.4         01.6         02.8         04.0         05.2         06.4         07.6         08.8         10.0         8         1.667         71         11.2         12.4         13.6         14.8         16.0         17.1         18.3         19.5         20.7         21.9         9         1.668         71         23.1         24.3         25.5         26.7         27.9         29.0         30.2         31.4         32.6         33.8         669         71         35.0         36.2         37.4         38.6         39.8         40.9         42.1         43.3         44.5         45.7         670         71         46.9         48.1         49.3         50.5         51.7         52.8         54.0         55.2         56.4         57.6         671         71         70.6         71.8         73.0         74.2         75.4         76.5         77.7         78.9         80.1         81.3         673         71         82.5         83.7         84.9         86.0         87.2         88.4         89.6         90.8         91.9         93.1         40.9         40.2         41.4         15.5         16.7         72.7         77.9         99.1 <td< td=""><td></td><td>1</td><td></td><td>00.4</td><td>00.0</td><td>30.0</td><td>32.0</td><td>90.2</td><td>34.4</td><td>33.0</td><td>30.0</td><td>30.0</td><td></td></td<>		1		00.4	00.0	30.0	32.0	90.2	34.4	33.0	30.0	30.0	
667         71         11.2         12.4         13.6         14.8         16.0         17.1         18.3         19.5         20.7         21.9         9         1.           668         71         23.1         24.3         25.5         26.7         27.9         29.0         30.2         31.4         32.6         33.8           669         71         35.0         36.2         37.4         38.6         39.8         40.9         42.1         43.3         44.5         45.7           670         71         46.9         48.1         49.3         50.5         51.7         52.8         54.0         55.2         56.4         57.6           671         71         58.8         60.0         61.2         62.3         63.5         64.7         65.9         67.1         68.2         69.4           672         71         70.6         71.8         73.0         74.2         75.4         76.5         77.7         78.9         80.1         81.3           673         71         82.5         83.7         84.9         86.0         87.2         88.4         89.6         90.8         91.9         93.1           674         72<			33.2	1,00	01.6	02.8	010	05.2	06.4	07.6	08.8	10.0	
668         71         23.1         24.3         25.5         26.7         27.9         29.0         30.2         31.4         32.6         33.8           669         71         35.0         36.2         37.4         38.6         39.8         40.9         42.1         43.3         44.5         45.7           670         71         46.9         48.1         49.3         50.5         51.7         52.8         54.0         55.2         56.4         57.6           671         71         58.8         60.0         61.2         62.3         63.5         64.7         65.9         67.1         68.2         69.4           672         71         70.6         71.8         73.0         74.2         75.4         76.5         77.7         78.9         80.1         81.3           673         71         82.5         83.7         84.9         86.0         87.2         88.4         89.6         90.8         91.9         93.1           674         71         94.3         95.5         96.7         97.8         99.0         00.2         01.4         02.6         03.7         04.9           674         72         19.1	- {	1	11.2			i .			1	Ī			1 1
669         71         35.0         36.2         37.4         38.6         39.8         40.9         42.1         43.3         44.5         45.7           670         71         46.9         48.1         49.3         50.5         51.7         52.8         54.0         55.2         56.4         57.6           671         71         58.8         60.0         61.2         62.3         63.5         64.7         65.9         67.1         68.2         69.4           672         71         70.6         71.8         73.0         74.2         75.4         76.5         77.7         78.9         80.1         81.3           673         71         82.5         83.7         84.9         86.0         87.2         88.4         89.6         90.8         91.9         93.1           674         72         06.1         07.3         08.5         09.6         10.8         12.0         13.2         14.4         15.5         16.7           674         72         29.7         30.9         32.0         33.2         34.4         35.5         36.7         37.9         39.1         40.2           675         72         29.7									1				0   1.1
670         71         46.9         48.1         49.3         50.5         51.7         52.8         54.0         55.2         56.4         57.6         671         71         58.8         60.0         61.2         62.3         63.5         64.7         65.9         67.1         68.2         69.4           672         71         70.6         71.8         73.0         74.2         75.4         76.5         77.7         78.9         80.1         81.3           673         71         82.5         83.7         84.9         86.0         87.2         88.4         89.6         90.8         91.9         93.1           674         71         94.3         95.5         96.7         97.8         99.0         00.2         01.4         02.6         03.7         04.9           674         72         06.1         07.3         08.5         09.6         10.8         12.0         13.2         14.4         15.5         16.7           674         72         17.9         19.1         20.3         21.4         22.6         23.8         25.0         26.2         27.3         28.5           677         72         29.7         30.9         <	1	1										1	
671													
672         71         70.6         71.8         73.0         74.2         75.4         76.5         77.7         78.9         80.1         81.3         86.0         87.2         88.4         89.6         90.8         91.9         93.1         93.1         674         71         94.3         95.5         96.7         97.8         99.0         00.2         01.4         02.6         03.7         04.9         04.9         675         72         06.1         07.3         08.5         09.6         10.8         12.0         13.2         14.4         15.5         16.7         676         72         17.9         19.1         20.3         21.4         22.6         23.8         25.0         26.2         27.3         28.5         677         72         29.7         30.9         32.0         33.2         34.4         35.5         36.7         37.9         39.1         40.2         678         72         41.4         42.6         43.8         44.9         46.1         47.3         48.5         49.7         50.8         52.0         66.2         67.7         71.9         73.1         74.3         75.4         75.4         681         72         64.9         66.1         67.2 <t< td=""><td>1</td><td>1</td><td>58.8</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td></t<>	1	1	58.8								1		
674         71         94.3         95.5         96.7         97.8         99.0         00.2         01.4         02.6         03.7         04.9           675         72         06.1         07.3         08.5         09.6         10.8         12.0         13 2         14.4         15.5         16.7           676         72         17.9         19.1         20.3         21.4         22.6         23.8         25.0         26.2         27.3         28.5           677         72         29.7         30.9         32.0         33.2         34.4         35.5         36.7         37.9         39.1         40.2           678         72         41.4         42.6         43.8         44.9         46.1         47.3         48.5         49.7         50.8         52.0           679         72         53.2         54.4         55.5         56.7         57.9         59.0         60.2         61.4         62.6         63.7           680         72         64.9         66.1         67.2         68.4         69.6         70.7         71.9         73.1         74.3         75.4           681         72         76.6	1		70.6	1						1		· ·	
674 72	673	71	82.5	83.7	84.9	86.0	87.2	88.4		90.8	91.9	93.1	
675	674	71	94.3	95.5	96.7	97.8	99.0						
676         72         17.9         19.1         20.3         21.4         22.6         23.8         25.0         26.2         27.3         28.5           677         72         29.7         30.9         32.0         33.2         34.4         35.5         36.7         37.9         39.1         40.2           678         72         41.4         42.6         43.8         44.9         46.1         47.3         48.5         49.7         50.8         52.0           679         72         53.2         54.4         55.5         56.7         57.9         59.0         60.2         61.4         62.6         63.7           680         72         64.9         66.1         67.2         68.4         69.6         70.7         71.9         73.1         74.3         75.4           681         72         76.6         77.8         78.9         80.1         81.3         82.4         83.6         84.8         86.0         87.1         1         0.1           682         72         88.3         89.5         90.6         91.8         93.0         94.1         95.3         96.5         97.7         98.8         2         0.2	674	72						00.2	01.4	02.6	03.7	04.9	
677	675	72	06.1	07.3	08.5	09.6	10.8	12.0	13 2	14.4	15.5	16.7	
678	676	72		19.1	20.3	21.4	22.6	23.8	25.0	26.2	27.3	28.5	
679         72         53.2         54.4         55.5         56.7         57.9         59.0         60.2         61.4         62.6         63.7           680         72         64.9         66.1         67.2         68.4         69.6         70.7         71.9         73.1         74.3         75.4           681         72         76.6         77.8         78.9         80.1         81.3         82.4         83.6         84.8         86.0         87.1         1         0.1           682         72         88.3         89.5         90.6         91.8         93.0         94.1         95.3         96.5         97.7         98.8         2         0.2           683         73         00.0         01.2         02.3         03.5         04.6         05.8         07.0         08.1         09.3         10.4         3         0.5           684         73         11.6         12.8         13.9         15.1         16.2         17.4         18.6         19.7         20.9         22.0         4         0.5           685         73         23.2         24.4         25.5         26.7         27.8         29.0         30.2	677	72	29.7	30.9	32.0	33.2	34.4	35.5	36.7	37.9	39.1	40.2	
680         72         64.9         66.1         67.2         68.4         69.6         70.7         71.9         73.1         74.3         75.4           681         72         76.6         77.8         78.9         80.1         81.3         82.4         83.6         84.8         86.0         87.1         1         0.1         0.6         91.8         93.0         94.1         95.3         96.5         97.7         98.8         2         0.2         683         73         00.0         01.2         02.3         03.5         04.6         05.8         07.0         08.1         09.3         10.4         3         0.6         684         73         11.6         12.8         13.9         15.1         16.2         17.4         18.6         19.7         20.9         22.0         4         0.5         685         73         23.2         24.4         25.5         26.7         27.8         29.0         30.2         31.3         32.5         33.6         5         0.6           687         73         34.8         36.0         37.1         38.3         39.4         40.6         41.8         42.9         44.1         45.2         6         0.7 <t< td=""><td>678</td><td>72</td><td>41.4</td><td>42.6</td><td>43.8</td><td>44.9</td><td>46.1</td><td>47.3</td><td>48.5</td><td>49.7</td><td>50.8</td><td>52.0</td><td></td></t<>	678	72	41.4	42.6	43.8	44.9	46.1	47.3	48.5	49.7	50.8	52.0	
681 72 76.6 77.8 78.9 80.1 81.3 82.4 83.6 84.8 86.0 87.1 1 0.1 682 72 88.3 89.5 90.6 91.8 93.0 94.1 95.3 96.5 97.7 98.8 2 0.2 683 73 00.0 01.2 02.3 03.5 04.6 05.8 07.0 08.1 09.3 10.4 3 0.3 684 73 11.6 12.8 13.9 15.1 16.2 17.4 18.6 19.7 20.9 22.0 4 0.5 685 73 23.2 24.4 25.5 26.7 27.8 29.0 30.2 31.3 32.5 33.6 5 0.6 686 73 34.8 36.0 37.1 38.3 39.4 40.6 41.8 42.9 44.1 45.2 6 0.7 687 73 46.4 47.6 48.7 49.9 51.0 52.2 53.4 54.5 55.7 56.8 7 0.8 688 73 58.0 59.2 60.3 61.5 62.6 63.8 65.0 66.1 67.3 68.4 8 0.5 689 73 69.6 70.7 71.9 73.0 74.2 75.3 76.5 77.6 78.8 79.9 9 1.1 8 6 689 73 69.6 70.7 71.9 73.0 74.2 75.3 76.5 77.6 78.8 79.9 9 1.1	1	72		54.4		1	57.9	59.0	60.2		62.6	63.7	
682         72         88.3         89.5         90.6         91.8         93.0         94.1         95.3         96.5         97.7         98.8         2 0.2           683         73         00.0         01.2         02.3         03.5         04.6         05.8         07.0         08.1         09.3         10.4         3 0.5           684         73         11.6         12.8         13.9         15.1         16.2         17.4         18.6         19.7         20.9         22.0         4 0.5           685         73         23.2         24.4         25.5         26.7         27.8         29.0         30.2         31.3         32.5         33.6         5 0.6           686         73         34.8         36.0         37.1         38.3         39.4         40.6         41.8         42.9         44.1         45.2         6 0.7           687         73         46.4         47.6         48.7         49.9         51.0         52.2         53.4         54.5         55.7         56.8         7 0.8           688         73         58.0         59.2         60.3         61.5         62.6         63.8         65.0         66.1	1			1					1	1	- 1		
683         73         00.0         01.2         02.3         03.5         04.6         05.8         07.0         08.1         09.3         10.4         3         0.5           684         73         11.6         12.8         13.9         15.1         16.2         17.4         18.6         19.7         20.9         22.0         4         0.5           685         73         23.2         24.4         25.5         26.7         27.8         29.0         30.2         31.3         32.5         33.6         5         0.6           687         73         34.8         36.0         37.1         38.3         39.4         40.6         41.8         42.9         44.1         45.2         6         0.7           687         73         46.4         47.6         48.7         49.9         51.0         52.2         53.4         54.5         55.7         56.8         7         0.8           688         73         58.0         59.2         60.3         61.5         62.6         63.8         65.0         66.1         67.3         68.4         8         0.5           689         73         69.6         70.7         71.9	- 1		1						1	- 1			1   0.1
684         73         11.6         12.8         13.9         15.1         16.2         17.4         18.6         19.7         20.9         22.0         4         0.6           685         73         23.2         24.4         25.5         26.7         27.8         29.0         30.2         31.3         32.5         33.6         5         0.6           686         73         34.8         36.0         37.1         38.3         39.4         40.6         41.8         42.9         44.1         45.2         6         0.7           687         73         46.4         47.6         48.7         49.9         51.0         52.2         53.4         54.5         55.7         56.8         7         0.8           688         73         58.0         59.2         60.3         61.5         62.6         63.8         65.0         66.1         67.3         68.4         8         0.5           689         73         69.6         70.7         71.9         73.0         74.2         75.3         76.5         77.6         78.8         79.9         9         1.1           Baromingteler         N.         0.0         0.1         0.2		- 1		1		- 1	- 1			i	1		)
685         73         23.2         24.4         25.5         26.7         27.8         29.0         30.2         31.3         32.5         33.6         5         0.6           686         73         34.8         36.0         37.1         38.3         39.4         40.6         41.8         42.9         44.1         45.2         6         0.7           687         73         46.4         47.6         48.7         49.9         51.0         52.2         53.4         54.5         55.7         56.8         7         0.8           688         73         58.0         59.2         60.3         61.5         62.6         63.8         65.0         66.1         67.3         68.4         8         0.8           689         73         69.6         70.7         71.9         73.0         74.2         75.3         76.5         77.6         78.8         79.9         9         1.1           Barom. Peter         N.         0.0         0.1         0.2         0.3         0.4         0.5         0.6         0.7         0.8         0.9         Parts for each for each for each for each for each for each for each for each for each for each for each for each for each for each for each for each f	11	1	- 1		- 1						1		1 1
686     73     34.8     36.0     37.1     38.3     39.4     40.6     41.8     42.9     44.1     45.2     6     0.7       687     73     46.4     47.6     48.7     49.9     51.0     52.2     53.4     54.5     55.7     56.8     7     0.8       688     73     58.0     59.2     60.3     61.5     62.6     63.8     65.0     66.1     67.3     68.4     8     0.5       689     73     69.6     70.7     71.9     73.0     74.2     75.3     76.5     77.6     78.8     79.9     9     1.1       Barom-reter     N.     0.0     0.1     0.2     0.3     0.4     0.5     0.6     0.7     0.8     0.9     Parts (or each for	31			l l				,			· · · · · · · · · · · · · · · · · · ·		1 1
687 73 46.4 47.6 48.7 49.9 51.0 52.2 53.4 54.5 55.7 56.8 7 0.6 688 73 58.0 59.2 60.3 61.5 62.6 63.8 65.0 66.1 67.3 68.4 8 0.5 689 73 69.6 70.7 71.9 73.0 74.2 75.3 76.5 77.6 78.8 79.9 9 1.1 8arom-geter N. 0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 Parts for each for e	11			1		- 1		1					5 0.6
688 73 58.0 59.2 60.3 61.5 62.6 63.8 65.0 66.1 67.3 68.4 8 0.9 689 73 69.6 70.7 71.9 73.0 74.2 75.3 76.5 77.6 78.8 79.9 9 1.1 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	- 1												
689 73 69.6 70.7 71.9 73.0 74.2 75.3 76.5 77.6 78.8 79.9 9 1.1  Barom. eter N. 0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 Parts for each	-			1		i		1			1	1	1 1
eter N. 0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 for each											í		8   0.9   9   1.1
the state of the s		 N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.0	Parts
	H or h.		0.0	0.1	0.2	0.0	0.4	0.5	0.0	0.7	0.8		for each 0.01mm.

690 to 730mm.

					000	to 7						
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
690	73	81.1	82.3	83.4	84.6	85.7	86.9	88.1	89.2	90.4	91.5	
691	73	92.7	93.8	95.0	96.1	97.3	98.4	99.6				
691	74								00.7	01.9	03.0	
692	74	04.2	05.3	06.5	07.6	08.8	09.9	11.1	12.2	13.4	14.5	
693	74	15.7	16.8	18.0	19.1	20.3	21.4	22.6	23.7	24.9	26.0	
694	74	27.2	28.3	29.5	30.6	31.8	32.9	34.1	35.2	36.4	37.5	
695	74	38.7	39.8	41.0	42.1	43.3	44.4	45.5	46.7	47.8	49.0	
696	74	50.1	51.2	52.4	53.5	54.7	55.8	56.9	58.1	59.2	60.4	
697	74	61.5	62.6	63.8	64.9	66.1	67.2	68.3	69.5	70.6	71.8	
698	74	72.9	74.0	75.2	76.3	77.5	78.6	79.7	80.9	82.0	83.2	
699	74	84.3	85.4	86.6	87.7	88.9	90.0	91.1	92.3	93.4	94.6	
700	74	95.7	96.8	98.0	99.1							
700	75					00.3	01.4	02.5	03.7	04.8	06.0	
701	75	07.1	08.2	09.4	10.5	11.6	12.7	13.9	15.0	16.1	17.3	
702	75	18.4	19.5	20.7	21.8	23.0	24.1	25.2	26.4	27.5	28.7	
703	75	29.8	30.9	32.1	33.2	34.3	35.4	36.6	37.7	38.8	40.0	
704	75	41.1	42.2	43.4	44.5	45.6	46.7	47.9	49.0	50.1	51.3	
705	75	52.4	53.5	54.7	55.8	56.9	58.0	59.2	60.3	61.4	62.6	
706	75	63.7	64.8	66.0	67.1	68.2	69.3	70.5	71.6	72.7	73.9	
707	75	75.0	76.1	77.2	78.4	79.5	80.6	81.7	82.8	84.0	85.1	
708	75	86.2	87.3	88.5	89.6	90.7	91.8	93.0	94.1	95.2	96.4	
709	75	97.5	98.6	99.7								
709	76				00.9	02.0	03.1	04.2	05.3	06.5	07.6	
710	76	08.7	09.8	10.9	12.1	13.2	14.3	15.4	16.5	17.7	18.8	
711	76	19.9	21.0	22.1	23.3	24.4	25.5	26.6	27.7	28.9	30.0	
712	76	31.1	32.2	33.3	34.4	35.5	36.6	37.8	38.9	40.0	41.1	1 0.1
713	76	42.2	43.3	44.4	45.6	46.7	47.8	48.9	50.0	51.2	52.3	2 0.2
714	76	53.4	54.5	55.6	56.8	57.9	59.0	60.1	61.2	62.4	63.5	3 0.3
715	76	64.6	65.7	66.8	67.9	69.0	70.1	71.3	72.4	73.5	74.6	4 0.4
716	76	75.7	76.8	77.9	79.0	80.1	81.2	82.4	83.5	84.6	85 7	5 0.5
717	76	86.8	87.9	89.0	90.1	91.2	92.3	93.5	94.6	95.7	96.8	6 0.7
718	76	97.9	99.0									7 0.8
718	77			00.1	01.2	02.3	03.4	04.6	05.7	06.8	07.9	8 0.9
719	77	09.0	10.1	11.2	12.3	13.4	14.5	15.7	16.8	17.9	19.0	9   1.0
720	77	20.1	21.2	22.3	23.4	24.5	25.6	26.7	27.8	28.9	30.0	
721	77	31.1	32.2	33.3	34.4	35.5	36.6	37.7	38.8	39.9	41.0	
722	77	42.1	43.2	44.3	45.4	46.5	47.6	48.7	49.8	50.9	52.0	
723	77	53.1	54.2	55.3	56.4	57.5	58.6	59.8	60.9	62.0	63.1	
724	77	64.2	65.3	66.4	67.5	68.6	69.6	70.7	71.8	72.9	74.0	
725	77	75.1	76.2	77.3	78.4	79.5	80.6	81.7	82.8	83.9	85.0	
726	77	86.1	87.2	88.3	89.4	90.5	91.6	92.7	93.8	94.9	96.0	
727	77	97.1	98.2	99.3	0.0			22.5	0.1.5	0.7.5		
727	78		1		00.4	01.5	02.5	03.6	04.7	05.8	06.9	
728	78	08.0	09.1	10.2	11.3	12.4	13 5	14.6	15.7	16.8	17.9	
729	78	19.0	20.1	21.2	22.3	23.4	24.4	25.5	26.6	27.7	28.8	
730	78	29.9	31.0	32.1	33.3	34.3	35.3	36.4	37.5	38.6	39.7	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm

731 to 770<sup>mm</sup>.

Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres	Metr.
731	78	40.8	41.9	43.0	44.1	45.2	46.2	47.3	48.4	49.5	50.6	
732	78	51.7	52.8	53.9	54.9	56.0	57.0	58.2	59.3	60.3	61.4	
733	78	62.5	63.6	64.7	65.8	66.9	67.9	69.0	70.1	71.2	72.3	:
734	78	73.4	74.5	75.6	76.6	77.7	78.8	79.9	81.0	82.0	83.1	
735	78	84.2	85.3	86.4	87.5	88.6	89.6	90.7	91.8	92.9	94.0	
736	78	95.1	96.2	97.3	98.3	99.4						
736	79						00.5	01.6	02.7	03.7	04.8	
737	79	05.9	07.0	08.1	09.1	10.2	11.3	12.4	13.5	14.5	15.6	
738	79	16.7	17.8	18.9	.19.9	21.0	22.1	23.2	24.3	25.3	26.4	
739	79	27.5	28.6	29.6	30.7	31.8	32.8	33.9	35.0	36.1	37.1	
740	79	38.2	39.3	40.4	41.4	42.5	43.6	44.7	45.8	46.8	47.9	
741	79	49.0	50.1	51.1	52.2	53.3	54.3	55.4	56.5	57.6	58.6	
742	79	59.7	60.8	61.8	62.9	64.0	65.0	66.1	67.2	68.3	69.3	
743	79	70.4	71.5	72.6	73.6	74.7	75.8	76.9	78.0	79.0	80.1	
744	79	81.2	82.3	83.3	84.4	85.5	86.5	87.6	88.7	89.8	90.8	ļ
745	79	91.9	93.0	94.0	95.1	96.1	97.2	98.3	99.3			
745	80									00.4	01.4	
746	80	02.5	03.6	04.6	05.7	06.8	07.8	08.9	10.0	11.1	12.3	
747	80	13.2	14.3	15.3	16.4	17.4	18.5	19.6	20.6	21.7	22.7	
748	80	23.8	24.9	25.9	27.0	28.0	29.1	30.2	31.2	32.3	33.3	
749	80	34.4	35.5	36.5	37.6	38.7	39.7	40.8	41.9	43.0	44.0	
750	80	45.1	46.2	47.3	48.4	49.4	50.5	51.6	52.6	53.7	54.7	
751	80	55.7	56.8	57.8	58.9	59.9	61.0	62.1	63.1	64.2	65.2	
752	80	66.3	67.4	68.4	69.5	70.5	71.6	72.7	73.7	74.8	75.8	
753	80	76.9	78.0	79.0	80.1	81.1	82.2	83.3	84.3	85.4	86.4	
754	80	87.5	88.5	89.6	90.6	91.7	92.7	93.8	94.8	95.9	96.9	1   0.1
755	80	98.0	99.1									2 0.2
755	81		Ì	00.1	01.2	02.2	03.3	04.4	05.4	06.5	07.5	3 0.3
756	81	08.6	09.6	10.7	11.7	12.8	13.8	14.9	15.9	17.0	18.0	4 0.4
757	81	19.1	20.1	21.2	22.2	23.3	24.3	25.4	26.4	27.5	28.5	5 0.5
758	81	29.6	30.6	31.7	32.7	33.8	34.8	35.9	36.9	38.0	39.0	6 0.6
759	81	40.1	41.1	42.2	43.2	44.3	45.3	46.4	47.4	48.5	49.5	7 0.7
760	81	50.6	51.6	52.7	53.7	54.8	55.8	56.9	57.9	59.0	60.0	8 0.8 9 0.9
761	81	61.1	62.1	63.2	64.2	65.3	66.3	67.3	68.4	69.4	70.5	
762	81	71.5	72.5	73.6	74.6	75.7	76.7	77.8	78.8	79.9	80.9	
763	81	82.0	83.0	84.1	85.1	86.2	87.2	88.2	89.3	90.3	91.4	
764	81	92.4	93.4	94.5	95.5	96.6	97.6	98.6	99.7			
764	82									00.7	01.8	
765	82	02.8	03.8	04.9	05.9	07.0	08.0	09.0	10.1	11.1	12.2	
766	82	13.2	14.2	15.3	16.3	17.4	18.4	19.4	20.5	21.5	22.6	
767	82	23.6	24.6	25.7	26.7	27.8	28.8	29.8	30.9	31.9	33.0	
768	82	34.0	35.0	36.1	37.1	38.2	39.2	40.2	41.3	42.3	43.4	
769	82	44.4	45.4	46.5	47.5	48.5	49.5	50.6	51.6	52.6	53.7	
770	82	54.7	55.7	56.8	57.8	58.8	59.8	60.9	61.9	62.9	64.0	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
D "						28						

771 to 810mm.

-					771	to 8	10 <sup>mm</sup> .					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
771	82	65.0	66.0	67.1	68.1	69.2	70.2	71.2	72.3	73.3	74.4	
772	82	75.4	76.4	77.5	78.5	79.5	80.5	81.6	82.6	83.6	84.7	
773	82	85.7	86.7	87.8	88.8	89.8	90.8	91.9	92.9	93.9	95.0	
774	82	96.0	97.0	98.0	99.1	00.1	01.1	02.1	00.1	040	0	
775	83	06.2	07.2	08.3	09.3	00.1	01.1 11.3	02.1 12.4	03.1	04.2	05.2	
776	83	16.5	17.5	18.5	19.6	20.6	21.6	22.6	13.4 23.6	14.4 24.7	15.5 25.7	
777	83	26.7	27.7	28.8	29.8	30.8	31.8	32.9	33.9	34.9	36.0	
778	83	37.0	38.0	39.0	40.1	41.1	42.1	43.1	44.1	45.2	46.2	
779	83	47.2	48.2	49.2	50.3	51.3	52.3	53.3	54.3	55.4	56.4	
					"""	02.0	02.0	33.0	0 1.0	50.1	00.1	
780	83	57.4	58.4	59.4	60.5	61.5	62.5	63.5	64.5	65.6	66.6	
781	83	67.6	68.6	69.6	70.7	71.7	72.7	73.7	74.7	75.8	76.8	
782	83	77.8	78.8	79.8	80.9	81.9	82.9	83.9	84.9	86.0	87.0	
783	83	88.0	89.0	90.0	91.1	92.1	93.1	94.1	95.1	96.2	97.2	
784	83	98.2	99.2									
784	84			00.2	01.2	02.2	03.2	04.3	05.3	06.3	07.3	
785	84	08.3	09.3	10.3	11.4	12.4	13.4	14.4	15.4	16.5	17.5	
786	84	18.5	19.5	20.5	21.5	22.5	23.5	24.6	25.6	26.6	27.6	
787	84	28.6	29.6	30.6	31.6	32.6	33.6	34.7	35.7	36.7	37.7	
788	84	38.7	39.7	40.7	41.7	42.7	43.7	44.8	45.8	46.8	47.8	
789	84	48.8	49.8	50.8	51.8	52.8	53.8	54.9	55.9	56.9	57.9	
700	0.1	58.9	50.0	CO 0	67.0	GD 0	CD O	05.0	00.0	0~0	00.0	
790 791	84	68.9	59.9 69.9	60.9 70.9	61.9 71.9	62.9 72.9	63.9 73.9	65.0 75.0	66.0 76.0	67.0 77.0	68.0 78.0	1101
792	84	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	$\begin{bmatrix} 1 & 0.1 \\ 2 & 0.2 \end{bmatrix}$
793	84	89.0	90.0	91.0	92.0	93.0	94.0	95.1	96.1	97.1	98.1	3 0.3
794	84	99.1		01.0	02.0	00.0	0 1.0	00.1	50.1		50.1	4 0.4
794	85		00.1	01.1	02.1	03.1	04.1	05.1	06.1	07.1	08.1	5 0.5
795	85	09.1	10.1	11.1	12.1	13.1	14.1	15.1	16.1	17.1	18.1	6 0.6
796	85	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.1	27.1	28.1	7 0.7
797	85	29.1	30.1	31.1	32.1	33.1	34.1	35.1	36.1	37.1	38.1	8 0.8
798	85	39.1	40.1	41.1	42.1	43.1	44.1	45.1	46.1	47.1	48.1	9 0.9
799	85	49.1	50.1	51.1	52.0	53.0	54.1	55.0	56.0	57.0	58.0	İ
800	85	59.0	60.0	61.0	62.0	63.0	64.0	65.0	66.0	67.0	68.0	
801	85	69.0	70.0	70.9	71.9	72.9	73.9	74.9	75.9	76.9	77.9	
802	85	78.9	79.9	80.9	81.9	82.9	83.9	84.9	85.8	86.8	87.8	
803	85	88.8	89.8	90.8	91.8	92.8	93.8	94.8	95.8	96.7	97.7	
804	85	98.7	99.7	00.~	01.7	00.5	02.7	017	05.7	06.6	07.0	
804	86	08.6	00.6	00.7	01.7	02.7	03.7	04.7	05.7	06.6	07.6	
805	86	18.5	09.6	10.6 20.5	11.6	12.6 22.5	13.6 23.4	14.6 24.4	15.5	$ \begin{array}{c c} 16.5 \\ 26.4 \end{array} $	17.5	
806	86 86	28.4	19.5 29.4	30.4	31.3	32.3	33.3	34.3	25.4 35.3	36.3	$\frac{27.4}{37.3}$	
808	86	38.3	39.2	40.2	41.2	42.2	43.2	44.2	45.1	46.1	47.1	
809	86	48.1	49.1	50.1	51.1	52.0	53.0	54.0	55.0	56.0	57.0	
003		2072	10.1	-	- 1		33.0	2	50.0	00.0	00	
810	86	57.9	58.9	59.9	60.9	61.9	62.8	63.8	64.8	65.8	66.8	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
	1						1			j		

TABLE II. CORRECTION FOR DIFFERENCE OF TEMPERATURE OF ATTACHED THERMOMETERS.

Temperature of Barometers at Station { Upper = T' Lower = T.

,						Lower =			
T' — T	Correct.	T' - T	Correct.	T' T	Correct.	T' - T	Correct.	T' - T	Correct.
Centig.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.
0.0		0.0	10.3	16.0	20.6	24.0	30.9	32.0	41.3
0.0	0.0	8.0 8.2	10.5	16.0	20.6	24.0 24.2	30.9	32.0	41.5
0.2		8.4	10.8	16.4	20.9			1	41.8
0.4	0.5	8.6	11.1	16.4	21.1	24.4	31.5	32.4	42.0
0.6	0.8		11.1	li l		24.6	31.7	32.6	
0.8	1.0	8.8		16.8	21.7	24.8	32.0	32.8	42.3
1.0	1.3 1.5	9.0 9.2	11.6 11.9	17.0 17.2	$21.9 \\ 22.2$	$25.0 \\ 25.2$	$32.2 \\ 32.5$	33.0 33.2	42.5 $42.8$
31	1.8		11.9	17.4	22.4	25.4	32.7	33.4	43.1
1.4	2.1	9.4 9.6	12.1	17.4	22.4	25.4	33.0	33.4	45.1
1.6	2.3	9.8	12.4	17.8	22.9	25.8	33.3	33.8	43.6
1.8		10.0	12.0	18.0				1	43.8
2.0	2.6			18.0	23.2	26.0	33.5	34.0	44.1
2.2	2.8 3.1	10.2 10.4	13.1 13.4	18.2	$23.5 \\ 23.7$	$26.2 \\ 26.4$	33.S 34.0	34.2 34.4	44.1
2.4	3.4	10.4	13.4	18.4	24.0	26.4	34.3	34.4	44.6
2.8	3.6	10.8	13.9	18.8	24.2	26.8	34.6	34.8	44.9
3.0	3.9	11.0	14.2	19.0	24.5	27.0	34.8	35.0	45.1
3.2	4.1	11.0	14.5	19.2	24.8	27.0	35.1	35.0	45.4
3.4	4.1	11.4	14.7	19.4	25.0	27.4	35.3	35.4	45.6
3.6	4.6	11.4	15.0	19.4	25.3	27.6	35.6	35.6	45.9
3.8	4.0	11.8	15.2	19.8	25.5	27.8	35.8	35.8	46.2
4 0	5.2	12.0	15.5	20.0	25.8	28.0	36.1	36.0	46.4
4.2	5.4	12.0	15.8	20.2	26.0	28.2	36.4	36.2	46.7
4.4	5.7	12.4	16.0	20.4	26.3	28.4	36.6	36.4	46.9
4.6	5.9	12.6	16.3	20.6	26.6	28.6	36.9	36.6	47.2
4.8	6.2	12.8	16.5	20.8	26.8	28.8	37.1	36.8	47.4
5.0	6.4	13.0	16.8	21.0	27.1	29.0	37.4	37.0	47.7
5.2	6.7	13.2	17.0	21.2	27.3	29.2	37.6	37.2	48.0
5.4	7.0	13.4	17.3	21.4	27.6	29.4	37.9	37.4	48.2
5.6	7.2	13.6	17.5	21.6	27.8	29.6	38.2	37.6	48.5
5 8	7.5	13.8	17.8	21.8	28.1	29.8	38.4	37.8	48.7
6.0	7.7	14.0	18.0	22.0	28.4	30.0	38.7	38.0	49.0
6.2	8.0	14.2	18.3	22.2	28.6	30.2	38.9	38.2	49.2
6.4	8.3	14.4	18.5	22.4	28.9	30.4	39.2	38.4	49.5
6.6	8.5	14.6	18.8	22.6	29.1	30.6	39.5	38.6	49.8
6.8	8.8	14.8	19.0	22.8	29.4	30.8	39.7	38.8	50.0
7.0	9.0	15.0	19.3	23.0	29.7	31.0	40.0	39.0	50.3
7.2	9.3	15.2	19.6	23.2	29.9	31.2	40.2	39.2	50.5
7.4	9.5	15.4	198	23.4	30.2	31.4	40.5	39.4	50.8
7.6	9.8	15.6	20.1	23.6	30.4	31.6	40.7	39.6	51.1
7.8	10.1	15.8	20.3	23.8	30.7	31.8	41.0	39.8	51.3
8.0	10.3	16.0	20.6	24.0	30.9	32.0	41.3	40.0	51 6
II	1	11		1	<u></u>	1		·	

This Table supposes the scale to be of *brass* from the top to the cistern. If it were of glass or of wood, the argument T'— T ought to be diminished at the ratio of 54 to 62.

In computing by the formula of Laplace, we begin by reducing the barometers to the same temperature by means of the following formula:  $H = h' + h' \left(\frac{T' - T}{6196}\right)$ . Table II. saves this trouble, and gives, in metres, the correction due to the difference of temperature of the barometers.

TABLE III. CORRECTION FOR DECREASE OF GRAVITATION IN LATITUDE.

 $\beta = (0.0028371 \text{ cosin. 2 L}). (A + \alpha + \beta).$ 

The Argument is the Mean Latitude between the two Stations.

	DELDE	1			the Mean L				<del></del>	
ļ	rude.				Co	rrection, in	metres, for			
Corre Added.	ction. Subtr'ct	1000	2000	3000	4000	5000	6000	7000	8000	9000
°	90	2.8	5.7	8.5	11.3	14.2	17.0	19 9	22.7	25.7
1	89	2.8	5.7	8.5	11.3	14.2	17.0	19.8	22.7	25.6
2	88	2.8	5.7	8.5	11.3	14.1	17.0	19.8	22.6	25.5
3	87	2.8	5.6	8.5	11.3	14.1	16.9	19.7	22.6	25.4
4	86	2.8	5.6	8.4	11.2	14.0	16.9	19.7	22.5	25.3
5	85	2.8	5.6	8.4	11.2	14.0	16.8	19.6	22.3	25.1
6	84	2.8	5.5	8.3	11.I	13.9	16.6	19.4	22.2	25.0
7	83	2.7	5.5	8.2	11.0	13.8	16.5	19.3	22.0	24.8
8	82	2.7	5.4	8.2	10.9	13.6	16.4	19.1	21.8	24.5
9	81	2.7	5.4	8.1	10.8	13.5	16.2	18.9	21.6	24.3
10	80	2.7	5.3	8.0	10.7	13.3	16.0	18.7	21.3	24.0
11	79	2.6	5.2	7.9	10.5	13.1	15.8	18.4	21.0	23.7
12	78	2.6	5.2	7.8	10.4	13.0	15.5	18.1	20.7	23.3
13	77	2.5	5.1	7.6	10.2	12.7	15.3	17.8	20.4	22.9
14	76	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5
15	75	2.5	4.9	7.4	9.8	12.3	14.7	17.2	19.7	22.1
16	74	2.4	4.8	7.2	9.6	12.0	14.4	16.8	19.2	21.6
17	73	2.4	4.7	7.0	9.4	11.8	14.1	16.5	18.8	21.2
18	72	2.3	4.6	6.9	9.2	11.5	13.8	16.1	18.4	20.7
19	71	2.2	4.5	6.7	8.9	11.2	13.4	15.6	17.9	20.1
20	70	2.2	4.3	6.5	8.7	10.9	13.0	15.2	17.4	19.6
21	69	2.1	4.2	6.3	8.4	10.5	12.6	14.7	16.9	19.0
22	68	2.0	4.1	6.1	8.2	10.2	12.2	14.3	16.3	18.4
23	67	2.0	3.9	5.9	7.9	9.8	11.8	13.8	15.8	17.7
24	66	1.9	3.8	5.7	7.6	9.5	11.4	13.3	15.2	17.1
25	65	1.8	3.6	5.5	7.3	9.1	10.9	12.8	14.6	16.4
26	64	1.7	3.5	5.2	7.0	8.7	10.5	12.2	14.0	15.7
27	63	1.7	3.3	5.0	6.7	8.3	10.0	11.7	13.3	15.0
28	62	1.6	3.2	4.8	6.3	7.9	9.5	11.1	12.7	14.3
29	61	1.5	3.0	4.5	6.0	7.5	9.0	10.5	12.0	13.5
30	60	1.4	2.8	4.3	5.7	7.1	8.5	9.9	11.3	12.8
31	59	1.3	2.7	4.0	5.3	6.6	8.0	9.3	10.6	12.0
32	58	1.2	2.5	3.7	5.0	6.2	7.5	8.7	9.9	11.2
33	57	1.1	2.3	3.5	4.6	5.8	6.9	8.1	9.2	10.4
34	56	1.1	2.1	3.2	4.2	5.3	6.4	7.4	8.5	9.6
35	55	1.0	1.9	2.9	3.9	4.8	5.8	6.8	7.8	8.7
36	54	0.9	1.7	2.6	3.5	4.4	5.3	6.1	7.0	7.9
37	53	0.8	1.6	2.3	3.I	3.9	4.7	5.5	6.2	7.0
38	52	0.7	1.4	2.1	2.7	3.4	4.1	4.8	5.5	6.2
39	51	0.6	1.2	1.8	2.4	2.9	3.5	4.1	4.7	5.3
40	50	0.5	1.0	1.5	2.0	2.5	3.0	3.4	3.9	4.4
41	49	0.4	0.8	1.2	1.6	2.0	2.4	2.8	3.2	3.5
42	48	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7
43	47	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8
44	46	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
D	•					31				

TABLE IV. Correction for Decrease of Gravitation on a Vertical Line.

$$\delta = \left(\frac{A + \alpha + \beta + \nu + 15296}{6366200}\right) \times A \left( + \alpha + \beta + \nu \right).$$

Argument =  $(A + \alpha + \beta + \nu)$ .

Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.
Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
100	0.2	2100	6.0	4100	12.9	6100	21.1
200	0.5	2200	6.3	4200	13.3	6200	21.6
300	0.8	2300	6.6	4300	13.7	6300	22.0
400	1.0	2400	6.9	4400	14.1	6400	22.5
500	1.3	2500	7.3	4500	14.5	6500	22.9
600	1.6	2600	7.6	4600	14.9	6600	23.4
700	1.8	2700	7.9	4700	15.3	6700	23.9
800	2.1	2800	8.3	4800	15.7	6800	24.3
900	2.4	2900	8.6	4900	16.1	6900	24.8
1000	2.7	3000	8.9	5000	16.5	7000	25.3
1100	2.9	3100	9.3	5100	16.9	7100	25.7
1200	3.2	3200	9.6	5200	17.3	7200	26.2
1300	3.5	3300	10.0	5300	17.7	7300	26.7
1400	3.8	3400	10.3	5400	18.1	7400	27.2
1500	4.1	3500	10.7	5500	18.5	7500	27.7
1600	4.4	3600	11.1	5600	19.0	7600	28.1
1700	4.7	3700	11.4	5700	19.4	7700	28.6
1800	5.0	3800	11.8	5800	19.8	7800	29.1
1900	5.3	3900	12.2	5900	20.3	7900	29.6
2000	5.6	4000	12.5	6000	20.7	8000	30.1

TABLE V. CORRECTION FOR THE ELEVATION OF THE LOWER STATION ABOVE OCEAN.

Argument = Height of Barometer at Lower Station.

A		He	ight of Baron	neter at Lowe	er Station in	Millimetres.		
Approximate Difference of Level.	400	450	500	550	600	650	700	750
Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
1000	1.7	1.4	1.1	0.9	0.6	0.4	0.2	0.0
2000	3.4	2.8	2.2	1.7	1.3	0.8	0.4	0.1
3000	5.1	4.2	3.3	2.6	1.9	1.3	0.7	0.1
4000	6.8	5.6	4.4	3.4	2.5	1.7	0.9	0.1
5000	8.5	6.9	5.5	4.3	3.1	2.1	1.1	0.1
6000	10.3	8.3	6.7	5.2	3.8	2.5	1.3	0.2
7000	12.0	9.7	7.8	6.0	4.4	2.9	1.5	0.2
8000	13.7	11.1	8.9	6.9	5.0	3.4	1.8	0.2
9000	15.4	12.5	10.0	7.7	5.7	3.8	2.0	0.3

### TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

BY A. GUYOT.

Tables which, like the preceding ones by Delcros, in metrical measures, are sufficiently extensive to save the necessity of interpolations, relieve the computer of most of his trouble, and considerably reduce the chances of error in the computations. They thus render to science itself a real service, by inducing observers to determine a larger number of points, and to secure the accuracy of the results by repeating their observations at the same point in various atmospheric circumstances, both of which they can do without fear of being overwhelmed by the labor of the computation.

Similar tables are here offered to the observers who use instruments graduated to English measures. Like those of Delcros, the new tables are based on Laplace's formula, with a slight modification of only one constant. They dispense with the use of logarithms, and give the differences of level corresponding to every thousandth of an inch from 12 to 31 inches by means of the simplest arithmetical operations, so that the data being prepared and corrected, the computation of an elevation takes but a few minutes, and is done with scarcely any chance of error.

Laplace's formula and constants were adopted for the computation of the tables in preference to others found in the following sets for reasons which a few words will explain.

It has been remarked, page 9, that, in consequence of Laplace's constants having been retained in Gauss's, Schmidt's, and Baily's formulæ, they all give similar results; but that Bessel's formula differs in separating the correction due to the moisture of the air from that due to its temperature, while in Laplace's, and in the formulæ just mentioned, both are united. To introduce a separate correction for the expansion of aqueous vapor is, in the writer's view, a doubtful improvement. The laws of the distribution and transmission of moisture through the atmosphere are too little known, and its amount, especially in mountain regions, is too variable, and depends too much upon local winds and local condensation, to allow a reasonable hope of obtaining the mean humidity of the layer of air between the two stations by means of hygrometrical observations taken at each of them. These doubts are confirmed by the experience of the author and of many other observers, which shows that, on an average, Laplace's method works not only as well as the other, but more uniformly well. At any rate, the gain, if there is any, is not clear enough to compensate for the undesirable complication of the formula.

Though the several co-efficients of Laplace's formula need perhaps to be modified according to more recent and probably more accurate determinations of the physical constants on which they depend, as has been proposed by Plantamour, E. Ritter, and lately by the writer himself in a paper read before the American Association for the Advancement of Science at their meeting in Montreal, they have been retained in preparing the following tables, partly because it was found that the errors due to

the various co-efficients nearly compensate each other; partly on the ground that, until a severe test, by means of actual comparative measurements made for the purpose, has shown the expediency of these modifications, it seemed desirable to adhere to the old constants, and thus to preserve a uniformity in the results with the tables of Oltmans, Delcros, Gauss, Baily, and others, which have already been extensively used. The substitution of the co-efficient 0.00260, expressing, according to Schmidt's computation (Mathem. und Physic. Geogr., II. p. 202), the variation of gravity in latitude, for the value 0.002837, does not sensibly alter the altitudes obtained.

The close agreement of the determinations furnished by Laplace's formula, in barometrical measurements carefully conducted, made in favorable circumstances, and during the warm season, with those obtained from repeated trigonometrical observations, or by the spirit-level, strongly testifies in favor of its general correctness. A few striking examples will suffice to show it.

The altitude of Mont Blanc, measured by the barometer, by MM. Bravais and Martins, on the 29th of August, 1844, and computed by Delcros, by means of nine corresponding stations situated on all sides of the mountain (see *Annuaire Météorologique de France*, for 1851, p. 274), was found to be 4810 metres. The altitude of the same point, being the mean of seven of the most elaborate and reliable geodetic measurements, which cost nearly twenty years of labor, is 4809.6 metres.

For smaller elevations the formula seems to answer equally well.

The barometrical measurement of Mount Washington, in New Hampshire, by the author, on the 8th and 9th of August, 1851, gave, by Delcros's Tables, for the mean of eight observations, taken at different hours of the day, 5466.7 English feet above Gorham, N. H., 6285.7 above high tide, and 6291.7 feet above the mean level of the ocean in Portland harbor. In August, 1852, W. A. Goodwin, Civil Engineer, starting from Gorham Railroad Station, found, by the spirit-level, Mount Washington to be 6285.5 feet above mean tide. In September, 1853, Captain T. J. Cram, of the Topographical Engineers, executed, in behalf of the Coast Survey, a careful measurement with the spirit-level, on the same line, for the purpose of testing the various methods of measuring altitudes, and found Mount Washington to be 6293 English feet above the mean level of the ocean.

In lower latitudes the formula showed equally good results. By a barometrical measurement in July, 1856, the altitude of the highest peak of the Black Mountain, North Carolina, about Lat. 36°, was found by the author to be 6701 English feet; and that of the highest Mountain House 5248 feet. In September, 1857, Major T. C. Turner, Chief Engineer of the Morganton Railroad, ran a line of levels from the same point which was used as the lower station for the barometrical measurement, to the top of the highest peak, and found its altitude to be 6711 English feet, and that of the Mountain House 5246 feet. Other points on the line agreed equally well.

Such an agreement, in so considerable elevations, is all that can be desired.

These figures show conclusively, that, when the errors which may arise from the great variability of the data furnished by the instruments have been removed by a repetition, in various states of the atmosphere, and by a proper combination of simultaneous observations at stations not too distant from each other, those which remain and may be attributed to the formula cannot be considerable. But, on the other

hand, we have no right to expect such results from single observations, taken, perhaps, in unsettled weather, without paying any regard to the time of the day at which they were made, to the distance or the non-simultaneity of the corresponding observations, or to other unfavorable circumstances. It is too well known that in such cases large errors may and do actually occur; but for these the formula ought not to be held responsible.

### ARRANGEMENT OF THE TABLES.

If we call

h = the observed height of the barometer  $\tau$  = the temperature of the barometer  $\begin{cases} \text{at the lower station }; \end{cases}$ t =the temperature of the air

h' = the observed height of the barometer

 $\tau'$  = the temperature of the barometer  $\{$  at the upper station. t' = the temperature of the air

If we make, further,

Z = the difference of level between the two barometers;

L = the mean latitude between the two stations;

H= the height of the barometer at the upper station reduced to the temperature of the barometer at the lower station; or,

 $H = h' \{1 + 0.00008967 (\tau - \tau')\};$ 

The expansion of the mercurial column, measured by a brass scale, for  $1^{\circ}$  Fahrenheit = 0.00008967;

The increase of gravity from the equator to the poles = 0.00520048, or 0.00260 to the 45th degree of latitude;

The earth's mean radius = 20,886,860 English feet;

Then, Laplace's formula, reduced to English measures, reads as follows:

$$Z = \log \frac{h}{H} \times 60158.6 \text{ English feet} \left\{ egin{align*} & \left(1 + rac{t + t' - 64}{900}
ight). \\ & \left(1 + 0.00260\cos 2\ L\right). \\ & \left(1 + rac{z + 52252}{20886860} + rac{h}{10443430}
ight). \end{aligned} 
ight.$$

Table I. gives, in English feet, the value of log H or  $h \times 60158.6$  for every hundredth of an inch, from 12 to 31 inches in the barometer, together with the value of the additional thousandths, in a separate column. These values have been diminished by a constant, which does not alter the difference required.

Table II. gives the correction 2.343 feet  $\times$   $(\tau - \tau')$  for the difference of the temperatures of the barometers at the two stations, or  $\tau - \tau'$ . As the temperature at the upper station is generally lower,  $\tau - \tau'$  is usually positive, and the correction negative. It becomes positive when the temperature of the upper barometer is higher, and  $\tau - \tau'$  negative. When the heights of the barometers have been reduced to the same temperature, or to the freezing point, this table will not be used.

Table IV. shows the correction  $D' = \frac{z + 52252}{20886860}$  to be applied to the approximate altitude for the decrease of gravity on a vertical acting on the density of the mercurial column. It is always additive.

Table V. furnishes the small correction  $\frac{h}{10443430}$  for the decrease of gravity on a vertical acting on the density of the air; the height of the barometer h at the lower station representing its approximate altitude. Like the preceding correction, it is always additive.

## USE OF THE TABLES.

In Table I. find first the numbers corresponding to the observed heights of the barometer h and h'. Suppose, for instance, h = 29.345 in.; find in the first column on the left the number 29.3; on the same horizontal line, in the column headed .04, is given the number corresponding to 29.34 = 28121.7; in the last column but one on the right, we find for .005 = 4.5, or for 29.345 = 28126.2. Take likewise the value of h', and find the difference.

If the barometrical heights have not been previously reduced to the same temperature, or to the freezing point, apply to the difference the correction found in Table II. opposite the number representing  $\tau - \tau'$ ; we thus obtain the approximate difference of level, D.

For computing the correction due to the expansion of the air according to its temperature, or  $D \times \left(\frac{t+t'-64}{900}\right)$ , make the sum of the temperatures, subtract from that sum 64; multiply the rest into the approximate difference D, and divide the product by 900. This correction is of the same sign as (t+t'-64). By applying it, we obtain a second approximate difference of level, D'.

In Table III., with D' and the mean latitude of the stations, find the correction for variation of gravity in latitude, and add it to D', paying due attention to the sign.

In Table IV. with D', and in Table V. with D' and the height of the barometer at the lower station, take the corrections for the decrease of gravity on a vertical, and add them to the approximate difference of level.

The sum thus found is the true difference of level between the two stations, or Z; by adding the elevation of the lower station above the level of the sea, when known, we obtain the *altitude* of the upper station.

The use of the small table, VI., by means of which approximate differences of level can be obtained by a single multiplication, is explained below, page 90.

# Example 1.

Measurement of Mount Washington, New Hampshire, by A. Guyot, August 8th, 1851, 4 p. m.; the barometer at the lower station being at 825 English feet above the mean level of the sea; at the upper station at one foot below the summit.

The observation gave,

Gorham, 
$$h=\frac{8 \text{arometer.}}{29.272 \text{ in.}}$$
 Attached Thermometer.  $t=72^{\circ}.05 \text{ F.}$  Mount Washington,  $h'=24.030$  "  $\tau'=54^{\circ}.52 \text{ F.}$   $t'=50^{\circ}.54 \text{ F.}$   $\tau-\tau'=16^{\circ}.38 \text{ F.}$   $\tau-64^{\circ}$   $t+t'-64=58^{\circ}.59 \text{ F.}$ 

#### BAROMETRICAL MEASUREMENT OF HEIGHTS.

Table I. gives for $h=29.272$ inches, for $h'=24.030$ "	28,061.00 22,905.60
Difference,	5,155.40
Table II. gives for $\tau - \tau' = 16^{\circ}.38$	<b>—</b> 37.64
Approximate difference of level, $D =$	5,117.76
$\frac{D \times (t + t' - 64)}{900} = \frac{5118 \times 58.6}{900} =$	333.19
Second approximate difference, $D'=$	5,450.95
Table III. gives for $D'=5450$ and Lat. $44^{\circ}$	0.50
Table IV. gives for $D'=5450$	14.94
Table V. gives for $h = 29.27$	0.00
Barometer below summit,	- 1.00
Mount Washington above Gorham, or $Z=$	5,465.39
Barometer at Gorham above sea level	825.00
Mount Washington above the sea, or altitude,	6,290.39 Eng. ft.

# Example 2.

Measurement of the highest peak of the Black Mountain, in North Carolina, July 11th, 1856, by A. Guyot.

By observation we have at,

•	Barometer.	Attached Thermometer.	Temperature of Air.
Mountain House		$\tau = 64^{\circ}.58 \text{ F}.$	
		$\tau' = 61^{\circ}.88 \text{ F.}$	
riighest reak,	n = 25.002	$\tau = 01.88 \text{ f.}$	t = 39.30  f.
	τ -	$-\tau' = 2^{\circ}.70 \text{ F}.$	120°.70 F.
			— 64°
		t+t'	$64 = 56^{\circ}.7 \text{ F.}$
Table I. gives	for $h = 24.934$ .		. 23,870.4
		ce,	
Table II. give	s for $\tau - \tau' = 2.7$		<b>—</b> 6.3
	Approvi	mate difference, $D$ =	= 1.361.7
	900	$\frac{4)}{1} = \frac{1362 \times 56.7}{900} =$	= 85.8
FF 11 TTT 1		mate difference, $D'$	•
		nd Lat. 36° .	
Table IV. giv	es for $D' = 1448$		3.8
Table V. give	es for $D'=1448$ and	nd h = 25 .	. 0.7
Highest neels	shove Mountain He	7	1 459 0
		use, or $Z$ =	
mountain Hot	ise above the sea	• • • •	5,248.4
Black Mounta	in, highest peak abo	ove the sea, or altitud	le, 6,701.6 Eng. ft
		•	, ,

=

# TABLES

FOR COMPUTING THE DIFFERENCE IN THE HEIGHT OF TWO PLACES FROM BAROMETRICAL OBSERVATIONS.

I.  $D = 60150.58 \times \log H$  or h. Argument, the observed Height of the Barometer at either Station.

Barometer	Eng. Inch.	0.61	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	13.0	13.1	13.2	13.3	13.4	
housandths	or an Inch.		\$	Feet.	1 2.1	2 4.2	3 6.2	4 8.3	5 10.4	6 12.5	7 14.6	8 16.6	9 18.7				_
	60.	Eng. Feet.	5173.8	5387.2	5599.0	5809.0	6017.4	6224.0	6429.2	6632.7	6834.5	7034.9	7233.8	7431.1	7627.0	7821.4	_
	80°	Eng. Feet.	5152.4	5367.0	5578.9	5788.1	5996.6	6203.5	8.8019	6612.4	6814.4	7014.9	7213.9	7411.4	7607.4	7802.0	_
	20.	Eng. Feet.	5130.9	5344.7	5556.8	5767.2	5975.8	6182.8	6388.3	6592.1	6794.3	6995.0	7194.1	7391.8	7587.9	7782.6	
	90.	Eng. Feet.	5109.4	5323.4	5535.7	5746.2	5955.0	6162.2	6367.8	6571.8	6774.1	6975.0	7174.3	7372.1	7568.4	7763.2	
of an Inch.	.05	Eng. Feet.	5087.9	5302.1	5514.5	5725.3	5934.2	6141.6	6347.3	6551.5	6754.0	6955.0	7154.4	7352.3	7548.8	7743.8	
Hundredths of an Inch.	.04	Eng. Feet.	\$000°*	5280.7	5193.4	5704.3	5913.4	6120.9	6326.8	6531.1	6733.8	6934.9	7134.5	7332.6	7529.2	7724.4	_
	.03	Eng. Feet.	6011.9	5259.4	5472.2	5683.2	5892.6	6100.2	6306.3	6510.8	6713.6	6914.9	7114.6	7312.9	7509.6	6.104.9	
	.00	Eng. Feet.	5023.4	5238.0	5452.0	5662.2	5871.7	9.6209	6285.8	£.06£9	6693.4	8.1689	7.094.7	7293.1	7490.0	7685.4	
	10.	Eng. Feet.	5001.8	5216.6	5429.8	5641.2	5850.8	8.8209	6265.2	6470.0	6673.2	6874.7	7074.8	7273.3	7470.4	0.9997	_
	00.	Eng. Feet.	4765.4	5195.2	5408.5	5620.1	5829.9	6038.1	6244.6	9.6119	6652.9	6854.7	7054.9	7253.6	7450.8	7646.5	
Barometer	in Eng. Inch.	9	12.0	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	13.0	13.1	13.2	13.3	13.4	

Deg. Feet.         Deg. Fe		.01 Eng. Feet. 7860.1					-						
Eng. Feet.         Eng. Feet.         Eng. Feet.         Eng. Feet.         T898.7         7918.0           7840.8         7860.1         7879.4         7898.7         7918.0           8033.6         8052.8         8071.9         8091.1         8110.3           8225.0         8244.0         8263.1         8282.1         8110.3           8415.0         8433.9         8452.8         8471.7         8490.6           8603.6         8622.3         8641.1         8659.9         8678.6           8603.6         895.4         9013.9         9032.4         9050.8           8976.8         8995.4         9013.9         9032.4         9050.8           916.4         9179.5         9198.2         9216.6         9234.9           934.7         936.3         9399.5         941.7         9779.6           934.4         918.2         9399.5         941.7         9790.8           934.4         918.2         954.0         954.0         9590.8           934.4         918.2         954.0         954.0         9590.9           936.6.         972.7         9743.7         9761.7         9779.6           9887.2         10053.3         10453	1	Eng. Feet. 7860.1	<b>60</b> .	.03	10.	.05	90.	20.	.08	60.	5 A	of an Inch.	in Eng. Inch.
8033.6 8052.8 8071.9 8091.1 8110.3 8225.0 8244.0 8263.1 8282.1 8110.3 8225.0 8244.0 8263.1 8282.1 8110.3 8115.0 8433.9 8452.8 8471.7 8490.6 8603.6 8622.3 8641.1 8659.9 8678.6 8679.8 8076.8 8955.4 9013.9 9032.4 9050.8 9161.4 9179.8 9189.2 9216.6 9234.9 9364.7 9363.0 9381.3 9399.5 9117.7 9526.8 9545.0 9563.1 9581.2 9593.9 9952.4 9070.6 9725.7 9743.7 9761.7 9779.6 9987.2 9905.1 9923.0 9940.9 9953.7 10242.7 10260.4 10278.0 10295.7 10313.3 10418.7 10418.7 10418.7 10418.7 10606.5 10676.9 10766.9 107784.1 10801.5 10818.7 10836.0 11110.6 11127.7 11144.7 11161.8 11177.8 11149.9 11466.7 11483.6 11500.4 11517.2 11617.9 11617.		7.000	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet. 7956.6	Eng. Feet.	Eng. Feet.	Eng Feet.			0.00
8225.0     8244.0     8263.1     8282.1     8301.1       8415.0     8432.9     8452.8     8471.7     8490.6       8603.6     8622.3     8641.1     8659.9     8678.6       8790.8     8895.4     9032.4     9050.8       8976.8     8995.4     9013.9     9032.4     9050.8       9161.4     9179.8     9188.2     9216.6     9234.9       934.7     9363.0     9381.3     9399.5     9417.7       956.8     9545.0     9563.1     9581.2     9599.3       9707.6     9725.7     9743.7     9761.7     9779.6       9887.2     9905.1     9940.9     9958.7       10065.5     10073.0     10101.1     10118.8     10136.6       10242.7     10260.4     10278.0     10295.7     10488.8       10593.4     10610.8     10628.2     10645.6     10662.9       10766.9     10784.1     10801.5     10990.8     11008.0       11110.6     11127.7     11144.7     11161.8     11178.8       11149.9     11466.7     11483.6     11577.2       11617.9     11661.4     11661.4     11661.4       11617.9     11661.4     11661.4     11684.4		8052.8	8071.9	8091.1	8110.3	8129.4	8148.6	8167.7	8186.8	8205.9		Feet.	13.6
8415.0       8432.8       8471.7       8490.6         8603.6       8622.3       8641.1       8659.9       8678.6         8790.8       8809.5       8816.8       8855.4         8976.8       8895.4       9013.9       9032.4       9050.8         9161.4       9179.8       9198.2       9216.6       9234.9         9161.4       9179.8       9381.3       9399.5       9417.7         956.8       9545.0       9583.1       9589.5       9417.7         956.8       9545.0       9583.1       9589.5       9417.7         9887.2       9905.1       9940.9       9940.9       9589.7         10065.5       10083.3       10101.1       10118.8       10136.6         10242.7       10260.4       10278.0       10458.8       1047.3         10593.4       10610.8       10628.2       10471.3       10488.8         10593.4       10610.8       10628.2       10645.6       10662.9         11010.6       11127.7       11144.7       11161.8       11168.8         11149.9       11267.8       1134.6       1154.7         11617.9       11665.1       11665.1       11665.1       11665.1 <tr< th=""><th></th><th>8244.0</th><th>8263.1</th><th>8282.1</th><th>8301.1</th><th>8320.1</th><th>8339.1</th><th>8358.1</th><th>8377.1</th><th>8396.0</th><th>-</th><th>1.9</th><th>13.7</th></tr<>		8244.0	8263.1	8282.1	8301.1	8320.1	8339.1	8358.1	8377.1	8396.0	-	1.9	13.7
8603.6     8622.3     8641.1     8659.9     8678.6       8790.8     8809.5     8828.2     8846.8     8855.4       8976.8     8995.4     9013.9     9032.4     9050.8       9161.4     9179.8     9198.2     9216.6     9234.9       934.7     9363.0     9381.3     9399.5     9417.7       9526.8     9545.0     9563.1     9589.2     9599.3       9707.6     9725.7     9743.7     9761.7     9779.6       9887.2     9905.1     9940.9     9958.7       10065.5     10063.3     10101.1     10118.8     10136.6       10242.7     10260.4     10278.0     10471.3     10458.8       10593.4     10610.8     10628.2     10645.6     10662.9       10766.9     10784.1     10801.5     10910.8     11088.0       11106.     11127.7     11144.7     11161.8     11178.8       11149.9     11466.7     11483.6     11500.4     11517.2       11617.9     11661.4     11661.4     11661.4     11661.4       11617.9     11661.4     11661.4     11661.4     11661.4		8433.9	8452.8	8471.7	8490.6	8509.4	8528.3	8547.1	8565.9	8584.8	63	3.8	13.8
8790.8       8899.5       8846.8       8865.4         8976.8       8995.4       9013.9       9032.4       9050.8         9161.4       9179.8       9198.2       9216.6       9234.9         934.7       9363.0       9381.3       9399.5       9417.7         956.8       9545.0       9563.1       9581.2       9593.2         9707.6       9725.7       9743.7       9761.7       9799.3         9887.2       9905.1       9940.9       9958.7         10065.5       10083.3       10113.8       10118.8       10136.6         10242.7       10260.4       10295.7       10313.3       10458.8         10593.4       10610.8       10628.2       10645.6       10662.9         10766.9       10784.1       10801.5       10458.8       11062.9         11106.       11127.7       11144.7       11161.8       11178.8         11149.9       11267.8       1134.7       11314.7       11517.2         11617.9       11665.1       11665.1       11665.1       11651.4		8622.3	8641.1	8659.9	8678.6	8697.4	8716.1	8734.8	8753.5	8772.2	က	9.6	13.9
8976.8     8995.4     9013.9     9032.4     9050.8       9161.4     9179.8     9198.2     9216.6     9234.9       9344.7     9363.0     9381.3     9399.5     9417.7       9526.8     9545.0     9563.1     9581.2     9599.3       9707.6     9725.7     9743.7     9761.7     9779.6       9887.2     9905.1     9923.0     9940.9     9958.7       10065.5     10085.3     10101.1     10118.8     10136.6       10242.7     10260.4     10278.0     10490.9     9958.7       10418.7     10416.8     10458.8     10471.3     10458.8       10766.9     10784.1     10801.5     10458.8     11062.9       11010.6     11127.7     11144.7     11161.8     11178.8       11149.9     11466.7     11483.6     11500.4     11517.2       11617.9     11665.1     11665.1     11665.1     11651.1       11817.2     11818.8     11665.1     11651.1     1157.1		8809.5	8828.2	8846.8	8865.4	8884.0	8902.6	8921.2	8939.7	8958.3	4	7.5	14.0
9161.4 9179.8 9198.2 9216.6 9234.9 934.7 9363.0 9381.3 9399.5 9417.7 9526.8 9545.0 9563.1 9581.2 9595.3 9417.7 9762.6 9525.7 9743.7 9761.7 9779.6 9887.2 9905.1 9923.0 9940.9 9958.7 10065.5 10065.3 10101.1 10118.8 10136.6 10242.7 10260.4 10278.0 10295.7 10313.3 10418.7 10418.7 10418.7 10610.8 10628.2 10645.6 10662.9 10766.9 10784.1 10801.5 10818.7 10836.0 10939.3 10956.5 10973.6 10990.8 11083.6 111449.9 11449.9 11466.7 11483.6 11500.4 11517.2 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11631.8 11517.2 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11631.8		8995.4	9013.9	9032.4	8.0206	9069.3	9087.8	9106.2	9124.6	9143.0	10	9.4	14.1
9344.7 9363.0 9381.3 9399.5 9417.7 9526.8 9545.0 9563.1 9581.2 9599.3 9417.7 9761.7 9779.6 9525.7 9743.7 9761.7 9779.6 9887.2 9905.1 9923.0 9940.9 9958.7 10065.5 10085.3 10101.1 10118.8 10136.6 10242.7 10260.4 10278.0 10295.7 10313.3 10418.7 10418.7 10418.7 10418.7 10610.8 10628.2 10645.6 10629.9 10766.9 10766.9 10784.1 10801.5 10818.7 10836.0 11110.6 11127.7 11144.7 11161.8 11348.6 11449.9 11449.9 1165.7 11651.4 11668.1 11681.2 11681.8 11781.7 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11617.9 11631.8 11267.9 11617.9 11617.9 11631.8 11267.9 11631.4 11665.1 11668.1 11684.1		8.6716	9198.2	9216.6	9234.9	9253.3	9271.6	9289.9	9308.2	9326.5	9	11.3	14.2
9526.8 9545.0 9563.1 9581.2 9599.3 9726.8 9779.6 9787.7 9761.7 9779.6 9987.2 9905.1 9923.0 9940.9 9958.7 10065.5 10085.3 101011.1 10118.8 10136.6 10242.7 10240.4 10278.0 10295.7 10313.3 10418.7 10418.7 10418.8 10478.1 10610.8 10628.2 10645.6 10662.9 10766.9 10766.9 10784.1 10801.5 10918.7 10836.0 11010.6 11127.7 11144.7 11161.8 11177.8 111449.9 11449.9 1166.7 11651.4 11668.1 11681.8 11787.2 11617.9 1161		9363.0	9381.3	9399.5	9417.7	9436.0	9454.2	9472.3	9490.5	9508.7	~	13.2	14.3
99707.6 9725.7 9743.7 9761.7 9779.6 9887.2 9905.1 9923.0 9940.9 9958.7 10065.5 10065.3 10101.1 10118.8 10136.6 10242.7 10260.4 10278.0 10295.7 10313.3 10418.7 10418.7 10436.3 10453.8 10471.3 10458.8 10766.9 10766.9 10784.1 10801.5 10818.7 10836.0 10939.3 10956.5 10973.6 10990.8 11008.0 11110.6 11127.7 11144.7 11161.8 11348.6 11449.9 11449.9 11466.7 11483.6 11500.4 11517.2 11617.9 11631.4 11651.4 11668.1 11681.8 11517.2 11617.9 11617.9 11617.9 11631.6 11517.2 11617.9 11617.9 11631.6 11531.6		9545.0	9563.1	9581.2	9599.3	9617.4	9635.5	9653.5	9.1796	9.6896	00	15.0	14.4
9887.2 9905.1 9923.0 9940.9 9958.7 10065.5 10053.3 10101.1 10118.8 10136.6 10242.7 10260.4 10278.0 10295.7 10313.3 10418.7 10436.3 10453.8 10471.3 10458.8 10766.9 10766.9 10784.1 10801.5 10818.7 10836.0 10939.3 10956.5 10973.6 10990.8 11008.0 11110.6 11127.7 11144.7 11161.8 1134.6 11449.9 11449.9 1146.7 11483.6 11500.4 11517.2 11617.9 11617.9 11617.9 11631.4 11651.1 11685.1 11685.1 11517.2		9725.7	9743.7	9761.7	9779.6	9797.6	9815.6	9833.5	9851.4	9869.3	6	17.0	14.5
10065.5     10053.3     10101.1     10118.8     10136.6       10242.7     10260.4     10278.0     10295.7     10313.3       10418.7     10436.3     10453.8     10471.3     10458.8       10593.4     10610.8     10628.2     10645.6     10662.9       10766.9     10784.1     10801.5     10836.0     1008.0       10110.6     11127.7     11144.7     11161.8     1175.8       11449.9     11466.7     11453.6     11500.4     11517.2       11617.9     11617.9     11651.4     11651.4     11651.1		9905.1	9923.0	9940.9	7.8566	9976.5	9994.4	10012.2	10030.0	10047.8		700	14.6
10242.7 10260.4 10278.0 10295.7 10313.3 10418.7 10436.3 10453.8 10471.3 10488.8 10471.3 10488.8 10593.4 10610.8 10628.2 10645.6 10662.9 10766.9 10784.1 10801.5 10818.7 10836.0 11039.3 10956.5 10973.6 10990.8 11088.7 11188.8 11280.8 11297.8 11314.7 11331.6 11348.6 11449.9 11466.7 11483.6 11500.4 11517.2 11617.9 11634.6 11651.4 11668.1 11684.1 11685.1 11684.1		10083.3	10101	10118.8	10136.6	10154.3	10172.0	10189.7	10207.4	10225.1			14.7
10418.7     10436.3     10453.8     10471.3     10488.8       10593.4     10610.8     10628.2     10645.6     10662.9       10766.9     10784.1     10801.5     10318.7     10836.0       10110.6     11127.7     11144.7     11161.8     11178.8       11280.8     11297.8     11314.7     11331.6     11348.6       11449.9     11466.7     11483.6     11500.4     11517.2       1167.9     11634.6     11651.4     11684.1     11684.1		10260.4	10278.0	10295.7	10313.3	10330.9	10348.5	10366.1	10383.6	10401.2	Н	1.7	14.8
10593.4     10610.8     10628.2     10645.6     10662.9       10766.9     10784.1     10801.5     10818.7     10836.0       10939.3     10956.5     10973.6     10990.8     11008.0       11110.6     11127.7     11144.7     11161.8     11178.8       11280.8     11297.8     11314.7     11331.6     11348.6       11449.9     11466.7     11483.6     11500.4     11517.2       1167.9     11634.6     11651.4     11684.1     11684.1       11781.9     11617.9     11631.6     11631.8     11631.9		10436.3	10453.8	10471.3	10488.8	10506.3	10523.7	10541.2	10558.6	10576.0	83	3.4	14.9
10766.9     10784.1     10801.5     10818.7     10836.0       10939.3     10956.5     10973.6     10990.8     11008.0       11110.6     11127.7     11144.7     11161.8     11178.8       11280.8     11297.8     11314.7     11331.6     11348.6       11449.9     11466.7     11483.6     11500.4     11517.2       11617.9     11631.6     11651.4     11668.1     11684.1		10610.8	10628.2	10645.6	10662.9	10680.3	10697.6	10715.0	10732.3	10749.6	ಣ	5.1	15.0
10939.3 10956.5 10973.6 10990.8 11008.0 11110.6 11127.7 11144.7 11161.8 11178.8 11280.8 11297.8 11314.7 11331.6 11348.6 11449.9 11466.7 11483.6 11500.4 11517.2 11617.9 11637.9 11631.4 11668.1 11684.1 11684.1		10784.1	10801.5	10818.7	10836.0	10853.2	10870.5	10887.7	10904.9	10922.1	7	8.9	15.1
11110.6 11127.7 11144.7 11161.8 11178.8 11280.8 11297.8 11314.7 11331.6 11348.6 11449.9 11466.7 11483.6 11500.4 11517.2 11617.9 11637.9 11631.4 11668.1 11684.1 11684.1		10956.5	10973.6	10990.8	11008.0	11025.1	11042.2	11059.3	11076.4	11093.5	20	8.5	15.2
11280.8 11297.8 11314.7 11331.6 11348.6 11449.9 11466.7 11483.6 11500.4 11517.2 11617.9 11631.4 11668.1 11684.1 11517.2	_	11127.7	11144.7	11161.8	11178.8	11195.8	11212.8	11229.8	11246.8	11263.8	9	10.2	15.3
11449.9 11466.7 11483.6 11500.4 11517.2 11617.9 11634.6 11651.4 11668.1 11684.8 11731.0 11531.6 11531.	_	11297.8	11314.7	11331.6	11348.6	11365.5	11382.4	11399.3	11416.2	11433.0	7	6.11	15.4
11617.9 11634.6 11651.4 11668.1 11684.8		11466.7	11483.6	11500.4	11517.2	11534.0	11550.8	11567.6	11584.4	11601.1	တ	13.6	15.5
1178.0 11801 5 11818 9 11831 4		11634.6	11651.4	11668.1	11684.8	11701.5	11718.2	11734.9	11751.6	11768.2	6	15.3	15.6
110011		11801.5	11818.2	11834.8	11851.4	11868.0	11884.6	119011	11917.7	11934.3			15.7
11950.8 11967.3 11983.8 12000.4 12016.9		11967.3	11983.8	12000.4	12016.9	12033.3	12049.8	12066.3	12082.7	12099.2			15.8
15.9   12115.6   12132.0   12148.4   12164.8   12181.2   1219		12132.0	12148.4	12164.8	12181.2	12197.6	12214.0	12230.4	12246.7	12263.1	_	=	15.9

Barometer	Eng. Inch.		16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	18.0	18.1	18.2	18.3	18.4
Thousandths	Inch.		F	reet.	1.6	3.1	4.7	6.3	7.8	9.4	11.0	12.5	14.1				1.5	2.9		5.8			10.2	11.7	13.1		
Ĕ,				_	_	ς1 -	က	4	rO	9	-	တ	6	_			_	61	ಣ	7	10	9	7	00	6		
	60.	Eng. Feet.	12426.1	12588.0	12748.9	12908.8	13067.7	13225.7	13382.7	13538.7	13693.9	13848.1	14001.5	14153.9	14305.5	14456.2	14605.9	14754.9	14903.0	15050.3	15196.7	15342.4	15487.1	15631.2	15774.4	15916.8	16058.5
	80.	Eng. Feet.	12409.9	12571.9	12732.9	12892.9	13051.9	13210.0	13367.1	13523.2	13678.4	13832.7	13986.2	14138.7	14290.3	14441.1	14591.0	14740.1	14888.2	15035.6	15182.1	15327.8	15472.7	15616.8	15760.1	15902.6	16044.4
	.07	Eng Feet.	12393.6	12555.7	12716.8	12876.9	13036.0	13194.2	13351.4	13507.6	13662.9	13817.3	13970.9	14123.5	14275.2	14426.1	14576.1	14725.2	14873.5	15020.9	15167.5	15313.3	15458.2	15602.4	15745.8	15888.4	16030.2
	90.	Eng. Feet.	12377.4	12539.6	12700.8	12861.0	13020.2	13178.4	13335.7	13492.0	13647.4	13801.9	13955.6	14108.3	14260.1	14411.0	14561.1	14710.3	14858.7	15006.2	15152.9	15298.7	15443.7	15588.0	15731.5	15874.2	16016.1
Hundredths of an Inch.	.05	Eng. Feet.	12561.1	12523.4	12684.7	12845.0	13004.3	13162.6	13320.0	13476.4	13631.9	13786.5	13940.2	14093.0	14244.9	14396.0	14546.1	14695.4	14843.9	14991.5	15138.2	15284.2	15429.3	15573.6	15717.2	15859.9	16001.9
Hundredth	.04	Eng. Feet.	12344.8	12507.2	12668.6	12829.0	12988.4	13146.8	13304.3	13460.8	13616.4	13771.1	13924.9	14077.8	14229.8	14380.9	14531.2	14680.5	14829.1	14976.8	15123.6	15269.6	15(14.8	15559.2	15702.9	15845.7	15987.8
	.03	Eng. Feet.	12328.5	12491.0	12652.5	12813.0	12972.5	13131.0	13288.6	13445.2	13600.9	13755.7	13909.6	14062.6	14214.6	14365.8	14516.2	14665.6	14814.3	14962.0	15109.0	15255.0	15400.3	15544.8	15658.5	15831.4	15973.6
	60.	Eng. Feet.	12312.2	12474.8	12636.4	12797.0	12956.6	13115.2	13272.9	13429.6	13585.4	13740.3	13894.2	14047.3	14199.4	14350.8	14501.2	14650.7	14799.4	14947.3	15094.3	15240.5	15385.8	15530.4	15674.2	15817.2	15959.4
	10.	Eng. Feet.	12295.9	12458.6	12620.3	12781.0	12940.7	13099.4	13257.2	13414.0	13569.8	13724.8	13878.8	14032.0	14184.3	14335.7	14486.2	14635.8	14784.6	14932.5	15079.6	15225.9	15371.3	15516.0	15659.9	15802.9	15945.2
	00.	Eng. Feet.	12279.6	12442.4	12604.2	12765.0	12924.8	13083.6	13241.5	13398.4	13554.3	13709.4	13863.5	14016.8	14169.1	14320.6	14471.2	14620.9	14769.8	14917.8	15065.0	15211.3	15356.8	15501.5	15645.5	15788.6	15931.0
Barometer	Eng. Inch.		16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	18.0	18.1	18.2	18.3	18.

Thousandths Barometer of an	.09 Inch. Eng. Inch.
	.08
	.07
	90.
Hundredths of an Inch.	.05
	₹0.
	.03
	.03
	10.
	00.
Barometer	in Eng. Inch.

Barometer	Eng. Inch.		21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	22.0	22.1	22.3	22.3	22.4	22.5	22.6	22.7	22.8	22.9	23.0	23.1	23.2	23.3	23.4
Thousandths	Inch.	Feet.		1.2	5.4	3.6	8:4	0.9	7.2		_	10.9				1:1	2.3	3.4	4.6	5.7	8.9	8.0	9.1	10.5			
_ i			-	_	ο <sub>1</sub>	ಣ	7	70	9	1	00	6.				_	Ø	ಣ	7	10	9	-	90	6			
	60.	Eng. Feet.	19490.0	19619.6	19742.6	19865.0	19986.9	20108.2	20228.9	20349.1	20468.7	20587.8	20706.3	20824.4	20941.9	21058.8	21175.3	21291.1	21406.5	21521.4	21635.8	21749.7	21863.0	21976.0	22088.4	22200.4	22311.8
	80.	Eng. Feet.	19459.0	19607.3	19730.3	19852.8	19974.7	20096.1	20216.9	20337.1	20456.8	20575.9	20694.5	20812.6	20930.1	21047.1	21163.6	21279.5	21395.0	21509.9	21624.4	21738.3	21851.7	21964.7	22077.2	22189.2	22300.7
	.07	Eng. Feet.	2.11.5	19594.9	19718.0	19840.6	19962.6	20083.9	20204.8	20325.1	20444.8	20564.0	20682.7	20801.8	20918.4	21035.4	21152.0	21268.0	21383.5	21498.5	21613.0	21727.0	21840.4	21953.4	22066.0	22178.0	22289.6
	90.	Eng. Feet.	13405.5	19582.6	19705.8	19828.4	19950.4	20071.8	20192.7	20313.1	20432.9	20552.1	20670.8	20789.0	20906.7	21023.8	21140.4	21256.4	21371.9	21487.0	21601.6	21715.6	21829.1	21942.1	22054.7	22166.8	22278.4
Hundredths of an Inch.	.05	Eng. Feet.	19440.4	19570.2	19693.5	19816.1	19938.2	20059.7	20180.7	20301.1	20420.9	20540.2	20659.0	20777.2	20894.9	21012.1	21128.7	21244.8	21360.4	21475.5	21590.1	21704.2	21817.7	21930.8	22043.5	22155.6	22267.3
Hundredth	.0€	Eng. Feet.	19454.0	19557.9	19681.2	19803.9	19926.0	20047.6	20168.6	20289.1	20409.0	20528.3	20647.1	20765.4	20883.2	21000.4	21117.1	21233.2	21348.9	2146.1.0	21578.7	21692.8	21806.4	21919.6	22032.3	22144.5	22256.2
	.03	Eng. Feet.	19421.5	19545.5	19668.9	19791.6	19913.9	20035.5	20156.5	20277.0	20397.0	20516.4	20635.3	20753.6	20871.4	20988.7	21105.4	21221.6	21337.3	21452.5	21567.2	21681.4	21795.1	21908.3	22021.0	22133.3	22245.0
	.03	Eng. Feet.	19409.1	19533.1	19656.6	19779.4	7.10661	20023.3	20144.4	20265.0	20385.0	20504.5	20623.4	20741.8	20859.7	20977.0	21093.8	21210.1	21325.8	21441.1	21555.8	21670.1	21783.7	21897.0	22009.8	22122.1	22233.9
	10.	Eng. Feet.	19390.7	19520.8	19644.3	19767.1	19889.5	20011.2	20132.3	20253.0	20373.0	20492.6	20611.5	20732.0	20847.9	20965.3	21082.1	21198.5	21314.2	21429.6	21544.3	21658.7	21772.4	21885.6	21998.5	22110.8	22222.7
	00.	Eng. Feet.	19384.3	19508.4	19632.0	19754.9	19877.3	199999.1	20120.3	20241.0	20361.1	20480.7	20599.7	20718.2	20836.2	20953.6	21070.5	21186.9	21302.6	21418.1	21532.9	21647.3	21761.0	21874.3	21987.2	22099.6	22211.5
Barometer	Eng. Inch.		21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	22.0	22.1	22.3	22.3	22.4	22.5	22.6	22.7	22.8	55.9	23.0	23.1	23.2	23.3	23.4

				finndredths of an Inch.	of an Inch.					Thous	Thousandths of an	Barometer in
	10.	.09	.03	₩0.	.03	90.	2.0.	80.	.00	: Ā	ų.	Eng. Inch.
Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng Feet.	Eng Feet.	Eng Feet	Eng. Feet			
22322.9	22334.0	22345.2	22356.3	22367.4	22378.4	22389.5	22400.6	22411.7	22422.8			23.5
22433.8	22444.9	22456.0	22467.0	22478.1	22489.1	22500.2	22511.2	22522.3	22533.3			23.6
22544.3	22555.4	22566.4	22577.4	22588.4	22599.4	22610.4	22621.4	22632.4	22643.4		Feet	23.7
22654.3	22665.3	22676.3	22687.2	22698.2	22709.1	22720.1	22731.0	22742.0	22752.9	-	1.1	23.8
22763.8	22774.8	22785.7	22796.6	22807.5	22818.4	22829.4	22840.3	22851.2	22862.0	61	2.2	23.9
0.823.0	6.88866	22894.7	22905.6	22916.5	22927.4	22938.2	22949.1	22960.0	22970.8	හ	; ;	24.0
22981.7	22992.5	23003.3	23014.2	23025.0	23035.8	23046.6	23057.5	23068.3	23079.1	7	4.3	24.1
23089.9	23100.7	23111.4	23122.2	23133.0	23143.8	23154.5	23165.3	23176.1	23186.8	20	5.4	24.2
23197.6	23208.3	23219.1	23229.8	23240.5	23251.3	23262.0	23272.7	23283.4	23294.2	9	6.5	24.3
23304.9	23315.6	23326.3	23337.0	23347.6	23358.3	23369.0	23379.7	23390.3	23401.0	1-	7.5	24.4
23411.7	23422.3	23433.0	23143.7	23454.3	23464.9	23475.6	23486.2	23496.8	23507.4	90	9.8	24.5
23518.1	23528.7	23539.3	23549.9	23560.5	23571.1	23581.7	23592.3	23602.9	23613.5	6	9.7	24.6
23624.1	23634.6	23645.2	23655.8	23666.3	23676.9	23687.5	23698.0	23708.6	23719.1			24.7
23729.7	23740.2	23750.7	23761.2	23771.7	23782.3	23792.8	23803.3	23813.8	23824.3			24.8
23834.8	23845.3	23855.7	23866.2	23876.7	23887.2	23897.7	23908.2	23918.6	23929.1	-	1.0	24.9
23939.5	23949.9	23960.4	23970.8	23981.3	23991.7	24002.1	24012.5	24023.0	24033.4	67	2.1	25.0
24043.8	24054.2	24064.6	24075.0	24085.4	24095.7	24106.1	24116.5	24126.9	24137.2	က	3.1	25.1
24147.6	24158.0	24168.3	24178.7	24189.0	24199.4	24209.7	24220.1	24230.4	24240.8	7	4.1	25.2
24251.1	24261.4	24271.8	24282.1	24292.4	24302.7	24313.0	24323.3	24333.6	24343.9	20	5.1	25.3
21354.2	24364.5	24374.7	24385.0	24395.3	24405.5	24415.8	24426.1	24436.3	24446.6	9	6.2	25.4
24456.8	24467.0	24477.3	24487.5	24497.8	24508.0	24518.2	21528.4	24538.7	24548.9	7	7.2	25.5
24559.1	24569.3	24579.5	24589.7	24599.9	24610.0	24620.2	21630.4	24640.6	24650.7	œ	6.5	25.6
24660.9	2-1671.1	24681.2	24691.4	24701.5	24711.7	24721.8	24732.0	24742.1	24752.3	6	9.5	25.7
24762.4	24772.5	24782.6	24792.8	24802.9	24813.0	24823.1	24833.2	24843.3	24853.4			25.8
91863.5	9 1279 6	600016	9 1502 7	9 1009 8	0.01010	0 10010	0 100 10	910111	940511			95.0

Barometer	Eng. Inch.	26.0	26.1	26.2	26.3	26.4	26.5	56.6	26.7	8.92	56.9	27.0	27.1	27.3	27.3	27.4	27.5	27.6	27.7	8.72	27.9	28.0	28.1	28.3	28.3	28.4
Thousandths	Inch.	Feet.		1.0	5.0	2.9	3.9	4.9	5.9	6.9	7.8	8.8				6.0	1.9	2.8	3.7	4.7	5.6	6.5	7.5	8.4		_
Thou				1	83	ေ	7	ro	9	1	00	6				_	61	ಣ	=	23	9	1	00	6		
	60.	Eng. Feet. 25054.5	25154.4	25254.0	25353.1	25451.9	25550.4	25648.5	25746.2	25843.5	25940.5	26037.2	26133.4	26229.3	26324.9	26420.1	26514.9	26609.5	26703.7	26797.6	26891.0	26981.3	27077.1	27169.6	27261.8	27353.7
	.0.8	Eng. Feet. 25044.5	25144.4	25244.0	25343.2	25442.1	25540.5	25638.7	25736.4	25833.8	25930.8	26027.5	26123.8	26219.8	26315.3	26410.6	26505.5	26600.0	26694.3	26788.2	26881.7	26975.0	27067.8	27160.4	27252.6	27344.5
	20.	Eng. Feet. 25034.4	25134.5	25234.1	25333.3	25432.2	25530.7	25628.9	25726.7	25824.0	25921.1	26017.9	26114.2	26210.2	26305.8	26401.1	26496.0	26590.6	26684.9	26778.8	26872.3	26965.6	27058.6	27151.2	27243.4	27335.3
	90.	Eng. Feet. 25024.4	25124.5	25224.1	25323.4	25422.3	25520.9	25619.1	25716.9	25814.3	25911.4	26008.2	26104.6	26200.6	26296.3	26391.6	26486.5	26581.2	26675.5	26769.5	26863.0	26956.3	27049.3	27141.9	27234.2	27326.2
Hundredths of an Inch.	.03	Eng. Feet. 25014.4	25114.5	25214.2	25313.5	25412.4	25511.0	25609.3	25707.1	25804.6	25901.7	25998.6	26095.0	26191.0	26286.7	26382.1	26477.1	26571.7	26666.1	26760.1	26853.7	26947.0	27040.0	27132.7	27225.0	27317.0
Hundredth	.0.	Eng. Feet. 25004.4	25104.5	25204.2	25303.6	25402.6	25501.2	25599.5	25697.4	25794.8	25892.0	25988.9	26085.3	26181.4	26277.2	26372.5	26467.6	26562.3	26656.7	26750.7	26844.3	26937.7	27030.7	27123.4	27215.7	27307.8
	.03	Eng. Feet. 24994.3	25094.5	25194.3	25293.7	25392.7	25491.4	25589.7	25687.6	25785.1	25882.3	25979.2	26075.7	26171.8	26267.6	26363.0	26458.1	26552.8	26647.2	26741.3	26835.0	26928.4	27021.5	27114.2	27206.5	27298.6
	.03	Eng. Feet., 24984.3	25084.5	25184.3	25283.8	25382.8	25481.5	25579.8	25677.8	25775.4	25872.6	25969.6	26066.1	26162.2	26258.0	26353.5	26448.6	26543.3	26637.8	26731.9	26825.6	26919.0	27012.2	27104.9	27197.3	27289.4
	10.	Eng. Feet. 24974.2	25074.5	25174.4	25273.8	25372.9	25471.7	25570.0	25668.1	25765.6	25862.9	25959.9	26056.5	26152.6	26248.5	26344.0	26439.1	26533.9	26628.4	26722.5	26816.3	26909.7	27002.9	27095.6	27188.1	27280.2
	00.	Eng. Feet. 24964.2	25064.5	25164.4	25263.9	25363.0	25461.8	25560.2	25658.3	25755.9	25853.2	25950.2	26046.8	26143.0	26238.9	26334.4	26429.6	26524.4	26618.9	26713.1	26806.9	26900.4	26993.6	27086.4	27178.9	27271.0
Barometer	Eng. Inch.	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	28.0	28.1	28.5	28.3	28.4

Thousandths Barometer of an	Eng. Inch.	28.5	_	_	_						3 29.3	2 29.4			29.6	29.7		6 29.9	7 30.0	6 30.1		_	30.4	0 30.5			30.8	30.9
ousandt of an	Inch.		Feet	0.0				3.6			6.3	7.2		· ·		_		9.8	2 1.7	3.6			6 5.2	7 6.0	8 6.9	9 7.		_
<u>_</u>		م ند	_	_		-			, ,C			00			_		_	_		-							~	
	60.	Eng. Feet.	97536.5	F.7697.2	97777	97808.3		27898.1	27987.7	28077.1	28166.2	28254.9	67 60 6	25545.4	28431.5	28519.3	28606.9	28694.2	28781.1	25867.9	28954.3	29040.3	29126.2	29211.8	29297.0	29382.0	29466.8	29551.2
	80.	Eng. Feet.	97597.1	97618.3	92708 0	97799 9	7.00117	27889.1	27978.8	28068.2	28157.3	28246.1		25334.5	28422.7	28510.6	28598.2	28685.5	28772.5	28859.2	28945.7	29031.7	29117.6	29203.2	29288.5	29373.5	29458.3	29542.8
	20.	Eng. Feet.	97518 9	2.01012	97699 0	97700 9	7100117	27880.2	27969.8	28059.2	28148.4	28237.2	1	28325.7	28413.9	28501.8	28589.4	28676.8	28763.8	28850.5	28937.0	29023.2	29109.0	29194.7	29280.0	29365.1	29449.8	29534.3
	90.	Eng. Feet.	97500 1	97600 9	97600 8	97761 9	7.101.7	27871.2	27960.9	28050.3	28139.5	28228.4		28316.9	28405.1	28493.0	28580.7	28668.1	28755.1	28841.9	28928.4	29014.6	29100.4	29186.1	29271.5	29356.6	29441.4	29525.9
of an Inch.	.05	Eng. Feet.	97500 0	97501 1	0.1001.1	0.1001.0	21112.2	27862.2	27951.9	28041.4	28130.6	28219.5		28308.0	28396.3	28484.2	28571.9	28659.3	28746.4	28833.2	28919.8	29006.0	29091.8	29177.6	29262.9	29348.1	29432.9	29517.5
Hundredths of an Inch.	.04	Eng. Feet.	971000	97509	0.202.2	27012.7	27763.1	27853.2	27943.0	28032.4	28121.7	28210.6		28299.2	28387.5	28475.4	28563.2	28650.6	28737.7	28824.5	28911.1	28997.4	29083.3	29169.0	29251.4	29339.6	29424.4	29509.0
	.03	Eng. Feet.	61090.4	57451.5	6.27672	27663.7	27754.1	27844.2	27934.0	28023.5	28112.8	28201.7		28290.3	28378.7	28466.7	28554.4	28641.9	98729.0	28815.9	28902.5	28988.8	29074.7	29160.4	29245.9	29331.1	29416.0	29500.6
	60.	Eng. Feet.	2.1351.2	27472.0	27563.5	27654.6	27745.1	27835.2	27925.0	28014.6	28103.8	28192.9		28281.5	28369.8	28457.9	28545.6	28633.2	98790.3	28807.2	28893.8	28980.1	29066.1	29151.9	29237.4	29322.5	29 107.5	29 192.1
	TO.	Eng. Feet.	27372.0	27463.5	27554.7	27645.5	27736.0	27826.2	27916.1	28005.6	28094.9	28184.0		28272.6	28361.0	28449.1	28536.9	28624.4	98711.6	28798.5	28885.2	28971.5	29057.5	99143.3	6.86666	29314.0	29399.0	29483.7
	00.	Eng. Feet.	27562.9	£.454.4	27545.6	27636.5	27727.0	27817.2	27907.1	27996.7	28086.0	28175.1		28263.8	28352.2	28440.3	28528.1	28615.7	0 60256	28789.8	28876.5	28962.9	29048.9	99181.7	99990.3	29305.5	29390.5	29 175.2
Barometer	In Eng. Inch.		2.5.5 G . 5.5	28.6	28.7	28.8	28.9	29.0	29.1	29.5	20.3	29.4		20.5	29.6	29.7	29.8	29.9	008	30.1	30.2	30.3	30.4	10 00	30.6	30.7	30.8	30.9

II. Correction for r-r', or Difference of the Temperature of the Barometers at the Two Stations.

This Correction is negative when the attached Thermometer at the Upper Station is lowest; positive, when the attached Thermometer at the Upper Station is highest.

							_		_					_						_		_
Correction in Eng.	213.2	214.3	215.5	216.7	217.9		219.0	220.2	221.4	222.5	223.7	224.9	226.1	227.2	228.4	229.6		230.7	231.9	233.1	234.3	995 1
au -  au'  Fahren-	0.16	91.5	92.0	92.5	93.0		93.5	94.0	94.5	95.0	95.5	96.0	96.5	97.0	97.5	98.0		98.5	99.0	99.5	100.0	100
Correction in Eng.	189.7	190.9	192.1	193.3	194.4		195.6	196.8	197.9	199.1	200.3	201.5	202.6	203.8	205.0	206.1		207.3	208.5	209.7	210.8	0100
τ — τ' Fahren- heit.	81.0	81.5	82.0	82.5	83.0		83.5	84.0	84.5	85.0	85.5	86.0	86.5	87.0	87.5	88.0		88.5	89.0	89.5	90.0	200
Correction in Eng.	166.3	167.5	168.7	8.691	171.0		172.2	173.4	174.5	175.7	176.9	178.0	179.2	180.4	181.6	182.7		183.9	185.1	186.2	187.4	3 001
$r - \tau'$ Fahren-	0.17	71.5	72.0	72.5	73.0		73.5	74.0	74.5	75.0	75.5	0.92	76.5	77.0	77.5	78.0		78.5	0.62	79.5	80.0	20
Correc- tion in Eng. Feet.	142.9	144.1	145.2	146.4	9.711		148.8	1.49.9	151.1	152.3	153.4	154.6	155.8	157.0	158.1	159.3		160.5	9.191	162.8	164.0	165.9
τ — τ' Fahren- heit.	0.19	61.5	62.0	62.5	63.0		63.5	0.19	64.5	65.0	65.5	0.99	66.5	67.0	67.5	0.89		68.5	0.69	69.5	0.02	1
Correc- tion in Eng. Feet.	119.5	120.6	121.8	123.0	124.2	1	125.3	126.5	127.7	128.8	130.0	131.2	132.4	133.5	134.7	135.9		137.0	138.2	139.4	140.6	111
τ — τ' Fahren- heit.	51.0	51.5	52.0	52.5	53.0		53.5	54.0	54.5	55.0	55.5	26.0	56.5	57.0	57.5	58.0		58.5	59.0	59.5	0.09	200
Correction in Eng.	96.0	97.2	98.4	9.66	100.7	1	101.9	103.1	104.2	105.4	9.901	107.8	108.9	110.1	111.3	112.4		113.6	114.8	116.0	117.1	110.9
τ — τ' Fahren- heit.	41.0	41.5	42.0	42.5	43.0	1	43.5	14.0	44.5	45.0	45.5	46.0	46.5	47.0	47.5	48.0		48.5	49.0	49.5	50.0	70
Correction in Eng.	72.6	73.8	75.0	76.1	77.3	1	78.5	9.62	80.8	82.0	83.2	84.3	85.5	86.7	87.8	89.0		90.5	91.4	92.5	93.7	010
$r - \tau'$ Fahren- heit.	31.0	31.5	32.0	32.5	33.0	(	33.5	34.0	34.5	35.0	35.5	36.0	36.5	37.0	37.5	38.0		38.5	39.0	39.5	40.0	10
Correction in Eng.	49.2	50.4	51.5	52.7	53.9	1	55.1	56.2	57.4	58.6	59.7	6.09	62.1	63.2	64.4	9.69	_=	8.99	6.7.9	69.1	70.3	71.
τ — τ' Fahren- heit.	21.0	21.5	22.0	22.5	23.0		23.5	24.0	24.5	25.0	25.5	56.0	26.5	27.0	27.5	28.0		28.5	29.0	29.2	30.0	20 %
Correction in Eng.	25.8	26.9	28.1	29.3	30.5	7	31.6	32.8	34.0	35.1	36.3	37.5	38.7	39.8	41.0	42.2		43.3	44.5	45.7	46.9	48.0
$\frac{\tau - \tau'}{\text{Fahren-}}$	0.11	11.5	12.0	12.5	13.0	1	13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0	17.5	18.0		18.5	19.0	19.5	20.0	90.5
Correction in Eng.	2.3	3.5	4.7	5.9	7.0	(	x 7.	9.4	10.5	11.7	12.9	14.1	15.2	16.4	17.6	18.7		19.9	21.1	22.3	23.4	9.1.6
$\tau - \tau'$ Fahren- heit.	1.0	1.5	2.0	2.5	3.0	1	0.0	4.0	4.5	5.0	5.5	0.9	6.5	7.0	7.5	8.0		8.5	0.6	9.5	10.0	10 2

Correction for the Difference of Gravity in Various Latitudes.

Correction positive from Latitude 00 to 450. Negative from 450 to 900.

or6   066   006   081   08		0	0	OF OGE OF
089	130	02 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	80 78 76 74 72	01 01 02 08 0 08 0 08 0 08 0 08 0 08 0 0
Feet. F	Feet. F	Feet. Feet. Feet. F	Feet, Feet, Feet, Feet, Feet, F	Feet. Feet. Feet. Feet. Feet. Feet. F
1.9	2.1		2.3 2.2 2.1	2.5 2.4 2.4 2.3 2.2 2.1
4.0 3.7 3.5	4.4 4.2 4	4.2	4.6 4.4 4.2	5.0 4.9 4.7 4.6 4.4 4.2
6.0 5.6 5.2	6.3		6.9 6.6 6.3	7.3 7.1 6.9 6.6 6.3
8.0 7.5 7.0	8.4		9.8 9.5 9.2 8.8 8.4	9.5 9.2 8.8 8.4
10.0 9.4 8.7	10.5	11.5 11.0 10.5	12.2 11.9 11.5 11.0 10.5	11.9 11.5 11.0 10.5
11.9 11.2 10.4	12.6	13.8 13.2 12.6	14.7 14.3 13.8 13.2 12.6	14.3 13.8 13.2 12.6
.9 13.1 12.2	5.4 14.7 13.9	16.1 15.4 14.7	17.1 16.6 16.1 15.4 14.7	16.6 16.1 15.4 14.7
.9 15.0 13.9	7.6 16.8 15.9	18.4 17.6 16.8	19.5 19.0 18.4 17.6 16.8	19.0 18.4 17.6 16.8
9 16.8 15.7	9.8 18.9 17.9	20.7 19.8 18.9	22.0 21.4 20.7 19.8 18.9	21.4 20.7 19.8 18.9
9 18.7 17.4	2.0 21.0 19.9	23.0 22.0 21.0	24.4 23.8 23.0 22.0 21.0	23.8 23.0 22.0 21.0
9 20.6 19.1	4.3 23.1 21.9	25.3 24.3 23.1	26.9 26.1 25.3 24.3 23.1	26.1 25.3 24.3 23.1
9 22.4 20.9	6.5 25.2 23.9	27.5 26.5 25.2	29.3 28.5 27.5 26.5 25.2	28.5 27.5 26.5 25.2
9 24.3 22.6	8.7 27.3 25.9	29.8 28.7 27.3	31.8 30.9 29.8 28.7 27.3	30.9 29.8 28.7 27.3
27.9 26.2 24.4	29.4	32.1 30.9 29.4	34.2 33.3 32.1 30.9 29.4	33.3 32.1 30.9 29.4
29.9 28.1 26.1	31.6	34.4 33.1 31.6	36.6 35.6 34.4 33.1 31.6	35.6 34.4 33.1 31.6
31.9 29.9 27.8	33.7	36.7 35.3 33.7	39.1 38.0 36.7 35.3 33.7	38.0 36.7 35.3 33.7
33.9 31.8 29.6	35.8	39.0 37.5 35.8	41.5 40.4 39.0 37.5 35.8	40.4 39.0 37.5 35.8
8 33.7 31.3	9.7 37.9 35.8	41.3 39.7 37.9	44.0 42.8 41.3 39.7 37.9	42.8 41.3 39.7 37.9
8 35.5 33.1	1.9 40.0 37.8	43.6 41.9 40.0	46.4 45.1 43.6 41.9 40.0	45.1 43.6 41.9 40.0
37.4 34.8	4.1 42.1 39.8	45.9 44.1 42.1	48.9 47.5 45.9 44.1 42.1	47.5 45.9 44.1 42.1
39.3 36.5	6.3 44.2 41.8	48.2 46.3 44.2	51.3 49.9 48.2 46.3 44.2	49.9 48.2 46.3 44.2
41.1 38.3	8.5 46.3 43.8	50.5 48.5 46.3	53.7 52.3 50.5 48.5 46.3	55.9 55.0 53.7 52.3 50.5 48.5 46.3
3 43.0 40.0	0.7 48.4 45.8	52.8 50.7 48.4	56.2 54.6 52.8 50.7 48.4	58.5 57.5 56.2 54.6 52.8 50.7 48.4
8 44.9 41	2.9 50.5 47.8	55.1 52.9 50.5	58.6 57.0 55.1 52.9 50.5	57.0 55.1 52.9 50.5
_				

A COLUMN OF AIR, CORRESPONDING TO ONE TENTH OF AN INCH IN THE BAROMETER.	Temperature of the Air, Fabrenheit, being	220 600 650 700 750 800 850	Feet.	149.3 150.9 152.5 154.0 155.7 157.2 158.8	145.4 146.9 148.4 150.0 151.5 153.1 154.6	141.6 143.1 144.6 146.1 147.6 149.1 150.6	141.0	134.7 136.1 137.6 139.0 140.4 141.8 143.3	131.5 132.9 134.3 135.7 137.0 138.4 139.8	128.4 129.7 131.1 132.4 133.8 135.1 136.5	125.5 126.8 128.2 129.5 130.8 132.2 133.5	122.7 124.0 125.3 126.6 127.9 129.2 130.5	120.0 121.3 122.6 123.8 125.1 126.4 127.7	117.5 118.7 120.0 121.2 122.5 123.7 124.9	115.0 116.2 117.4 118.6 119.9 121.1 122.3	112.6 113.8 115.0 116.2 117.3 118.6 119.8	110.4 111.6 112.8 113.9 115.1 116.3 117.4	110.5 111.6 112.8 113.9	111.7	104.2 105.3 106.4 107.5 108.6 109.7 110.8	102.3   103.3   104.4   105.5   106.6   107.6   108.7	105.6	103.8	96.9 97.9 98.9 99.9 100.9 101.9 103.0	98.2 99.2 100.2		92.0 92.9 93.9 94.9 95.9 96.8 97.8	
	Teml	45° 50°	Feet. Feet.	146.1 147.7	142.3 143.8	138.6 140.1	135.2 136.6	131.9 133.3	128.7 130.1	125.7 127.0	122.9 124.2	120.1 121.4	117.5 118.8	115.0 116.2	112.6 113.8	110.8 111.5	108.1 109.3	105.9 107.1	103.9 105.0	102.0 103.1	100.1 101.2	98.2 99.3	96.5 97.5	94.8 95.8	93.1 94.1	91.6 92.6	90.0 91.0	1
VI. Невант ов	Barometer Reading	Inches.	Feet.	18.5 144.6	19.0 140.8	19.5 137.1	20.0 133.7	20.5 130.5	21.0 127.3	21.5 124.3	22.0 121.5	22.5 118.8	23.0 116.2	23.5 113.7	24.0 111.3	24.5 109.1	25.0 106.9	25.5 104.8	26.0 102.7	26.5 100.9	27.0 99.0	27.5 97.2	28.0 95.4	28.5 93.8	29.0 92.1	29.5 90.6	30.0 89.1	
ов тнв		88	Feet.	4 0.2			4 0.7	8 0.8	1 1.0	5 1.2	8 1.3	2 1.5	5 1.7	9 1.8	2 2.0	6 2.2	9 2.3	3 2.5	6 2.7	0 2.8	3 3.0		0 3.3	4 3.5	7 3.7	3.8	4.0	_
HEIGHT OF — Positive.	Height of the Barometer, in English Inches, at Lower Station.	54 56	Feet. Feet.	0.6	1.1 0.7	1.7 1.1	2.2 1.4	2.8 1.8	3.3 2.1	3.9 2.5	4.4 2.8	5.0 3.2	5.5 3.5	6.1 3.9	6.6 4.2	7.2 4.6	7.7 4.9	8.3 5.3	8.8 5.6	9.4 6.0	6.9	10.5 6.7	11.0 7.0	11.6 7.4	12.1 7.7	12.7 8.1	13.2 8.4	
N FOR THE STATION	rometer, in Lower Statio	88	Feet.	0.8	0 1.5	0 2.3	0 3.1	9.8	9.4 0	1 5.4	1 6.2	1 6.9	1.7	1 8.5	1 9.2	1 10.0	1 10.8	11.5	1 12.3	1 13.1	13.8	2 14.6	15.4	16.1	2 16.9	17.7	18.5	_
CORRECTION LOWER S	ht of the Ba	18 20	Feet. Feet.	1.3 1.0	2.5 2.0	3.8 3.0	5.1 4.0	6.4 5.0	7.6 6.0	8.9 7.1	10.2 8.1	11.4 9.1	12.7 10.1	14.0 11.1	15.3 12.1	16.5 13.1	17.8 14.1	19.1 15.1	20.3 16.1	21.6 17.1	22,9   18.1	24.1   19.2	25.4 20.2	26.7 21.2	28.0 22.2	29.2 23.2	30.5 24.2	_
V. Cor	Heig	91	Feet. F	1.6	3.1		6.3	7.8	9.1	11.0	12.5		15.7		18.8					9.6	3.5	8.6	65				37.6	_
CORRECTION	Decrease of Gravity on a Vertical.  Positive.	+200	t. Feet.		9.9 2	9.3	8 12.2			9 21.5	1 24.7	4 28.1	8 31.5	3 35.1	9 38.7	6 42.5	4 46.3	3 50.3	3 54.3	4 58.4	5 62.6	8 67.0	2 71.4	6 75.9	2 80.5	9 85.2	0.06 9	_
IV. CORRI	-2 4	ference of Level.	Eng Feet. Feet.	1000 2.5	2000 5.2	3000 7.9	4000 10.8	5000 13.7	6000 16.7	7000 19.9	8000 23.1	9000 26.4	10000 29.8	11000 33.3	12000 36.9	13000 40.6	14000 44.4	15000 48.3	16000 52.3	17000 56.4	18000 60.5	19000 64.8	20000 69.2	21000 73.6	22000 78.2	23000 82.9	24000 87.6	

### III.

#### TABLE

FOR

COMPUTING THE DIFFERENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER.

By Prof. Elias Loomis.

This table was computed from the formula of Laplace, modified in accordance with the results of more recent determinations.

Suppose that we have observed

At the lower station. 
$$\begin{cases} H, \text{ the height of the barometer,} \\ T, \text{ the temperature of the barometer,} \\ t, \text{ the temperature of the air,} \end{cases}$$
 At the upper station. 
$$\begin{cases} h', \text{ the height of the barometer,} \\ T', \text{ the temperature of the barometer,} \\ t', \text{ the temperature of the air.} \end{cases}$$

Represent by s the height of the lower station above the level of the sea, by L the lattude of the place, and by h the observed height h' reduced to the temperature T.

The difference of level x between the two stations is given by the formula,

$$x = 60158. 6 \text{ ft.} \times \log_{\frac{1}{h}} \times \left\{ \frac{\left(1 + \frac{t + t' - 64}{900}\right)}{\left(1 + 0.00265 \cos_{\frac{1}{h}} 20588629} + \frac{s}{10444315}\right)}{\left(1 + \frac{x + 52251}{20588629} + \frac{s}{10444315}\right)} \right\}$$

But h represents the height h' reduced from the temperature T' to the temperature T. The expansion of mercury for 1° Fahr. is 0.0001000; that of the brass which forms the scale of the barometer is 0.0000104; the difference is 0.0000896. we have  $h = h' \{1 + 0.0000896 (T - T')\}$ .

Therefore,

D

60158. 6 ft. log. 
$$\frac{H}{h} = 60158.6$$
 ft. log.  $\frac{H}{h'} = 2.3409$  ft. (T  $-$  T').

Part I. of the accompanying Table furnishes in English feet the value of the expression 60158.6 log. H for heights of the barometer from 11 to 31 inches; only they have all been diminished by the constant 27541.5 feet which does not change the difference

60158.6 log. H — 60158.6 log. 
$$h$$
.

Part II. furnishes the correction - 2.3409 (T - T) depending upon the difference T - T' of the temperatures of the barometers at the two stations. This cor-49

rection is generally negative. It would be positive if T - T' were negative; that is, if the temperature T' of the barometer at the upper station exceeded the temperature T at the lower station.

Part III. gives the correction  $A \times 0.00265$  cos. 2 L, to be applied to the approximate altitude A, and which arises from the variation of gravity from the latitude of 45 degrees, to the latitude L of the place of observation. This correction has the same sign as cos. 2 L; that is, it is positive from the equator to 45 degrees, and negative from 45 degrees to the pole.

Part IV. gives the correction  $\Lambda \times \frac{\Lambda + 52251}{20888629}$ , which is always to be added to the approximate height  $\Lambda$ , and which is due to the diminution of gravity on the vertical.

Part V. furnishes for the approximate difference of level A the small correction  $A \times \frac{s}{10444315}$  corresponding to several values of the height s of the lower station. But in place of s there has been substituted as the argument of the table, the height H of the barometer at this station.

## Method of Computation.

Take from Part I. the two numbers corresponding to the observed barometric heights H and h'. From their difference subtract the correction 2.3409 (T — T') found in Part II. with the difference T — T' of the thermometers attached to the barometers. We thus obtain an approximate altitude a.

We then calculate the correction  $a^{\frac{t+t'-64}{900}}$  for the temperature of the air, by multiplying the nine-hundredth part of a by the sum of the temperatures t and t' diminished by 64. This correction is of the same sign as t+t'-64. We thus obtain a second approximate altitude A.

With A and the latitude of the place L, we seek in Part III. the correction  $A \times 0.00265$  cos. 2 L arising from the variation of gravity with the latitude.

For the approximate height A, Part IV. gives the correction A  $\times \frac{A + 52251}{20888629}$  arising from the diminution of gravity on a vertical. This correction is always additive.

Finally, when the height s of the lower station is considerable, the small correction  $A \times \frac{s}{10114315}$  may be found in Part V. This correction is always additive.

## Example 1.

M. Humboldt made the following observations on the mountain of Guanaxuato, in Mexico, in Latitude 21°, viz.

Upl	per station. Lower station near the sea.
Thermometer in open air, $t'$ :	$= 70^{\circ}.3$ $t = 77^{\circ}.5$
Thermometer to barometer, T'	$= 70^{\circ}.3$ $T = 77^{\circ}.5$
Barometer, h':	= 23.66 H $= 30.046$

Required the difference in the height of the two stations.

$_{\rm H}$ . (for H = 30.046 inches	27649.7
Part I. gives $\begin{cases} \text{for H} = 30.046 \text{ inches} \\ \text{for } h = 23.66 \text{ inches} \end{cases}$	21406.9
Difference	${6242.8}$
Part II. gives for $T - T' = 7^{\circ}.2$ ,	16.9
Approximate altitude $a$ ,	6225.9
$\frac{a}{900}(t+t'-64)=6.918\times 83.8,$	+579.7
Second approximate altitude A,	6805.6
Part III. gives for $A = 6806$ , and $L = 21^{\circ}$ ,	+13.3
Part IV. gives for 6806,	+19.3
Height above the sea,	6838.2 feet.

# Example 2.

M. Gay Lussac in his celebrated balloon ascent in 1805, found his barometer to indicate 12.945 English inches, the temperature being 14°.9 Fahrenheit. The barometer at Paris at the same time indicated 30.145 English inches with a temperature of 87°.44 Fahrenheit. Required the elevation of the balloon above Paris.

27735.6
5650.4
22085.2
169.9
21915.3
+933.6
22848.9
-8.2
+82.1
22922.8 feet.

		A	41			T I.		4h C44	ta		
		1 1	· ·			)	ometer at ei			1	
Inches.	Feet.	Diff.	Inches.	Feet.	Diff.	Inches.	Feet.	Diff.	Inches.	Feet.	Diff.
11.0	1396.9	996 4	16.0	11186.3	100.0	21.0	18291.0	10/1	26.0	23871.0	100.3
11.1	1633.3	236.4 234.3	16.1	11349.1	162.8 161.8	21.1	18415.1	124.1 123.6	26.1	23971.3	99.9
11.2	1867.6	232.3	16.2	11510.9	160.8	21.2	18538.7	122.9	26.2	24071.2	99.5
11.3	2099.9	230.2	16.3	11671.7	159.8	21.3	18661.6	122.4	26.3	24170.7	99.1
11.4	2330.1	228.2	16.4	11831.5	158.8	21.4	18784.0	121.8	26.4	24269.8	98.8
11.5	2558.3	226.2	16.5	11990.3	157.9	21.5	18905.8	121.2	26.5	24368.6	98.4
11.6	2784.5	224.2	16.6	12148.2	156.9	21.6	19027.0	120.7	26.6	24467.0	98.1
11.7	3008.7	222.4	16.7	12305.1 12461.0	155.9	21.7	19147.7	120.1	26.7	24565.1	97.6
11.8	3231.1 3451.6	220.5	16.8 16.9	12401.0	155.1	21.8 21.9	19267.8 19387.4	119.6	26.8 26.9	24662.7	97.3
12.0	3670.2	218.6	17.0	12770.2	154.1	22.0	19506.4	119.0	27.0	24857.0	97.0
12.1	3887.0	216.8	17.1	12923.5	153.3	22.1	19624.9	118.5	27.1	24953.6	96.6
12.2	4102.0	215.0	17.2	13075.8	152.3	22.2	19742.9	118.0	27.2	25049.8	96.2
12.3	5315.3	213.3	17.3	13227.3	151.5	22.3	19860.3	117.4	27.3	25145.7	95.9
12.4	4526.9	211.6	17.4	13377.9	150.6	22.4	19977.2	116.9	27.4	25241.2	95.5
12.5	4736.7	209.8	17.5	13527.6	149.7	22.5	20093.6	116.4	27.5	25336.4	95.2
12.6	4944.9	208.2	17.6	13676.5	148.9	22.6	20209.4	115.8	27.6	25431.2	94.8
12.7	5151.4	206.5 205.0	17.7	13824.5	148.0 147.2	22.7	20324.8	115.4	27.7	25525.7	94.2
12.8	5356.4	203.3	17.8	13971.7	146.3	22.8	20439.6	114.4	27.8	25619.9	93.8
12.9	5559.7	201.7	17.9	14118.0	145.6	22.9	20554.0	113.8	27.9	25713.7	93.4
13.0	5761.4	200.2	18.0	14263.6	144.7	23.0	20667.8	113.3	28.0	25807.1	93.2
13.1	5961.6	198.7	18.1	14408.3	144.0	23.1	20781.1	112.9	28.1	25900.3	92.8
13.2	6160.3	197.2	18.2	14552.3	143.1	23.2	20894.0	112.4	28.2	25993.1	92.5
13.3	6357.5	195.7	18.3	14695.4	142.4	23.3	21006.4	111.9	28.3	26085.6	92.1
13.4 13.5	6553.2 6747.5	194.3	18.4	14837.8 14979.4	141.6	23.4	21118.3 21229.7	111.4	28.4 28.5	26177.7 26269.6	91.9
13.6	6940.3	192.8	18.5 18.6	15120.3	140.9	23.6	21340.6	110.9	28.6	26361.1	91.5
13.7	7131.7	191.4	18.7	15260.3	140.0	23.7	21451.1	110.5	28.7	26452.3	91.2
13.8	7321.7	190.0	18.8	15399.7	139.4	23.8	21561.1	110.0	28.8	26543.2	90.9
13.9	7510.3	188.6	18.9	15538.3	138.6	23.9	21670.6	109.5	28.9	26633.7	90.5
14.0	7697.6	187.3	19.0	15676.2	137.9	24.0	21779.7	109.1	29.0	26724.0	90.3
14.1	7883.6	186.0	19.1	15813.3	137.1	24.1	21888.4	108.7	29.1	26813.9	89.9
14.2	8068.2	184.6	19.2	15949.8	136.5	24.2	21996.6	108.2	29.2	26903.5	89.6 89.3
14.3	8251.5	183.3	19.3	16085.5	135.7	24.3	22104.3	107.7	29.3	26992.8	89.1
14.4	8433.6	182.1 180.8	19.4	16220.5	135.0 134.3	24.4	22211.6	106.8	29.4	27081.9	88.7
14.5	8614.4	179.6	19.5	16354.8	133.7	24.5	22318.4	106.4	29.5	27170.6	88.4
14.6	8794.0	178.3	19.6	16488.5	132.9	24.6	22424.8	106.0	29.6	27259.0	88.1
14.7	8972.3	177.2	19.7	16621.4	132.3	24.7	22530.8	105.6	29.7	27347.1	87.8
14.8	9149.5	176.0	19.8	16753.7	131.6	24.8	22636.4	105.1	29.8	27434.9	87.6
14.9	9325.5	174.8	19.9	16885.3	131.0	24.9	22741.5 22846.3	104.8	29.9 30.0	27522.5	87.2
15.1	9500.3 9673.8	173.5	$20.0 \\ 20.1$	17016.3 17146.6	130.3	$25.0 \\ 25.1$	22950.6	104.3	30.1	27696.6	86.9
15.2	9846.2	172.4	20.1	17276.3	129.7	25.2	23054.4	103.8	30.2	27783.3	86.7
15.3	10017.5	171.3	20.3	17405.3	129.0	25.3	23157.9	103.5	30.3	27869.7	86.4
15.4	10187.7	170.2	20.4	17533.7	128.4	25.4	23261.0	103.1	30.4	27955.7	86.0
15.5	10356.8	169.1	20.5	17661.4	127.7	25.5	23363.6	102.6	30.5	28041.5	85.8
15.6	10524.8	168.0	20.6	17788-6	127.2	25.6	23465.9	102.3	30.6	28127.1	85.6
15.7	10691.8	167.0	20.7	17915-1	126.5	25.7	23567.7	101.8	30.7	28212.3	85.2 85.0
15.8	10857.7	165.9 164.8	20.8	18041.0	125.9	25.8	23669.2	101.5	30.8	28297.3	84.7
15.9	11022.5	163.8	20.9	18166.3	125.3 $124.7$	25.9	23770.3	100.7	30.9	28382.0	84.4
16.0	11186.3	200.0	21.0	18291.0	124.1	26.0	23871.0	200.1	31.0	28466.4	

PART IL

Correction due to T.—T', or the Difference of the Temperatures of the Barometers at the two Stations.

This Correction is Negative when the Temperature at the Upper Station is lowest, and vice versi.

T — T'.	Correc-	T — T'.	Correc- tion.	T — T'.	Correction.	T - T'.	Correction.	т—т.	Correction.	T T'.	Correc- tion.
Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.
0	`	0		0		0		0		0	
1	2.3	14	32.8	27	63.2	40	93.6	53	124.1	66	154.5
2	4.7	15	35.1	28	65.5	41	96.0	54	126.4	67	156.8
3	7.0	16	37.5	29	67.9	42	98.3	55	128.7	68	159.2
4	9.4	17	39.8	30	70.2	43	100.7	56	131.1	69	161.5
5	11.7	18	42.1	31	72.6	44	103.0	57	133.4	70	163.9
6	14.0	19	44.5	32	74.9	45	105.3	58	135.8	71	166.2
7	16.4	20	46.8	33	77.3	46	107.7	59	138.1	72	168.6
8	18.7	21	49.2	34	79.6	47	110.0	60	140.4	73	170.9
9	21.1	22	51.5	35	81.9	48	112.4	61	142.8	74	173.3
10	23.4	23	53.8	36	84.3	49	114.7	62	145.1	75	175.6
11	25.8	24	56.2	37	86.6	50	117.0	63	147.5	76	177.9
12	28.1	25	58.5	38	89.0	51	119.4	64	149.8	77	180.3
13	30.4	26	60.9	39	91.3	52	121.7	65	152.2	78	182.6
		PAR	T III.		PAI	RT		PAR	т V.		

	0	Correction due to the Change of Gra					PART	PART V.							
	ity	from t	he Lat	itude o	f 450	to the	IV.	Com	Correction due to the Height of the Lower						
			of the P				Correction	Com	ссион		Station		· viic ii	01101	
	N N	egative	from I from	Lat. 45	0 to 90	0.	Decrease of Gravity			Alwa	ys Pos	itive.			
			Lati	tude.			on a Vertical.	He	ight of	Baron	eter at	Lower	. Static	n.	
App.	00	100	200	300	400	450	Always				1	2		1	App
Alt.	900	800	700	600	500		Positive.	16 in.	18 in.	20 in.	22 in.	24 in.	26 in.	28 in.	Alt.
Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	)	Feet.	Feet.
1000	2.6	2.5	2.0	1.3	0.5	0	2.5	1.6	1.3	1.0	0.8	0.6	0.4	0.2	1000
2000	5.3	5.0	4.1	2.6	0.9	0	5.2	3.1	2.5	2.0	1.5	1.1	0.7	0.3	2000
3000	7.9	7.5	6.1	4.0	1.4	0	7.9	4.7	3.8	3.0	2.3	1.7	1.1	0.5	3000
4000	10.6	10.0	8.1	5.3	1.8	0	10.8	6.3	5.1	4.0	3.1	2.2	1.4	0.7	4000
5000	13.2	12.4	10.1	6.6	2.3	0	13.7	7.8	6.4	5.0	3.8	2.8	1.8	0.8	5000
6000	15.9	14.9	12.2	7.9	2.8	0	16.7	9.4	7.6	6.0	4.6	3.3	2.1	1.0	6000
7000	18.5	17.4	14.2	9.3	3.2	0	19.9	11.0	8.9	7.1	5.4	3.9	2.5	1.2	7000
8000	21.2	19.9	16.2	10.6	3.7	0	23.1	12.5	10.2	8.1	6.2	4.4	2.8	1.3	8000
9000	23.9	22.4	18.3	11.9	4.1	0	26.4	14.1	11.4	9.1	6.9	5.0	3.2	1.5	9000
10000	26.5	24.9	20.3	13.2	4.6	0	29.8	15.7	12.7	10.1	7.7	5.5	3.5	1.7	10000
11000	29.1	27.4	22.3	14.6	5.1	0	33.3	17.2	14.0	11.1	8.5	6.1	3.9	1.8	11000
12000	31.8	29.9	24.4	15.9	5.5	0	36.9	18.8	15.3	12.1	9.2	6.6	4.2	2.0	12000
13000	34.4	32.4	26.4	17.2	6.0	0	40.6	20.4	16.5	13.1	10.0	7.2	4.6	2.2	13000
14000	37.1	34.9	28.4	18.5	6.4	0	44.4	21.9	17.8	14.1	10.8	7.7	4.9	2.3	14000
15000	39.7	37.3	30.4	19.9	6.9	0	48.3	23.5	19.1	15.1	11.5	8.3	5.3	2.5	15000
16000	42.4	39.8	32.5	21.2	7.4	0	52.3	25.1	20.3	16.1	12.3	8.8	5.6	2.7	16000
17000	45.0	42.3	34.5	22.5	7.8	0	56.4	26.6	21.6	17.1	13.1	9.4	6.0	2.8	17000
18000	47.7	44.8	36.5	23.8	8.3	0	60.5	28.2	22.9	18.1	13.8	9.9	6.3	3.0	18000
19000	50.3		1	25.2	8.7	0	64.8	29.8	24.1	19.2	14.6	10.5	6.7	3.2	19000
20000	53.0			26.5	9.2	0	69.2	31.3	25.4	20.2	15.4	11.0	7.0	3.3	20000
21000	55.6	52.3	42.6	27.8	9.7	0	73.6	32.9	26.7	21.2	16.1	11.6	7.4	3.5	21000
22000	58.3	54.8	44.7	29.1	10.1	0	78.2	34.5	28.0	22.2	16.9	12.1	7.7	3.7	22000
23000	60.9	1		1	10.6	0	82.9	36.0	29.2	23.2	17.7	12.7	8.1	3.8	23000
24000	63.6	59.8	48.7	31.8	11.0	0	87.6	37.6	30.5	24.2	18.5	13.2	8.4	4.0	24000
25000	66.2	62.2	50.7	33.1	11.5	0	92.5	39.1	31.8	25.2	19.2	13.8	8.8	4.1	25000
1															

#### TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANY OTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

The following tables, published by M. C. Dippe, in the Astronomische Nachrichten, No. 1056, November, 1856, are a modification and extension of Gauss's tables, published in Schumacher's Jahrbuch, for 1836 and the following years, which are based on the formula of Laplace. In this new form they answer a double purpose. They give the means of solving a problem which often occurs in Meteorology, viz.: The difference of elevation between two stations, and the temperature of the air at both, being known, to reduce the height of the barometer at one of the stations to the height it would have at the other. They are likewise adapted to the computation of heights from barometrical observations.

The formula of Laplace, which has been used, the Metres being reduced to Toises,

and the Centigrade degrees to degrees of Reaumur, reads as follows:

$$h = 9407.73 \left( 1 + \frac{t+t'}{400} \right) \left( 1 + a \cos 2 \phi \right) \left( 1 + \frac{h}{r} \right) \left\{ \log \frac{b}{b'} + 2 \log \left( 1 + \frac{h}{r} \right) \right\}.$$

Where t and t' = the temperatures of the air, in degrees of Reaumur, at the lower and upper station,

b and b' = the height of the barometer, in any scale, reduced to the freezing point, at the lower and upper station,

h = the difference of level, in toises, between the two stations,

r = the distance, in toises, of the lower station to the centre of the Earth,

 $\phi$  = the latitude of the place of observation,

a = the increase of gravity from the equator to the poles.

Making, besides, m = the modulus of the common logarithms, the formula becomes, with sufficient accuracy,

$$\log b - \log b' = h \left\{ \frac{1}{9407.73} \cdot \frac{1}{1 + \frac{t + t'}{400}} - \frac{2 m}{r} \right\} \cdot \frac{1}{1 + a \cos 2 \phi} \cdot \frac{1}{1 + \frac{h}{r}}.$$

Assuming r, or the radius of the Earth, at 45° latitude = 3266631 toises, and a = 0.002595, instead of 0.002845 adopted in Gauss's tables, and making

$$u = \log b - \log b',$$

$$a = \log \left(\frac{1}{9407.73} \cdot \frac{1}{1 + \frac{t + t'}{400}} - \frac{2 m}{r}\right),$$

$$c = -m a \cos 2 \phi,$$

$$c' = -\frac{m h}{r},$$

then the reduction of the height of the barometer to another level is given by the formula,

#### BAROMETRICAL MEASUREMENT OF HEIGHTS.

1. 
$$\log u = \log h + a + c + c';$$

$$2. \quad \log b = \log b' + u.$$

Table I. contains the values of a for the argument t + t'; 10 units are to be subtracted from the characteristic.

Table II. gives the values of c for the argument  $\phi$ , or the correction for the change of gravity in latitude, which is negative from 0° to 45°, positive from 45° to 90°.

Table III. furnishes the values of c' for the argument h in toises, or the correction for the decrease of gravity on the vertical. Both in Tables II. and III. the values of c and c' are given in units of the fifth decimal place.

The difference of elevation of the two stations is given by the formula,

1. 
$$u = \log b - \log b'$$
,  
2.  $\log h = \log u + A + c + c'$ ,

in which A is the arithmetical complement of a, and the corrections c and c' receive contrary signs. For the sake of convenience, the values of A have been placed in Table II, and in Table III. the correction for A is found in another column, with the more convenient argument  $v = \log u + \Lambda$ .

If the heights of the barometers have not been reduced to the freezing point, then, B and B' being the unreduced heights of the barometers, and T and T' the temperature of the attached thermometer in degrees of Reaumur,

$$b:b'=rac{\mathrm{B}}{1+rac{\mathrm{T}}{4140}}:rac{\mathrm{B}'}{1+rac{\mathrm{T}'}{4440}}$$

and making  $\frac{m}{4440} = \beta$ ,

$$u = \log b - \log b' = (\log B - \beta T) - (\log B' - \beta T').$$

Instead of  $\beta = 0.000098$ , we can write with sufficient accuracy 0.00010.

#### USE OF THE TABLES.

These tables can be used in any latitude, and for any barometrical scale; but the indications of the barometers must be reduced to the freezing point; and the temperatures of the air must be given in degrees of Reaumur. The tables suppose the use of logarithms with 5 decimals, such as those of Lalande, and give the results in toises.

# I. For Reducing Barometrical Observations to another Level.

Given h in toises, t, t',  $\phi$ , and b or b'. To find b or b'.

In Table I. with the argument t + t', take a,

In Table II. with the argument  $\phi$ , take c,

In Table III. with the argument h, take c',

the last two corrections being given in units of the fifth decimal, making

$$\log h + a + c + c' - 10$$
 (whole units) =  $\log u$ .

Then we have

for a level lower by h toises,  $\log b = \log b' + u$ ; for a level higher by h toises,  $\log b' = \log b - u$ .

If h, or the difference of elevation, is given in metres, take c', which is always negative, from Table III. (for A) with the argument  $v = \log h + 9.71$ , and write

$$\log u = 9.71018 + \log h + a + c + c' - 10$$
 (whole units).

Then again is  $\log b = \log b' + u$ .

### Example 1.

Suppose the height of the barometer, reduced to the freezing point, to be b'=295.39 Paris lines; the temperature of the air  $t'=11^{\circ}.8$  Reaumur, and the latitude  $\phi=51^{\circ}.48'$ ; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer, reduced to the freezing point, at a station lower by h=498.2 toises?

In th' case 
$$t = t' + 4^{\circ}.98 = 16^{\circ}.78$$
, and  $t + t' = 28^{\circ}.58$ .

Table I. for 28°.58 gives a = 5.99538Table II. for 51° 48' gives c = +0.00026Table III. for 498 toises gives c' = -0.00007

 $\begin{array}{ccc} \log u = & 8.69297 - 10 \\ u = & 0.04931 \\ \log b' = & 2.47040 \end{array}$ 

 $\log b = 2.51971$ 

Barometer at the lower station b = 330.90 Paris lines.

## Example 2.

Suppose the reduced barometer b'=598.6 millimetres; the temperature of the air  $t'=18^{\circ}.0$  Centigrade = 14°.4 Reaumur; the difference of elevation h=2217 metres;  $\phi=3^{\circ}$ . The temperature of the air at the lower station  $t=27^{\circ}.5$  Centigrade = 22°.0 Reaumur, and  $t+t'=36^{\circ}.4$  Reaumur.

Then 
$$\log h = \begin{cases} \log 2217 = 3.34577 \\ + 9.71018 \\ \hline 3.05595 \end{cases} \quad v = 3.06$$

$$a = 5.98750$$

$$c = -0.00112$$

$$c' = -0.00015$$

$$\log u = 9.04218 - 10$$

$$u = 0.11020$$

$$\log b' = 9.77714$$

$$\log b = 9.88734$$

Barometer at the lower station b = 771.5 millimetres.

# 2. For Computing Differences of Elevation from Barometrical Observations.

Given the unreduced height of the barometer at the lower and upper station, B and B'; the temperatures of the attached thermometers, T and T'; the temperatures of the air, t and t'; and the latitude,  $\phi$ .

To find h, or the difference of elevation between the two stations.

Subtract (log B' — 10 T') from (log B — 10 T), paying due attention to the nature of the signs of T and T', and taking the numbers 10 T and 10 T' as units of the fifth decimal. Calling then (log B — 10 T) — (log B' — 10 T') = u, or if the heights of the Barometers are reduced to the freezing point, log b — log b' = u, take,

In Table I., A with the argument t + t', and make  $v = \log u + A$ . In Table II., with the argument  $\phi$ , take c reversing the sign.

Then

In Table III., for A, with the argument v, take c', which, in this case, is always positive; then, remembering that the values of c and c' are given in units of the fifth decimal, we have,

$$\begin{array}{ll} v+c+c' &= \log h \text{ in toises,} \\ v+c+c'+0.28982 &= \log h \text{ in metres,} \\ v+c+c'+0.80584 &= \log h \text{ in English feet.} \end{array}$$

## Example 1.

L. station B = 329.013 Paris lines; T = 
$$+15.88 \, \text{R.}$$
;  $t = +15.96 \, \text{R.}$ ;  $\phi = 45.32$ .  
U. station B' = 268.215 Paris lines; T' =  $+8.40 \, \text{R.}$ ;  $t = +\frac{7.92 \, \text{R.}}{23.88 \, \text{R.}}$ .  

$$t + t' = 23.88 \, \text{R.}$$

$$\log B = 2.51722 - 10 \times 15.88 = 2.51563$$

$$\log B' = 2.42848 - 10 \times 8.4 = 2.42764$$

$$u = 0.08799$$

$$\log u = 8.94443$$

$$A = 3.99982$$

$$v = 2.94425$$

$$c = -0.00002$$

$$c' = +0.00012$$

$$\log h = 2.94435$$

$$h = 879.74 \, \text{toises.}$$

## Example 2.

```
L. station B = 763.15 millimetres; T = t = 25.3 Cent. = 20.24 R.; \phi = 21.0 U. station B' = 600.95 millimetres; T' = t' = 21.3 Cent. = 17.04 R.
                                                          t + t' = 37.28 \, \text{R}.
                \log B = 9.88261 - 10 \times 20.24 =
                                                             9.88059
                \log B' = 9.77884 - 10 \times 17.04 =
                                                              9.77714
                                                              0.10345
                                                \log u =
                                                              9.01473
                                                    A =
                                                              4.01337
                                                              3.02810
                                                    v =
                                                    c = +0.00084
                                                    c' = + 0.00014
                                                              3.02908 for toises.
                                                \log h =
                                                              0.28982
                                                \log h =
                                                              3.31890 for metres.
                                                \log h =
                                                              3.02908 for toises.
                                                              0.30584
                                                              3.83492 for English feet.
                                                \log h =
```

h = 1069.3 toises = 2084.0 metres = 6837.9 English feet.

I. Argument: Sum of the Temperatures of the Air in Degrees of Reaumur.

t+t'		Correction for	,	t+t'		Correction for	
Reaumur.	а	Difference.	A	Reaumur.	а	Difference.	A
-60°	6.09617		3.90383	-20°	6.04776		3.95224
-59	6.09489	128	3.90511	-19	6.04661	115	3.95339
-58	6.09362	127	3.90638	-18	6.04547	114	3.95453
-57	6.09235	127	3.90765	-17	6.04434	113	3.95566
-56	6.09108	127	3.90892	-16	6.04320	114	3.95680
-55	6.08982		3.91018	-15	6.01207		3.95793
-54	6.08856	126	3.91144	-14	6.04094	113	3.95906
-53	6.08730	126	3.91270	-13	6.03981	113	3.96019
-52	6.08605	125	3.91395	-12	6.03869	112	3.96131
-51	6.08480	125 124	3.91520	-11	6.03757	112	3.96243
-50	6.08356		3.91644	-10	6.03645		3.96355
-49	6.08231	125	3.91769	- 9	6.03533	112	3.96467
-48	6.03108	123	3.91892	- 8	6.03422	111	3.96578
-47	6.07984	124	3.92016	- 7	6.03311	111	3.96689
-46	6.07861	123 123	3.92139	- 6	6.03201	110	3.96799
-45	6.07738		3.92262	- 5	6.03090		3.96910
-44	6.07616	122	3.92384	- 4	6.02980	110	3.97020
-43	6.07494	122	3.92506	- 3	6.02871	109	3.97129
-42	6.07372	122	3.92628	_ 2	6.02761	110	3.97239
-41.	6.07250	122 121	3.92750	- 1	6.02652	109	3.97348
-40	6.07129		3.92871	0	6.02543		3.97457
-39	6.07009	120	3.92991	+ 1	6.02434	109	3.97566
-38	6.06888	121	3.93112	2	6.02326	108	3.97674
-37	6.06768	120	3.93232	3	6.02217	109	3.97783
-36	6.06648	120 119	3.93352	4	6.02109	108	3.97891
-35	6.06529		3.93471	5	6.02002		3.97998
-34	6.06410	119	3.93590	6	6.01895	107	3.98105
-33	6.06291	119	3.93709	7	6.01787	108	3.98213
-32	6.06173	118	3.93827	8	6.01680	107	3 98320
-31	6.06055	118	3.93945	9	6.01574	106 106	3.98426
-30	6.05937	110	3.94063	10	6.01468	100	3.98532
-29	6.05819	118	3.94181	11	6.01362	106	3.98638
-28	6.05702	117	3.94298	12	6.01256	106	3.98744
-27	6.05585	117	3.94415	13	6.01150	106	3.98850
-26	6.05469	116	3.94531	14	6.01045	105	3.98955
-25	6.05352		3.94648	15	6.00940		3.99060
-24	6.05236	116	3.94764	16	6.00835	105	3.99165
-23	6.05121	115	3.94879	17	6.00731	104	3.99269
-22	6.05005	116	3.94995	18	6.00626	105	3.99374
-21	6.04890	115	3.95110	19	6.00522	104	3.99478
-20	6.04776	114	3.95224	+20	6.00418	104	3.99582

( Continued.)

1			_					( )	07111	nued.)						
   t+	· ť				Correct	ion fo	r			t+t'			Co	orrection i	or -	
Reaur	- 1		a		Differe	ence.		A		Reaumur.		а	]	Difference		A
+20	)°	6.0	—- 004	18			3.	99582		+40°		5.983	93		4.0	1607
21			003		10			99685		41		5.982		99		1706
22	2	6.0	002	12	10:	ł	3.	99788		42		5.981	95	99	4.0	1805
28	3	6.0	00 I	.08	10		3.	99892	ļ	43		5.980	97	98	4.0	1903
24	1	6.0	000	006	10:	1	3.	99994		44		<b>5.97</b> 9	98	99 98	4.0	2002
25			999		10:	,		00097		45		5.979	000	97	t	2100
26			998		10			00199		46		5.978		98		2197
27			996		10	- 1		00301		47		5.977		97		2295
28	- 1	-	995		10	Ì		00403		48		5.976	1	97		2392
29			994		10	1		00505		49		5.975		97		2489
30	- 1		993		10	1		00606		50	1	5.974		97		2586
31			992		10	1		00707		51		5.978	1	96		2683
33 33			991 990		10	1		$00808 \\ 00909$		52 53		5.972 $5.971$	1	97		2779 28 <b>7</b> 6
34			989 989		10			01009	Ì	54	1	5.97		96		29 <b>72</b>
35	,	5.9	988	90	10		4.	01110		55		5.969	933	95	4.0	30 <b>67</b>
36	5		987		10			01210		56	1	5.968		96		3163
37	7	5.9	986	91	9	i	4.	01309		57		5.967	742	95	4.0	3258
38	3	5.9	985	91	10		4.	01409		58		5.966	646	96	4.0	3354
39	)	5.9	984	92	9	9	4.	01508	-	59		5.963	551	95	4.0	3449
II —	. L		_		- Cor			FOR	a.	III.	V a, ar	ERTI	CAL. —	- CORF	For A,	arg. v,
	*·	1	or A	1 revei	se the S		1	1	1	_	c'al	lways	Negative		c' always	Positive.
φ	c	9	<i>þ</i>	φ	c	φ	φ	c	φ	h		c'	h	c'	v	c'
0	-113	· 0	00	0 15	<b>-</b> 98+	0 75	30	-56+	60		2	1	1600	21	1.8	1
1	113		89	16	96	74	31	53	59			3	1700	23	1.9	1
2	112		38	17	93	73	32	49	58			4	1800	24	2.0	1
3	112		37	18	91	72	33	46	57		)	5	1900	25	2.1	2
4	112	8	6	19	89	71	34	42	56	500	0	7	2000	27	2.2	2
															2.3	3
5	111		35	20	86	70	35	39	55	11		8	2100	28	2.4	3
6	110	1 -	34	21	84	69	36	35	54		1	9	2200	29	2.5	4
7	109		33	22	81	68	37	31	53	11		11	2300	31	2.6	5
8	103	- 1	32	23	78	67	38	27	52	11		12	2400	32	2.7	7
9	107	S	31	24	75	66	39	23	51	1000	,	13	2500	33	2.8 2.9	8 11
10	106	8	80	25	72	65	40	20	50	1100		15	2600	35	3.0	13
11	104		9	26	69	64	41	16	49	1200	)	16	2700	36	3.1	17
12	103	7	8	27	66	63	42	12	48	1300	)	17	2800	37	3.2	21
13	101	7	7	28	63	62	43	8	47		1	19	2900	39	3.3	27
14	100	7	6	29	60	61	41	4	46	1500	)	20	3000	40	3.4	33
15	-98	+ ~	5	30	-56+	60	45	-0+	45	1600	,	21	3500	47	3.5 3.6	42 53
10	-93		0	30	-907	00	40	-0 -	40	1000		21	0000	1 31	0.0	00

#### TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

In No. 1088 of the Astronomische Nachrichten, published in June, 1857, Dr. DIPPE gives the following set of Tables for reducing barometrical observations to another level, and for computing heights. These tables, being based, as the preceding ones (IV.), on the formula of Laplace, and computed with the same constants, give results nearly identical, but dispense with the use of logarithms.

### USE OF THE TABLES.

The tables suppose the height of the barometer to be expressed in French inches or Paris lines, and the temperature in degrees of Reaumur; they give the differences of level in French toises.

The signs used have the following signification: -

At Lower Station.  $\begin{cases} B = \text{Observed Height of Barometer in Paris lines.} \\ T = \text{Attached Thermometer in degrees of Reaumur.} \\ b = \text{Barometer reduced to the freezing point.} \\ t = \text{Temperature of the air, detached Thermometer.} \end{cases}$ 

At Upper Station.  $\begin{cases} B' = \text{Observed Height of Barometer.} \\ T' = \text{Attached Thermometer.} \\ b' = \text{Barometer at the freezing point.} \\ t' = \text{Temperature of the air.} \end{cases}$ 

 $\phi$  = Latitude of the place.

h = Difference of elevation between the two stations.

I. For Reducing Barometrical Observations to another Level.

Given, h in toises, t, t',  $\phi$ , and b or b'. To find b or b'.

Make first 
$$2 \tau = \frac{t+t}{2}$$
 and  $\tau$ , and

In Table I., with the argument  $2\tau$ , take  $\tau'$ ; In Table III., with the arguments h and  $\tau$ , take C; In Table IV., with the arguments h and  $\phi$ , take C';

Make, further,

$$u = h + C + C'$$
 and  $\frac{u}{100} \tau'$ ;

And if b' be given, and b required,

In Table II., with the argument b, take H;

then is

$$H = H' + (u - \frac{u}{100} \tau'),$$

and the height of the barometer, in Table II., due to H, is b required.

If b be given, and b' required for a level higher by h toises, then,

In Table II., with the argument b, take H'.

Make, further,

$$H' = H - (u - \frac{u}{100} \tau'),$$

and b' is the height of the barometer in Table II., corresponding to H'.

## Example 1.

Suppose the height of the barometer reduced to the freezing point to be b' = 295.39 Paris lines; the temperature of the air  $t' = 11^{\circ}.8$  Reaumur; and the latitude  $\phi = 51^{\circ}.48$ ; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer reduced to the freezing point, at a station lower by h = 498.2 toises?

In this case, 
$$t'=11^{\circ}.8$$
;  $t=11^{\circ}.8+4^{\circ}.98$ ;  $t+t'=28^{\circ}.58$ ;  $2\,\tau=\frac{t+t}{2}=14^{\circ}.29$ ;  $\tau=7^{\circ}.15$ ; and according to Table I.  $\tau'=+6.67$ .

With h and  $\tau$ , in Table III., we find C = -1.4

With h and  $\phi$ , in Table IV., we find C'=+0.3We add h=498.2and we have u=497.1;  $\frac{u}{100}=4.97$  $-\frac{u}{100}$   $\tau'=-33.15$   $\frac{u}{463.95}$   $\frac{29.83}{2.98}$ 

With b', in Table II., we find  $H' = \frac{367.86}{831.81}$ 

Finally, with H, in Table II., we find b = 330.91 Paris lines, which is the required height of the barometer at the lower station. Gauss's tables (IV.) would give b = 330.90 lines.

### Example 2.

Suppose b'=330.46 Paris lines;  $t'=-12^{\circ}.3$  Reaumur; h'=92.7 toises;  $\phi = 62^{\circ}$ .

In this case, assuming t = t',

$$2\tau = \frac{t+t'}{2} = -12^{\circ}.3; \ \tau = -6.15;$$

and according to Table I.

$$\tau' = -6.55$$
.

With h and  $\tau$ , in Table III., take C = -0.2

With h and  $\phi$ , in Table IV., take C' = + 0.1

Add 
$$h = 92.7$$
We have  $u = 92.6$ 

$$-\frac{u}{100}\tau' = +6.07$$

$$\frac{u}{98.67}$$
II., take H' = 826.22
$$\frac{0.926}{100} = 0.926$$

$$\frac{u}{100} = 0.926$$

$$\frac{u}{100} = 0.926$$

$$\frac{u}{100} = 0.926$$

With b', in Table II., take H' =

$$H = 924.89$$

With H, in Table II., we find b = 338.53 Paris lines. Gauss's tables (IV.) would give b = 338.54 lines.

II. For Computing Differences of Elevation from Barometrical Observations.

Suppose to be given B, B', T, T', t, t',  $\phi$ ; required h.

Make first 
$$\tau = \frac{t+t'}{4}$$
 and  $T-T'$ .

Then in Table II., with the argument  $\begin{cases} B \text{ take } H, \\ B' \text{ take } H', \end{cases}$ 

and make

$$u = (H - H') + \frac{H - H'}{100} \tau - (T - T'),$$

in which each full degree of T - T' corresponds to a toise.

Further, in Table III., with u and  $\tau$ , take C reversing the sign;

in Table IV., with u and  $\phi$ , take C' reversing the sign;

in Table V., with T - T' and  $\tau$ , take C'' with the signs of T - T'.

Then the difference of elevation required is

$$h = u + C + C' + C''.$$

If the heights of the barometer, reduced to the freezing point, or b and b', are given,

then in Table II., with the argument,  $\begin{cases} b \text{ take H} \\ b' \text{ take H}' \end{cases}$ 

and make

$$u = H - H' + \frac{H - H'}{100} \tau$$
.

Further, in Table III., take C reversing the sign; in Table IV., take C' reversing the sign;

and

$$h = u + C + C'.$$

### Example 1.

Suppose to be given,

B = 333.6 Paris lines; T = 
$$+$$
 17°.0 Reaumur;  $t = +$  19°.0 R.;  $\phi = 48^\circ$ . B' = 289.9 Paris lines; T' =  $+$  16°.3 Reaumur;  $t' = +$  15°.2 R.

$$T - T' = 0^{\circ}.7$$
  $t + t' = +34^{\circ}.2$   $\tau = +8.55$ 

In Table II. with B take H = 864.9  
" with B' take H' = 291.2  
H — H' = 573.7  

$$\frac{\text{H} - \text{H'}}{100} = 5.737$$
  
 $\frac{\text{H} - \text{H'}}{100} = 49.06$   
 $\frac{11 - \text{H'}}{100} = 5.737$   
 $\frac{11 - \text{H'}}{100} = 5.737$   
 $\frac{15.90}{2.87}$   
 $\frac{29}{10.95}$   
 $\frac{29}{10.95}$ 

u = 622.06

In Table III., with u and  $\tau$ , take C = +1.8In Table IV., with u and  $\phi$ , take C' In Table V., with T — T' and  $\tau$  take C" = 0.0

Difference of elevation, or h = 623.66 to ses.

Gauss's Tables give 623.64 toises.

### Example 2.

Suppose to be given,

$$b = 342.68 \text{ Paris lines}; t = -10^{\circ}.38 \text{ Reaumur}; \phi = 65^{\circ}.$$

$$b'=285.47$$
 Paris lines;  $t'=-14^{\circ}.94$  Reaumur;  $T-T'=0^{\circ}.$  R.

$$t + t' = -25^{\circ}.32$$
  
 $\tau = -6.33$ 

In Table II. with 
$$b$$
 take H = 974.58

" with 
$$b'$$
 take  $H' = 228.28$ 

$$H - H' = 746.30$$

$$\frac{\text{II} - \text{II}'}{100} \tau = -47.24 \qquad \qquad \frac{\tau = -6.33}{44.73} \\
 u = 699.06 \qquad \qquad \frac{\text{II} - \text{II}'}{100} \tau = -47.24$$

100

$$u = 699.06$$
  
In Table III., with  $u$  and  $\tau$ , take  $C = +1.8$ 

In Table IV., with 
$$u$$
 and  $\phi$ , take  $C' = -1.2$ 

$$h = 699.66$$

Gauss's Tables give h = 699.72 toises.

## V.

## TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION, BY M. C. DIPPE.

Table I. - Argument, the observed Height of the Barometer at either Station.

Barom-					Tenths	of a Line.				
eter in Paris Lines.	0	11	2	3	4	5	6	7	8	9
B or B'					II or II' iı	a Toises =		*	·	
270	0.7	2.2	3.7	5.2	6.7	8.2	9.7	11.2	12.8	14.3
271	15.8	17.3	18.8	20.3	21.8	23.3	24.8	26.3	27.8	29.3
272	30.8	32.3	33.8	35.3	36.8	38.3	39.8	41.3	42.8	44.3
273	45.8	47.3	48.8	50.3	51.8	53.3	54.8	56.3	57.8	59.3
274	60.8	62.2	63.7	65.2	66.7	68.2	69.7	71.2	72.7	74.1
275	75.6	77.1	78.6	80.1	81.6	83.1	84.5	86.0	87.5	89.0
23 Inch.										
276	90.5	91.9	93.4	94.9	96.4	97.9	99.3	100.8	102.3	103.8
277	105.2	106.7	108.2	109.7	111.1	112.6	114.1	115.6	117.0	118.5
278	120.0	121.4	122.9	124.4	125.8	127.3	128.8	130.2	131.7	133.2
279	134.6	136.1	137.6	139.0	140.5	142.0	143.4	144.9	146.3	147.8
280	149.3	150.7	152.2	153.6	155.1	156.5	158.0	159.5	160.9	162.4
281	163.8	165.3	166.7	168.2	169.6	171.1	172.5	174.0	175.4	176.9
282	178.3	179.8	181.2	182.7	184.1	185.6	187.0	188.5	189.9	191.4
283	192.8	194.2	195.7	197.1	198.6	200.0	201.4	202.9	204.3	205.8
284	207.2	208.6	210.1	211.5	213.0	214.4	215.8	217.3	218.7	220.1
285	221.6	223.0	224.4	225.9	227.3	228.7	230.2	231.6	233.0	234.5
286	235.9	237.3	238.7	240.2	241.6	243.0	244.4	245.9	247.3	248.7
287	250.1	251.6	253.0	254.4	255.8	257.3	258.7	260.1	261.5	262.9
24 Inch.										
288	264.4	265.8	267.2	268.6	270.0	271.4	272.9	274.3	275.7	277.1
289	278.5	279.9	281.3	282.8	284.2	285.6	287.0	288.4	289.8	291.2
290	292.6	294.0	295.4	296.8	298.3	299.7	301.1	302.5	303.9	305.3
291	306.7	308.1	309.5	310.9	312.3	313.7	315.1	316.5	317.9	319.3
292	320.7	322.1	323.5	324.9	326.3	327.7	329.1	330.5	331.9	333.3
293	334.7	336.1	337.5	338.9	340.2	341.6	343.0	344.4	345.8	347.2
294	348.6	350.0	351.4	352.8	354.2	355.5	356.9	358.3	359.7	361.1
295	362.5	363.9	365.2	366.6	368.0	369.4	370.8	372.2	373.5	374.9
296	376.3	377.7	379.1	380.4	381.8	383.2	384.6	385.9	387.3	388.7
297	390.1	391.5	392.8	394.2	395.6	397.0	398.3	399.7	401.1	402.4
298	403.8	405.2	406.5	407.9	409.3	410.7	412.0	413.4	414.8	416.1
299	417.5	418.9	420.2	421.6	423.0	424.3	425.7	427.1	428.4	429.8
25 Inch.										
300	431.1	432.5	433.9	435.2	436.6	437.9	439.3	440.7	442.0	443.4
301	444.7	446.1	447.5	448.8	450.2	451.5	452.9	454.2	455.6	456.9
302	458.3	459.6	461.0	462.3	463.7	465.0	466.4	467.S	469.1	470.5
303	471.8	473.1	474.5	475.8	477.2	478.5	479.9	481.2	482.6	483.9
304	485.3	486.6	487.9	489.3	490.6	492.0	493.3	494.7	496.0	497.3
305	498.7	500.0	501.4	502.7	504.0	505.4	506.7	508.0	509.4	510.7
306	512.0	513.4	514.7	516.0	517.4	518.7	520.1	521.4	522.7	524.0

Table I. Continued.

TABLE 1. Continued.											
Barom- eter in Paris		1			Tenths	of a Line.					
Lines.	0	1	2	3	4	5	6	7	8	9	
306	512.0	513.4	514.7	516.0	517.4	518.7	520.1	521.4	522.7	524.0	
307	525.4	526.7	528.0	529.4	530.7	532.0	533.4	534.7	536.0	537.4	
308	538.7	540.0	541.3	542.6	544.0	. 545.3	546.6	547.9	549.3	550.6	
309	551.9	553.2	554.6	555.9	557.2	558.5	559.8	561.2	562.5	563.8	
310	565.1	566.4	567.8	569.1	570.4	571.7	573.0	574.3	575.6	576.9	
311	578.3	579.6	580.9	582.2	583.5	584.8	586.1	587.5	588.8	590.1	
26 Inch.		**************************************									
312	591.4	592.7	594.0	595.3	596.6	597.9	599.2	600.6	601.9	603.2	
313	604.5	605.8	607.1	608.4	609.7	611.0	612.3	613.6	614.9	616.2	
314	617.5	618.8	620.1	621.4	622.7	624.0	625.3	626.6	627.9	629.2	
315	630.5	631.8	633.1	634.4	635.7	637.0	638.3	639.5	640.8	642.1	
316	643.4	644.7	646.0	647.3	648.6	649.9	651.2	652.5	653.8	655.1	
317	656.3	657.6	658.9	660.2	661.5	662.8	664.1	665.4	666.6	667.9	
318	669.2	670.5	671.8	673.1	674.3	675.6	676.9	678.2	679.5	680.S	
319	652.0	683.3	684.6	685.9	687.2	688.4	689.7	691.0	692.3	693.6	
320	694.8	696.1	697.4	698.7	699.9	701.2	702.5	703.8	705.0	706.3	
321	707.6	708.9	710.1	711.4	712.7	713.9	715.2	716.5	717.7	719.0	
322	720.3	721.6	722.8	724.1	725.4	726.6	727.9	729.2	730.4	731.7	
323	733.0	734.2	735.5	736.7	738.0	739.3	740.5	741.8	743.1	744.3	
27 Inch.											
324	745.6	746.8	748.1	749.4	750.6	751.9	753.2	754.4	755.7	756.9	
325	758.2	759.4	760.7	761.9	763.2	764.5		767.0	768.2	769.5	
326	770.7	772.0	773.2	774.5	775.7	777.0	778.2	779.5	780.7	782.0	
327	783.2	784.5	785.7	787.0	788.2	789.5	790.7	792.0	793.2	794.5	
328	795.7	797.0	798.2	799.4	800.7	801.9	803.2	804.4	805.7	806.9	
329	808.2	809.4	810.6	811.9	S13.1	814.4	815.6	816.8	818.1	819.3	
330	820.6	821.8	823.0	824.3	825.5	826.7	828.0	829.2	830.4	831.7	
331	832.9	834.2	835.4	836.6	837.9	839.1	840.3	841.6	842.8	844.0	
332	845.2	846.5	847.7	848.9	850.2	851.4	852.6	853.9	855.1	856.3	
333	857.5	858.8	860.0	861.2	862.4	863.7	864.9	866.1	867.3	868.6	
334	869.8	871.0	872.2	873.4	874.7	875.9	877.1	878.3	879.6	880.8	
335	882.0	883.2	884.4	885.7	886.9	888.1	889.3	890.5	891.7	893.0	
28 Inch.	0010	00- 4	2000	20# 0	000.0	000.0	007.5	000 ~	000.0	007	
336	894.2	895.4	896.6	897.8	899.0	900.3	901.5	902.7	903.9	905.1	
337	906.3	907.5	908.7	909.9	911.2	912.4	913.6	914.8	916.0	917.2	
338	918.4	919.6	920.8	922.0	923.3	924.5	925.7	926.9	928.1	929.3	
339	930.5	931.7	932.9	934.1	935.3	936.5	937.7	938.9	940.1	941.3	
340 341	942.5 954.5	943.7	944.9	946.1 958.1	947.3	948.5 960.5	949.7	950.9 962.9	952.1 964.1	953.3 965.3	
	0.00										
342	966.5	967.7	968.9	970.1	971.3	972 5	973.7	974.8	976.0	977.2	
343	978.4	979.6	980.8	982.0	983.2	984.4	985.6	986.8	987.9	989.1	
344	990.3	991.5	992.7	993.9	995.1	996.2	997.4	998.6	999.8	1001.0	
345	1002.2	1003.4	1004.5	1005.7	1006.9	1008.1	1009.3	1010.5	1011.6	1012.8	
346	1014.0	1015.2	1016.4	1017.5	1018.7	1019.9	1021.1	1022.3	1023.4	1024.6	
347 29 Inch	1025.8	1027.0	1028.1	1029.3	1030.5	1031.7	1032.8	1034.0	1035.2	1036.4	
	1037.5	1038.7	1039.9	1011.1	1042.2	1043.4	1044.6	1045.8	1046 9	1048.1	

Table II. correction for the temperature of the air.

Argument,  $2\tau = \frac{t+t'}{2}$ .

$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	τ' -14.29 -13.64	0.65	2 τ -12 -11	-6.38 -5.82	Diff.	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	+0.50 0.99	Diff.	2 τ +14 15	+ 6.54 6.98	Diff.
-23 -22 -21	-13.00 -12.36 -11.73	0.64 0.64 0.63 0.62	-10 - 9 - 8	-5.26 -4.71 -4.17	0.56 0.55 0.54 0.54	3 4 5	1.48 1.96 2.44	0.49 0.48 0.46 0.47	16 17 18	7.41 7.83 8.26	0.43 0.42 0.43 0.42
-20 -19 -18 -17 -16	-11.11 -10.50 - 9.89 - 9.29 - 8.70	0.61 0.61 0.60 0.59 0.59	- 7 - 6 - 5 - 4 - 3	-3.63 -3.09 -2.56 -2.04 -1.52	0.54 0.53 0.52 0.52 0.51	6 7 8 9	2.91 3.38 3.85 4.31 4.76	0.47 0.47 0.46 0.45 0.45	19 20 21 22 23	8.68 9.09 9.50 9.91 10.31	0.41 0.41 0.41 0.40 0.40
-15 -14 -13 -12	- 8.11 - 7.53 - 6.95 - 6.38	0.58 0.58 0.57	$\begin{vmatrix} -2 \\ -1 \\ 0 \\ +1 \end{vmatrix}$	-1.01 -0.50 0.00 +0.50	0.51 0.50 0.50	11 12 13 +14	5.21 5.66 6.10 +6.54	0.45 0.44 0.44	24 25 26 +27	10.71 11.11 11.50 +11.89	0.40 0.39 0.39

TABLE III. FOR C.

Arguments, h and  $\tau$ .

In computing Heights reverse the signs of C.—Arguments,  $\tau$  and u.

h, (u)	τ, in Degrees of Reaumur =											
Toises.	<b>-16</b> °	-12°	<b>-8</b> °	-40	. 00	+4°	+8°	+12°	+16°			
50	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1			
100	0.2	0.2	0.2	0.2	0.3	0.3	0.3	0.3	0.3			
150	0.3	0.3	0.4	0.4	0.4	0.4	0.4	0.4	0.4			
200	0.4	0.5	0.5	0.5	0.5	0.5	0.6	0.6	0.6			
250	0.5	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.7			
300	0.7	0.7	0.7	0.7	0.8	0.8	0.8	0.9	0.9			
350	0.8	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.1			
400	0.9	0.9	1.0	1.0	1.0	1.1	1.1	1.2	1.2			
450	1.0	1.1	1.1	1.1	1.2	1.2	1.3	1.3	1.4			
500	1.1	1.2	1.2	1.3	1.3 .	1.4	1.4	1.5	1.5			
550	1.2	1.3	1.4	1.4	1.5	1.5	1.6	1.6	1.7			
600	1.4	1.4	1.5	1.6	1.6	1.7	1.7	1.8	1.9			
650	1.5	1.6	1.6	1.7	1.8	1.8	1.9	1.9	2.0			
700	1.6	1.7	1.8	1.8	1.9	2.0	2.0	2.1	2.2			
750	1.7	1.8	1.9	2.0	2.0	2.1	2.2	2.3	2.3			
800	1.9	2.0	2.0	2.1	2.2	2.3	2.4	2.4	2.5			
850	2.0	2.1	2.2	2.3	2.3	2.4	2.5	2.6	2.7			
900	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9			
950	2.3	2.4	2.5	2.6	2.7	2.7	2.9	3.0	3.1			
1000	2.4	2.5	2.6	2.7	2.8	2.9	3.1	3.2	3.3			

TABLE IV. FOR C'.

CORRECTION IN TOISES FOR THE CHANGE OF GRAVITY IN LATITUDE.

In computing Heights, reverse the signs of C'. Arguments  $\varphi$  and u.

Lati	tude.			AI	proximat	e Differen	ce of Lev	el, in Tois	es.		
_	+	100	200	300	400	500	600	700	800	900	1000
0	90	0.3	0.5	0.8	1.0	1.3	1.6	1.8	2.1	2.3	2.6
5	85	0.3	0.5	0.8	1.0	1.3	1.5	1.8	2.0	2.3	2.6
10	80	0.2	0.5	0.7	1.0	1.2	1.5	1.7	2.0	2.2	2.4
15	75	0.2	0.4	0.7	0.9	1.1	1.3	1.6	1.8	2.0	2.3
20	70	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0
25	65	0.2	0.3	0.5	0.7	0.8	1.0	1.2	1.3	1.5	1.7
30	60	0.1	0.3	0.4	0.5	0.6	0.8	0.9	1.0	1.2	1.3
35	55	0.1	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.8	0.9
36	54	0.1	0.2	0.2	0.3	0.4	0.5	0.6	0.6	0.7	0.8
37	53	0.1	0.1	0.2	0.3	0.4	0.5	0.5	0.6	0.6	0.7
38	52	0.1	0.1	0.2	0.3	0.3	0.4	0.4	0.5	0.6	0.6
39	51	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5	0.5
40	50	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5
41	49	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.3	0.4
42	48	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.3
43	47	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.2
44	46	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1
45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

TABLE V. FOR C".

Arguments  $\tau$  and T — T'. To be used only in computing Heights.

T — T'			Correction	on for T —	· T , in Toi	ses, with t	the same s	ign; τ =		
Reaumur.	-12°	-10°	-80	<b>-6</b> °	-4°	<b>_2</b> °	<b>O</b> °	+2°	+40	+6°
0	0.0	0.0	0.0	. 0.0	0.0	0.0	0.0	0.0	0.0	0.0
1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0
2	0.4	0.3	0.3	0.3	0.2	0.2	0.2	0.1	0.1	0.0
3	0.6	0.5	0.5	0.4	0.4	0.3	0.2	0.2	0.1	0.1
4	0.8	0.7	0.6	0.5	0.5	0.4	0.3	0.2	0.2	0.1
5	1.0	0 9	0.8	0.7	0.6	0.5	0 4	0.3	0.2	0.1
6	1.1	1.0	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.1
7	1.3	1.2	1.1	0.9	0.8	0.7	0.6	0.4	0.3	0.2
8	1.5	1.4	1-2	1.1	0.9	0.8	0.6	0.5	0.3	0.2
9	1.7	1.6	1.4	1.2	1.1	0.9	0.7	0.6	0.4	0.2
10	1.9	1.7	1.5	1.4	1.2	1.0	0.8	0.6	0.4	0.2

Correction	for T -	<ul> <li>T' with</li> </ul>	contrary	$sign: \tau =$

T — T'	+8°	+10°	+12°	+140	T — T'	+8°	+100	+12°	+140
1	0.0	0.0	0.0	0.0	6	0.0	0.1	0.2	0.3
2	0.0	0.0	0.1	0.1	7	0.0	0.1	0.2	0.3
3 '	0.0	0.0	0.1	0.1	8	0.0	0.1	0.2	0.4
4	0.0	0.0	0.1	0.2	9	0.0	0.1	0.2	0.4
5	0.0	0.1	0.2	0.2	10	0.0	0.1	0.3	0.4

LAPLACE'S FORMULA FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS, MODIFIED BY BABINET.

In the Comptes Rendus de l'Académie des Sciences for March, 1851, M. Babinet proposes the following modification of Laplace's formula, the object of which is to dispense both with the use of logarithms and with tables of any kind.

Laplace's formula is,

$$z = 18393 \text{ metres (log H} - \log h) \left[ 1 + \frac{2 \cdot (T + t)}{1000} \right],$$

z being the difference of level between the two stations,

H, the height of barometer at the lower station,

h, the height of barometer at the upper station,

T, temperature of air at the lower station,

t, temperature of air at the upper station.

The two barometers are supposed to be reduced to the same temperature. The small correction for the latitude is omitted.

For elevations less than 1000 metres, and even for much greater elevations, if approximate results only are needed, the formula may be transformed into the following:

 $z = 16000 \text{ metres } \frac{\mathbf{H} - h}{\mathbf{H} + h} \left[ 1 + \frac{2(\mathbf{T} + t)}{1000} \right].$ 

## Example 1.

Suppose,

at lower station, barometer at zero Cent. =  $755^{mm}$ ; temperature of air 15° Cent. at upper station, barometer at zero Cent. =  $745^{mm}$ ; temperature of air 10° Cent.

$$H - h = 10^{mm}$$
  $T + t = 25^{\circ} \text{ Cent.}$   
 $H + h = 1500^{mm}$   $2 (T + t) = \frac{5}{15} \frac{9}{50} = .05$ .

Then

 $z = 16000_{\frac{10}{1500}} \times (1.05) = 112$  metres.

Laplace's formula, by Delcros's tables, would give 111.6 metres.

## Example 2.

Suppose,

at lower station, barometer at zero Cent. = 730<sup>mm</sup>; temperature of air 20° Cent. at upper station, barometer at zero Cent. = 635<sup>mm</sup>; temperature of air 15° Cent.

$$H - h = 95^{\text{mm}}$$
  $T + t = 35^{\circ} \text{ Cent.}$   
 $H + h = 1365^{\text{mm}}$   $2 (T + t) = \frac{730}{1000} = .07$ .

Then

 $z = 16000_{\frac{9}{3}\frac{6}{6}\frac{5}{6}} \times (1.07) = 1191.5$  metres.

Laplace's formula, by Delcros's tables, would give 1191.1 metres.

For greater elevations an intermediate station may be supposed.

Babinet's formula reduced to English measures becomes,

$$z = 52494$$
 English feet  $\frac{II - h}{II + h} \left[ 1 + \frac{(T + t - 64)}{900} \right];$ 

but as, in this form, it loses the simplicity of its coefficient, it will be found, on trial, that its use requires rather more computing than the author's tables (II.), p. 38, which give more accurate results.

### VII.

#### TABLES

FOR COMPUTING THE DIFFERENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER. -- BAILY.

Bailly, in his Astronomical Tables and Formulæ, page 111, gives the following final formula:

$$x = 60345.51 \{1 + .0011111 (t + t' - .64^{\circ})\} \times \log \text{ of } \left\{ \frac{\beta}{\beta'} \times \frac{1}{1 + .0001 (\tau - \tau')} \right\} \times \{1 + .002695 \cos 2 \phi\}.$$

Where  $\phi$  = the latitude of the place,

 $\beta$  = the height of the barometer,  $\tau$  = the temperature, Fahrenheit, of the mercury, t = the temperature, Fahrenheit, of the air,

 $\beta'$  = the height of the barometer,  $\tau'$  = the temperature, Fahrenheit, of the mercury, t' = the temperature, Fahrenheit, of the air.

The numerical values assumed are as follows: -

The constant barometrical coefficient = 60158.53 English feet.

The expansion of moist air for 1° Fahrenheit = .0022222.

The expansion of mercury for 1° Fahrenheit = .0001001.

The increase of gravitation from Equator to Poles = .00539.

The radius of the Earth at  $\phi$  = 20898240 English feet.

The height of lower station assumed = 4000 English feet.

Make A = the log of the first term, in English feet.

B = the log of 1 + .0001  $(\tau - \tau')$ .

C = the log of the last term.

 $D = \log \beta - (\log \beta' + B).$ 

Then, by the tables which follow, the logarithm of the difference of altitude in English feet

 $= A + C + \log D.$ 

Baily's Tables have been recomputed and extended by Downes, for Lee's Collection of Tables and Formulæ (2d edit. pp. 84, 85). These new tables are given here as revised by Mr. Downes for this volume.

I. THERMOMETERS IN THE OPEN AIR.

t+t'	A	t+t'	A	t+t'	A	t+t'	A	t+t'	A
0		0		0	4 = 2 + 0 =	0	4 00300	0	4.0300#
1	4.74913	37	4.76742	73	4.78497	109	4.80183	145	4.81807
2	4.74965	38	4.76791	74	4.78544	110	4.80229	146	4.81851
3	4.75016	39	4.76841	75	4.78592	111	4.80275	147	4.81896
4	4.75068	40	4.76891	76	4.78640	112	4.80321	148	4.81940
5	4.75120	41	4.76940	77	4.78687	113	4.80367	149	4.81984
6	4.75171	42	4.76990	78	4.78735	114	4.80413	150	4.82028
7	4.75223	43	4.77039	79	4.78782	115	4.80458	151	4.82072
8	4.75274	44	4 77089	80	4.78830	116	4.80504	152	4.82116
9	4.75326	45	4.77138	81	4.78877	117	4.80550	153	4.82160
10	4.75377	46	4.77187	82	4.78925	118	4.80595	154	4.82204
11	4.75429	47	4.77236	83	4.78972	119	4.80641	155	4.82248
12	4.75480	48	4.77285	84	4.79019	120	4.80686	156	4.82291
13	4.75531	49	4.77335	85	4.79066	121	4.80731	157	4.82335
14	4.75582	50	4.77384	86	4.79113	122	4.80777	158	4.82379
15	4.75633	51	4.77433	87	4.79160	123	4.80822	159	4.82423
	11,000								
16	4.75684	52	4.77482	88	4.79207	124	4.80867	160	4.82466
17	4.75735	53	4.77530	89	4.79254	125	4.80913	161	4.82510
18	4.75786	54	4.77579	90	4.79301	126	4.80958	162	4.82553
19	4.75837	55	4.77628	91	4.79348	127	4.81003	163	4.82597
20	4.75888	56	4.77677	92	4.79395	128	4.81048	164	4.82640
21	4.75938	57	4.77725	93	4 79442	129	4.81093	165	4.82684
22	4.75989	58	4.77774	94	4.79489	130	4.81138	166	4.82727
23	4.76040	59	4.77823	95	4.79535	131	4.81183	167	4.82770
24	4.76090	60	4.77871	96	4.79582	132	4.81228	168	4.82814
25	4.76141	61	4.77919	97	4.79628	133	4.81273	169	4.82857
26	4.76191	62	4.77968	98	4.79675	134	4.81317	170	4.82900
27	4.76241	63	4.78016	99	4.79721	135	4.81362	171	4.82943
28	4.76292	64	4.78065	100	4.79768	136	4.81407	172	4.82986
29	4.76342	65	4.78113	101	4.79814	137	4.81452	173	4.83029
30	4.76392	66	4.78161	102	4.79861	138	4.81496	174	4.83072
31	4.76442	67	4.78209	103	4.79907	139	4.81541	175	4.83115
32	4.76492	68	4.78257	104	4.79953	140	4.81585	176	4.83158
33	4.76542	69	4.78305	105	4.79999	141	4.81630	177	4.83201
34	4.76592	70	4.78353	106	4.80045	142	4.81674	178	4.83244
35	4.76642	71	4.78401	107	4.80091	143	4.81719	179	4.83287
36	4.76692	72	4.78449	108	4.80137	144	4.81763	180	4.83330
				4		1			

	II.	Аттасне	THERMOM	ETER.			ATITUDE OF PLACE.
ττ'	В	$\tau - \tau'$	В	τ-τ΄	В	φ	C
0	0.00000	0 20	0.00087	0 40	0.00174	0	0.00117
ì	0.00004	21	0.00091	41	0.00174	5	0.00117
2	0.00009	22	0.00096	42	0.00118	10	0.00113
3	0.00013	23	0.00100	43	0.00187	15	0.00110
4	0.00017	24	0.00104	44	0.00191	20	0.00090
5	0.00022	25	0.00109	45	0.00195	25	0.00075
6	0.00026	26	0.00113	46	0.00200	30	0.00058
7	0.00030	27	0.00117	47	0.00204	35	0.00040
8	0.00035	28	0.00122	48	0.00208	40	0.00020
9	0.00039	29	0.00126	49	0.00212	45	0.00000
10	0.00043	30	0.00130	50	0.00217	50	9.99980
11	0.00048	31	0.00135	51	0.00221	55	9.99960
12	0.00052	32	0.00139	52	0.00225	60	9.99942
13	0.00056	33	0.00143	53	0.00230	65	9.99925
14	0.00061	34	0.00148	54	0.00234	70	9.99910
15	0.00065	35	0.00152	55	0.00238	75	9.99900
16	0.00069	36	0.00156	56	0.00243	80	9.99890
17	0.00074	37	0.00161	57	0.00247	85	9.99885
18	0.00078	38	0.00165	58	0.00251	90	9.99883
19	0.00083	39	0.00169	59	0.00256		
		1					

## EXAMPLE.

	Upper Station.	Lower Station.
Thermometer in open air,	t' = 70.4,	t = 77.6.
Attached Thermometer,	$\tau' = 70.4$ ,	$\tau = 77.6.$
Barometer,	$\beta' = 23.66$ inches,	$\beta = 30.05$ inches.
Latitude of the place	$\phi = 21^{\circ}$ .	
B = 0.00031	$\log D = 9.0$	1502
$\log \beta' = 1.37401$	C = 0.0	00087
$\overline{1.37432}$	A = 4.8	31940
$\log \beta = 1.47784$	$\overline{3.8}$	33529
D = 0.10352	=68	43.7 English feet.

### VIII.

#### TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS,

BASED ON BESSEL'S FORMULA.

BY E. PLANTAMOUR.

[These Tables, computed by Professor E. Plantamour, Director of the Observatory at Geneva, Switzerland, are found in Vol. XIII. Part 1, of the Mémoires de la Société de Physique, &c. de Genève, p. 63, together with the following explanations.]

In No. 356 of the Astronomische Nachrichten, Bessel published a paper on the measurement of heights by means of the barometer, in which he deduces a formula which contains a factor depending on the humidity of the air. This formula is:

$$\log \frac{P}{P'} = \frac{(g) \cdot H' - H}{L(1 + KT)} \left[ 1 - a \frac{0.002561}{\sqrt{PP'}} \cdot 10^{-0.0279712 T} - 0.0000625826 T^{2} \right],$$

where the various quantities have the following signification: -

h being the elevation of the lower station, and

h' the elevation of the upper station above the level of the sea,

a = the radius of the Earth,

$$H = \frac{a h}{a + h},$$

$$H' = \frac{a \, h'}{a + h'};$$

P = the weight of the atmosphere at the lower station,

P' = the weight of the atmosphere at the upper station,

the unit of weight assumed being the pressure of a column of mercury

#### BAROMETRICAL MEASUREMENT OF HEIGHTS.

of 336.905 Paris lines, at the temperature of the freezing point, or zero Reaumur, and under the 45th degree of latitude.

(g) = the gravity, at the level of the sea, in the mean latitude between the two places of observation.

Therefore, calling  $\phi$  the latitude,

 $(g) = 1 - 0.0026257 \cos \phi,$ 

L = the constant barometrical coefficient depending on the relative density of the mercury and of the air,

K = the coefficient of the expansion of the air,

T = the mean temperature of the layer of air between the lower and upper station,

a = the fraction of saturation of the same layer.

The second term in the parenthesis, destined to take into account the aqueous vapor in the air, was obtained by assuming that the elastic force of vapor for a temperature T is represented, in unit of weight, by the expression,

$$p = 0.0067407 \times 10^{-0.0279712} \,\mathrm{T} - 0.0000625826 \,\mathrm{T}^2$$
.

Multiplying the second member by 336.905 we find the expression of the elastic force of vapor that Laplace deduced from Dalton's experiments. Substituting, in the computation, Regnault's results, the numerical value of these coefficients is somewhat changed, and we find then

$$p = 0.0060527 \times 10^{-0.0301975} \text{ T} - 0.000080170 \text{ T}$$
.

Bessel's tables give the difference of elevation in toises. The logarithm of the difference is obtained by the sum of four logarithms. The same form is preserved in the following tables; but the differences of elevation are given in metres.

The term due to the expansion of the air is computed in Bessel's tables for two values of the coefficient, viz. that of Gay-Lussac, 0.00375, and that of Rudberg, 0.003648; in the new tables it is only computed for that of Regnault, 0.003665.

The relative density of dry air at the freezing point, under a barometrical pressure of 0<sup>m</sup>·.76, and at the 45th degree of latitude, and of mercury in the same circumstances, adopted by Bessel, is that determined by the experiments of Biot and Arago, viz.

1 10466.8. The value of that constant derived from Regnault's experiments has been substituted. Regnault found the weight of a litre of dry air, at zero Centigrade, under a pressure of 0<sup>m</sup>.76, and at the latitude of Paris, to be 1.293187 grammes, which, reduced to the gravity of the 45th degree of latitude, becomes 1.292732 grammes. The weight of a litre of mercury, at zero Centigrade, he found to be 13596 grammes; the ratio is thus:

$$D = \frac{1}{10517.3}$$

or about  $\frac{1}{200}$  smaller than the value adopted by Bessel. If the constant coefficient L is expressed by  $L = \frac{0^{m_1}.76}{D \cdot \mu}$ ,  $\mu$  being the modulus of the common logarithms, its numerical value becomes

$$L = 18404^{m}.8$$

In order to reduce the formula into tables, Bessel caused it to undergo several modifications, which we have followed, introducing the values of the constants above mentioned.

Let b and b' be the heights of the barometer, expressed in the metrical scale, at the two stations; t and t', the temperatures of the mercury measured with a brass scale; we have,

$$P = \frac{b}{0^{m} \cdot .76} \cdot (g) \cdot \left(\frac{a}{a+h}\right)^{2} \frac{(1+0.00001879 t)}{(1+0.00018018 t)},$$

and

$$P' = \frac{b'}{0^{m_*,76}} \cdot (g) \cdot \left(\frac{a}{a+b'}\right)^2 \frac{(1+0.00001879\,t')}{(1+0.00018018\,t')}.$$

Therefore,

$$\log P = \log b + \log (g) - \log 0^{m} \cdot .76 - \frac{2 \text{ H } \mu}{a} - \mu t [0.00018018 - 0.00001879],$$

$$\log P' = \log b' + \log (g) - \log 0^{m} \cdot .76 - \frac{2 H' \mu}{a} - \mu t' [0.00018018 - 0.00001879].$$

If we call B, B' the heights of the barometer reduced to the freezing point, which we obtain by making

$$\log\,\mathrm{B} = \log\,b - t \,.\, 0.000070095 \,; \qquad \log\,\mathrm{B'} = \log\,b' - t' \,.\, 0.000070095,$$

$$\log \frac{P}{P'} = \log B - \log B' + \frac{H' - H}{7329755},$$

and with sufficient accuracy,

$$\checkmark P P' = \frac{\sqrt{B B'}}{0^{m_*}.76}$$

Substituting these expressions in the formula, it becomes,

$$\log B - \log B' = \frac{(g) \cdot H' - H}{L(1 + KT)} \left[ 1 - \frac{L(1 + KT)}{(g) \cdot 7329755} - \frac{a \cdot 0.001748}{\sqrt{BB'}} \cdot 10^{0.0301975} T - 0.000080170 T^{2} \right].$$

If we set instead of  $\alpha$  the half sum  $\frac{\alpha + \alpha}{2}$  of the fraction of saturation observed at both stations, we find, after some transformations,

BAROMETRICAL MEASUREMENT OF HEIGHTS.

$$\log B - \log B' = \frac{(g) (H' - H) (397.25 - KT)}{398.25 \cdot L (1 + KT)} \times \left[1 - \frac{(a + a') \cdot 0.34807}{(397.25 - KT) \sqrt{BB'}} \cdot 10^{0.0301975 T} - 0.000080170 T^{2}\right].$$

Making further,

$$V = \frac{398.25}{397.25 - KT} L (1 + KT),$$

$$W = \frac{0.34807}{397.25 - KT} \cdot 10^{-0.0301975 T - 0.000080170 T^2},$$

we shall have for the logarithm of the approximate difference of level between the two stations H' — H,

$$\log (H' - H) = \log [\log B - \log B'] + \log V + \log \frac{1}{1 - W \frac{a + a'}{V B B'}} + \log \frac{(g)}{1}.$$

Table I. gives the values of log V and log W, both of which only depend on the temperature; the argument is the sum of the temperature of the air,  $\tau$  and  $\tau'$ , observed at both stations, supposing  $\tau + \tau' = 2 \text{ T}$ .

Table II. gives the factor depending on the humidity of the air; with the argument

W.  $\log \frac{(a+a')}{\sqrt{BB'}}$ ,

we obtain

$$\log \frac{1}{1 - W \frac{(a + a')}{\sqrt{B B'}}} = \log V'.$$

Table III. gives the factor depending on the latitude for every degree, viz.

$$\log G' = \log \frac{1}{(g)}.$$

The logarithm of the approximate difference is thus given by the sum of four logarithms. To obtain the exact elevation, the small correction found in Table IV. must be added to the number corresponding to that logarithm. For we have, with the necessary accuracy,

$$h' - h = H' - H + \frac{H'^2}{a} - \frac{H^2}{a}$$
.

Table IV. gives, for every 200 metres, the quantity  $\frac{H^2}{a}$ ; the number in the table corresponding to  $\frac{H'^2}{a}$  must be *added* to the approximate elevation; and the number corresponding to  $\frac{H^2}{a}$  must be subtracted from the same.

#### USE OF THE TABLES.

Reduce first the observed height of the barometer at both stations to the freezing point by means of the usual tables, or by the logarithmic formula,

$$\log B = \log b - t \cdot 0.00007, \quad \log B' = \log b' - t' \cdot 0.00007;$$

b and b' being, in fractions of metre, the observed heights at the temperatures t and t' marked by the attached thermometers; and B and B' the reduced height at the lower and upper station.

Take the difference of log B and log B', and find, in the tables of the common logarithms, the logarithm of that difference, viz. log (log B — log B'); find also the logarithm of the product  $\checkmark$  B B', or

$$\log \checkmark B B' = \frac{\log B + \log B'}{2}.$$

Make further the sum  $\tau + \bar{\tau}'$  of the temperature of the air at both stations, and likewise the sum of a + a' of the fraction of saturation.

Then, in Table I., with argument  $\tau + \tau'$ , take  $\log V$  and  $\log W$ ; further, to  $\log W$  add  $\log (a + a')$ , and subtract  $\log \checkmark BB'$ ; and with the logarithm thus obtained as argument, take in Table II.  $\log V'$ .

Table III. with the mean latitude of the stations gives log G'.

H' — H being the approximate difference of level between the two stations, we have

$$\log (H' - H) = \log (\log B - \log B') + \log V + \log V' + \log G'.$$

The altitude of the lower station being known, we deduce from H' - H the approximate altitude, H', of the upper station; h', the exact altitude, or h' - h, the difference of elevation, is given by the formula,

$$h' - h = H' - H + \frac{H'^2}{a} - \frac{H^2}{a}$$
.

Table IV. gives the values of  $\frac{H^{\prime 2}}{a}$  and  $\frac{H^2}{a}$  for the values of H' or H for every 200 metres.

# Example 1.

Computing the height of St. Bernard, taking Geneva, 407 metres above the level of the sea, as the lower station. The observation gives,

$$\log \left[\log B - \log B'\right] = 9.04215$$
In Table I. argt.  $\tau + \tau' = +7.08$ ,  $\log V = 4.27164$ 
In Table II. argt. 7.4409,  $\log V' = 0.00120$ 
In Table III. argt. 46°,  $\log G' = -0.00004$ 

$$\log (H' - H) = 3.31495$$

$$H' - H = 2065.1 \text{ metres.}$$
In Table IV.  $\frac{H'^2}{a} - \frac{H^2}{a} = + 0.9$ 

$$h' - h = 2066.0$$
Geneva altitude  $h = 407.0$ 

St. Bernard above the level of the sea h' = 2473.0 metres.

## Example 2.

Computing the height of Mont Blanc from the observations of Bravais and Martins, on the 29th of August, 1844, taking St. Bernard (2473.0 metres) as the lower station. The observation gives,

				TABLE	I.				TABL	E IV.
		Argu	ment =	$\tau + \tau'$ . Cer	ntigrade Deg	grees.	`		Arg't. =	Height.
			<u> </u>						777	
$\tau + \tau'$ .	log. V.	log. W.	$\tau + \tau'$ .	log. V.	log. W.	T + T1.	log. V.	log. W.	H'. H.	+
									Metres.	Metres.
-24	4.24644	6.5362	+15	4.27783	7.1692	+54	4.30711	7.7033	200	0.01
-23	4.24728	6.5441	+16	4.27861	7.1839	+55	4.30784	7.7160	400	0.03
-22	4.24811	6.5620	+17	4.27938	7.1985	+56	4.30856	7.7287	600	0.06
-21	4.24894	6.5797	+18	4.28016	7.2131	+57	4.30929	7.7413	800	0.10
-20	4.24977	6.5974	+19	4.28093	7.2275	+58	4.31001	7.7539	1000	0.16
	4.05050	0.0155	100							
-19	4.25059 4.25142	6.6157	+20 +21	4.28170 4.28247	7.2420	+59	4.31073	7.7664	1200	0.23
-18 -17	4.25142	6.6341 6.6521	+21	4.28247	7.2564	+60 +61	4.31145	7.7789	1400 1600	0.31
-16	4.25223	6.6700	+23	4.28400	7.2708 7.2850	+62	4.31288	7.8038	1800	0.40
-15	4.25389	6.6879	+24	4.28477	7.2993	+63	4.31360	7.8161	2000	0.63
	1.23000	0.0010	4	1,50411	1.2333		1.01000	7.0101	2300	0.00
-14	4.25471	6.7057	+25	4.28553	7.3135	+64	4.31432	7.8285	2200	0.76
-13	4.25553	6.7232	+26	4.28629	7.3276	+65	4.31503	7.8407	2400	0.90
-12	4.25634	6.7407	+27	4.28705	7.3417	+66	4.31574	7.8530	2600	1.06
-11	4.25716	6.7581	+28	4.28781	7.3557				2800	1.23
-10	4.25797	6.7755	+29	4.28857	7.3697				3000	1.41
	4.05000	0.0000								
- 9	4.25878	6.7926	+30	4.28933	7.3837				3200	1.61
- 8   - 7	4.25959 4.26040	6.8096	+31	4.29008 4.29084	7.3975				3400	1.82
- 6	4.26121	6.8266 6.8436	+33	4.29084	7.4114				3600 3800	2.04
- 5	4.26202	6.8603	+34	4.29133	7.4389				4000	2.51
	1,20202	0.000		4.20204	1.4003				4000	2.01
- 4	4.26282	6.8770	+35	4.29319	7.4526				4200	2.77
- 3	4.26362	6.8935	+36	4.29384	7.4662				4400	3.04
- 2	4.26443	6.9100	+37	4.29459	7.4798				4600	3.32
- 1	4.26523	6.9263	+38	4.29534	7.4933				4800	3.62
0	4.26603	6.9426	+39	4.29608	7.5068				5000	3.93
	4 00000	0.0503	1.40	4.00000					F000	4.05
+ 1 + 2	4.26682	6.9581 6.9736	+40	4.29683	7.5202				5200 5400	4.25
+ 2 + 3	4.26762 $4.26841$	6.9889	+41	4.29757 4.29831	7.5336				5600	4.93
+ 4	4.26921	7.0043	+43	4.29831	7.5470 7.5602				5800	5.28
+ 5	4.27000	7.0195	+44	4.29979	7.5735				6000	5.65
+ 6	4.27079	7.0347	+45	4.30053	7.5867				6200	6.04
+ 7	4.27157	7.0499	+46	4.30127	7.5999				6400	6.43
+ 8	4.27236	7.0650	+47	4.30200	7.6130				6600	6.84
+ 9	4.27315	7.0800	+48	4.30273	7.6260				6800	7.26
+10	4.27393	7.0950	+49	4.30347	7.6390				7000	7.70
411	1 97477	F 1000	150	4.90400	m 0=10				7000	0.14
+11 +12	4.27471	7.1099 7.1248	+50	4.30420	7.6519				7200 7400	8.14
+13	4.27628	7.1248	+51 +52	4.30493 4.30566	7.6648 7.6777				1400	0.00
+14	4.27705	7.1545	+53	4.30639	7.6905					
+15	4.27783	7.1692	+54	4.30711	7.7033					
									·	

			LE II.				TABL	E III	.
	Arg	gument = lo	og. W. $\frac{(z+\alpha)}{\sqrt{B}}$	<del>;')</del> •			Argument =	= Latit	ude.
Argum't.	log. ∇′.	Argum't.	log. ∇'.	Argum't.	log. ∇'.	φ.	log. G'.	φ.	log. G'.
6.5	0.00014	7.70	0.00218	8.09	0.00538	0	+0.00114	o 40	+0.00020
6.6	0.00017	7.71	0.00223	8.10	0.00550	1	+0.00114	41	+0.00016
6.7	0.00022	7.72	0.00229	8.11	0.00563	2	+0.00114	42	+0.00012
6.8	0.00027	7.73	0.00234	8.12	0.00576	3	+0.00114	43	+0.00008
6.9	0.00034	7.74	0.00239	8.13	0.00590	4	+0.00113	44	+0.00004
7.0	0.00043	7.75	0.00245	8.14	0.00604	5	+0.00112	45	0.00000
7.1	0.00055	7.76	0.00251	8.15	0.00618	6	+0.00112	46	-0.00004
7.2	0.00069	7.77	0.00256	8.16	0.00632	7	+0.00111	47	-0.00008
7.3	0.00087	7.78	0.00262	8.17	0.00647	8	+0.00110	48	-0.00012
7.4	0.00109	7.79	0.00269	8.18	0.00662	9	+0.00109	49	-0.00016
7.41	0.00112	7.80	0.00275	8.19	0.00678	10	+0.00107	50	-0.00020
7.41	0.00112	7.81	0.00273	8.20	0.00694	11	+0.00106	51	-0.00024
7.43	0.00117	7.82	0.00281	8.21	0.00334	12	+0.00104	52	-0.00028
7.44	0.00120	7.83	0.00295	8.22	0.00727	13	+0.00103	53	-0.00031
7.45	0.00123	7.84	0.00302	8.23	0.00744	14	+0.00101	54	-0.00035
									]
7.46	0.00125	7.85	0.00309	8.24	0.00761	15	+0.00099	55	-0.00039
7.47	0.00128	7.86	0.00316	8.25	0.00779	16	+0.00097	56	-0.00043
7.48	0.00131	7.87	0.00323	8.26	0.00798	17	+0.00095	57	-0.00046
7.49	0.00134	7.88	0.00331	8.27	0.00816	18	+0.00092	58	-0.00050
7.50	0.00138	7.89	0.00338	8.28	0.00835	19	+0.00090	59	-0.00054
7.51	0.00141	7.90	0.00346	8.29	0.00855	20	+0.00087	60	-0.00057
7.52	0.00141	7.91	0.00344	8.30	0.00875	21	+0.00085	61	-0.00060
7.53	0.00147	7.92	0.00363	8.31	0.00896	22	+0.00082	62	-0.00064
7.54	0.00141	7.93	0.00371	8.32	0.00917	23	+0.00079	63	-0.00067
7.55	0.00154	7.94	0.00380	8.33	0.00939	24	+0.00076	64	-0.00070
7.56	0.00158	7.95	0.00389	8.34	0.00961	25	+0.00073	65	-0.00073
7.57	0.00162	7.96	0.00398	8.35	0.00983	26	+0.00070	66	-0.00076
7.58	0.00165	7.97	0.00407			27	+0.00067	67	-0.00079
7.59	0.00169	7.98	0.00417			28	+0.00064	68	-0.00082
7.60	0.00173	7.99	0.00427			29	+0.00060	69	-0.00085
7 61	0.00177	8.00	0.00437			30	+0.00057	70	-0.00087
7.61	0.00177	8.01	0.00437			31	+0.00054	71	-0.00090
7.63	0.00186	8.02	0.00447			32	+0.00050	72	-0.00092
7.64	0.00190	8.03	0.00468	1		33	+0.00046	73	-0.00094
7.65	0.00194	8.04	0.00479			34	+0.00043	74	-0.00097
								1	
7.66	0.00199	8.05	0.00490			35	+0.00039	75	-0.00099
7.67	0.00204	8.06	0.00502			36	+0.00035	76	-0.00101
7.68	0.00208	8.07	0.00513			37	+0.00031	77	-0.00102
7.69	0.00213	8.08	0.00525			38	+0.00028	78 79	-0.00104 -0.00106
7.70	0.00218	8.09	0.00538			39	+0.00024	80	-0.00106
	1	1	1	1		40	70.00020	1 30	-0.00107

#### CORRECTION

FOR THE HOUR OF THE DAY AND THE SEASON OF THE YEAR AT WHICH THE OBSERVATIONS HAVE BEEN TAKEN.

In all the preceding tables, the mean temperature of the layer of air between the two stations is assumed to be given by the half-sum of the temperatures observed at each station, or by  $\frac{t+t'}{2}$ . Experience, however, has proved that this assumption is not true under all meteorological circumstances, and that, not to speak of more irregular influences, the temperature expressed by  $\frac{t+t'}{2}$  differs in + or - from the true mean temperature by a quantity which considerably varies with the hour of the day, the season of the year, and the elevation at which the observations are taken. The amount of the correction for the temperature of the air, as given by the various formulas, thus needs to be modified accordingly. In the absence of the data necessary for establishing the law of the decrease of heat on the vertical in the various layers of the atmosphere, at the different periods of the day and of the year, and in different latitudes, which alone would furnish the means of determining the true value of this correction in these various circumstances, the following empirical tables enable us to form a judgment of the importance of that correction.

Tables IX. and X. are taken from Berghaus, Grundriss der Geographie, p. 91, and in the Tables accompanying the same work, p. 71. The correction to be applied for the hour of the day at which the observations have been taken, is found by multiplying the approximate height obtained by the factors in Table IX., giving to the correction the sign of the factor. This table and the following are calculated to be used in the climate of Germany, and for elevations not much exceeding 5,000 feet. The influence of the seasons on the correction is not taken into the account; judging from Table X., the correction may be, perhaps, too small for the summer months, and may better answer for the autumn. Using these factors, we obtain for the differences of level, in toises, placed at the head of each column, in Table X., the correction corresponding to each hour, from 6 A. M. to 10 P. M.

TABLE IX.

Hour.	Factor.	Hour.	Factor,	Hour.	Factor.
A. M. 6	+0.0075	Noon.	-0.0054	P. M. 5	-0.0011
7	+0.0050	P. M. 1	-0.0057	6	+0.0013
8	+0.0025	2	-0.0059	7	+0.0022
9	-0.0005	3	-0.0045	8	+0.0032
10	-0.0035	4	-0.0031	9	+0.0043
11	-0.0044	5	-0.0011	10	+0.0054
		1			

TABLE X.

CORRECTION FOR THE HOUR OF THE DAY.

ARGUMENT, THE HOUR, AND THE APPROXIMATE HEIGHT IN TOISES.

				Correct	ion, in To	ises, for				
Hour.	100	200	300	400	500	600	700	800	900	Hour.
A. M. 6	+0.7	+1.5	+2.2	+3.0	+3.7	+4.5	+5.2	+6.0	+6.7	6 A. M.
7	+0.5	+1.0	+1.5	+2.0	+2.5	+3.0	+3.5	+4.0	+4.5	7
8	+0.2	+0.5	+0.7	+1.0	+1.2	+1.5	+1.8	+2.0	+2.3	8
9	-0.0	-0.1	-0.1	-0.2	-0.2	-0.3	-0.3	-0.4	-0.4	9
10	-0.3	-0.7	-1.0	-1.4	-2.1	-2.4	-2.8	-3.1	-3.5	10
11	-0.4	-0.9	-1.3	-1.8	-2.2	-2.7	-3.1	-3.6	-4.0	11
Noon.	-0.5	-1.1	-1.6	-2.2	-2.7	-3.3	-3.8	-4.4	-4.9	Noon.
P. M. 1	-0.6	-1.1	-1.7	-2.3	-2.8	-3.4	-4.0	-4.5	-5.1	1 P. M.
2	-0.6	-1.2	-1.8	-2.4	-3.0	-3.5	-4.1	-4.7	-5.3	2
3	-0.4	-0.9	-1.3	-1.8	-2.2	-2.7	-3.1	-3.6	-4.0	3
4	-0.3	-0.6	-0.9	-1.2	-1.5	-1.8	-2.1	-2.4	-2.7	4
5	-0.1	-0.2	-0.3	-0.4	-0.5	-0.6	-0.7	-0.8	-0.9	5
6	+0.1	+0.2	+0.4	+0.5	+0.5	+0.8	+0.9	+1.0	+1.1	6
7	+0.2	+0.4	+0.7	+0.9	+1.1	+1.3	+1.6	+1.8	+2.0	7
8	+0.3	+0.6	+0.9	+1.3	+1.6	+1.9	+2.2	+2.5	+2.9	8
9	+0.4	+0.8	+1.3	+1.7	+2.1	+2.6	+3.0	+3.4	+3.8	9
10	+0.5	+1.1	+1.6	+2.1	+2.7	+3.2	+2.8	+4.3	+4.8	10

Table XI. is found in the Résumé des Observations Thermométrique et Barométriques faites à Genève et au Grand St. Bernard pendant les dix années 1841 à 1850, a very elaborate paper by Professor E. Plantamour, Director of the Observatory at Geneva, published in Vol. XIII. of the Mémoires de la Société de Physique de Genève. The author, after having determined the difference of elevation between Geneva (407.0 metres above the level of the sea) and the Great St. Bernard, by means of the corresponding observations, made during these 10 years, and using his own tables given above, reversed the problem. Assuming the difference of level thus found, viz. 2066 metres, to be the true height of the layer of air between the two stations, and its weight being given by the barometrical observations, he deduced from these data its mean density, and from the density its mean temperature at every even hour in every month of the year. Comparing these mean temperatures with those given at the same hours by the half-sum of the temperatures taken at the upper and the lower station, he found the differences contained in Table XI., which are the corrections to be applied to the half-sums of the temperatures to obtain, in this particular case, the true mean temperatures. The second part of the table has been computed by multiplying each temperature in the first by 7.5 metres, in order to show the value of that correction in barometrical measurements.

## TABLE XI.

CORRECTION TO BE APPLIED TO THE HALF-SUMS OF THE TEMPERATURES OF THE AIR, OBSERVED AT GENEVA AND AT THE GREAT ST. BERNARD, TO OBTAIN THE TRUE MEAN TEMPERATURE OF THE AIR BETWEEN THE TWO STATIONS.

				Ce	orrection	, in Cen	tigrade I	Degrees, f	or				
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-0.5	-1.7	-3.0	-3.9	o -4.1	-4.4	-4.4	-3.8	-2.7	-1.6	-0.4	+0.7	0 -2.5
2	-0.2	-1.5	-2.8	-3.7	-4.0	-4.4	-4.4	-3.8	-2.6	-1.5	-0.2	+0.7	-2.3
4	+0.4	-0.6	-1.6	-2.5	-2.7	-3.4	-3.6	-2.9	-1.7	-0.7	+0.4	+1.3	-1.5
6	+1.2	+0.7	-0.2	-0.9	-1.3	-2.1	-2.2	-1.6	-0.5	+0.4	+1.3	+2.1	-0.3
8	+1.5	+1.4	+0.6	0.0	0.0	-0.6	-0.7	-0.5	+0.3	+1.3	+1.7	+2.6	+0.6
10	+1.7	+1.5	+1.2	+0.6	+0.7	+0.5	-0.1	+0.1	+0.8	+1.7	+1.8	+2.6	+1.1
Mid- night.	+1.9	+1.8	+1.9	+1.3	+1.8	+1.6	+0.9	+1.2	+1.3	+2.3	+2.1	+2.5	+1.7
2	+2.0	+2.2	+2.5	+1.9	+2.2	+2.0	+1.5	+2.0	+1.9	+2.5	+2.4	+2.6	+2.2
4	+2.3	+2.5	+2.6	+1.8	+1.7	+1.4	+1.1	+1.8	+2.1	+2.5	+2.7	+2.9	+2.1
6	+2.0	+2.0	+1.7	+0.7	+0.4	+0.1	0.0	+0.7	+1.5	+1.7	+2.3	+2.9	+1.3
8	+1.5	+1.1	0.0	-1.3	-2.0	-2.2	-2.4	-1.7	-0.4	+0.6	+1.7	+2.5	-0.3
10	+0.4	-0.4	-2.0	-3.1	-3.5	-3.8	-3.7	-3.1	-2.0	-1.0	+0.3	+1.3	-1.7
Mean,	+1.2	+0.8	+0.1	-0.8	-0.9	-1.2	-1.5	-0.9	-0.2	+0.7	+1.3	+2.1	0.0
			l		1	<u> </u>	1	1	<u> </u>	1	1	1	<u> </u>
			I		Cor	rection, i	n Metres	s, for	<u> </u>	1	ı		
Hour.	Jan.	Feb.	March.	April.	Cor	June.	n Metres	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Hour.	Jan 3.7	Feb	March22.5	April29.2	1	ĺ	<u> </u>	· 	Sept20.2	Oct.		Dec. + 5.2	
					May.	June.	July.	Aug.			- 3.0 - 1.5	+ 5.2 + 5.2	-18.
Noon.	- 3.7 - 1.5 + 3.0	-12.7 -11.2 - 4.5	-22.5 -21.0 -12.0	-29.2 -27.7 -18.7	May.  -30.7  -30.0  -20.2	June33.0 -33.0 -25.5	July33.0 -33.0 -27.0	Aug28.5 -28.5 -21.7	-20.2 -19.5 -12.7	-12.0 -11.2 - 5.2	- 3.0 - 1.5 + 3.0	+ 5.2 + 5.2 + 9.7	-18. <sup>7</sup>
Noon. 2 4 6	- 3.7 - 1.5 + 3.0 + 9.0	-12.7 $-11.2$ $-4.5$ $+5.2$	-22.5 -21.0 -12.0 - 1.5	-29.2 -27.7 -18.7 - 6.7	May.  -30.7  -30.0  -20.2  - 9.7	June.  -33.0  -33.0  -25.5  -15.7	July33.0 -33.0 -27.0 -16.5	Aug.  -28.5  -28.5  -21.7  -12.0	-20.2 -19.5 -12.7 - 3.7	-12.0 -11.2 - 5.2 + 3.0	- 3.0 - 1.5 + 3.0 + 9.7	+ 5.2 + 5.2 + 9.7 +15.7	-18.7 -17.5 -11.5 - 2.5
Noon. 2 4 6 8	- 3.7 - 1.5 + 3.0 + 9.0 +11.2	-12.7 $-11.2$ $-4.5$ $+5.2$ $+10.5$	-22.5 -21.0 -12.0 - 1.5 + 4.5	-29.2 -27.7 -18.7 - 6.7 0.0	-30.7 -30.0 -20.2 - 9.7 0.0	June.  -33.0 -33.0 -25.5 -15.7 - 4.5	July33.0 -33.0 -27.0 -16.5 - 5.2	Aug.  -28.5 -28.5 -21.7 -12.0 - 3.7	-20.2 -19.5 -12.7 - 3.7 + 2.2	-12.0 -11.2 - 5.2 + 3.0 + 9.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7	+ 5.2 + 5.2 + 9.7 +15.7 +19.5	-18.1 -17.1 -11.1 - 2.1 + 4.5
Noon. 2 4 6 8 10	- 3.7 - 1.5 + 3.0 + 9.0	-12.7 $-11.2$ $-4.5$ $+5.2$	-22.5 -21.0 -12.0 - 1.5	-29.2 -27.7 -18.7 - 6.7 0.0	May.  -30.7  -30.0  -20.2  - 9.7	June.  -33.0  -33.0  -25.5  -15.7	July33.0 -33.0 -27.0 -16.5	Aug.  -28.5  -28.5  -21.7  -12.0	-20.2 -19.5 -12.7 - 3.7	-12.0 -11.2 - 5.2 + 3.0	- 3.0 - 1.5 + 3.0 + 9.7	+ 5.2 + 5.2 + 9.7 +15.7	-18.3 -17.3 -11.5 - 2.5 + 4.5
Noon. 2 4 6 8	- 3.7 - 1.5 + 3.0 + 9.0 +11.2	-12.7 $-11.2$ $-4.5$ $+5.2$ $+10.5$ $+11.2$	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0	-29.2 -27.7 -18.7 - 6.7 0.0	May.  -30.7  -30.0  -20.2  - 9.7  0.0  + 5.2	June.  -33.0  -33.0  -25.5  -15.7  - 4.5  + 3.7	July33.0 -33.0 -27.0 -16.5 - 5.2	Aug.  -28.5 -28.5 -21.7 -12.0 - 3.7	-20.2 -19.5 -12.7 - 3.7 + 2.2	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7	+ 5.2 + 5.2 + 9.7 +15.7 +19.5	-18.7 -17.3 -11.5 - 2.5 + 4.5 + 8.5
Noon. 2 4 6 8 10 Mid-	- 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7	-12.7 $-11.2$ $-4.5$ $+5.2$ $+10.5$ $+11.2$	$ \begin{array}{r} -22.5 \\ -21.0 \\ -12.0 \\ -1.5 \\ + 4.5 \\ + 9.0 \\ +14.5 \end{array} $	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5	May.  -30.7  -30.0  -20.2  - 9.7  0.0  + 5.2	June.  -33.0  -33.0  -25.5  -15.7  - 4.5  + 3.7	July.  -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7	Aug.  -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5	-18.7 -17.5 -11.5 - 2.5 + 4.5 + 8.6
Noon. 2 4 6 8 10 Mid-night. 2 4	- 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5	-30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7	June.  -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7	July.  -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7	Aug.  -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7	$ \begin{array}{r} -20.2 \\ -19.5 \\ -12.7 \\ -3.7 \\ +2.2 \\ +6.0 \\ +9.7 \end{array} $	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +18.7 +18.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2	+ 5.2 + 5.2 + 5.7 + 15.7 + 19.5 + 19.5 + 19.5 + 19.5 + 21.7	Year18.7 -17.2 -11.5 - 2.2 + 4.5 + 8.5 +12.7 +16.5 +15.7
Noon.  2 4 6 8 10  Midnight. 2 4 6	- 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2 +15.0	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7 +15.0	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5	$\begin{array}{c} -29.2 \\ -27.7 \\ -18.7 \\ -6.7 \\ 0.0 \\ +4.5 \\ +9.7 \\ +14.2 \\ +13.5 \\ +5.2 \end{array}$	-30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7 + 3.0	June.  -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +10.5 + 0.7	July.  -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 +11.2	Aug.  -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +17.2 +18.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2 +17.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5 +21.7 +21.7	-18.: -17.: -11.: - 2.: + 4.: + 8.: +12.: +16.: +15.: + 9.:
Noon.  2 4 6 8 10  Midnight. 2 4 6 8	- 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2 +15.0 +11.2	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7 +15.0 + 8.2	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5 +12.7	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5 + 5.2 - 9.7	May.  -30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7 + 3.0 -15.0	June.  -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +15.0 +10.5 + 0.7 -16.5	July.  -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 +11.2 + 8.2 0.0 -18.0	Aug.  -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2 -12.7	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7 +11.2 - 3.0	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +18.7 +18.7 +12.7 + 4.5	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2 +17.2 +12.7	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +19.5 +21.7 +21.7 +18.7	-18.2 -17.3 -11.3 - 2.3 + 4.3 + 8.4 + 12.3 + 16.5 + 9.7 - 2.2
Noon. 2 4 6 8 10 Midnight. 2 4 6	- 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2 +15.0	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7 +15.0	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5 +12.7	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5 + 5.2 - 9.7	-30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7 + 3.0	June.  -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +10.5 + 0.7	July.  -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2 0.0	Aug.  -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7 +11.2	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +17.2 +18.7 +18.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2 +17.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5 +21.7 +21.7	-18.3 -17.3 -11.3 - 2.3 + 4.8 + 8.8 +12.3 +16.8

The elevation of a place in the interior of a continent where regular meteorological observations are made, may be ascertained by taking the yearly means of the barometer reduced to the freezing point, and of the temperature of the air, as data for the upper station, and the yearly means of the reduced barometer and of the free thermometer at the level of the sea, as the data for the lower station. The Hypsometric Tables then will give the difference of level. As observation, however, has shown that the mean height of the barometer at the level of the sea is not the same in all latitudes, it is necessary to take for such a comparison the mean height of the barometer which belongs to the latitude of the station the elevation of which is to be computed, or that which is nearest to it.

Table XII., published by Schouw, in Poggendorf's Annalen, and in the Comptes Rendus de l'Académie des Sciences, Tom. III. p. 573, gives in Paris lines the mean height of the barometer in various latitudes. The reduction into millimetres is from Martins's French translation of Kaemtz's Meteorology, p. 278; the corresponding values in English inches, and the new stations, Savannah, Ga., Philadelphia, Pa., and Cambridge, Mass., have been added. The mean heights last mentioned have been derived from three years of observations at Savannah, by Dr. John F. Posey, from June, 1853, to June, 1856, published in the American Almanac; from four years of hourly observations at Girard College, Philadelphia, by Prof. A. D. Bache; and from ten years of observations at Cambridge Observatory. They have been reduced to a common absolute standard and to mean tide-water at the respective places.

These mean barometric heights, corrected for the variation of gravity in latitude, according to the proposition of Poggendorf, by the formula b=b 45 (1 — 0.0025935 cos 2  $\phi$ ), where b is the height of the barometer in latitude  $\phi$ , and b 45 the corresponding height at the forty-fifth degree of latitude, are found in another column. For computing the elevations, the uncorrected heights are to be used.

The mean barometric pressure, as shown by Table XIII. from Kaemtz's Précis de Météorologie, French translation, p. 281, is not the same in all seasons, and the monthly means differ by a quantity which also varies with the latitude. If, therefore, the height of an inland station is to be ascertained from the barometrical means of one or more months only, the computation must be made with the mean pressure in the corresponding months at the level of the sea; or if this is not known, the yearly means taken from Table XII. must be corrected for the difference between the monthly means of the given month, or months, and the annual mean in the same latitude, as derived from the comparison of the numbers in Table XIII.

## Example.

Suppose an inland station, in latitude 40° N.; the mean barometric pressure for July is 26.30 inches, and its elevation is to be computed from it.

Table XII. gives for latitude  $40^\circ$ , at Philadelphia, reduced to the level of the sea, 30.053 inches. Table XIII. gives as the mean for July, at the same place, 759.80 millimetres, and for the year, 760.25 millimetres (both not reduced to the level of the sea), difference — 0.45 millimetres = -0.017 English inches, which is to be subtracted from the annual mean, 30.053, to reduce it to the mean of July; or

30.053 - 0.017 = 30.036. This last number is to be used in the computation, with the mean temperature of July at both stations.

Towards the tropical regions, the irregular or non-periodic variations of the barometer, which in high and middle latitudes are so considerable as to render simultaneous observations indispensable for the measurement of heights, gradually decrease and nearly cease to exist, while the monthly and daily periodic variations, which are small in high latitudes, considerably increase. Within the tropics, therefore, the oscillations of the barometer being far more uniform, observations made during a short period of time, or even single observations, may be used for computing heights, without corresponding observations, by referring them to the mean pressure at the level of the sea as to a constant, provided this last has been corrected for the monthly and daily periodic variation at the place.

Table XIII. furnishes the means of applying the correction for the monthly variation, as described above. Table XIV., which gives the mean height of the barometer at all hours of the day in various latitudes, enables the observer to correct the data according to the hour at which the observations have been taken. This table is from Kaemtz's Vorlesungen über Meteorologie, French translation, p. 249. The column Bossekop is from the observations of the French Scientific Expedition in the North; the column Philadelphia, from the observations at Girard College, has been added.

The correction for the hourly variation is found by taking the difference between the mean of the hour of observation and the daily mean, and correcting accordingly, with due regard to the signs, either the yearly mean at the sea level, or the observation at the upper station.

## Example.

The barometer at Caracas, latitude 10° 30′ N., on the 20th of August, at 4 o'clock P. M., reads 680.57 millimetres.

which is the number to be used for the computation of the height of Caracas. In this case, however, the monthly correction, being derived from a higher latitude, may be too small. Both corrections can of course be applied, with contrary signs, to the observation at Caracas, leaving then the mean height at the level of the sea as a constant.

# TABLE XII.

### MEAN HEIGHT OF THE BAROMETER,

IN VARIOUS LATITUDES, REDUCED TO THE LEVEL OF THE SEA, AND TO THE FREEZING POINT.

		In Milli	metres.	In Englis	h Inches.	In Pari	s Lines.
Places.	Latitude.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.
Cape of Good Hope,	o , 33 S.	763.01	762.20	30.041	30.008	338.24	337.88
Rio Janeiro, Brazil,	23 s.	764.03	762.65	30.080	30.026	338.69	338.08
Christiansborg, Guinea,	5 30N.	760.10	758.16	29.925	29.850	336.95	336.09
La Guayra, Venezuela,	10	760.17	758.32	29.928	29.855	336.98	336.16
St. Thomas, W. Indies,	19	760.51	758.95	29.942	29.881	337 13	336.44
Macao, China,	23	762.99	761.61	30.040	29.986	338.23	337.62
Teneriffe, Canary Isles,	28	764.21	763.10	30.087	30.044	338.77	338.28
Savannalı, Georgia,	32	764.59	763.74	30.102	30.070	338.93	338.57
Funchal, Madeira,	32 30	765.18	764.34	30.126	30.093	339.20	338.83
Tripoli, Northern Africa,	33	767.41	766.60	30.214	30.182	340.19	339.83
Palermo, Sicily,	38	762.95	762.47	30.038	30.019	338.21	338.00
Philadelphia, Penn.	40	763.35	763.00	30.053	30.040	338.38	338.23
Naples, Italy,	41	762.34	762.06	30.014	30.003	337.94	337.82
Cambridge, Mass.	42	762.44	762.24	30.018	30.010	337.99	337.90
Florence, Italy,	43 30	761.93	761.81	29.997	29.993	337.76	337.71
Avignon, France,	44	762.02	761.95	30.001	29.998	337.80	337.77
Bologna, Italy,	44 30	762.18	762.13	30.007	30.005	337.87	337.85
Padua, Italy,	45	762.18	762.18	30.007	30.007	337.87	337.87
Paris, France,	49	761.41	761.68	29.978	29.988	337.53	337.65
London, England,	51 30	760.96	761.41	29.960	29.978	337.33	337.53
Altona, Denmark,	53 30	760.42	761.01	29.938	29.961	337.09	337.35
Dantzig, Prnssia,	54 30	760.10	760.76	29.925	29.952	336.95	337.24
Königsberg, Prussia,	54 30	760.49	761.14	29.941	29.967	337.12	337.41
Apenrade, Denmark,	55	759.58	760.71	29.906	29.950	336.72	337.22
Edinburgh, Scotland,	56	758.25	759.00	29.853	29.882	336.13	336.46
Christiania, Norway,	60	758.64	759.63	29.868	29.908	336.30	336.74
Hardanger, Norway,	60	756.94	757.04	29.801	29.841	335.55	335.99
Bergen, Norway,	60	757.01	758.00	29.804	29.844	335.58	336.02
Reikiavig, Iceland,	64	752.00	753.20	29.607	29.654	333.36	333.89
Godthaab, S. Greenland,	64	751.94	753.13	29.605	29.651	333.33	333.86
Eyafiord, Iceland,	66	753.58	754.89	29.669	29.721	334.06	334.64
Godhavn, Disco, Greenl.	. 68	753.76	755.16	29.677	29.731	334.14	334.76
Upernavik, N. Greenl.	73	755.18	756.80	29.732	29.796	331.77	335.49
Melville Isl., Arct. Amer.	1	757.08	758.75	29.807	29.872	335.61	336.35
Spitzbergen,	75 30	756.76	758.48	29.794	29.862	335.47	336.23

# XIII. MEAN HEIGHT OF THE BAROMETER, IN ALL MONTHS OF THE YEAR, IN VARIOUS LATITUDES.

Not reduced to the Level of the Sea.

Places,	HAVANA.	CAL-	MACAO.	CAIRO.	SA- VANNAH.	PHILA- DELPHIA.	CAM- BRIDGE.	PARIS.	St. Pe-
Latitude,	230 9'	220 33'	220 11'	30° 2′	320 5/	39° 58′	42° 23′	48° 50′	59° 56′
Jan.	765.24	764.57	767.93	762.40	762.80	760.97	761.37	758.86	762.54
Feb.	760.15	758.86	767.01	66	763.76	759.63	760.90	759.09	763.10
March,	760.98	756.24	766.08	759.43	763.05	760.51	759.09	756.33	760.76
April,	759.58	753.83	761.93	760.10	763.10	760.05	759.37	755.18	761.19
May,	758.19	750.81	761.64	758.23	763.39	759.09	759.63	755.61	760.94
June,	760.67	748.10	757.31	754.42	764.37	759.22	758.91	757.28	759.83
July,	760.67	747.54	757.91	753.90	764.02	759.80	760.34	756.52	758.25
Aug.	757.33	748.53	757.91	754.06	765.54	760.54	761.11	756.74	759.94
Sept.	757.46	751.83	762.22	756.70	763.36	761.25	761.83	756.61	761.19
Oct.	758.19	755.25	763.37	759.70	763.13	760.68	761.07	754.42	760.82
Nov.	761.25	758.37	766.17	760.76	763.41	760.49	760.85	755.75	758.05
Dee.	763.62	760.59	768.65	761.82	761.12	760.82	760.80	755.09	760.22
Year,	760.28	754.54	763.18	758.32	763.41	760.25	760.44	756.46	760.57

# XIV. MEAN HEIGHT OF THE BAROMETER, AT ALL HOURS OF THE DAY, IN VARIOUS LATITUDES.

Not reduced to the Level of the Sca.

	Not reduced to the Level of the Sca.												
Places,	PACIFIC OCEAN.	CUMANA.	LA GUAYRA.	CAL- CUTTA.	PHILADEL- PHIA.	PADUA.	HALLE	St. Pe- TERSBURG	Bossekop.				
Latitude,	00 0'	10° 28′N.	10° 36′n.	22° 35′n.	39° 58′N.	45° 24′n.	51° 29'n.	59° 56′N.	69° 58'N.				
Observers,	Horner.	Hum- boldt.	Boussin- gault.	Balfour.	Bache.	Ciminello.	Kaemtz.	Kupffer.	Bravais.				
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.				
Midnight,	752.47	756.86	759.64	758.80	760.49	757.01	753.23	759.35	754.90				
1	752.20	756.53	759.34	758.62	760.46	756.90	753.14	66	66				
2	751.77	756.21	759.05	758.57	760.41	756.84	753.05	759.32	754.79				
3	751.63	755.89	758.81	758.49	760.34	756.78	752.99	66	66				
4	751.32	755.66	758.68	758.47	760.39	756.74	752.99	759.32	754.70				
5	751.65	755.79	758.85	758.44	760.49	756.75	753.34	46	66				
6	751.95	756.18	759.32	758.68	760.75	756.79	753.12	759.39	754.68				
7	752.48	756.58	759.94	759.16	761.00	756.89	753.24	66	66				
8	752.95	756.98	760.50	759.88	761.15	757.01	753.37	759.49	754.75				
9	753.16	757.31	759.63	760.11	761.22	757.08	753.44	66	66				
10	753.15	757.32	760.50	760.19	761.17	757.14	753.46	759.51	754.96				
11	752.80	757.01	759.99	760.09	760.97	757.07	753.40	66	66				
Noon,	752.35	756.57	759.41	759.61	760.56	757.02	753.29	759.47	755.01				
1	751.87	755.99	758.91	759.22	760.13	756.85	753.11	66	66				
2	751.55	755.47	758.41	758.39	759.83	756.67	752.99	759.38	754.96				
3	751.15	755.14	758.12	758.12	759.65	756.54	752.89	66	66				
4	751.02	754.96	758.05	757.91	759.65	756.47	753.84	759.32	754.82				
5	751.31	755.14	758.10	757.93	759.70	756.46	752.86	66	66				
6	751.71	755.41	758.40	758.01	759.85	756.50	752.91	759.31	754.87				
7	751.93	755.81	758.90	758.02	760.08	756.63	753.02	66	66				
8	752.35	756.21	759.19	758.54	760.31	756.79	753.14	759.32	754.89				
9	752.74	756.59	759.69	759.24	760.49	756.92	753.24	66	66				
10	752.85	756.87	759.93	759.33	760.59	757.02	753.31	759.36	754.92				
11	752.86	757.15	759.98	759.09	760.72	757.02	753.29	66					
Mean,	752.13	756.33	759.22	758.87	760.43	756.83	753.19	759.38	754.85				

#### BAROMETRICAL MEASUREMENT OF HEIGHTS.

Table XIV. shows that, after all irregular variations of the barometer have been eliminated, there remains a double period of rise and fall within the twenty-four hours, and that the amplitude of these daily oscillations is greatest within the tropics, and goes on diminishing towards the polar regions.

According to Kaemtz, the mean time of the daily maxima and minima, or the mean tropic hours for the northern hemisphere, are as follows:—

The minimum of the afternoon is reached at 7.05 P. M.

The maximum of the evening is reached at 7.10.11 P. M.

The minimum of the night is reached at 7.345 A. M.

The maximum of the morning is reached at 7.37 A. M.

Even in temperate and high latitudes these diurnal variations, though small, must be taken into account, if great accuracy is required, in reducing corresponding observations made at a somewhat different hour to the time of the observation at the station the height of which is to be determined. But in so doing, it must be remembered that the times of the minima and maxima change with the seasons, as is shown by Table XV. from Kaemtz, p. 251 of the French translation.

XV. TROPIC HOURS OF THE DAILY VARIATION OF THE BAROMETER AT HALLE. LAT.  $51^{\circ}~30'$  N.

Month.	Minimum, P. M.	Maximum, P. M.	Minimum,	Maximum, A. M.	Month.	Minimum, P. M.	Maximum, P. M.	Minimum, A. M.	Maximum, A. M.
	h.	h.	h.	h.		h.	h.	h.	h.
Jan.	2.81	9.17	4.91	9.91	July,	5.21	11.04	3.04	8.73
Feb.	3.43	9.46	3.86	9.66	Aug.	4.86	10.66	3.06	8.96
March,	3.82	9.80	3.87	10.10	Sept.	4.55	10.45	3.45	9.71
April,	4.46	10.27	3.53	9.53	Oct.	4.17	10.24	3.97	10.07
May,	5.43	10.93	3.03	9.13	Nov.	3.52	9.85	4.68	10.08
June,	5.20	10.93	2.83	8.73	Dec.	3.15	9.11	4.91	10.18

This shifting of the times of maxima and minima with the seasons diminishes with the latitude, and tends to disappear towards the equator, with the inequality of the days and nights. The elevation above the level of the sea also causes a change in the tropic hours of the daily variation which is not yet sufficiently studied.

Table XIV. gives evidence that the amplitude of the hourly oscillation is greatest under the equator, and gradually decreases towards the pole. Kaemtz computes its mean value in various latitudes and at the level of the sea, as follows:—

XV'. AMPLITUDE OF DAILY VARIATIONS IN VARIOUS LATITUDES.

Latitude. Variati	on. Latitude.	Variation.	Latitude.	Variation.	Latitude	Variation.
0 0 0 2.28 5 26 N. 2.20 17 52 2.00	3 23 55 5 29 28	Millim. 1.80 1.58 1.35	39 4 43 34 48 1	Millim. 1.13 0.90 0.67	52 33 57 17 62 25	Millim. 0.45 0.23 0.00

The amplitude also decreases with the elevation, at least in our latitudes; it was found to be on the Faulhorn, in Switzerland, 9000 feet above the sea level, 0.27 millimetres, while it was 0.90 millimetres at Geneva.

#### TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANOTHER LEVEL.

To reduce barometric means taken at a given elevation to the height they would have if taken at the level of the sea, or barometric observations made at different elevations to a common level, in order to eliminate the influence of altitude in the comparison of barometric pressures, is a problem, the solution of which is often needed in meteorology.

For a complete and accurate reduction, embracing all cases, Tables IV. and V., by Dippe, given above, pages 54 et seq., may be used. But when the difference of height between the two stations, or above the sea-level, does not exceed a few hundred feet, the small tables XVI. to XIX., in three different scales, will be found more convenient.

Tables XVI. and XVII. have been computed from the constants of Laplace's formula, the barometric coefficient, including the correction for the decrease of gravity on a vertical, being respectively 60,345.51 English feet and 56,621.83 Paris feet; and the coefficient for expansion of moist air 0.00222 and 0.005.

In Table XVIII. the coefficient 18,420 metres, deduced from Regnault's experiments (see *Proceedings of the Amer. Assoc. for Adv. of Science*, 1857), and his coefficient for expansion of dry air, 0.003665, increased to 0.0039, in order to include the effect of moisture, have been used.

### Use of the Tables.

The correction for reducing the barometer to the level of the sea is found by the formula

$$C = \frac{f}{N} \times \frac{h'}{h},$$

where C is the correction required; f, the elevation of the station; N, the number in the tables; h', the reading of the barometer; h, the normal height of barometer at the sea-level.

## Example.

At Cambridge Observatory, Massachusetts, at 71.34 English feet above mean tide, the mean barometer is = 29.939 inches; the mean temperature 47°.3 Fahrenheit; what would be the height at the level of the sea?

In Table XVI. we take for  $47^{\circ}.3 = 90.49$ , or, in order to get the correction in a fraction of an inch, 904.9.

Then

$$C = \frac{71.34}{904.9} \times \frac{29.939}{30} = 0.079$$
, correction required;

and

29.939 + 0.079 = 30.018 inches, height of the barometer at the level of the sea.

It will be seen that the quantity represented by the second member can be neglected without causing a sensible error in the correction. In this case the error does not amount to .001; it scarcely would reach .002 for 250 feet of elevation; so that the reduction can be made in most cases by a simple division; viz.  $\frac{f}{N}$ .

XVI. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR CORRESPONDING TO A TENTH OF AN ENGLISH INCH IN THE BAROMETER, AT TEMPERATURES BETWEEN  $32^\circ$  AND  $100^\circ$  FAHRENHEIT,

The Barometric Pressure at the Lower Station being = 30 English Inches.

Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.
32°	87.51	46°	90.23	60°	92.95	74°	95.67	87°	98.20
33	87.70	47	90.42	61	93.15	75	95.87	88	98.40
34	87.90	48	90.62	62	93.34	76	96.06	89	98.59
35	88.09	49	90.81	63	93.53	77	96.26	90	98.79
36	88.28	50	91.01	64	93.73	78	96.45	91	98.98
37	88.48	51	91.20	65	93.92	79	96.65	92	99.17
38	88.67	52	91.40	66	94.12	80	96.84	93	99.37
39	88.87	53	91.59	67	94.31	81	97.04	94	99.56
40	89.06	54	91.78	68	94.51	82	97.23	95	99.76
41	89.26	55	91.98	69	94.70	83	97.42	96	99.95
42	89.45	56	.92.17	70	94.90	84	97.62	97	100.15
43	89.65	57	92.37	71	95.09	85	97.81	98	100.34
44	89.84	58	92.56	72	95.29	86	98.01	99	100.54
45	90.03	59	92.76	73	95.48	87	98.20	100	100.73

XVII. HEIGHT, IN FRENCH FEET, OF A COLUMN OF AIR CORRESPONDING TO A PARIS LINE IN THE BAROMETER, AT TEMPERATURES OF THE AIR BETWEEN  $0^\circ$  AND  $34^\circ$  REAUMUR,

The Barometric Pressure at the Lower Station being = 337 Paris Lines.

Temper- ature of Air, Reaumur.	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Feet
0°	73.08	7°	75.63	14°	78.19	21°	80.75	28°	83.31
1	73.44	8	76.00	15	78.56	22	81.11	29	83.67
2	73.81	9	76.36	16	78.92	23	\$1.48	30	84.04
3	74.17	10	76.73	17	79.29	24	81.85	31	84.40
4	74.54	11	77.10	18	79.65	25	82.21	32	84.77
5	74.90	12	77.46	19	80.02	26	82.58	33	85.13
6	75.27	13	77.83	20	80.38	27	82.94	34	85.50

XVIII. HEIGHT, IN METRES, OF A COLUMN OF AIR CORRESPONDING TO A MILLIMETRE IN THE BAROMETER, AT TEMPERATURES BETWEEN  $0^{\circ} \ \, \text{AND} \ \, 39^{\circ} \ \, \text{CENTIGRADE},$ 

The Barometric Pressure at the Lower Station being = 760 Millimetres.

Temper- ature of Air, Centigr	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.
0°	10.54	s°	10.86	16°	11.19	24°	11.52	32°	11.85
1	10.58	9	10.91	17	11.23	25	11.56	33	11.89
2	10.62	10	10.95	18	11.28	26	11.60	34	11.93
3	10.66	11	10.99	19	11.32	27	11.64	35	11.97
4	10.70	12	11.03	20	11.36	28	11.69	36	12.01
5	10.74	13	11.07	21	11.40	29	11.73	37	12.06
6	10.78	14	11.11	22	11.44	30	11.77	38	12.10
7	10.82	15	11.15	23	11.48	31	11.81	39	12.14

Table XIX. gives, in metrical measure, the values of a millimetre in the barometer at different elevations and Centigrade temperatures. The values are derived from Laplace's constants, as in Tables XVI. and XVII.

This table may be used, as the preceding ones, for reducing barometrical observations to the level of the sea, and also to any other level by a similar process.

### Example.

Suppose the barometer to read 700 millimetres at the altitude of 750 metres, the temperature of air being = 16° Centigrade; what would be the reading at a station lower by 350 metres, assuming the temperature of the air downwards to increase at the rate of 1° Centigrade for 185 metres?

The temperature of air at lower station will be  $16^{\circ} + 1^{\circ}.9 = 17^{\circ}.9$ 

The approximate height of barometer about 73 centimetres.

Then, in Table XIX. we find for 16° and 70 centimetres, 12.15

" for 17°.9 and 73 centimetres, 11.73

Mean 11.94

And

 $\frac{350}{11.94} = 29.31$ , or barometer at lower station 700 + 29.31 = 729.31 millimetres.

Delcros's tables, with these data, would give for the difference of level 349.76, instead of 350 metres; the corresponding error in the height of the barometrical column does not exceed 0.08 millimetre, and thus remains within the limits of error which may be expected in an ordinary observation.

The principal object of this table, however, is to furnish the scientific traveller with the means of readily computing on the spot approximate differences of level, by simply multiplying the difference between the readings of the barometer at each station by the half sum of the numbers in the table corresponding to the data given by the observations.

### Example.

Suppose the barometer at the lower station to read 732.5, and at the upper station 703.2 millimetres; the temperature of the air being respectively 18° and 16° Centigrade.

The difference of the barometers, supposed to be reduced to the same temperature, is 29.3 millimetres.

Then, Table XIX. gives for 18° Centigrade and 73 centimetres, 11.73 " for 16° Centigrade and 70 centimetres, 12.15

Half sum, or mean, 11.94

And,  $29.3 \times 11.94 = 349.8$  metres = difference of level required.

By the large tables of Delcros, we find for the same data 350.1 metres.

This table can be considered as a complement to Delcros's tables, and may save the traveller the trouble of carrying the larger tables.

A similar table in English measures is found above, at the end of the author's larger tables (Table VI.), page 48 of this series, and another, more extensive one, below, page 92, the use of which is explained by the examples just given.

XIX. HEIGHT, IN METRES, OF A COLUMN OF AIR, CORRESPONDING TO A MILLIMETRE IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

Temper- ature of			Barome	eter at the	Lower Sta	tion, Readi	ng in Cent	imetres.					
Air, Centig.	76	75	74	73	72	71	70	69	68	67			
0	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre			
0	10.52	10.66	10.80	10.94	11.10	11.26	11.42	11.59	11.75	11.9			
2	10.60	10.74	10.89	11.03	11.19	11.35	11.51	11.68	11.85	12.03			
4	10.69	10.83	10.97	11.12	11.28	11.44	11.60	11.77	11.94	12.1			
6	10.77	10.91	11.06	11.20	11.37	11.53	11.69	11.86	12.04	12.2			
8	10.85	11.00	11.15	11.29	11.46	11.62	11.78	11.96	12.13	12.3			
10	10.94	11.08	11.23	11.38	11.55	11.71	11.87	12.05	12.22	12.4			
12	11.02	11.17	11.32	11.47	11.63	11.80	11.97	12.14	12.32	12.5			
14	11.11	11.25	11.41	11.55	11.72	11.89	12.06	12.23	12.41	12.6			
16	11.19	11.34	11.49	11.64	11.81	11.98	12.15	12.33	12.51	12.7			
18	11.27	11.43	11.58	11.73	11.90	12.07	12.24	12.42	12.60	12.7			
20	11.36	11.51	11.67	11.82	11.99	12.16	12.33	12.51	12.69	12.8			
22	11.44	11.60	11.75	11.90	12.08	12.25	12.42	12.61	12.79	12.9			
24	11.53	11.68	11.84	11.99	12.17	12.34	12.51	12.70	12.88	13.0			
26	11.61	11.77	11.93	12.08	12.26	12.43	12.61	12.79	12.98	13.1			
28	11.70	11.85	12.01	12.17	12.35	12.52	12.70	12.88	13.07	13.2			
30	11.78	11.94	12.10	12.25	12.43	12.61	12.79	12.98	13.16	13.3			
32	11.86	12.02	12.18	12.34	12.52	12.70	12.88	13.07	13.26	13.4			
34	11.95	12.11	12.27	12.43	12.61	12.79	12.97	13.16	13.35	13.5			
36	12.03	12.19	12.36	12.52	12.70	12.88	13.06	13.25	13.45	13.6			
38	12.12	12.28	12.44	12.60	12.79	12.97	13.15	13.35	13.54	13.7			
Temper-	1			Ba	rometer in	Centimetr	es.						
Air, Centig.	66	65	64	63	62	61	60	59	58	57			
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres			
0	12.11	12.30	12.49	12.69	12.89	13.10	13.32	13.55	13.78	14.0			
2	12.21	12.40	12.59	12.79	13.00	13.21	13.43	13.66	13.89	14.1			
4	12.31	12.50	12.69	12.89	13.10	13.31	13.54	13.77	14.00	14.2			
6	12.40	12.60	12.79	13.00	13.20	13.42	13.64	13.88	14.11	14.3			
8	12.50	12.69	12.89	13.10	13.31	13.52	13.75	13.98	14.22	14.4			
10	12.60	12.79	12.99	13.20	13.41	13.63	13.86	14.09	14.34	14.5			
12	12.69	12.89	13.09	13.30	13.51	13.73	13.96	14.20	14.45	14.70			
14	12.79	12.99	13.19	13.40	13.62	13.84	14.07	14.31	14.56	14.81			
16	12.89	13.09	13.29	13.50	13.72	13.94	14.18	14.42	14.67	14.92			
18	12.98	13.19	13.39	13.61	13.82	14.05	14.28	14.53	14.78	15.0			
20	13.08	13.28	13.49	13.71	13.93	14.15	14.39	14.63	14.89	15.15			
22	13.18	13.38	13.59	13.81	14.03	14.26	14.50	14.74	15.00	15.26			
24	13.27	13.48	13.69	13.91	14.13	14.36	14.60	14.85	15.11	15.37			
26	13.37	13.58	13.79	14.01	14.24	14.47	14.71	14.96	15.22	15.48			
28	13.47	13.68	13.89	14.11	14.34	14.57	14.82	15.07	15.33	15.60			
30	13.57	13.78	13.99	14.22	14.44	14.68	14.92	15.18	15.44	15.71			
32	13.66	13.87	14.09	14.32	14.55	14.78	15.03	15.28	15.55	15.85			
34	13.76	13.97	14.19	14.44	14.65	14.89	15.14	15.39	15.66	15.98			
			14.29	14.52	14.75	14.99	15.24		15.77	16.05			

XIX'. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR, CORRESPONDING TO A TENTH OF AN INCH IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

		Temperature of the Air, Fahrenheit, being											
Barometer Reading in		1		1		1	1	1	1		1		
English Inches.	40°	450	<b>50</b> °	55°	60°	65°	70°	75°	800	85°	90°	950	
22.0	121.5	122.8	124.2	125.5	126.8	128.2	129.5	130.8	132.1	133.5	134.8	136.1	
22.2	120.4	121.7	123.1	124 4	125.7	127.0	128.3	129.6	130.9	132.2	133.6	134.9	
22.4	119.3	120.6	121.9	123.2	124.6	125.9	127.2	128.5	129.8	131.1	132.4	133.7	
22.6	118.2	119.5	120.8	122.1	123.4	124.7	126.0	127.3	128.6	129.9	131.2	132.	
22.8	117.2	118.5	119.8	121.1	122.3	123.6	124.9	126.2	127.5	128.8	130.0	131.	
23.0	116.2	117.5	118.7	120.0	121.3	122.6	123.8	125.1	126.4	127.6	129.9	130.	
23.2	115.2	116.5	117.7	119.0	120.2	121.5	122.7	124.0	125.3	126.5	127.8	129.	
23.4	114.2	115.5	116.7	118.0	119.2	120.5	121.7	123.0	124.2	125.4	126.7	127.	
23.6	113 2	114.4	115.7	116.9	118.1	119.4	120.6	121.8	123.1	124.3	125.5	126.	
23.8	112.3	113.5	114.8	116.0	117.2	118.4	119.7	120.9	122.1	123.3	124.6	125.	
24.0	111.4	112.6	113.8	115.0	116.2	117.4	118.7	119.9	121.1	122.3	123.5	124.	
24.2	110.5	111.7	112.9	114.1	115.3	116.5	117.7	118.9	120.1	121.3	122.5	123.	
24.4	109.5	110.7	111.9	113.1	114.3	115.5	116.7	117.9	119.1	120.3	121.5	122.	
24.6	108.6	109.8	111.0	112.2	113.4	114.6	115.8	116.9	118.1	119.3	120.5	121.	
24.8	107.8	108.9	110.1	111.3	112.5	113.7	114.8	116.0	117.2	118.4	119.5	120.	
25.0	106.9	108.1	109.2	110.4	111.6	112.7	113.9	115.1	116.2	117.4	118.6	119.	
25.2	106.0	107.2	108.4	109.5	110.7	111.8	113.0	114.1	115.3	116.5	117.6	118.	
25.4	105.2	106.4	107.5	108.7	109.8	111.0	112.1	113.3	114.4	115.6	116.7	117.	
25.6	104.4	105.5	106.7	107.8	108.9	110.1	111.2	112.4	113.5	114.6	115.8	116.	
25.8	103.6	104.7	105.8	107.0	108.1	109.2	110.4	111.5	112.6	113.8	114.9	116.	
26.0	102.8	103.9	105.0	106.1	107.3	108.4	109.5	110.6	111.8	112.9	114.0	115.	
26.2	102.0	103.1	104.2	105.3	106.5	107.6	108.7	109.8	110.9	112.0	113.1	114.	
26.4	101.2	102.3	103.4	104.6	105.7	106.8	107.9	109.0	110.1	111.2	112.3	113.	
26.6	100.5	101.6	102.7	103.8	104.9	106.0	107.1	108.2	109.3	110.4	111.4	112.	
26.8	99.7	100.8	101.9	103.0	104.1	105.2	106.3	107.4	108.5	109.5	110.6	111.	
27.0	99.0	100.1	101.2	102.2	103.3	104.4	105.5	106.6	107.6	108.7	109.8	110.	
27.2	98.3	99.3	100.4	101.5	102.6	103.6	104.7	105.8	106.8	107.9	109.0	110.	
27.4	97.5	98.6	99.7	100.7	101.8	102.9	103.9	105.0	106.1	107.1	108.2	109.	
276	96.8	97.9	98.9	100.0	101.1	102.1	103.2	104.2	105.3	106.3	107.4	108.	
27.8	96.1	97.2	98.2	99.3	100.3	101.4	102.4	103.5	104.5	105.6	106.6	107.	
28.0	95.4	96.5	97.5	98.6	99.6	100.6	101.7	102.7	103.8	104.8	105.9	106.	
28.2	94.8	95.8	96.8	97.9	98.9	99.9	101.0	102.0	103.0	104.1	105.1	106.	
28.4	94.1	95.1	96.1	97.2	98.2	99.2	100.2	101.3	102.3	103.3	104.3	105.	
28.6	93.4	94.4	95.5	96.5	97.5	98.5	99.5	100.6	101.6	102.6	103.6	104.	
28.8	92.8	93.8	94.8	95.8	96.8	97.8	98.8	99.8	100.8	101.8	102.8	103.	
29.0	92.1	93.1	94.1	95.1	96.2	97.2	98.2	99.2	100.2	101.2	102-2	103.	
29.2 29.4	91.5	92.5	93.5	94.5	95.5	96.5	97.5	98.5	99.5	100.5	101.5	102.	
29.4	90.9	91.9	92.9	93.9	94.8	95.8	96.8	97.8	98.8	99.8	100.8 100.1	101.	
29.8	89.7	91.3	92.2 91.6	93.2 92.6	94.2 93.6	95.2 94.5	96.2 95.5	97.2 96.5	$98.2 \\ 97.5$	99.1 98.5	99.4	100.	
30.0	89.1	90.0		92.0		93.9	94.9	95.9	96.8	97.8	98.8	99.	
30.2	88.5	89.4	91.0 90.4	91.4	$92.9 \\ 92.3$	93.9	94.9	95.9	96.2	97.2	98.1	99.	
30.4	87.9	88.8	89.8	90.8	91.7	92.7	1	94.6	95.6	96.5	97.5	98.	

When the Barometrical means to be used have been derived from observations taken at such hours of the day as, if combined, do not give the true mean pressure, they must be reduced to the true means by using the Tables XX. and XXI. These tables give the corrections to be applied to the hourly means, in each month, for reducing them to the means which would have been given by observations made at each of the twenty-four hours. The correction for any given set of hours is found by taking the mean of the corrections due to each of the combined hours, paying due attention to the signs. Table XX. has been computed from the hourly observations made under the superintendence of Professor A. D. Bache, at Girard College, Philadelphia. Table XXI. is from the Greenwich Observations, by Glaisher.

XX.

North America. — Philadelphia. Lat. 39° 58' N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Barometric Pressure of the respective Days, Months, and of the Year.

Barometer	in	English	Inches.
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Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	Inch.	Inch.	Inch.	Inch.	Inch	Inch.	Inch.	Inch.	Inch.	Iuch.	Inch.	Inch.	Inch.
Midnight.	+.002	009	007	004	002	+.003	007	003	002	+.007	+.003	010	0024
1	+.001	007	002	001	+.003	+.007	+.001	001	+.005	+.007	+.007	011	+.0007
2	007	003	001	+.006	+.007	+.010	+.004	+.004	+.010	+.011	+.011	016	+.0030
3	00s	+.002	+.009	+.005	+.007	+.007	+.003	+.005	+.009	+.011	+.007	014	+.0036
	ł												
4					+.003					1			+.0038
5	003			1				1	3	4			0050
6	009	[004]	011	020	019	022	019	017	016	012	012	015	0147
7	021	013	020	029	026	024	025	023	023	021	019	023	0222
8	_ 022	_ 022	_ 028	_ 024	_ 021	020	- 028	_ 026	_ 020	020	- 098	_ 020	0290
9	li .		l l							1			0307
	1						į.				į.		0296
10								1		1		1	0296
11	023	019	016	023	018	019	019	022	021	014	017	011	0155
Noon.	+.006	004	002	008	006	010	012	012	009	+.001	+.006	+.005	0037
1	+.028	+.017	+.014	+.006	+.005	.000	.000	.000	+.005	+.006	+.023	+.024	+.0107
2	+.037	+.032	+.031	+.021	+.017	+.011	+.011	+.012	+.020	+.028	+.033	+.034	+.0240
3	+.034	+.034	+.034	+.034	+.028	+.019	+.020	+.022	+.024	+.028	+.033	+.034	+.0287
4													+.0306
5		1	1		1								+.0267
6	I.	1	1					1					+.0202
7	+.003	+.006	+.007	+.022	+.016	+.018	+.021	+.018	+.016	+.001	002	+.018	+.0123
8	+.003	000	_ 003	+ 000	± 002	± 010	+ 01.1	+.008	+ 007	_ 000	_ 006	+ 013	+.0040
9			1		1	1		+.003					0027
_		1	1	1							ř.	+.012	
10			1									+.005	11
11	+.002	011	017	010	019	005	002	002	001	009	003	7.003	0064
C 9 10		1 00=	1 000	001	00-	005	00.1	002	000	000	1 00 1	1 000	+ .001
6, 2, 10													31
7, 2, 9													.000
9, 12, 3, 9	.000	001	001	J002	004	004	004	004	004	003	001	+.003	002
D							0						

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XXI. England. — Greenwich. Lat. 51° 29′ N.; Long. 0° 0′. Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Barometric Pressure for the respective Months.—Glaisher.

English Inches.

						3118H IN	,11Co.						
Hours.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
Midn	.000	001	002	008	005	.000	006	010	005	005	011	004	005
1	.001	.004	.013	.000	.002	.004	.000	.000	.000	.004	005	.001	.002
2	.002	.008	.020	.007	.004	.005	.003	.007	.005	.010	.003	.006	.007
3	.005	.012	.023	.010	.005	.004	.005	.011	.010	.015	.008	.010	.009
4	.011	.014	.022	.011	.005	.001	.005	.014	.012	.020	.013	.012	.012
5	.015	.015	.019	.011	.006	002	.006	.011	.014	.022	.016	.014	.012
6	.015	.012	.012	.006		006	.002	.005	.010	:018	.015	.011	.009
7	.010	.007	.005	í		010		.000	.001	.008	.010	.006	.003
	.010		.000	.000	.000	*****	,004		,001	.000	.010	.000	.000
8	.003	000	004	_ 008	003	- 012	- 008	007	_ 006	- 003	.003	.004	003
9		ì	010					008				1	1 1
10		1	015					009	,	1	007		012
													1 1
11	014	016	015	011	006	009	009	008	010	014	005	015	011
	00-	010	010	000	000	000	000	00=	00=	010	000	000	000
Noon	1	012		008	002		006		1		.002	009	1
1	.002	}			.000	003		.000		003	.007	.003	
2	.005	.003	.000	.003	.003	.003	.001	.003	.004	.004	.011	.008	.004
3	.004	.006	003	.009	.006	.007	.005	.005	.008	.005	.010	.010	.006
	000	000	00-	00.	070	010	000	000	0.0	000			00=
4	.002	.008	.005	.004	.010	.013	.009	.009	.010	.003	.008	.009	.007
5	.000	.006	.004	.014	.014	.017	.013	.011	.011	.000	.004	.006	.008
6	003	.002	.000	.011	.015	.017	.013	.011	.006	005	.000	.002	.006
7	005	004	006	007	.010	.014	.010	.005	.000	008	006	003	.000
-	000	000	010	005	000	000	004	00=	00-	011	010	000	005
8	1		012		.000	.008		005					i t
9			015		1	1		010				1	, I
10			012		1	,	•	015				1	
11	-,004	005	010	012	008	002	012	015	011	009	017	009	009
6. 6	.006	.007	.006	.008	.011	.005	.008	.008	.008	.006	.007	.006	.008
7. 7	.002	.002	1	005	.008	.002	.003	1	.000	.000		.002	.001
8. 8	002		008			002		1	006		1	1	
0. 0	.002	.005	.505	.500	.002	1002	.002	.500	.500	.507	.504	.501	1004
9. 9	007	008	013	010	006	004	005	009	010	012	011	009	009
10.10	007	1		013	1			012			ł	012	011
7. 2. 9	.003	.001		003	1		001	1	001	į.	.001	.002	.001
1. 2. 9	.003	.001	1005	.005	.001	-1001	.501	.002	.001	.001	.001	.502	
6. 2. 8	.005	.003	.000	.001	.003	.002	.002	.001	.003	.004	.005	.004	.003
6. 2.10	.005	.003	1	5		002			.001	.003	1	.003	.001
6. 2. 6	.006	.006	1	.007		002	ŧ	.006	.007	.006		.007	.006
0. 2. 0	.000	.000	1004	.007	.008	.003	.005	.000	.007	1000	.505	.507	
7. 2	.007	.005	.003	.000	.004	004	001	.002	.002	.006	.010	.007	.003
8. 2	.004	1	002		1			002		.000		.006	.001
8. 1	.002			006			006	l .	003	003	.005	.003	002
7. 1	.002			003		006		.000	.000	.002	.008	.004	.001
	1000				1000					_			
9.12.3.9	004	005	008	005	002	002	003	004	004	007	002	004	004
	11		1	1		1							

### XXII. TABLE TO REDUCE, BY INTERPOLATION,

THE OBSERVATIONS TO THE SAME ABSOLUTE TIME.

#### DECIMALS OF AN HOUR.

Min.  1 2 3 4	.017 .033 .050	Min. 11 12 13 14	.183 .200 .217 .233	Min. 21 22 23 24	.350 .367 .383	Min. 31 32 33 34	Decimal.	Min. 41 42 43 44	.683 .700 .717	Min. 51 52 53 54	Decimal
5 6 7 8 9	.083 .100 .117 .133 .150	15 16 17 18 19 20	.250 .267 .283 .300 .317	25 26 27 28 29 30	.417 .433 .450 .467 .483	35 36 37 38 39 40	.583 .600 .617 .633 .650	45 46 47 48 49 50	.750 .767 .783 .800 .817	55 56 57 58 59 60	.917 .933 .950 .967 .983

### TABLE FOR CORRECTION OF CURVATURE AND REFRACTION.

From a mountain, when furnished with a barometer, or with an apparatus for determining the temperature of boiling water, and a pocket level, an observer can find the elevations of distant points, which are in sight, but lower than the mountain itself on which he stands. He has only to seek, with the level, the point on the slope of the mountain which corresponds to the point at a distance that he wishes to determine, and to take there a barometrical, or a boiling point observation. This observation is to be calculated in the usual way, but the result must be corrected for the curvature of the surface of the globe, and for the atmospheric refraction, by means of the following Table.

This method, which furnishes the means of multiplying, without much trouble, the measurements of heights, gives approximations which are sufficient for most of the purposes of Physical Geography. It may even seem preferable to direct measurements for determining the mean elevation of certain physical lines, which are best estimated when seen from a distance; such as the upper limit of the growth of trees, the limits of different kinds of vegetation, that of permanent snow, that of the mean elevation of the crest of a mountain range, &c.

Table XXIII. is taken from Captain Lee's Collection of Tables and Formulæ, 2d edit., page 81.

### XXIII. CORRECTIONS FOR CURVATURE AND REFRACTION.

Showing the Difference of the Apparent and True Level, in feet and decimals, for Distances in feet and miles.

Lilo Willia	the Difference			1	1		t and miles.
	С	orrection in F	eet.		c	Correction in F	eet.
Distances		1		Distances			1
in Feet.	For Curvature,	For Re- fraction.	For Curva- ture and Refraction.	in Miles.	For Curvature.	For Re- fraction.	For Curva- ture and Refraction.
100	.00024	.00004	.00020	1/4	.0417	.0060	.0357
150	.00054	.00008	.00046	14 10 34	.1668	.0238	.1430
200	.00094	.00013	.00083		.3752	.0536	.3216
250	.00149	.00021	.00128	1	.6670	.0953	.5717
300	.00215	.00031	.00184	$1\frac{1}{2}$	1.5008	.2144	1.2864
350	.00293	.00042	.00251	2	2.6680	.3811	2,2869
400	.00383	.00055	.00328	$2\frac{1}{2}$	4.1688	•5955	3.5733
450	.00484	.00069	.00415	3	6.0030	.8561	5.1469
500	.00598	.00085	.00513	$3\frac{1}{2}$	8.1708	1.1673	7.0035
550	.00724	.00103	.00621	4	10.6720	1.5246	9.1474
600	.00861	.00123	.00738	$4\frac{1}{2}$	13.5468	1.9295	11.5773
650	.01010	.00144	.00866	5	16.6750	2.3821	14.2929
700	.01172	.00167	.01005	5½	20.1769	2.8824	17.2945
750	.01345	.00192	.01153	6	24.0120	3.4303	20.5817
800	.01531	.00219	.01312	$6\frac{1}{2}$	28.1809	4.0258	24.1551
850	.01728	.00247	.01481	7	32.6830	4.6690	28.0143
900	.01938	.00277	.01661	$7\frac{1}{2}$	37.5190	5.3599	32.1591
950	.02159	.00308	.01851	8	42.6880	6.0997	36.5883
1000	.02392	.00333	.02059	81/2	48.1910	6.8844	41.3066
1050	.02638	.00377	.02261	9	54.0270	7.7181	46.3089
1100	.02895	.00414	.02481	$9^{1}_{2}$	60.1971	8.5996	51.5975
1150	.03164	.00452	.02712	10	66.7000	9.5286	57.1714
1200	.03445	.00492	.02953	11	80.7070	11.5296	69.1774
1250	.03738	.00534	.03204	12	96.0480	13.7211	82.3269
1300	.04043	.00578	.03465	13	112.7230	16.1033	96.6197
1350	.04361	.00623	.03738	14	130.7320	18.6760	112.0560
1400	.04689	.00670	.04019	15	150.0750	21.4393	128.6357
1450	.05030	.00719	.04311	16	170.7520	24.3931	146.3589
1500	.05383	.00769	.04614	17	192.7630	27.5376	165.2254
1550	.05748	.00821	.04927	18	216.1086	30.8727	185.2359
1600	.06125	.00875	.05250	19	240.7870	34.3981	206.3889
1650	.06514	.00931	.05583	20	266.8000	38.1143	228.6857
1700	.06914	.00988	.05926				
1750	.07327	.01047	.06280				
1800	.07752	.01107	.06645				
1850	.08188	.01170	.07018				
1900	.08637	.01234	.07403				
1950	.09098	.01300	.07798				
2000	.09570	.01367	.08203				
				l H			

# THERMOMETRICAL

# MEASUREMENT OF HEIGHTS,

OR

# TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM OBSERVATIONS OF THE TEMPERATURE OF BOILING WATER.

### THERMOMETRICAL MEASUREMENT OF HEIGHTS.

#### TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM THE TEMPERATURE OF THE BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of the vapors produced from it gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles, and the water boils. The temperature at which, in the open air, water boils, thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the higher the station where an observation is taken, the lower the temperature at which water boils at that station will be.

The difference of elevation between two places, therefore, can be deduced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and, the atmospheric pressures at both places being known, to compute the difference of level by a formula, or by the tables given above for computing heights from barometrical observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometrical observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water gives only indirectly the atmospheric pressure, which is given directly by the barometer. This method is thus liable to all the chances of error which may affect the measurements by means of the barometer, besides adding to them new ones peculiar to itself, the principal of which, not to speak of the differences exhibited in the various tables of the force of vapor, is the difficulty of ascertaining with the necessary accuracy the true temperature of boiling water. In the present state of thermometry it would hardly be safe, indeed, to answer, in the most favorable circumstances, for quantities so small as hundredths of degrees, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and the substance of the vessel containing the water, the nature of the water itself, the place at which the bulb of the thermometer is placed, whether in the current of steam or in the water, - all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric

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pressure. Owing to these various causes, an observation of the boiling point, differing by one tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimetres in the barometric pressure, or of from 70 to 80 feet in the final result, while with a good barometer the error of pressure will hardly ever exceed one tenth of a millimetre, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer, or thermobarometer, is of the greatest utility to travellers traversing distant or rough countries, on account of its being more conveniently transported, and much less liable to accidents than the mercurial barometer. The best form for it is that contrived and described by Regnault in the Annales de Chimie et de Physique, Tom. XIV. p. 202. It consists of an accurate thermometer with long degrees, subdivided into tenths, whose bulb is placed, about 2 or 3 centimetres above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp. The whole instrument when closed is about 6 inches long; when drawn out for observation, about 14 inches.

Table XXIV. of barometric pressures corresponding to temperatures of boiling water, has been calculated by Regnault from his Tables of Forces of Vapor, and published in the *Annales de Chimie et de Physique*, Tom. XIV. p. 206. It gives, in millimetres of mercury, the barometric pressures corresponding to every tenth of a Centigrade degree; for greater convenience, the values for every hundredth have been added.

The accuracy of this table has been tested by direct observation by Mr. Wisse, a traveller competent in such matters, who noted down simultaneously the temperatures of the boiling point of water and the height of the barometer, in various parts of the Andes, up to the summit of the volcano of Pichincha, including in his observations barometrical pressures ranging from 752 to 430 millimetres of mercury. The agreement between the barometric pressures given here by Regnault and those found by Wisse are very satisfactory, the differences never exceeding a few tenths of a millimetre. See Annales de Chimie et de Physique, Tom. XXVIII. p. 123.

Table XXV. is the same table, revised by A. Moritz, who, in a communication to the Académie des Sciences, in October, 1856, called the attention to some slight errors of computation in Regnault's table, and gave the corrected numbers for every whole degree from 40° to 102° Centigrade. Those numbers are given here from 80° upwards, as published in the *Journal de l'Institut*; the values for every tenth of a degree, and their differences, have been computed to fit the table for practical use. The comparison of the two tables will show that the corrections mostly amount to a few hundredths, and never exceed one tenth of a millimetre.

Table XXVI. is table XXV. reduced to English measures.

	1		-							
Centig.			1	I	Hundredths	of a Degr	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
85.0	433.04	433.21	433.38	433.55	433.72	1	434.07	434.24	434.41	434.58
85.1	434.75	434.92	435.09	435.26	435.43	1	435.78	435.95	436.12	436.29
85.2	436.46	436.63	436.80	436.97	437.14		437.49	437.66	437.83	438.00
85.3	438.17	438.34	438.51	438.69	438.86		439.20	439.37	439.55	439.72
85.4	439.89	440.06	440.23	440.41	440.58	440.75	440.93	441.10	441.27	441.45
85.5	441.62	441.79	441.97	442.14	442.31	442.48	442.66	442.83	443.00	443.18
85.6	443.35	443.52	443.70	443.87	444.05	444.22	444.39	444 57	444.74	444.92
85.7	445.09	445.26	445.44	445.61	445.79	445.96	446.14	446.31	446.49	446.67
85.8	446.84	447.01	447.19	447.36	447.54	447.71	447.89	448.06	448.24	448.41
85.9	448.59	448.76	448.94	449.11	449.29	449.46	449.64	449.81	449.99	450.16
86.0	450.34	450.52	450.69	450.87	451.04	451.22	451.40	451.57	451.75	451.92
86.1	452.10	452.28	452.45	452.63	452.81	452.98	453.16	453.34	453.52	453.69
86.2	453.87	454.05	454.22	454.40	454.58	454.75	454.93	455.11	455.29	455.46
86.3	455.64	455.82	456.00	456.17	456.35	456.53	456.71	456.89	457.06	457.24
86.4	457.42	457.60	457.78	457.96	458.14	458.31	458.49	458.67	458.85	459.03
86.5	459.21	459.39	459.57	459.75	459.93	460.10	460.28	460.46	460.64	460.82
86.6	461.00	461.18	461.36	461.54	461.72	461.90	462.08	462.26	462.44	462.62
86.7	462.80	462 98	463.16	463.34	463.52	463.70	463.88	464.06	464.24	464.42
86.8	464.60	464.78	464.96	465.14	465.32	465.50	465.69	465.87	466.05	466.23
86.9	466.41	466.59	466.77	466.95	467.13	467.31	467.50	467.68	467.86	468.04
87.0	468.22	468.40	468.58	468.77	468.95	469.13	469.31	469.49	469.68	469.86
87.1	470.04	470.22	470.41	470.59	470.77	470.95	471.14	471.32	471.50	471.69
87.2	471.87	472.05	472.24	472.42	472.60	472.78	472.97	473.15	473.33	473.52
87.3	473.70	473.88	474.07	474.25	474.44	474.62	474.80	474.99	475.17	475.36
87.4	475.54	475.72	475.91	476.09	476.28	476.46	476.64	476.83	477.01	477.20
87.5	477.38	477.56	477.75	477.93	478.12	478.30	478.49	478.67	478.86	479.04
87.6	479.23	479.41	479.60	479.78	479.97	480.15	480.34	480.52	480.71	480.89
87.7	481.08	481.27	481.45	481.64	481.82	482.01	482.20	482.38	482.57	482.75
87.8	482.94	483.13	483.31	483.50	483.69	483.87	484.06	484.25	484.44	484.62
87.9	484.81	485.00	485.19	485.37	485.56	485.75	485.94	486.13	486.31	486.50
88.0	486.69	486.88	487.07	487.25	487.44	487.63	487.82	488.01	488.19	488.38
88.1	488.57	488.76	488.95	489.13	489.32	489.51	489.70	489.89	490.07	490.26
88.2	490.45	490.64	490.83	491.02	491.21	491.39	491.58	491.77	491.96	492.15
88.3	492.34	492.53	492.72	492.91	493.10	493.29	493.48	493.67	493.86	494.05
88.4	494.24	494.43	494.62	494.81	495.00	495.19	495.39	495.58	495.77	495.96
88.5	496.15	496.34	496.53	496.72	496.91	497.10	497.30	497.49	497.68	497.87
88.6	498.06	498.25	498.44	498.64	498.83	499.02	499.21	499.40	499.60	499.79
88.7	499.98	500.17	500.36	500.56	500.75	500.94	501.13	501.32	501.52	501.71
88.8	501.90	502.09	502.28	502.48	502.67	502.86	503.05	503.24	503.44	503.63
88.9	503.82	504.01	504.21	504.40	504.60	504.79	504.98	505.18	505.37	505.57
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1	П									
Centig.				ŀ	Hundredths	of a Degr	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin.	Millim.
89.0	505.76	505.95	506.15	506.34	506.54	506.73	506.92	507.12	507.31	507.51
89.1	507.70	507.89	508.09	508.28	508.48	508.67	508.87	509.06	509.26	509.45
89.2	509.65	509.84	510.04	510.23	510.43	510.62	510.82	511.01	511.21	511.40
89.3	511.60	511.80	511.99	512.19	512.38	512.58	512.78	512.97	513.17	513.36
89.4	513.56	513.76	513.95	514.15	514.35	514.54	514.74	514.94	515.14	515.33
89.5	515.53	515.73	515.92	516.12	516.32	516.51	516.71	516.91	517.11	517.30
89.6	517.50	517.70	517.90	518.09	518.29	518.49	518.69	518.89	519.08	519.28
89.7	519.48	519.68	519.88	520.07	520.27	520.47	520.67	520.87	521.06	521.26
89.8	521.46	521.66	521.86	522.06	522.26	522.46	522.66	522.86	523.05	523.25
89.9	523.45	523.65	523.85	524.05	524.25	524.45	524.65	524.85	525.05	525.25
90.0	525.45	525.65	525.85	526.05	526.25	526.45	526.65	526.85	527.05	527.25
90.1	527.45	527.65	527.85	528.05	528.25	528.45	528.66	528.86	529.06	529.26
90.2	529.46	529.66	529.86	530.07	530.27	530.47	530.67	530.87	531.08	531.28
90.3	531.48	531.68	531.88	532.09	532.29	532.49	532.69	532.89	533.10	533.30
90.4	533.50	533.70	533.91	534.11	534.31	534.51	534.72	534.92	535.12	535.33
90.5	535.53	535.73	535.94	536.14	536.35	536.55	536.75	536.96	537.16	537.37
90.6	537.57	537.77	537.98	538.18	538.39	538.59	538.79	539.00	539.20	539.41
90.7	539.61	539.81	540.02	540.22	540.43	540.63	540.84	541.04	541.25	541.45
90.8	541.66	541.87	542.07	542.28	542.48	542.69	542.90	543.10	543.31	543.51
90.9	543.72	543.93	544.13	544.34	544.54	544.75	544.96	545.16	545.37	545.57
91.0	545.78	545.99	546.19	546.40	546.61	546.81	547.03	547.23	547.44	547.64
91.1	547.85	548.06	548.26	548.47	548.68	548.88	549.09	549.30	549.51	549.71
91.2	549.92	550.13	550.34	550.54	550.75	550.96	551.17	551.38	551.58	551.79
91.3	552.00	552.21	552.42	552.63	552.84	553.04	553.25	553.46	553.67	553.88
91.4	554.09	554.30	554.51	554.72	554.93	555.14	555.35	555.56	555.77	555.98
91.5	556.19	556.40	556.61	556.82	557.03	557.24	557.45	557.66	557.87	558.08
91.6	558.29	558.50	558.71	558.92	559.13	559.34	559.55	559.76	559.97	560.18
91.7	560.39	560.60	560.81	561.03	561.24	561.45	561.66	561.87	562.09	562.30
91.8	562.51	562.72	562.93	563.15	563.36	563.57	563.78	563.99	564.21	564.42
91.9	564.63	564.86	565.06	565.27	565.48	565.69	565.91	566.12	566.33	566.55
92.0	566.76	566.97	567.19	567.40	567.61	567.85	568.04	568.25	568.46	563.6
92.1	568.89	569.10	569.32	569.53	569.75	569.96	570.17	570.39	570.60	570.82
92.2	571.03	571.24	571.46	571.67	571.89	572.10	572.32	572.53	572.75	572.96
92.3	573.18	573.40	573.61	573.83	574.04	574.26	574.48	574.69	574.91	575.12
92.4	575.34	575.56	575.77	575.99	576.20	576.42	576.64	576.85	577.07	577.28
92.5	577.50	577.72	577.93	578.15	578.37	578.58	578.80	579.02	579.24	579.45
92.6	579.67	579.89	580.10	580.32	580.54	580.75	580.97	581.19	581.41	581.62
92.7	581.84	582.06	582.28	582.49	582.71	582.93	583.15	583.37	583.58	°583.80
92.8	584.02	584.24	584.46	584.68	584.90	585.11	585.33	585.55	585.77	585.99
92.9	586.21	586.43	586.65	586.87	587.09	587.31	587.53	587.75	587.97	588.19
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	1									
Centig.				,	Hundredth	s of a Degr	ee.			,
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
93.0	Millim. 588.41	Millim. 588.63	Millim. 588.85	Millim. 589.07	Millim. 589.29	Millim. 589.51	Millim. 589.73	Millim. 589.95	Millim. 590.17	Millim 590.39
93.1	590.61	590.83	591.05	591.27	591.49	591.71	591.94	592.16	592.38	592.60
93.2	592.82	593.04	593.26	593.49	593.71	593.93	594.15	594.37	594.60	594.8
93.3	595.04	595.26	595.48	595.71	595.93	596.15	596.37	596 59	596.82	597.0
93.4	597.26	597.48	597.71	597.93	598.15		598.60	598.82	599.04	599.2
93.5	599.49	599.71	599.94	600.16	600.38	600.60	600.83	601.05	601.27	601.5
93.6	601.72	601.94	602.17	602.39	602.62	602.84	603.07	603.29	603.52	603.7
93.7	603.97	604.19	604.42	604.64	604.87	1	605.32	605.54	605.77	605.99
93.8	606.22	606.45	606.67	606.90	607.12	607.35	607.58	607.80	608.03	608.2
93.9	608.48	608.71	608.93	609.16	609.38	609.61	609.84	610.06	610.29	610.5
94.0	610.74	610.97	611.19	611.42	611.65	611.87	612.10	612.33	612.56	612.78
94.1	613.01	613.24	613.47	613.69	613.92	614.15	614.38	614.61	614.83	615.00
94.2	615.29	615.52	615.75	615.97	616.21	616.43	616.66	616.89	617.12	617.3
94.3	617.58	617.81	618.04	618.27	618.50	618.72	618.95	619.18	619.41	619.6
94.4	619.87	620.10	620.33	620.56	620.79	621.02	621.25	621.48	621.71	621.9
94.5	622.17	622.40	622.63	622.86	623.09	623.32	623.56	623.79	624.02	624.23
94.6	624.48	624.71	624.94	625.17	625.40	625.63	625.87	626.10	626.33	626.56
94.7	626.79	627.02	627.25	627.49	627.72	627.95	628.18	628.41	628.65	628.88
94.8	629.11	629.34	629.58	629.81	630.04	630.27	630.51	630.74	630.97	631.21
94.9	631.44	631.67	631.91	632.14	632.38	632.61	632.84	633.08	633.31	633.55
95.0	633.78	634.01	634.25	634.48	634.72	634.95	635.18	635.42	635.65	635.89
95.1	636.12	636.35	636.59	636.82	637.06	637.29	637.53	637.76	638.00	638.23
95.2	638.47	638.71	638.94	639.18	639.41	639.65	639.89	640.12	640.36	640.59
95.3	640.83	641.07	641.30	641.54	641.77	642.01	642.25	642.48	642.72	642.95
95.4	643.19	643.43	643.67	643.90	644.14	644.38	644.62	644.86	645.09	645.33
95.5	645.57	645.81	646.05	646.28	646.52	646.76	647.00	647-24	647.47	647.71
95.6	647.95	648.19	648.43	648.67	648.91	649.14	649.38	649.62	649.86	650.10
95.7	650.34	650.58	650.82	651.06	651.30	651.53	651.77	652.01	652.25	652.49
95.8	652.73	652.97	653.21	653.45	653.69	653.93	654.17	654.41	654.65	654.89
95.9	655.13	655.37	655.61	655.85	656.09	656.33	656.58	656.82	657.06	657.30
96.0	657.54	657.78	658.02	658.26	658.50	658.74	658.99	659.23	659.47	659.71
96.1	659.95	660.19	660.43	660.68	660.92	661.16	661.40	661.64	661.89	662.13
96.2	662.37	662.61	662.86	663.10	663.34	663.58	663.83	664.07	664.31	664.56
96.3	664.80	665.04	665.29	665.53	665.78	666.02	666.26	666.51	666.75	667.00
96.4	667.24	667.48	667.73	667.97	668.22	668.46	668.71	668.95	669.20	669.44
96.5	669.69	669.93	670.18	670.42	670.67	670.91	671.16	671.40	671.65	671.99
96.6	672.14	672.39	672.63	672.88	673.12	673.37	673.62	673.86	674.11	674.35
96.7	674.60	674.85	675.09	675.34	675.59	675.83	676.08	676.33	676.58	676.82
96.8	677.07	677.32	677.57	677.81	678.06	678.31	678.56	678.81	679.05	679.30
96.9	679.55	679.80	680.05	680.29	680.54	680.79	681.04	681.29	681.53	681.78
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centig.				Н	lundredths	of a Degr	ee.		1	,
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
97.0	682.03	682.28	682.53	682.78	683.03	683.27	683.52	683.77	684.02	684.27
97.1	684.52	684.77	685.02	685.27	685.52	685.77	686.02	686.27	686.52	686.77
97.2	687.02	687.27	687.52	687.77	688.02	688.27	688.53	688.78	689.03	689.28
97.3	689.53	689.78	690.03	690.28	690.53	690.78	691.04	691.29	691.54	691.79
97.4	692.04	692.29	692.54	692.80	693.05	693.30	693.55	693.80	694.06	694.31
97.5	694.56	694.81	695.06	695.32	695.57	695.82	696.07	696.32	696.58	696.S3
97.6	697.08	697.33	697.59	697.84	698.09	698.34	698.60	698.85	699.10	699.36
97.7	699.61	699.86	700.12	700.37	700.63	700.88	701.13	701.39	701.64	701.90
97.8	702.15	702.40	702.66	702.91	703.17	703.42	703.68	703.93	704.19	704.44
97.9	704.70	704.96	705.21	705.47	705.72	705.98	706.24	706.49	706.75	707.00
98.0	707.26	707.52	707.77	708.03	708.28	708.54	708.80	709.05	709.31	709.56
98.1	709.82	710.08	710.33	710.59	710.85	711.10	711.36	711.62	711.88	712.13
98.2	712.39	712.65	712.91	713.16	713.42	713.68	713.94	714.20	714.45	714.71
98.3	714.97	715.22	715.49	715.75	716.01	716.26	716.52	716.78	717.04	717.30
98.4	717.56	717.82	718.08	718.34	718.60	718.85	719.11	719.37	719.63	719.89
98.5	720.15	720.41	720.67	720.93	721.19	721.45	721.71	721.97	722.23	722.49
98.6	722.75	723.01	723.27	723.53	723.79	724.05	724.31	724.57	724.83	725.09
98.7	725.35	725.61	725.87	726.13	726.39	726.65	726.92	727.18	727.44	727.70
98.8	727.96	728.22	728.48	728.75	729.01	729.27	729.53	729.79	730.06	730.32
98.9	730.58	730.84	731.11	731.37	731.63	731.89	732.16	732.42	732.68	732.95
99.0	733.21	733.47	733.74	734.00	734.27	734.53	734.79	735.06	735.32	735.59
99.1	735.85	736.11	736.38	736.64	736.91	737.17	737.44	737.70	737.97	738.23
99.2	738.50	738.77	739.03	739.30	739.56	739.83	740.10	740.36	740.63	740.89
99.3	741.16	741.43	741.69	741.96	742.23	742.49	742.76	743.03	743.30	743.56
99.4	743.83	744.10	744.36	744.63	744.90	745.16	745.43	745.70	745.97	746.23
99.5	746.50	746.77	747.04	747.30	747.57	747.84	748.11	748.38	748.64	748.91
99.6	749.18	749.45	749.72	749.99	750.26	750.52	750.79	751.06	751.33	751.60
99.7	751.87	752.14	752.41	752.68	752.95	753.22	753.49	753.76	754.03	754.30
99.8	754.57	754.84	755.11	755.38	755.65	755.92	756.20	756.47	756.74	757.01
99.9	757.28	757.55	757.82	758.10	758.37	758.64	758.91	759.18	759.46	759.73
100.0	760.00	760.27	760.55	760.82	761.09	761.36	761.64	761.91	762.18	762.46
100.1	762.73	763.00	763.28	763.55	763.82	764.09	764.37	764.64	764.91	765.19
100.2	765.46	765.73	766.01	766.28	766.56	766.83	767.10	767.38	767.65	767.93
100.3	768.20	768.47	768.75	769.02	769.30	769.57	769.85	770.12	770.40	770.67
100.4	770.95	771.23	771.50	771.78	772.05	772.33	772.61	772.88	773.16	773.43
100.5	773.71	773.99	774.26	774.54	774.82	775.09	775.37	775.65	775.93	776.20
100.6	776.48	776.76	777.04	777.31	777.59	777.87	778.15	778.43	778.70	<b>778.9</b> S
100.7	779.26	779.54	779.82	780.09	780.37	780.65	780.93	781.21	781.48	781.76
100.8	782.04	782.32	782.60	782.88	783.16	783.43	783.71	783.99	784.27	784.55
100.9	784.83	785.11	785.39	785.67	785.95	786.23	786.51	786.79	787.07	787.35
101.0	787.63	787.91	788.19	788.47	788.75	789.03	789.31	789.59	789.87	790.15
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

# TABLE XXV.

# BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

### EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

BY REGNAULT, REVISED BY MORITZ.

,									
	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres,	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.
the state of the s	80.0 80.1 80.2 80.3 80.4 80.5 80.6 80.7	354.62 356.06 357.50 358.96 360.41 361.87 363.34 364.51	1.44 1.45 1.45 1.46 1.46	83.0 83.1 83.2 83.3 83.4 83.5 83.6 83.7	400.07 401.66 403.26 404.87 406.48 408.10 409.72 411.35	1.60 1.60 1.61 1.61 1.62 1.62	86.0 86.1 86.2 86.3 86.4 86.5 86.6 86.7	450.30 452.06 453.83 455.60 457.38 459.17 460.96 462.75	1.76 1.77 1.77 1.78 1.78
The same of the sa	80.8 80.9 81.0	366.29 367.77 369.26	1.48 1.48 1.49	83.8 83.9 84.0	411.53 412.98 414.62 416.26	1.63 1.64 1.64	86.8 86.9	462.73 464.55 466.36 468.17	1.80 1.81 1.81
the same of the same of the same of the same of	81.1 81.2 81.3 81.4	370.75 372.25 373.75 375.25	1.49 1.50 1.50 1.51	84.1 84.2 84.3 84.4	417-91 419.57 421.23 422.89	1.65 1.66 1.66 1.67	87.1 87.2 87.3 87.4	469.99 471.82 473.65 475.49	1.92 1.63 1.83 1.84 1.84
	81.5 81.6 81.7 81.8 81.9	376.77 378.28 379.81 381.33 382.87	1.52 1.52 1.53 1.53	84.5 84.6 84.7 84.8 84.9	424.56 426.24 427.92 429.61 431.30	1.68 1.69 1.69 1.70	87.5 87.6 87.7 87.8 87.9	477.33 479.18 481.04 482.90 484.76	1.85 1.86 1.86 1.87
	82.0 82.1 82.2 82.3 82.4	384.40 385.95 387.49 389.05 390.61	1.54 1.55 1.55 1.56 1.56	85.0 85.1 85.2 85.3 85.4	433.00 434.71 436.42 438.13 439.85	1.70 1.71 1.72 1.72 1.73	88.0 88.1 88.2 88.3 88.4	486.64 488.52 490.40 492.29 494.19	1.88 1.89 1.89 1.90
	82.5 82.6 82.7 82.8 82.9 83.0	392.17 393.74 395.31 396.89 398.48 400.07	1.57 1.57 1.59 1.56 1.59	85.5 85.6 85.7 85.8 85.9 86.0	441.58 443.31 445.05 446.80 448.55 450.30	1.73 1.74 1.74 1.75	88.5 88.6 88.7 88.8 88.9 89.0	496.09 498.00 500.92 501.84 503.77 505.70	1.91 1.92 1.92 1.93 1.93

1								-
Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.
0			0			0		
89.0	505.70	1.94	93.0	588.33	2.20	97.0	681.93	2.49
89.1	507.65	1.95	93.1	590.53	2.21	97.1	684.42	2.50
89.2	509.59	1.95	93.2	592.74	2.22	97.2	686.92	2.51
89.3	511.54	1.96	93.3	594.96	2.22	97.3	689.42	2.51
89.4	513.50	1.97	93.4	597.18	2.23	97.4	691.94	2.52
89.5	515.47		93.5	599.41		97.5	694.46	
89.6	517.44	1.97	93.6	601.65	2.24	97.6	696.98	2.53
89.7	519.42	1.98	93.7	603.89	2.24	97.7	699.52	2.54
89.8	521.40	1.98	93.8	606.14	2.25	97.8	702.06	2.54
89.9	523.39	1.99	93.9	608.40	2.26	97.9	704.62	2.55
00.0	929.93	2.00	90.9	005.40	2.26	31.9	704.02	2.56
90.0	525.39	2.00	94.0	610.66	2.27	98.0	707.17	0.55
90.1	527.40		94.1	612.93	2.27	98.1	709.74	2.57
90.2	529.41	2.01	94.2	615.21	2.28	98.2	712.31	2.57
90.3	531.42	2.02	94.3	617.50	2.29	98.3	714.90	2.58
90.4	533.44	2.02	94.4	619.79	2.29	98.4	717.49	2.59 2.60
90.5	535.47		94.5	622.09		98.5	720.08	
90.6	537.51	2.04	94.6	624.39	2.31	98.6	722.69	2.61
90.7	539.55	2.04	94.7	626.71	2.31	98.7	725.30	2.61
90.8	541.60	2.05	94.8	629.93	2.32	98.8	727.93	2.62
90.9	543.65	2.05	94.9	631.36	2.33	98.9	730.55	2.63
30.3	949.09	2.06	94.9	091.90	2.33	90.9	790.99	2.64
91.0	545.71		95.0	633.69		99.0	733.19	
91.1	547.78	2.07	95.1	636.03	2.34	99.1	735.84	2.64
91.2	549.86	2.07	95.2	638.38	2.35	99.2	738.49	2.65
91.3	551.94	2.08	95.3	640.74	2.36	99.3	741.15	2.66
91.4	554.03	2.09	95.4	643.10	2.36	99.4	743.82	2.67
		2.09			2.37			2.68
91.5	556.12	2.10	95.5	645.48	2.38	99.5	746.50	2.68
91.6	558.22	2.11	95.6	647.86	2.39	99.6	749.18	2.69
91.7	560.33	2.11	95.7	650.24	2.39	99.7	751.87	2.70
91.8	562.44	2.12	95.8	652.63	2.40	99.8	754.57	2.71
91.9	564.56	2.13	95.9	655.04	2.41	99.9	757.28	2.72
92.0	566.69		96.0	657.44		100.0	760.00	
92.1	568.82	2.13	96.1	659.86	2.42	100.1	762.73	2.73
92.2	570.96	2.14	96.2	662.28	2.42	100.2	765.46	2.73
92.3	573.11	2.15	96.3	664.71	2.43	100.3	768.20	2.74
92.4	575.27	2.15	96.4	667.15	2.44	100.4	770.95	2.75
		2.16			2.44			2.76
92.5	577.43	2.17	96.5	669.59	2.45	100.5	773.71	2.77
92.6	579.59	2.17	96.6	672.05	2.46	100.6	776.47	2.77
92.7	581.77	2.18	96.7	674.51	2.47	100.7	779.25	2.78
92.8	583.95	2.19	96.8	676.97	2.47	100.8	782.03	2.79
92.9	586.14	2.19	96.9	679.45	2.48	100.9	784.82	2.19
93.0	588.33	2110	97.0	681.93	2140	101.0	787.62	2.00

### TABLE XXVI.

# BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

### EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHEIT.

REDUCED FROM REGNAULT'S TABLE, REVISED BY MORITZ.

Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.
0 185.0 185.1 185.2 185.3 185.4	17.048 17.085 17.122 17.160 17.197	0.037 .037 .037 .037	0 188.0 188.1 188.2 188.3 188.4	18.195 18.235 18.274 18.314 18.353	0.039 .039 .039 .040	191.0 191.1 191.2 191.3 191.4	19.407 19.448 19.490 19.532 19.573	0.042 .042 .042 .042	0 194.0 194.1 194.2 194.3 194.4	20.685 20.729 20.773 20.817 20.861	0.044 .044 .044 .044
185.5 185.6 185.7 185.8 185.9	17.235 17.272 17.310 17.348 17.385	.038 .038 .038 .038	188.5 188.6 188.7 188.8 188.9	18.393 18.432 18.472 18.512 18.552	.040 .040 .040 .040	191.5 191.6 191.7 191.8 191.9	19.615 19.657 19.699 19.741 19.783	.042 .042 .042 .042	194.5 194.6 194.7 194.8 194.9	20.905 20.949 20.993 21.038 21.082	.044 .044 .044 .044
186.0 186.1 186.2 186.3 186.4	17.423 17.461 17.499 17.537 17.575	.038 .038 .038 .038	189.0 189.1 189.2 189.3 189.4	18.592 18.632 18.672 18.712 18.753	.040 .040 .040 .040	192.0 192.1 192.2 192.3 192.4	19.825 19.868 19.910 19.952 19.995	.042 .042 .042 .042 .043	195.0 195.1 195.2 195.3 195.4	21.126 21.171 21.216 21.260 21.305	.045 .045 .045 .045
186.5 186.6 186.7 186.8 186.9	17.614 17.652 17.690 17.729 17.767	.038 .038 .038 .038	189.5 189.6 189.7 189.8 189.9	18.793 18.833 18.874 18.914 18.955	.040 .040 .041 .041	192.5 192.6 192.7 192.8 192.9	20.037 20.080 20.123 20.166 20.208	.043 .043 .043 .043	195.5 195.6 195.7 195.8 195.9	21.350 21.395 21.440 21.485 21.530	.045 .045 .045 .045
187.0 187.1 187.2 187.3 187.4	17.806 17.844 17.883 17.922 17.961	.039 .039 .039 .039	190.0 190.1 190.2 190.3 190.4	18.996 19.036 19.077 19.118 19.159	.041 .041 .041 .041	193.0 193.1 193.2 193.3 193.4	20.251 20.294 20.338 20.381 20.424	.043 .043 .043 .043	196.0 196.1 196.2 196.3 196.4	21.576 21.621 21.666 21.712 21.758	.045 .045 .046 .046
187.5 187.6 187.7 187.8 187.9 188.0	18.000 18.039 18.078 18.117 18.156 18.195	.039 .039 .039 .039 0.039	190.5 190.6 190.7 190.8 190.9 191.0	19.200 19.241 19.283 19.324 19.365 19.407	.041 .041 .041 .041	193.5 193.6 193.7 193.8 193.9 194.0	20.467 20.511 20.554 20.598 20.641 20.685	.043 .043 .044 .044	196.5 196.6 196.7 196.8 196.9 197.0	21.803 21.849 21.895 21.941 21.987 22.033	.046 .046 .046 .046

197.1 2: 197.2 2:	2.033 2.079 2.125 2.172	0.046	° 201.0				English Inches.	ence.	Fahren.	in English Inches.	ence.
197.1 2: 197.2 2:	2.079 2.125 2.172	- 1	201.0			0			0		
197.2 2	2.125 2.172	- 1		23.943	0.049	205.0	25.990	0.053	209.0	28.180	0.057
	2.172		201.1	23.993	.050	205.1	26.043		209.1	28.237	.057
107 2 9		.046	201.2	24.042	.050	205.2	26.096	•053	209.2	28.293	.057
131.0 4	0 010	.046	201.3	24.092	.050	205.3	26.149	.053	209.3	28.350	.057
197.4 22	2.218	.046	201.4	24.142	.050	205.4	26 202	.053	209.4	28.407	.057
197.5 25	2.264	.047	201.5	24.191	.050	205.5	26.255	0.53	209.5	28.464	0.25
197.6 22	2.311	.047	201.6	24.241	.050	205.6	26.309	.053	209.6	28.521	.057
197.7 2	2.358	-047	201.7	24.291	.050	205.7	26.362	.054	209.7	28.579	.057
197.8 22	2.404	.047	201.8	24.341	.050	205.8	26.416	.054	209.8	28.636	.057
197.9 25	2.451	.047	201.9	24.391	.050	205.9	26.470	.054	209.9	28.693	.051
198.0 25	2.498	.047	202.0	24.442	.050	206.0	26.523	.054	210.0	28.751	.058
	2.545	.047	202.1	24.492	.050	206.1	26.577	.054	210.1	28.809	.058
198.2 2:	2.592	.047	202.2	24.542	.050	206.2	26.631	.054	210.2	28.866	.058
	2.639	.047	202.3	24.593	.051	206.3	26.685	.054	210.3	28.924	.058
198.4 25	2.686	.047	202.4	24.644	.051	206.4	26.740	.054	210.4	28.982	.058
198.5 22	2.734	•047	202.5	24.694	.051	206.5	26.794	0.5.4	210.5	29.040	
198.6 22	2.781	.047	202.6	24.745	.051	206.6	26.848	.054	210.6	29.098	.058
198.7 22	2.829	.048	202.7	24.796	.051	206.7	26.903	.054	210.7	29.156	.058
198.8 2	2.876	.048	202.8	24.847	.051	206.8	26.957	.055	210.8	29.215	.058
198.9 22	2.924	.048	202.9	24.898	.051	206.9	27.012	.055	210.9	29.273	.058
199.0 25	2.971		203.0	24.949		207.0	27.066		211.0	29.331	
199.1 23	3.019	.048	203.1	25.000	.051	207.1	27.121	•055	211.1	29.390	.059
199.2 2	3.067	.048	203.2	25.051	.051	207.2	27.176	.055	211.2	29.449	.059
199.3 23	3.115	.048	203.3	25.103	.051	207.3	27.231	•055	211.3	29.508	.059
199.4 2	3.163	.048	203.4	25.154	.051	207.4	27.286	.055	211.4	29.566	.059 .059
199.5 2	3.211	242	203.5	25.206	0.50	207.5	27.341		211.5	29.625	
199.6 23	3.259	.048	203.6	25.257	.052	207.6	27.397	.055	211.6	29.684	•059
199.7 2	3.308	.048	203.7	25.309	.052	207.7	27.452	.055 .055	211.7	29.744	.059
199.8 23	3.356	.048	203.8	25.361	.052	207.8	27.507	.056	211.8	29.803	.059
199.9 23	3.405	.049	203.9	25.413	.052	207.9	27.563	.056	211.9	29.862	.059
200.0 25	3.453		204.0	25.465		208.0	27.618		212.0	29.922	
200.1 23	3.502	.049	204.1	25.517	.052	208.1	27.674	.056	212.1	29.981	.060
	3.550	.049	204.2	25.569	.052	208.2	27.730	.056	212.2	30.041	.060
200.3 2	3.599	.049	204.3	25.621	.052	208.3	27.786	.056	212.3	30.101	.060
200.4 2	3.648	.049	204.4	25.674	.052	208.4	27.842	.056	212.4	30.161	.060
200.5 2	3.697		204.5	25.726		208.5	27.898		212.5	30.221	
1	3.746	.049	204.6	25.779	.053	208.6	27.954	•056	212.6	30.281	•060
	3.795	.049	204.7	25.831	.053	208.7	28.011	.056	212.7	30.341	.060
200.8 23	3.845	.049	204.8	25.884	.053	208.8	28.067	.056	212.8	30.401	•060
200.9 23	3.894	.049	204.9	25.937	.053	208.9	28.123	.056	212.9	30.461	.060
201.0 25	3.943	0.049	205.0	25.990	0.053	209.0	28.180	0.057	213.0	30.522	0.060



# APPENDIX

70

# THE HYPSOMETRICAL TABLES.

COMPARISON OF THE DIFFERENT MEASURES OF LENGTH MOST GENERALLY USED FOR INDICATING ALTITUDES.

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### COMPARISON

OF THE MEASURES OF LENGTH MOST GENERALLY USED FOR INDICATING ALTITUDES.

It is too well known that the measures used in scientific researches among civilized nations are not uniform, as the convenience of all would require. In France the metre is employed; in England and North America, the yard and its third part, the English foot; in Germany, most commonly, the Old French or Paris foot, the sixth part of the French toise called the Toise du Pérou; at the same time, however, though not so extensively, the Rhine foot, in Denmark and Holland, and especially in Prussia, where it has been declared, under the name of Prussian foot, the legal measure in that kingdom; in Austria, the klafter of Vienna and its sixth part, the foot of Vienna; in Switzerland, the Swiss or federal foot, which has been adjusted to the metrical system, and is three tenths of a metre; and so on.

The numerous altitudes ascertained, either by private efforts, or in connection with the public works, and quite especially with the extensive geodetic operations carried on by the governments of these various countries for the survey of a regular map, are expressed in the measures respectively adopted by each of them. These heights, however, before they can be compared, require to be uniformly reduced to any one of these measures. Their relation to each other, therefore, is given here, together with numerous reduction tables, designed to save both the useless expenditure of time and the almost unavoidable errors arising from so numerous reductions.

The exact relation of the standard measures above mentioned is not easily ascertained, and the numbers given by the best authorities by no means always agree; for the manufacture of exact copies of a standard scale, and the accurate comparison of it, require considerable skill, and belong to the most delicate operations of physics. The numbers used for computing the following tables have been adopted, after a careful review of the authorities, as the most reliable. A few words on the most important original legal standards of measures may not be unwelcome. For further details on the subject the reader is referred principally to Dove's work, Maas und Messen, 2d edition, Berlin, 1835.

The principal original, legal standards are the following: -

1. The Toise du Pérou, the old French standard, made in 1735, in Paris, by Langlois, under the direction of Godin, is a bar of iron which has its standard length at the temperature of 13° Reaumur. It is known as the Toise du Pérou, because it was used by the French Academicians Bouguer and La Condamine in their measurement

of an arc of the meridian in Peru. What follows will show that it may almost be called the only common standard, to which all the others are referred for comparison.

- 2. The Metre is a standard bar of platina, made by Lenoir in Paris, which has its normal length at the temperature of zero Centigrade, or the freezing point. Its length is intended to make it a natural standard, and to represent the ten-millionth part of the terrestrial arc comprised between the equator and the pole, or of a quarter of the meridian. The length of this arc given by the measurement ordered for the purpose by the Assemblée Nationale, of the arc of the meridian between Barcelona, through France, to Dunkirk, combined with the measurements previously made in Peru and in Lapland, gave for the distance of the equator from the pole 5,130,740 toises, with an ellipticity of  $\frac{1}{334}$ , and for the length of the metre 443.29596 lines of the toise du Perou, assumed to be 443.296 lines, or 3 feet 11.296 lines. This last quantity was declared in 1799 to be the length of the legal metre, and rrai et définitif, and is the length of Lenoir's platina standard. Later and more extensive measurements in various parts of the globe, however, seem to indicate that this quantity is somewhat too small. The latest and most exact results we now possess, combined and computed by Bessel, would make the quarter of the meridian 10,000,856 metres, and the metre = 443.29979 Paris lines; Schmidt's computation would make it 443.29977 lines, and both numbers are confirmed by Airy's results. The legal metre is thus, in fact, as Dove remarks, a legalized part of the toise du Pérou, and this last remains the primitive standard. But it must be added that a natural standard, in the absolute sense of the word, is a utopian one, which ever-changing Nature never will give us. The metre is, for all practical purposes, what it was intended to be, a natural standard; though it must be confessed that, in practice, the question is not whether and how far a standard is a natural or a conventional one, but how readily and accurately it can be obtained, or recovered when lost.
- 3. The English Standard Yard is a brass bar, made by Bird in 1760, which was declared, by act of Parliament, 1st May, 1825, the legal measure of length when at the temperature of 62° Fahrenheit, under the name of Imperial Standard. Another standard, sometimes also called Parliamentary Standard, was made by Bird in 1758. Sir George Shuckburgh found both to be nearly identical, at least within 0.0002 of an inch. (Philos. Trans. for 1798, p. 170.)

Another scale of brass, however, made by Troughton for Sir George Shuckburgh, described in the *Philosophical Transactions for* 1798, and known as Shuckburgh's scale, obtained among scientific men, perhaps, a higher degree of authority, on account of the great accuracy of its division, and of its apparatus, devised by Troughton, for delicate comparisons. That scale was used by Captain Kater, in 1818, in his researches for determining the length of the pendulum beating a second at London, and also the length of the metre, expressed in English inches of the imperial standard. (*Phil. Trans. for* 1818.)

Numerous attempts to determine the relation between the English and the French measures show no inconsiderable discrepancies in their results. Omitting the older comparisons with the toise, we give here the value of the metre in English imperial inches, as resulting from the most reliable comparisons.

A standard scale made and divided by Troughton, and in all particulars identical

with Shuckburgh's scale, was brought to France in 1801 by Pictet. The comparison of it with the standard metre, made by Prony, Legendre, and Méchain, gave, after due reduction of the two standards to their respective normal temperatures,

1 metre at 32° Fahr. = 39.371 English imperial inches at 62° Fahr.

This determination was adopted for all reductions in Kelly's *Universal Cambist*, and in the French translation of the work, published in Paris in 1823.

A new comparison was made with great care by Captain H. Kater, in 1818. (See *Philos. Trans. for* 1818, p. 103.) The standards used were a brass scale metre, by Fortin, terminated with parallel planes (*mètre à bouts*), and a bar of platina on which the length of the metre was marked by two very fine lines (*mètre à traits*). Both were compared with Shuckburgh's scale, and a double series of experiments gave as the mean result:

Brass metre at 32° Fahr. = 39.37076 inches of Shuckburgh's scale at 62° Fahr.

Platina metre at 32° Fahr. =  $\frac{39.37081}{39.37079}$  " " " " "

On this value of the metre are based the reduction tables by Matthieu, published yearly in the *Annuaire du Bureau des Longitudes*; and it has come into general use, both in Europe and in this country.

Captain Kater gives besides, in the same paper, p. 109, note, the value of the metre compared with Bird's Parliamentary standard as being

1 metre at 32° F. = 39.37062 imp. inches of Bird's Parliamentary standard at 62° F. This value has been adopted by Dove, as being the legal one, in his reduction tables in his work, *Maas und Messen*, p. 175, &c., and by many German authorities.

According to Baily's experiments, made in 1835, when engaged in constructing a new standard for the Royal Astronomical Society (Memoirs R. Ast. Soc., Vol. IX.), the value of the metre is (Lee, Collection of Tables and Formula, p. 62)

1 metre at 32° F. = 39.370092 imperial standard inches at 62° F.

The original legal standards having been lost in the fire which destroyed, several years ago, the Parliament Houses, an act of Parliament provided for the construction of new ones; but as the report of the committee having charge of the construction of the new British standard has not yet been published, the discussion of the subject must be postponed.

The value adopted in the following tables, is that determined by Captain Kater, viz. 1 metre = 39.37079 English inches.

It may not be out of place to remark that Schumacher, in the first edition of his Sammlung von Hülfstafeln, used the value 1 metre = 39.3827 English inches, as given in the Base du Système Métrique; but this number, which expresses the relation of both standards when at the freezing point, becomes 39.37079 when they are respectively reduced to their normal temperatures. Schumacher's tables, therefore, must be corrected accordingly.

4. The actual standard of length of the United States is a brass scale of eighty-two inches in length, prepared for the Coast Survey of the United States, by Troughton of London, meant to be identical with the English Imperial Standard, and deposited in the office of weights and measures. The temperature at which it is a standard is 62° Fahrenheit, and the yard measure is between the 27th and 63d inches of the

scale. (See Report on the Construction and Distribution of Weights and Measures, by Prof. A. D. Bache, 1857.)

Hassler, first Superintendent of the United States Coast Survey, made an elaborate comparison of eleven different standard metres with the brass scale of eighty-two inches, by Troughton. Three of the standard metres, certified to be correct by high authorities, seem to deserve especial confidence: - 1. An iron metre, presented to Mr. Hassler by Tralles, which was one of the three that Tralles had made by Lenoir at the same time with those distributed to the committee on the weights and measures. 2. Another metre of iron, also by Lenoir, verified by Bouvard and Arago, and declared by them to be identical with the original. 3. A platina standard by Fortin, verified by Arago, and found to be  $\frac{1}{1000}$  of a millimetre too long, for which error allowance was made. Their comparison with the Troughton scale at the temperature of the freezing point gave:

- 1. Iron metre of Tralles = 39.3809171 inches of the Troughton scale.
- 2. Iron metre of Lenoir = 39.3799487
- 3. Platina metre of Fortin = 39.3804194

Or, correcting for expansion, and reducing them to their respective standard temper-

- = 39.36850 = 39.36754 = 39.36789 English inches of the Trough-ton scale of 82 inches at 62° F. 1. Iron metre of Tralles at 32° F. 2. Iron metre of Lenoir at 32° F. = 39.36754
- 3. Platina metre of Fortin at 32° F. = 39.36789

Hassler, in his Report to Congress on Weights and Measures, in 1832, adopts the first value, viz.:

1 metre at  $32^{\circ}$  F. = 39.3809171 inches of the Troughton scale at  $32^{\circ}$  F; and the Troughton scale was declared the United States standard, from which copies were to be made.

This value materially differs from those given by other careful comparisons, while, on the other hand, the close accordance of the numbers corresponding to the various standard metres proves the accuracy of Hassler's method and comparison. It is, therefore, difficult not to ascribe, with Baily, this discrepancy to some inaccuracy in the length of the Troughton scale of \$2 inches. But as that scale has been declared the standard of length of the United States, it seems better to call it, as is done in the Coast Survey Reports, the American yard, and its subdivisions the American foot and inch, and to consider it as a new standard, similar to, but not identical with, the English imperial standard. The value of the metre expressed in American standard inches is given in the Coast Survey Report for 1853, as

1 metre at 32° F. = 39.36850535 United States standard inches at 62° F.

We learn from the Report on Weights and Measures, by Prof. A. D. Bache, 1857, p. 18, that two copies of the new British standards, now in progress of construction, viz. a bronze standard, No. 11, and a malleable iron standard, No. 57, have been presented by the British government to the United States. A series of careful comparisons, made in 1856, by Mr. Saxton, under the direction of Prof. A. D. Bache, of the British bronze standard, No. 11, with the Troughton scale of eighty-two inches, showed that the British bronze standard yard is shorter than the American yard by 0.00087 inch.

Comparisons of the American standards with new French standards, recently presented to the United States by the French government, are still in progress.

For the present, however, it seems best to adhere to the value of the metre, expressed in American standard inches, adopted by the Coast Survey as given above. From this value the separate tables, which will be found below, for the reduction of the American yard and foot, were computed.

- 5. The Klafter of Vienna is a silver line let into a prismatic bar of iron, on which the length of the klafter was engraved by Voigtländer. It has its normal length at 13° Reaumur, and was declared by law, in 1816, the standard Klafter of Vienna. On the same silver line the French toise is marked, from the standard toise sent, in 1760, by La Caille and La Condamine to the Observatory of Vienna. According to a recent and very careful comparison by Struve (Mem. of the Austrian Acad., Vol. V., I. p. 117), the value of the klafter of Vienna is 0.9730317 toise du Pérou.
- 6. The *Prussian Foot* is marked on a standard iron bar, 3 feet long, made by Pistor in Berlin; it is a standard at the temperature of 13° Reaumur. The length of the Prussian foot was declared by law to be = 139.13 lines of the toise du Pérou.
- 7. A Mexican Vara, the standard length, brought from Mexico at the close of the war, by Major Turnbull of the Topographical Engineers, was presented to the Office of Weights and Measures. This standard was made by soldering sheet-brass upon the tinned surface of an iron bar. A careful comparison of its length with the American standard was made under the direction of Prof. Bache, which gave its length to be = 32.9682 inches at 58°.7 Fahrenheit, or 32.9680 when reduced to 62° Fahrenheit.

The relation of that particular Mexican standard to the Spanish standard not being known, it was thought better to adopt, for the present, the value of the Spanish Vara, and of its third part, the Castilian foot, found in Thionville, *Traité des Poids et Mesures*, &c., in Balbi's *Abrégé de Géographie*, viz. 1 vara = 0.847965 metre.

From the fundamental equations indicated above have been derived all those which have been used for computing the reduction tables given in the Appendix. At the head of each table will be found the value from which it was computed.

The tables are so arranged as to give *directly* the reduction of any whole number not exceeding three or four figures, and larger numbers within the limits needed for altitudes, by means of a *single* addition.

# Example.

Reduce 25,351 English feet into metres.

In Table XVI., on the line beginning with 25,000 and in the column headed 300, take for 25,300 = 7711.30 metres.

In the second part of the table, on the line beginning with 50, and in column headed 1, take for

$$51 = 15.54$$
 "

English feet 25,351 = 7726.84 "

The fractions, which seldom occur, are treated as whole numbers, taking care only properly to move the decimal point.

Tables XL. to XLIV. will be found convenient for converting fractional parts of a toise or of a foot into each other.

# TO CONVERT

# FRENCH TOISES

### INTO DIFFERENT MEASURES OF LENGTH

#### I. CONVERSION OF FRENCH TOISES INTO METRES.

1 Toise = 1.94903631 Metre.
Units.

Toises.										
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.000	1.949	3.898	5.847	7.796	9.745	11.694	13.643	15.592	17.541
10	19.490	21.439	23.388	25.337	27.287	29.236	31.185	33.124	35.073	37.022
20	38.931	40.930	42.879	44.828	46.777	48.726	50.675	52.624	54.573	56.522
30	58.471	60.420	62.369	64.318	66.267	68.216	70.165	72.114	74.063	76.012
40	77.961	79.911	81.860	83.809	85.758	87.707	89.656	91.605	93.554	95.503
50	97.452	99.401	101.350	103.299	105.248	107.197	109.146	111.095	113.044	114.993
60	116.942	118.891	120.840	122.789	124.738	126.687	128.636	130.585	132.534	134.484
70	136.433	138.382	140.331	142.280	144.229	146.178	148.127	150.076	152.025	153.974
80	155.923	157.872	159.821	161.770	163.719	165.668	167.617	169.566	171.515	173.464
90	175.413	177.362	179.311	181.260	183.209	185.158	187.108	189.057	191.006	192.955
					Hune	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	194.90	389.81	584.71		974.52	1169.42	1364.33		1754.13
1000	1949.04	2143.94	2338.84	2533.75	2728.65	2923.55	3118.46	3312.36	3507.27	3702.17
2000	3898.07	4092.98	4287.88	4482.78	4677.69	4872.59	5067.50	5262.40	5457.30	5652.21
3000	5847.11	6042.01	6236.92	6431.82	6626.72	6821.63	7016.53	7211.44	7406.34	7601.24
4000	7796.15	7991.05	8185.95	8380.86	8575.76	8770.66	8965.57	9160.47	9355.38	9550.28
5000	9745.18	9940.09	10135.0	10329.9	10524.8	10719.7	10914.6	11109.5	11304.4	11499.3
	II. CO	NVERSIO	ON OF		INTO FI = 6 French	RENCH (	OR PARI	S FEET.		
Toises.					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par Feet	Par.Feet.	Par.Feet.	Par. Feet.	Par. Fect.	Par Feet.	Par.Feet.	Par. Feet	Par Feet	Par Feet
0	0.00	6	12	18	24	30	36	42	48	54
10	60	66	72	78	84	90	96	102	108	114
20	120	126	132	138	144	150	156	162	168	174
30			300	100	204	210	216	222	228	234
	180	186	192	198		1				
40	180 240	186 246	192 252	258	264	270	276	282	288	294
50	240 300	246 306	252 312	258 318	264 324	270 330	336	342	348	354
50 60	300 360	246 306 366	252 312 372	258 318 378	264 324 384	270 330 390	336 396	342 402	348 408	354 414
50	240 300	246 306	252 312	258 318 378 438	264 324 384 444	270 330 390 450	336 396 456	342 402 462	348 408 468	354 414 474
50 60	300 360	246 306 366	252 312 372	258 318 378	264 324 384	270 330 390	336 396	342 402	348 408	354 414

1 Toise = 6.3945916 English Feet.

			1 '	Foise = 6.3	8945916 En	glish Feet.	·						
maiaaa	Units.												
Toises. Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
0	Eng. feet. 0.000	Eng. feet. 6.395	Eng feet. 12.789	Eng. feet. 19.184	Eng. feet. 25.578	Eng. feet. 31.973		Eng feet. 44.762		Eng. feet. 57.551			
10	63.946	70.340	76.735	83.130			102.313						
20		134.286			153.470		166.259		179.049				
30	191.838				217.416	1	230.205						
40	255.784			274.967			1	300.546	1				
50	319.729	326.124	332.519	338.913	345.308	351.702	358.097	364.492	370.886	377.281			
60	383.675	390.070	396.465	402.859	409.254	415.648	422.043	428.438	434.832	441.22			
70	447.621	454.016	460.410	466.805	473.200	479.594	485.989	492.383	498.778	505.173			
80	511.567	517.962	524.356	530.751	537.146	543.540	549.935	556.329	562.724	569.119			
90	575.513	581.908	588.302	594.697	601.091	607.486	613.881	620.275	626.670	633.06			
	<u></u>				Hund	reds.							
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng feet.	Eng feet	Eng feet.	Eng feet			
0	0.0	639.5	1278.9	-	2557.8	3197.3	3836.8	4476.2	_	5755.			
1000	6394.6	7034.0			f .		10231.3	10870.8					
2000					15347.0					1			
3000	19183.8	19823.2	20462.7	21102.1	21741.6	22381.1	23020.5	23660.0	24299.4	24938.9			
4000	25578.4	26217.8	26857.3	27496.7	28136.2	28775.7	29415.1	30054.6	30694.0	31333.			
	31972.9							1	1	Į.			
	1			0.00	942205 Ame - Un								
Toises. Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Am. Feet.	Am.Feet	Am. Feet.	Am. Feet.	Am. Feet.	Am. Feet	Am. Feet	Am Feet.	Am. Feet.	Am.Feet			
0	0.000	6.394	12.788	19.183	25.577	31.971	38.365	44.760	51.154	57.548			
10	63.942	70.336	76.731	83.125	89.519	95.913	102.308	108.702	115.096	121.490			
20	1				153.461			l .					
30	191.827	198.221	204.615	211.009	217.403	223.798	230.192	236.586	242.980	249.37			
40	255.769	262.163	268.557	274.951	281.346	287.740	294.134	300.528	306.923	313.31			
50	319.711	326.105	332.499	338.894	345.288	351.682	358.076	364.470	370.865	377.259			
60	ll .	1			409.230								
70					473.172		485.961						
80	1	1			537.114								
90	575.480	581.874	588.268	594.662	601.057		613.845	620.239	626.633	633.028			
Thousands.		1 700	1000	000		ireds.	600	1 P 0 4	600	000			
	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
	Am. Feet	Am Feet	Am Feet			Am Feet	Am Feet.						
0	0.0	1	1278.8		1	3197.1	3836.5	4476.0		5754.8			
1000	6394.2	1		1	8951.9	ł	10230.8						
2000	11	13427.9	14067.3		15346.1			17264.4					
3000		19822.1			21740.3								
4000					28134.6 34528.8								
5000	31971.1	32610.5	33249.9	33889.4	134528.8	135 168.2	135507.6	136447.0	37086.5	37725			

### TO CONVERT

# METRES

### INTO DIFFERENT MEASURES OF LENGTH.

1 LEGAL METRE = 443.296 FRENCH OR PARIS LINES.

### V. CONVERSION OF METRES INTO TOISES AND DECIMALS.

1 Metre = 0.513074074 Toise.

Metres.					Hune	dreds.							
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.			
0	0.00	51.31	102.61	153.92	205.23	256.54	307.84	359.15	410.46	461.77			
1000	513.07	564.38	615.69	667.00	718.30	769.61	820.92	872.23	923.53	974.84			
2000	1026.15	1077.46	1128.76	1180.07	1231.38	1282.69	1333.99	1385.30	1436.61	1487.91			
3000	1539.22	1590.53	1641.84	1693.14	1744.45	1795.76	1847.07	1898 37	1949.68	2000.99			
4000	2052.30	2103.60	2154.91	2206.22	2257.53	2308.83	2360.14	2411.45	2462.76	2514.06			
5000	2565.37	2616.68	2667.98	2719.29	2770.60	2821.91	2873.21	2924.52	2975.83	3027.14			
6000	3078.44	3129.75	3181.06	3232.37	3283.67	3334.98	3386.29	3437.60	3488.90	3540.21			
7000	3591.52	3642.83	3694.13	3745.44	3796.75	3848.06	3899.36	3950.67	4001.98	4053.28			
8000	t	i			1	4361.13							
9000	4617.67	4668.97	4720.28	4771.59	4822.90	4874.20	4925.51	4976.82	5028.13	5079.43			
Metres.	Units.												
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.			
0	0.000	0.513	1.026	1.539	2.052	2.565	3.078	3.592	4.105	4.618			
10	5.131	5.644	6.157	6.670	7.183	7.696	8.209	8.722	9.235	9.748			
20	10.261	10.775	11.288	11.801	12.314	12.827	13.340	13.853	14.366	14.879			
30	15.392	15.905	16.418	16.931	17.445	17.958	18.471	18.984	19.497	20.010			
40	20.523	21.036	21.549	22.062	22.575	23.088	23.601	24.114	24.628	25.141			
50	25.654	26.167	26.680	27.193	27.706	28.219	28.732	29.245	29.758	30.271			
60	30.784	31.298	31.811	32.324	32.837	33.350	33.863	34.376	34.889	35.402			
70	35.915	36.428	36.941	37.454	37.967	38.481	38.994	39.507	40.020	40.533			
80	41.046	41.559	42.072	42.585	43.098	43.611	44.124	44.637	45.151	45.664			
90	46.177	46.690	47.203	47.716	48.229	48.742	49.255	49.768	50.281	50.794			

1 Metre = 3.078444 Paris Feet.

Metres.	Metres. Units.												
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Fr. Feet.	Fr Feet.	Fr. Feet.										
0	0.00	3.08	6.16	9.24	12.31	15.39	18.47	21.55	Į.	27.71			
10	30.78	33.86	36.94	40.02	43.10	46.18	49.26		1	58.49			
20 30	61.57 92.35	64.65	67.73 98.51			76.96	80.04						
40	123.14	95.43 $126.22$	129.29	132.37	104.67 135.45	107.75 138.53	110.82 141.61	113.90 144.69	1	120.06 150.84			
40	120.14	120-22	140.40	102.07	100.40	100.00	141.01	144.09	141.11	190.04			
50	153.92	157.00	160.08	163.16	166.24	169.31	172.39	175.47	178.55	181.63			
60	184.71	187.79	190.86	193.94	197.02	200.10	203.18	206.26	209.33	1			
70	215.49	218.57	221.65	224.73	227.80	230.88	233.96	237.04	240.12	243.20			
80	246.28	249.35	252.43	255.51	258.59	261.67	264.75	267.82	270.90	273.98			
90	277.06	280.14	283.22	286.30	289.37	292.45	295.53	298.61	301.69	304.77			
100	00~ 0	010.03	01.00	015 00	000 -	990.0	000	000					
100	307.84	310.92	314.00	1	320.16	323.24	326.32	329.39	332.47	335.55			
110 120	338.63 369.41	341.71 372.49	344.79 375.57	347.86 378.65	350.94	354.02	357.10		363.26	366.33			
130	400.20	403.28	406.35	409.43	381.73 412.51	384.81 415.59	387.88 418.67	390.96	394.04	397.12			
140	430.98	434.06	437.14	440.22	443.30	416.37	449.45	421.75 452.53	424.83 455.61	427.90 458.69			
110	1.90.80	101100	101111	140.22	440.00	140.51	440.40	402.00	433.01	400.00			
150	461.77	464.85	467.92	471.00	474.08	477.16	480.24	483.32	486.39	489.47			
160	492.55	495.63	498.71	501.79	504.86	507.94	511.02	514.10	517.18				
170	523.34	526.41	529.49	532.57	535.65	538.73	541.81	544.88	547.96	551.04			
180	554.12	557.20	560.28	563.36	566.43	569.51	572.59	575.67	578.75	581.83			
190	584.90	587.98	591.06	594.14	597.22	600.30	603.38	606.45	609.53	612.61			
200	615.69	618.77	621.85	624.92	628.00	631.08	634.16	637.24	640.32	643.39			
210	646.47	649.55	652.63	655.71	658.79	661.87	664.94	668.02	671.10	674.18			
220 230	677.26 708.04	680.34 711.12	683.41 $714.20$	686.49	689.57	692.65	695.73	698.81	701.89	704.96			
240	738.83	741.90	744.98	717.28 748.06	720.36 751.14	723.43 754.22	726.51 757.30	729.59 760.38	732.67 763.45	735.75			
240	130.00	141.50	144.30	140.00	191.14	104.22	191.30	100.55	109.49	766.53			
250	769.61	772.69	775.77	778.85	781.92	785.00	788.08	791.16	794.24	797.32			
260	800.40	803.47	806.55	809.63	812.71	815.79	818.87	821.94	825.02	828.10			
270	831.18	834.26	837.34	840.42	843.49	846.57	849.65	852.73	855.81	858.89			
280	861.96	865.04	868.12	871.20	874.28	877.36	880.43	883.51	886.59	889.67			
290	892.75	895.83	898.91	901.98	905.06	908.14	911.22	914.30	917.38	920.45			
-00	000 55	000.01	0.20 62	000 5									
300	923.53	926.61	929.69	932.77	935.85					951.24			
310	954.32	957.40		963.55	966.63								
320 330	985.10				997.42	1000.49	1003.57						
340						1031.28							
040	}												
350						1092.85							
360						1123.63							
370	1139.02	1142.10	1145.18	1148.26	1151.34	1154.42	1157.49	1160.57	1163.65	1166.73			
380	1169.81	1172.89	1175.97	1179.04	1182.12	1185.20	1188.28	1191.36	1194.44	1197.51			
390	1200.59	1203.67	1206.75	1209.83	1212.91	1215.99	1219.06	1222.14	1225.22	1228.30			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

1 Metre = 3.078444 Paris Feet.

Metres. Tens.	Metres. Units.												
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
		Fr. Feet.			Fr. Feet.		Fr. Feet.			Fr. Fee			
400	1				1243.69								
410					1274.48				1286.79				
420					1305.26				1317.57				
430					1336.04				1348.36	}			
440	1354.52	1357.59	1360.67	1363.75	1366.83	1369.91	1372.99	1376.06	1379.14	1382.			
450	1385.30	1388.38	1391.46	1394.54	1397.61	1400.69	1403.77	1406.85	1409.93	1413.			
460	1416.08	1419.16	1422.24	1425.32	1428.40	1431.48	1434.55	1437.63	1440.71	1443.			
470	1446.87	1449.95	1453.03	1456.10	1459.18	1462.26	1465.34	1468.42	1471.50	1474.			
480	1477.65	1480.73	1483.81	1486.89	1489.97	1493.05	1496.12	1499.20	1502.28	1505.			
490	1508.44	1511.52	1514.59	1517.67	1520.75	1523.83	1526.91	1529.99	1533.07	1536.			
500	1539.22	1542.30	1545.38	1548.46	1551.54	1554.61	1557.69	1560.77	1563.85	1566.			
510	1570.01	1573.08	1576.16	1579.24	1582.32	1585.40	1588.48	1591.56	1594.63	1597.			
520	1600.79	1603.87	1606.95	1610.03	1613.10	1616.18	1619.26	1622.34	1625.42	1628.			
530	1631.58	1634.65	1637.73	1640.81	1643.89	1646.97	1650.05	1653.12	1656.20	1659.			
540	1662.36	1665.44	1668.52	1671.60	1674.67	1677.75	1680.83	1683.91	1686.99	1690.			
550	1693.14	1696.22	1699.30	1702.38	1705.46	1708.54	1711.61	1714.69	1717.77	1720.			
560		- 1			1736.24								
570					1767.03				1779.34				
580					1797.81				1810.13				
590	1 1				1828.60				1840.91				
coo	3047 07	1050 14	1059 99	1956 20	1859.38	1969 46	1005 54	1000 00	1971 60	1074			
600	1				1890.16								
620	1				1920.95				1933.26				
630	ì				1951.73				1964.05				
640					1982.52				1994.83				
650	(				2013.30								
660	1				2044.09								
670	1				2074.87				2087.19				
680					2105.66 2136.44				2117.97				
690	2124.13	2127.20	2130.28	2100.00	2130.44	2139.52	2142.00	2140.08	2148.75	2101.			
700					2167.22				5	1			
710					2198.01				2210.32				
720	1				2228.79				2241.11				
730					2259.58				2271.89				
740	2278.05	2281.13	2284.21	2287.28	2290.36	2293.44	2296.52	2299.60	2302.68	2305.			
750	1				2321.15								
760					2351.93				2364.24	1			
770					2382.72				2395.03				
780	1				2413.50				2425.81	1			
790	2431.97	2435.05	2438.13	2441.21	2444.28	2447.36	2450.44	2453.52	2456.60	2459.			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

1 Metre = 3.078444 Paris Feet.

Metres.					Metres.	Units.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
000		Fr. Feet.			Fr. Feet.		Fr. Feet.			Fr. Feet.
800	H H				2475.07	3	1	1		
810	11	1			2505.85		1			
820 830	III .	ł .		1	2536.64		1	1		
840	H				2567.42 2598.21	1	2604.36			
850	2616.68	2619.76	2622.83	2625.91	2628.99	2632.07	2635.15	2638.23	2641.30	2644.38
860	11		i .	1	2659.78					
870	17				2690.56				1	
880	H	l .	1		2721.34		1	J.		
890	III				2752.13	Į.			ŧ	
900	2770.60	2773.68	2776.76	2779.83	2782.91	2785.99	2789.07	2792.15	2795.23	2798.3
910	2801.38	2804.46	2807.54	2810.62	2813.70	2816.78	2819.85	2822.93	2826.01	2829.0
920	2832.17	2835.75	2838.33	2841.40	2844.48	2847.56	2850.64	2853.72	2856.80	2859.8
930	2862.95	2866.03	2869.11	2872.19	2875.27	2878.35	2881.42	2884.50	2887.58	2890.6
940	2893.74	2896.82	2899.89	2902.97	2906.05	2909.13	2912.21	2915.29	2918.36	2921.4
950	2924.52	2927.60	2930.68	2933.76	2936.84	2939.91	2942.99	2946.07	2949.15	2952.2
960	2955.31	2958.38	2961.46	2964.54	2967.62	2970.70	2973.78	2976.86	2979.93	2983.0
970					2998.40					
980	3016.88	3019.95	3023.03	3026.11	3029.19	3032.27	3035.35	3038.42	3041.50	3044.5
990	3047.66	3050.74	3053.82	3056.89	3059.97	3063.05	3066.13	3069.21	3072.29	3075.3
Metres.	French F	eet. M	etres. F	rench Fee	t. Metr	es. Fre	nch Feet.	Metre	s. Fren	ch Feet.
1000	3078.	44 5	000	15392.22	90	00 2	706.00	13000	0 400	019.78
2000	6156.	15	1	18470.67	11		784.44	14000	1	098.22
3000	9235.	- 11	1	21549.11	- 11		8862.89	15000		176.67
4000	12313.	- 11	8000	24627.56	120		6941.33	16000	0   492	255.11
					Decim	etres.				•
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fr Feet.	Fr Feet.	Fr.Feet.	Fr.Feet.	Fr Feet.	Fr.Feet	Fr. Feet.	Fr. Feet.	Fr.Feet.	Fr. Feet.
0	0.0000	0.3078	0.6157	0.9235	1.2314	1.5392	1.8471	2.1549		2.770
1	3.0784	3.3863		4.0020	4.3098	4.6177	4.9255		ł	
2	6.1569	6.4647						8.3118		
3 4					10.4667 13.5452					
5					16.6236					
6					19.7020					
7	11				22.7805					
8					25.8589					
9	27.7060	28.0138	28.3217	28.6295	28.9374	29.2452	29.5531	29.8609	30.1688	30.476

1 Metre = 3.28089917 English Feet.

27.					Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng.Feet.		Eng.Feet.		Eng.Feet.	Eng.Feet.	Eng Feet.	Eng. Feet.	Eng.Feet.	Eng. Fee
0	0.0	3.28	6.56	9.84	13.12	16.40	19.69	22.97	26.25	29.5
10	32.81	36.09	39.37	42.65	45.93	49.21	52.49	55.78	59.06	62.3
20	65.62	68.90	72.18	75.46	78.74	82.02	85.30	88.58	91.87	95.1
30	98.43	101.71	104.99	108.27	111.55	114.83	118.11	121.39	124.67	127.9
40	131.24	134.52	137.80	141.08	144.36	147.64	150.92	154.20	157.48	160.7
50	164.04	167.33	170.61	173.89	177.17	180.45	183.73	187.01	190.29	193.5
60	196.85	200.13	203.42	206.70	209.98	213.26	216.54	219.82	223.10	226.3
70	229.66	232.94	236.22	239.51	242.79	246.07	249.35	252.63	255.91	259.1
80	262.47	265.75	269.03	272.31	275.60	278.88	282.16	285.44	288.72	292.0
90	295.28	298.56	301.84	305.12	308.40	311.69	314.97	318.25	321.53	324.8
100	328.09	331.37	334.65	337.93	341.21	344.49	347.78	351.06	354.34	357.6
110	360.90	364.18	367-46	370.74	374.02	377.30	380.58	383.87	387.15	390.4
120	393.71	396.99	400.27	403.55	406.83	410.11	413.39	416.67	419.96	423.2
130	426.52	429.80	433.08	436.36	439.64	442.92	446.20	449.48	452.78	456.0
140	459.33	462.61	465.89	469.17	472.45	475.73	479.01	482.29	485.57	488.8
150	492.13	495.42	498.70	501.98	505.26	508.54	511.82	515.10	518.38	521.6
160	524.94	528.22	531.51	534.79	538.07	541.35	544.63	547.91	551.19	554.4
170	557.75	561.03	564.31	567.60	570.88	574.16	577.44	580.72	584.00	587.2
180	590.56	593.84	597.12	600.40	603.69	606.97	610.25	613.53	616.81	620.0
190	623.37	626.65	629.93	633.21	636.49	639.78	643.06	646.34	649.62	652.9
200	656.18	659.46	662.74	666.02	669.30	672.58	675.87	679.15	682.43	685.7
210	688.99	692.27	695.55	698.83	702.11	705.39	708.67	711.96	715.24	718.5
220	721.80	725.08	728.36	731.64	734.92	738.20	741.48	744.76	748.05	751.3
230	754.61	757.89	761.17	764.45	767.73	771.01	774.29	777.57	780.85	784.1
240	787.42	790.70	793.98	797.26	800.54	803.82	807.10	810.38	813.66	816.9
250	820.22	823.51	826.79	830.07	833.35	S36.63	839.91	843.19	846.47	849.7
260	853.03	856.31	859.60	862.88	866.16	869.44	872.72	876.00	879.28	882.5
270	885.84	889.12	892.40	895.69	898.97	902.25	905.53	908.81	912.09	915.3
280	918.65	921.93	925.21	928.49	931.78	935.06	938.34	941.62	944.90	948.1
290	951.46	954.74	958.02	961.30	964.58	967.87	971.15	974.43	977.71	980.9
300	984.27	987.55	990.83	994.11		1000.67	1003.96	1	1010.52	1013.8
310	1017.08		1023.64	1	1030.20			1040.05	1043.33	1046.6
320	1049.89	1053.17	1056.45	1059.73	1063.01	1	1069.57	1072.85	1076.13	1079.4
330	1082.70	1085.98	1089.26	1092.54		1099.10		1105.66	1108.94	1112.2
340	1115.51	1118.79	1122.07	1125.35	1128.63	1131.91	1135.19	1138.47	1141.75	1145.0
350	1148.31				1161.44					
360	1181.12		1187.69	1190.97	1			1204.09	1207.37	1210.6
370	1213.93	1	1220.49	1	1		1233.62		1240.18	
380	1246.74		1253.30	1256.58	1	1263.15	1266.43	1269.71	1272.99	1276.2
390	1279.55	1282.83	1286.11	1289.39	1292.67	1295.96	1299.24	1302.52	1305.80	1309.0
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

D

400 to 799.

Metres.					Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
400	Eng.Feet. 1312.36	Eng.Feet. 1315.64	Eng.Feet. 1318.92	Eng.Feet. 1322.20		Eng.Feet. 1328.76	Eng. Feet. 1332.05	Eng. Feet. 1335.33	Eng.Feet.	Eng.Fe
410	1345.17		1351.73		1358.29	1	1364.85		1371.42	1
420	1377.98	1381.26	İ	1387.82	f .	1394.38	1397.66	1400.94	1404.22	1
430	1410.79	1414.07	1417.35	1420.63		1427.19	1430.47	1433.75	1437.03	
440	1443.60	1446.88	1450.16		1456.72	1	1463.28	1466.56	1469.84	1473.
450	1476.40	1479.69	1482.97	1486.25	1489.53	1492.81	1496.09	1499.37	1502.65	1505.9
460	1509.21	1512.49	1515.78	1519.06	1522.34	1525.62	1528.90	1532.18	1535.46	1538.7
470	1542.02	1545.30	1548.58	1551.87	1555.15	1558.43	1561.71	1564.99	1568.27	1571.5
480	1574.83	1578.11	1581.39	1584.67	1587.96	1591.23	1594.52	1597.80	1601.08	1604.3
490	1607.64	1610.92	1614.20	1617.48	1620.76	1624.05	1627.33	1630.61	1633.89	1637.1
500	1640.45	1643.73	1647.01	1650.29	1653.57	1656.85	1660.13	1663.42	1666.70	1669.9
510	1673.26	1676.54	1679.82	1683.10	1686.38	1689.66	1692.94	1696.22	1699.51	1702.7
520	1706.07	1709.35	1712.63	1715.91	1719.19	1722.47	1725.75	1729.03	1732.31	1735.6
530	1738.88		1745.44				1758.56		1765.12	
540	1771.69	1774.97	1778.25	1781.53	1784.81	1788.09	1791.37	1794.65	1797.93	1801.2
550	1804.49	1807.78	1811.06	1814.34	1817.62	1820.90	1824.18	1827.46	1830.74	1834.0
560	1837.30	1840.58	1843.87	1847.15	1850.43	1853.71	1856.99	1860.27	1863.55	1866.8
570	1870.11	1873.39	1876.67	1879.96	1883.24	1886.52	1889.80	1893.08	1896.36	1899.6
580	1902.92	1906 20	1909.48		1916.05		1922.61	1925.89	1929.17	1932.4
590	1935.73	1939.01	1942.29	1945.57	1948.85	1952.13	1955.42	1958.70	1961.98	1965.2
600	1968.54		1975.10							1998.0
610		2004.63					2021.03			
620	2034.16		2040.72			2050.56		1		2063.6
630	2066.97		2073.53				2086.65			2096.4
640	2099.78	2103.06	2106.34	2109.62	2112.90	2116.18	2119.46	2122.74	2126.02	2129.3
650	2132.58	2135.87	2139.15	2142.43	2145.71	2148.99	2152.27	2155.55	2159.83	2162.1
660	2165.39	2168.67	2171.96	2175.24	2178.52	2181.80	2185.08	2188.36	2191.64	2194.9
670	2198.20	2201.48	2204.76	2208.05	2211.33	2214.61	2217.89	2221.17	2224.45	2227.7
680	2231.01	2234.29	2237.57	2240.85	2244.13	2247.42	2250.70	2253.98	2257.26	2260.5
690	2263.82	2267.10	2270.38	2273.66	2276.94	2280.22	2283.51	2286.79	2290.07	2293.3
700	2296.63	2299.91	2303.19	2306.47	2309.75	2313.03	2316.31	2319.60	2322.88	2326.1
710	2329.44	2332.72	2336.00	2339.28	2342.56	2345.84	2349.12			
720		2365.53				2378.65		2385.21		2391.7
730	2395.06	2398.34	2401.62	2404.90	2408.18	2411.46	2414.74	2418.02	2421.30	2424.5
740	2427.87	2431.15	2434.43	2437.71	2440.99	2441.27	2447.55	2450.83	2454.11	2457.3
750		2463.96								
760	11	2496.76						2516.45		2523.0
770		2529.57				2542.70		2549.26		
780	2559.10				2572.22		2578.79		2585.35	2588.6
790	2591.91	2595.19	2598.47				2611.60			
	0.	1.	2.	3.	4.	5.	6.	7.	- 8.	9.

800 to 1199.

					Metres.	(Units.)				
Metros.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
200	Eng.Feet.		Eng.Feet.						1 -	1
800	2624.72	2628.00	2631.28	2634.56		2641.12		1		2654.
810 820	2657.53 $2690.34$	2660.S1 2693.62	2664.09 2696.90	$\begin{vmatrix} 2667.37 \\ 2700.18 \end{vmatrix}$		2673.93 2706.74	$\begin{vmatrix} 2677.21 \\ 2710.02 \end{vmatrix}$	2680.49		2687.
830	2723.15	2095.02  $ 2726.43 $	2729.71	2732.99		2739.55	2742.83	2713.30 2746.11	2716.58 2749.39	2719. 2752.
840	2755.96	2759.24	2762.52	2765.80		2772.36	2775.64		2782.20	2785.
850	2788.76	2792.05	2795.33	2798.61	2801.89	2805.17	2808.45	2811.73	2815.01	2818.
860	2821.57	2824.85	2828.14	2831.42		2837.98	2841.26	2844.54	2847.82	2851.
870	2854.38	2857.66	2860.94	2864.22		2870.79	2874.07	2877.55	§	2883.
880	2887.19	2890.47	2893.75	2897.03		2903.60	2906.88	2910.16	2913.44	2916.
890	2920.00	2923.28	2926.56			2936.40	2939.69	2942.97	2946.25	2949
900	2952.81	2956.09	2959.37	2962.65	2965.93	2969.21	2972.49	2975.78	2979.06	2982.
910	2985.62	2988.90	2992.18	2995.46		3002.02	3005.30	3008.58	3011.87	3015.
920	3018.43	3021.71	3024.99	3028.27	1	3034.83	3038.11	3041.39	3044.67	3047.
930	3051.24	3054.52	3057.80	3061.08		3067.64	3070.92		3077.43	3080.
940	3084.05	3087.33	3090.61	3093.89	3097.17	3100.45	3103.73	3107.01	3110.29	3113.
950	3116.85	3120.14	3123.42	3126.70	3129.98	3133.26	3136.54	3139.82	3143.10	3146.
960	3149.66	3152.94	3156.22	3159.51	1	3166.07	3169.35	3172.63	3175.91	3179.
970	3182.47		3189.03	3192.31		3198.88	3202.16	3205.44	3208.72	3212.
980	3215.28	3218.56	3221.84	3225.12		3231.69	3234.97	3238.25	3241.53	3244.
990	3248.09	3251.37	3254.65	3257.93	3261.21	3264.49	3267.78	3271.06	3274.34	3277.
1000	3280.90	3294.18	3287.46	3290.74	3291.02	3297.30	3300.58	3303.87	3307.15	3310.
1010	3313.71	3316.99	3320.27	3323.55	3326.83	3330.11	3333.39	3336.67	3339.96	3343.
1020	3346.52	3349.80	3353.08	3356.36	3359.64	3362.92	3366.20	3369.48	3372.76	3376.
1030	3379.33	3382.61	3385.89	3389.17	3392.45	3395.73	3399.01	3402.29	3405.57	3408.
1040	3412.14	3415.42	3418.70	3421.98	3425.26	3428.54	3431.82	3435.10	3438.38	3441.
1050	3444.94	3448.22	3451.51	3454.79	3458.07	3461.35	3464.63	3467.91	3471.19	3474.
1060	3477.75	3481.03	3484.31	3487.60	3490.88	3494.16	3497.44	3500.72	3504.00	3507.
1070	3510.56	3513.84	3517.12	3520.40	3523.69	3526.97	3530.25	3533.53	3536.81	3540.
1080	3543.37	3546.65	3549.93	3553.21	3556.49	3559.78	3563.06	3566.34	3569.62	3572.
1090	3576.18	3579.46	3582.74	3586.02	3589.30	3592.58	3595.87	3599.15	3602.43	3605.
1100	3608.99	3612.27	3615.55		3622.11	3625.39			3635.24	3638.
1110	3641.80	3645.08	3648.36	3651.64	3654.92	3658.20	3661.48	3664.76	3668.05	3671.
1120	3674.61	3677.89	3681.17	3684.45	3687.73		3694.29	3697.57	3700.85	3704.
1130	3707.42		3713.98		3720.54				3733.66	3736.9
1140	3740.22	3743.51	3746.79	3750.07	3753.35	3756.63	3759.91	3763.19	3766.47	3769.
1150		3776.31					3792.72	1	3799.28	3802.
1160		3809.12	3812.40		3818.97		3825.53		3832.09	3835.3
1170	3838.65	3841.93	3845.21		3851.78			3861.62	3864.90	3868.1
1180	3871.46	3874.74	3878.02		3884.58		3891.15	3894.43	3897.71	3900.9
1190	3904.27	3907.55	3910.83	3914.11	3917.39	3920.67	3923.96		3930.52	3933.8
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1200 to 1599.

Matrix					Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng.Feet.	Eng.Feet.		Eng. Feet.	0		0		"	
1200	3937.08		3943.64		ł .	3953.48	1	3960.05	3963.33	
1210	3969.89	3973.17	3976.45			3986.29	3989.57	3992.85	3996.14	3999.4
1220	4002.70	4005.98	4009.26	4012.54		4019.10	4022.38	4025.66	4028.94	4032.2
1230	4035.51	4038.79	4042.07	4045.35	1	4051.91	4055.19		4061.75	1
1240	4068.31	4071.60	4074.88	4078.16	4081.44	4084.72	4088.00	4091.28	4094.56	4097.8
1250	4101.12	4104.40	4107.69	4110.97	4114.25	4117.53	4120.81	4124.09	4127.37	4130.6
1260	4133.93	4137.21	4140.49	4143.78	4147.06	4150.34	4153.62	4156.90	4160.18	4163.4
1270	4166.74	4170.02	4173.30	4176.58	4179.87	4183.15	4186.43	4189.71	4192.99	4196.2
1280	4199.55	4202.83	4206.11	4209.39	4212.67	4215.96	4219.24	4222.52	4225.80	4229.08
1290	4232.36	4235.64	4238.92	4242.20	4245.48	4248.76	4252.05	4255.33	4258.61	4261.89
1300	4265.17	4268.45	4271.73	4275.01	4278.29	4281.57	4284.85	4288.14	4291.42	4294.70
1310	4297.98	4301.26	4304.54	4307.82				4320.94		4327.5
1320	4330.79	4334.07	4337.35	4340.63				4353.75	4357.03	4360.3
1330	4363.60	4366.88	4370.16	4373.44	4376.72	4380.00	4383.28	4386.56	4389.84	4393.13
1340	4396.40	4399.69	4402.97	4406.25	4409.53	4412.81	4416.09	4419.37	4422.65	4425.9
1350	4429.21	4432.49	4435.78	4439.06	1112.31	1112 65	4148.90	4452.18	4455.46	4458.7
1360	4462.02	4465.30	4468.58				- 1		4488.27	4491.5
1370	1494.83	4498.11	4501.39	4504.67			4514.52		4521.08	4524.3
1380	4527.64	4530.92	4534.20	4537.48		4544.05			4553.89	4557.13
1390	4560.45	4563.73	4567.01	4570.29			4580.14		4586.70	4589.98
1400	4593.26	4596.54	4599.82	4603.10	1606.38	1609 66	4612.94	1616 23	4619.51	4622.79
1410	4626.07	4629.35	4632.63	4635.91	4639.19		1	4649.03		4655.60
1420	4658.88	4662.16	4665.44	4668.72	4672.00	1	1	4681.84		4688.40
1430	4691.69	4694.97	4698.25	4701.53	4704.81			1	4717.93	4721.2
1440	4724.49	4727.78	4731.06	4734.34		1		1	4750.74	4754.05
1450	4757.30	4760.58	4763.87	4767.15	4770.43	1772 71	4776.99	1780 27	4783.55	4786.8
1460	4790.11	4793.39	4796.67	4799.96	4803.24		4809.80		(	4819.6
1470	4822.92	4826.20	4829.48	4832.76	4836.05				4849.17	4852.4
1480	4855.73	4859.01	4862.29	4865.57	4868.85				4881.98	4885.20
1490	4888.54		4895.10	4898.38			4908.23	i		4918.0
1500	4921.35	1001.60	4927.91	4931.19	102 1 47	4937.75	4941.03	10 11 21	19 17 60	4950.8
1500 1510	4921.33	4957.44	4960.72	4964.00	4967.28		1	4944.31	4980.40	4983.69
1520	4986.97	4990.25	4993.53	4996.81	5000.09				5013.21	5016.4
1530	5019.78			5029.62	5032.90				5046.02	5049.30
1540	5052.58	5055.87		5062.43			5072.27			5082.1
	-00- 00	5000 OF	F001 00	-00- 04	-000 FO	=101.00	5105 00	=100 gc	5111 64	E1140
1550		5088.67					5105.08			5114.9
1560	41		5124.76	5128.05	5131.33			5141.17	5144.45	5147.7
1570	5151.01	5154.29	5157.57	5160.85	5164.14		5170.70	5173.98	5177.26 5210.07	5180.5
1580 1590	5183.82 5216.63	5187.10 5219.91	5190.38 5223.19	5193.66 5226.47		5200.23 5233.03	5203.51 5236.32	5206.79 5239.60	5242.88	5213.3 5246.1
							6.	7.		9.
	0.	1.	2.	3.	4.	5.	O.		8.	9.

1600 to 2000.

				1000		(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng.Feet.					Eng.Feet				
1600	5249.44	5252.72	5256.00	5259.28		5265.84	5269.12	5272.40	5275.69	5278.97
1610	5282.25	5285.53	5288.81	5292.09		5298.65		1	5308.49	5311.78
1620	5315.06	1	5321.62	1	5328.18			5338.02	5341.30	5344.58
1630	5347.87	5351.15	5354.43	5357.71		5364.27	5367.55	5370.85	5374.11	5377.39
1640	5380.67	5383.96	5387.24	5390.52	5393.80	5397.08	5400.36	5403.64	5406.92	5410.20
1650	5413.48	5416.76	5420.05	5423.33	5426.61	5429.89	5433.17	5436.45	5439.73	5443.01
1660	5446.29	5449.57	5452.85	5456.14	5459.42	5462.70	5465.98	5469.26	5472.54	5475.82
1670	5479.10	5482.38	5485.66	5488.94	5492.23	5495.51	5498.79	5502.07	5505.35	5508.63
1680	5511.91	5515.19	5518.47	5521.75	5525.03	5528.32	5531.60	5534.88	5538.16	5541.44
1690	5544.72	5548.00	5551.28	5554.56	5557.84	5561.12	5564.40	5567.69	5570.97	5574.25
1700	5577.53	5580.81	5584.09	5587.37	5590.65	5593.93	5597.21	5600.49	5603.78	5607.06
1710	5610.34	5613.62	5616.90	5620.18		5626.74	5630.02	5633.30	5636.58	5639.87
1720	5643.15	5646.43	5649.71	5652.99		5659.55	5662.83	5666.11	5669.39	5672.67
1730	5675.96	5679.24	5682.52	5685.80		5692.36	5695.64	5698.92	5702.20	5705.48
1740	5708.76	5712.05	5715.33	5718.61		5725.17	5728.45	5731.73	5735.01	5738.29
1750	5741.57	5744.85	5748.14	5751.42		5757.98	5761.26	5764.54	5767.82	5771.10
1760	5774.38	5777.66	5780.94	5784.23	5787.51	5790.79	5794.07	5797.35	5800.63	5803.91
1770	5807.19	5810.47	5813.75	5817.03		5823.60	5826.88	5830.16	5833.44	5836.72
1780	5840.00	5843.28	5846.56	5849.84		5856.40	5859.69	5862.97	5866.25	5869.53
1790	5872.81	5876.09	5879.37	5882.65	5885.93	5889.21	5892.49	5895.78	5899.06	5902.34
1800	5905.62	5908.90	5912.18	5915.46	5918.74	5922.02	5925.30	5928.58	5931.87	5935.15
1810	5938.43	5941.71	5944.99	5948.27	5951.55	5954.83	5958.11	5961.39	5964.67	5967.96
1820	5971.24	5974.52	5977.80	5981.08	5984.36	5987.64	5990.92	5994.20	5997.48	6000.76
1830	6004.05	6007.33	6010.61	6013.89	6017.17	6020.45	6023.73	6027.01	6030.29	6033.57
1840	6036.85	6040.14	6043.42	6046.70	6049.98	6053.26	6056.54	6059.82	6063.10	6066.38
1850	6069.66	6072.94	6076.23	6079.51	6082.79	6086.07	6089.35	6092.63	6095.91	6099.19
1860	6102.47			6112.32	6115.60		6122.16	6125.44	6128.72	6132.00
1870	6135.28	6138.56	6141.84	6145.12	6148.40	6151.69	6154.97	6158.25	6161.53	6164.81
1880	6168.09	6171.37	6174.65	6177.93	6181.21	6184.49	6187.78	6191.06	6194.34	6197.62
1890	6200.90	6204.18	6207.46	6210.74	6214.02	6217.30	6220.58	6223.87	6227.15	6230.43
1900	6233.71	6236.99	6240.27	6243.55	6246.83	6250.11	6253.39	6256.67	6259.96	6263.24
1910	6266.52			6276.36	6279.64	1				6296.05
1920	6299.33	6302.61	6305.89	6309.17	6312.45			1		6328.85
1930	6332.14	6335.42	6338.70	6341.98	6345.26	1	6351.82	6355.10		6361.66
1940	6364.94	6368.23	6371.51	6374.79	6378.07		6384.63			6394.47
1050	690* **	6401 02	6404.99	6107 60	6410.00	601116	C417 44	6 190 79	6121.00	6427.28
1950	6397.75		6404.32					1		6450.09
1960	6430.56		6437.12			6446.97 6479.78	6450.25		6456.81 6489.62	
1970	6463.37	6466.65		1				6486.34	6522.43	6492.90 6525.71
1980 1990	6496.18 6528.99	6499.46 $6532.27$	6502.74 6535.55	6506.02	6509.30	6545.39	6515.87 6548.67		6555.24	6558.52
2000	6561.80	6565.08		6571.64		6578.20	6581.48	6584.76	6588.05	6591.33
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

2000 to 2399.

77.45					Metres.	(Units)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
2000	Eng.Feet.					Eng.Feet.			Eng. Feet.	
2000	6561.80	6565.08			6574.92		6581.48		6588.05	
2010	6594.61	6597.89		6604.45		6611.01	6614.29	6617.57	6620.85	6624.1
2020	6627.42	6630.70		6637.26		6643.82	6647.10		6653.66	
2030 2040	6660.23 6693.03	6663.51 6696.32		6670.07 6702.88	6673.35 6706.16	6676.63 6709.44	6679.91 6712.72	6683.19 6716.00	6686.47 6719.28	6689.78 6722.50
2050	6725.84	6729.12		6735.69 6768.49	1	6742.25 6775.06	6745.53		6752.09	
	6758.65	6761.93					6778.34		6784.90	6788.1 6820.9
2070	6791.46	6794.74		6801.30	1	6807.87	6811.15		6817.71	
2080 2090	6824.27 6857.08	6827.55 6860.36		6834.11 6866.92		6840.67 6873.48	6843.96 6876.76	1	6850.52 6883.33	
2100	6889.89	6893.17		6899.73		6906.29	6909.57	1	6916.14	
2110	6922.70	6925.98		6932.54	1	6939.10	6942.38		6948.94	6952.2
2120	6955.51	6958.79		6965.35	1	6971.91	6975.19	i	6981.75	
2130	6988.32	6991.60		6998.16	1	7004.72	7008.00		7014.56	
2140	7021.12	7024.41	7027.69	7030.97	7034.25	7037.53	7040.81	7044.09	7047.37	7050.6
2150	7053.93	7057.21	7060.49	7063.78	7067.06	7070.34	7073.62	7076.90	7080.18	7083.4
2160	7086.74	7090.02	7093.30	7096.58	7099.87	7103.15	7106.43	7109.71	7112.99	7116.2
2170	7119.55	7122.83	7125.11	7129.39	7132.67	7135.96	7139.24	7142.52	7145.80	7149.0
2180	7152.36	7155.64	7158.92	7162.20	7165.48	7168.76	7172.05	7175.33	7178.61	7181.8
2190	7185.17	7188.45	7191.73	7195.01	7198.29	7201.57	7204.85	7208.14	7211.42	7214.7
2200	7217.98	7221.26	7224.54	7227.82	7231.10	7234.38	7237.66	7240.94	7244.23	7247.5
2210	7250.79	7254.07		7260.63		7267.19	7270.47	1	7277.03	İ
2220	7283.60	7286.88		7293.44	1	7300.00	7303.28	1	7309.84	7313.1
2230	7316.41	7319.69	7322.97		1	7332.81	7336.09	1	7342.65	
2240	7349.21	7352.49	7355.78	7359.06	ł.	7365.62	7368.90	7372.18	7375.46	7378.7
0050	<b>7900 00</b>	*90= 90	#900 E0	*901 O*	~00° 1°	m200 40	~ 401 ~ 1	~ 40 4 00	7 100 07	7411.5
2250	7382.02	7385.30	7421.39	7391.87	7427.96	7398.43 7431.24	7401.71 7434.52	1	7408.27 7441.08	7444.3
2260 2270	7414.55	7418.11 7450.92		7457.48		7464.05	7467.33		1	
2280	7480.45	7483.73	7487.01	7490.29		7496.85	7500.14	7503.42	7506.70	7509.9
2290	7513.26	7516.54		7523.10		7529.66	7532.94		7539.51	
2300	7546.07	7549.35		7555.91		7562.47	7565.75	•	7572.32	
2310	7578.88	7582.16		7588.72		7595.28	7598.56	1	7605.12	
2320	7611.69	7614.97		7621.53		7628.09	7631.37	7634.65	1	7641.2
2330	7644.50	7647.78		7654.34		7660.90	7664.18		7670.74	
2340	7677.30	7680.58	7683.87	7687.15	7690.43	7693.71	7696.99	7700.27	7703.55	7706.8
2350	7710.11	7713.39	7716.67	7719.96	7723.24	7726.52	7729.80	7733.08	7736.36	7739.6
2360	7742.92	7746.20	7749.48	7752.76	7756.05	7759.33	7762.61	7765.89	7769.17	7772.4
2370	7775.73	7779.01	7782.29	7785.57	7788.85	7792.14	7795.42	7798.70	7801.98	7805.2
2380	7808.54	7811.82	7815.10	7818.38	7821.66	7824.94	7828.23	7831.51	7834.79	7838.0
2390	7841.35	7844.63	7847.91	7851.19	7854.47	7857.75	7861.03	7864.32	7867.60	7870.8
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

2400 to 2799.

					Metres.	(Units)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
2400	_	Eng. Feet.			Eng.Feet.		Eng.Feet.	_	Eng.Feet.	
	7874.16	7877.44			7887.28		7893.84	7897.12		7903.6
2410 2420	7906.97 7939.78	7910.25 7943.06		7916.81	7920.09	1	7926.65		7933.21	7936.5
2430	7972.59			7949.62	7952.90		7959.46		7966.02	7969.3
2440	8005.39	7975.87 8008.67		7982.43 8015.24	7985.71 8018.52	7988.99 8021.80	7992.27 8025.08		7998.83 8031.64	8002. 8034.
2450	8038.20	8041.48	8044.76	8048.05	8051.33	8054.61	8057.89	8061.17	8064.45	8067.
2460	8071.01	8074.29			8084.14		8090.70		8097.26	8100.
2470	8103.82	8107.10			8116.94		8123.51		8130.07	8133.
2480	8136.63	8139.91		8146.47	1	8153.03	8156.32		8162.88	8166.
2490	8169.44	8172.72			8182.56		8189.12		8195.69	8198.
2500	8202.25	8205.53	8208.81	8212.09	8215.37	8218.65	8221.93	8225.21	8228.50	8231.
2510	8235.06	8238.34	8241.62	8244.90	8248.18	8251.46	8254.74	8258.02	8261.30	8264.
2520	8267.87	8271.15	8274.43	8277.71	8280.99	8284.27	8287.55	S290.S3	S294.11	8297.
2530	8300.67	8303.96	8307.24	8310.52	8313.80	8317.08	8320.36	8323.64	8326.92	8330.
2540 0	8333.48	8336.76	8340.05	8343.33	8346.61	8349.89	8353.17	8356.45	8359.73	8363.
2550	8366.29	8369.37	8372.85	8376.14	8379.42	8382.70	8385.98	8389.26	8392.54	8395.
2560	8399.10	8402.38	8405.66	8408.94	8412.23	8415.51	8418.79	8422.07	8425.35	8428.
2570	8431.91	8435.19	8438.47	8441.75	8445.03	8448.32	8451.60	8454.88	8458.16	8461.
2580	8464.72	8468.00	8471.28	8474.56	8477.84	8481.12	8484.41	8487.69	8490.97	8494.
2590	8497.53	8500.81	8504.09	8507.37	8510.65	8513.93	8517.21	8520.50	8523.78	8527.
2600	8530.34	8533.62			1	8546.74			8556.58	8559.
2610	8563.15	8566.43		i	8576.27		8582.83		8589.39	8592.
2620	8595.96	8599.24		8605.80	8609.08	8612.36			8622.20	8625.
2630	8628.76	8632.05		8638.61	8641.89	8645.17	8648.45		8655.01	8658.
2640	8661.57	8664.85	8668.14	8671.42	8674.70	8677.98	8681.26	8684.54	8687.82	8691.
2650	8694.38	8697.66		8704.23	1	8710.79			8720.63	8723.
2660	8727.19	8730.47		8737.03	1	8743.60	8746.88		8753.44	8756.
2670	8760.00	8763.28		8769.84		8776.41	8779.69		8786.25	8789.
2680	8792.81	8796.09			8805.93		8812.50		8819.06	8822.
2690	8825.62	8828.90	8832.18	8835.46	8838.74	8842.02	8845.30	8848.59	8851.87	8855.
2700	8858.43	8861.71	8864.99	8868.27	8871.55	8874.83	8878.11	8881.39	8884.67	8887.
2710	8891.24	8894.52	8897.80	8901.08	8904.36		8910.92	8914.20	8917.48	8920.
2720	8926.05	8927.33	8930.61	8933.89	8937.17	8940.45	8943.73	8947.01	8950.29	8953.
2730	8956.85	8960.14		8966.70		8973.26	8976.54	8979.82		8986.
2740	\$989.66	8992.94	8996.23	8999.51	9002.79	9006.07	9009.35	9012.63	9015.91	9019.
2750	9022.47	9025.75				9038.88				9052.
2760	9055.28		9061.84			9071.69	- (	9078.25		9084.
2770	9088.09	9091.37		9097.93		9104.50	9107.78	9111.06		9117.
2780	9120.90	9124.18		9130.74		9137.30	9140.59	9143.87		9150.
2790	9153.71	9156.99	9160.27	9163.55	9166.83	9170.11	9173.39	9176.68	9179.96	9183.
	0.	1.	2.	3.	4.	5.	6.	7.	9.	9.

2800 to 3000.

·					Metres.	(Units.)		-112		
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng.Feet.	Eng. Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng. Feet.	Eng.Feet.	Eng.Feet.	Eng. Feet.
2800						9202.92				
2810	9219.33	9222.61	9225.89	9229.17	9232.45	9235.73	9239.01	9242.29	9245.57	9248.85
2820	9252.14	9255.42	9258.70	9261.98	9265.26	9268.54	9271.82	9275.10	9278.38	9281.66
2830	9284.94	9288.23	9291.51	9294.79	9298.07	9301.35	9304.64	9307.91	9311.19	9314.47
2840	9317.75	9321.03	9324.32	9327.60	9330.88	9334.16	9337.44	9340.72	9344.00	9347.28
2850	9350.56	9353.84	9357.12	9360.41	9363.69	9366.97	9370.25	9373.53	9376.81	9380.09
2860	9383.37	9386.65	9389.93	9393.21	9396.50	9399.78	9403.06	9406.34	9409.62	9412.90
2870	9416.18	9419.46	9422.74	9426.02	9429.30	9432.59	9435.87	9439.15	9442.43	9445.71
2880	9448.99	9452.27	9455.55	9458.83	9462.11	9465.39	9468.68	9471.96	9475.24	9478.52
2890	9481.80	9485.08	9488.36	9491.64	9494.92	9498.20	9501.48	9504.76	9508.05	9511.33
2900						9531.01				
2910	1					9563.82				
2920				)		9596.63				
2930	1 .					9629.44				
2940	9645.84	9649.12	9652.41	9655.69	9658.97	9662.25	9665.53	9668.81	9672.09	9675.37
2950	9678.62						- 1			
2960		1		- 1		9727.87			i	- 1
2970	9744.27									
2980	9777.08	- 1								
2990	9809.89	- 1								
3000	9842.70	9845.98	9849.26	9852.54	9855.82	9859.10	9862.38	9865.66	9868.94	9872.23

## Proportional Parts.

Metres.		Decimetres.									
Metica.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	
0	0.0000	0.3281	0.6562	0.9843	1.3124	1.6404	1.9685	2.2966	2.6247	2.9528	
1	3.2809	3.6090	3.9371	4.2652	4.5933	4.9213	5.2494	5.5775	5.9056	6.2337	
2	6.5618	6.8899	7.2180	7.5461	7.8742	8.2022	8.5303	8.8584	9.1865	9.5146	
3	9.8427	10.1708	10.4989	10.8270	11.1551	11.4831	11.8112	12.1393	12.4674	12.7955	
4	13.1236	13.4517	13.7798	14.1079	14.4360	14.7640	15.0921	15.4202	15.7483	16.0764	
5	16.4045	16.7326	17.0607	17.3888	17.7169	18.0449	18.3730	18.7011	19.0292	19.3573	
6	19.6854	20.0135	20.3416	20.6697	20.9978	21.3258	21.6539	21.9820	22.3101	22.6382	
7	22.9663	23.2944	23.6225	23.9506	24.2787	24.6067	24.9348	25.2629	25.5910	25.9191	
8	26.2472	26.5753	26.9034	27.2315	27.5596	27.8876	28.2157	28.5438	28.8719	29.2000	
9	29.5281	29.8562	30.1843	30.5124	30.8405	31.1685	31.4966	31.8247	31.1528	32.4809	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

1 Metre = 3.28070878 American Feet.

Metres.					Hund	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Am Feet	Am Feet	Am. Feet.	Am Feet	Am Feet	Am. Feet	Am.Feet.	Am. Feet.		Am Feet
0	0.0	328.1	656.1	984.2	1312.3	1640.4	1968.4	2296.5		2952.6
1000	3280.7	3608.8	3936.9	4264.9		4921.1	5249.1	5577.2		6233.3
2000	6561.4	6889.5	7217.6	7545.6	7873.7	8201.8	8529.8	8857.9	9186.0	9514.1
3000	9842.1	10170.2	10498.3	10826.3	11154.4	11482.5	11810.6	12138.6	12466.7	12794.8
4000	13122.8	13450.9	13779.0	14107.0	14435.1	14763.2	15091.3	15419.3	15747.4	16075.5
5000	16403.5	16731.6	17059.7	17387.8	17715.8	18043.9	18372.0	18700.0	19028.1	19356.2
6000	19684.3	20012.3	20340.4	20668.5	20996.5	21324.6	21652.7	21980.7	22308.8	22636.9
7000	22965.0	23293.0	23621.1	23949.2	24277.2	24605.3	24933.4	25261.5	25589.5	25917.6
8000	26245.7	26573.7	26901.8	27229.9	27558.0	27886.0	28214.1	28542.2	28870.2	29198.3
9000	29526.4	29854.4	30182.5	30510.6	30838.7	31166.7	31494.8	31822.9	32150.9	32479.0
	14									
_					Un	its.	-			
Tens.	0.	1.	2.	3.	<b>4.</b>	its.	6.	7.	8.	9.
Tens.	O. Am Feet	Am Feet.	2.	3. Am Feet.	l		6. Am. Feet.	7.	S. Am Feet.	
0					4.	5.				Am. Feet
0 10	Am Feet	Am Feet.	Am Feet	Am Feet.	4.	5. Am Feet.	Am. Feet.	Am.Feet.	Am Feet.	Am. Feet 29.526
0	Am Feet 0.000	Am Feet. 3.281	Am Feet 6.561	Am Feet. 9.842	4. Am.Feet 13.123	5. Am Feet. 16.404	Am. Feet. 19.684	Am.Feet. 22.965	Am Feet. 26.246	Am. Feet 29.526 62.333
0 10	Am Feet 0.000 32.807	Am Feet. 3.281 36.088	Am Feet 6.561 39.369	Am Feet. 9.842 42.649 75.456	4. Am.Feet 13.123 45.930	5. Am Feet. 16.404 49.211	Am. Feet. 19.684 52.491 85.298	Am.Feet. 22.965 55.772	Am Feet. 26.246 59.053 91.860	Am. Feet 29.526 62.333 95.141
0 10 20	Am Feet 0.000 32.807 65.614	Am Feet. 3.281 36.088 68.895 191.702	Am Feet 6.561 39.369 72.176 104.983	Am Feet. 9.842 42.649 75.456 108.263	Am.Feet 13.123 45.930 78.737 111.544	Am Feet, 16.404 49.211 82.018	Am. Feet. 19.684 52.491 85.298 118.106	Am.Feet. 22.965 55.772 88.579	Am Feet. 26.246 59.053 91.860 124.667	Am. Feet 29.526 62.333 95.141 127.948
0 10 20 30	Am Feet 0.000 32.807 65.614 98.421 131.228	Am Feet. 3.281 36.088 68.895 191.702 134.509	Am Feet 6.561 39.369 72.176 104.983 137.790	Am Feet. 9.842 42.649 75.456 108.263 141.070	Am.Feet 13.123 45.930 78.737 111.544	5. Am Feet. 16.404 49.211 82.018 114.825 147.632	Am. Feet. 19.684 52.491 85.298 118.106 150.913	Am.Feet. 22.965 55.772 88.579 121.386 154.193	Am Feet. 26.246 59.053 91.860 124.667 157.474	Am. Feet 29.526 62.333 95.141 127.948 160.755
0 10 20 30 40	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035	Am Feet. 3.281 36.088 68.895 191.702 134.509	Am Feet 6.561 39.369 72.176 104.983 137.790 170.597	Am Feet. 9.842 42.649 75.456 108.263 141.070 173.878	Am. Feet 13.123 45.930 78.737 111.544 144.351	5. Am Feet. 16.404 49.211 82.018 114.825 147.632 180.439	Am. Feet. 19.684 52.491 85.298 118.106 150.913	Am.Feet. 22.965 55.772 88.579 121.386 154.193	Am Feet. 26.246 59.053 91.860 124.667 157.474	Am Feet 29.526 62.338 95.141 127.948 160.755
0 10 20 30 40	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035 196.843	Am Feet. 3.281 36.088 68.895 191.702 134.509	Am Feet 6.561 39.369 72.176 104.983 137.790 170.597 203.404	Am Feet. 9.842 42.649 75.456 108.263 141.070 173.878 206.685	4. Am.Feet 13.123 45.930 78.737 111.544 144.351 177.158 209.965	5.  Am Feet. 16.404 49.211 82.018 114.825 147.632 180.439 213.246	Am. Feet. 19.684 52.491 85.298 118.106 150.913 183.720 216.527	Am. Feet. 22.965 55.772 88.579 121.386 154.193 187.000 219.807	Am Feet. 26.246 59.053 91.860 124.667 157.474	Am Feet 29.526 62.333 95.141 127.948 160.755 193.562 226.369
0 10 20 30 40 50	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035 196.843 229.650	Am Feet. 3.281 36.088 68.895 191.702 134.509 167.316 200.123	Am Feet 6.561 39.369 72.176 104.983 137.790 170.597 203.404 236.211	Am Feet. 9.842 42.649 75.456 108.263 141.070 173.878 206.685 239.492	4.  Am.Fect 13.123 45.930 78.737 111.544 144.351 177.158 209.965 242.772	5.  Am Feet. 16.404 49.211 82.018 114.825 147.632 180.439 213.246 246.053	Am. Feet. 19.684 52.491 85.298 118.106 150.913 183.720 216.527 249.334	Am.Feet. 22.965 55.772 88.579 121.386 154.193 187.000 219.807 252.615	Am Feet. 26.246 59.053 91.860 124.667 157.474 190.281 223.088	Am. Feet 29.526 62.333 95.141 127.948 160.755 193.562 226.369 259.176

#### IX. CONVERSION OF METRES INTO RHINE OR PRUSSIAN FEET AND DECIMALS.

1 Metre = 3 1861995 Rhine Feet.

Metres.					Hun	dreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Rhine Ft.	Rhine Ft.	Rhine Ft	Rhine Ft	Rhine Ft.	Rhine Ft	Rhine Ft.	Rhine Ft.	Rhine Ft.	Rhine Ft
0	0.0	318.6	637.2	955.9	1274.5	1593.1	1911.7	2230.3	2549.0	2867.6
1000	3186.2	3504.8	3823.4	4142.1	4460.7	4779.3	5097.9	5416.5	5735.2	6053.8
2000	6372.4	6691.0	7009.6	7328.3	7646.9	7965.5	8284.1	8602.7	8921.4	9240.0
3000	9558.6	9877.2	10195.8	10514.5	10833.1	11151.7	11470.3	11788.9	12107.6	12426.2
4000	12744.8	13063.4	13382.0	13700.7	14019.3	14337.9	14656.5	14975.1	15293.8	15612.
5000	15931.0	16249.6	16568.2	16886.9	17205.5	17524.1	17842.7	18161.3	18480.0	18798.6
6000	19117.2	19435.8	19754.4	20073.1	20391.7	20710.3	21028.9	21347.5	21666.2	21984.8
7000	22303.4	22622.0	22940.6	23259.3	23577.9	23896.5	24215.1	24533.7	24852.4	25171.0
8000	25489.6	25803.2	26126.8	26445.5	26764.1	27082.7	27401.3	27719.9	28038.6	28357.2
9000	28675.8									

## PARIS OR FRENCH FEET

### INTO DIFFERENT MEASURES OF LENGTH.

#### X. CONVERSION OF PARIS OR FRENCH FEET INTO TOISES.

1 French Foot = 0.1666666 Toise.

French Feet.					Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.	Toises-
0	0.00	16.67	33.33	50.00	66.67	83.33	100.00	116.67	133.33	150.00
1000	166.67	183.33	200.00	216.67	233.33	250.00	266.67	283.33	300.00	316.67
2000	333.33	350.00	366.67	383.33	400.00	416.67	433.33	450.00	466.67	483.33
3000	500.00	516.67	533.33	550.00	566.67	583.33	600.00	616.67	633.33	650.00
4000	666.67	683.33	700.00	716.67	733.33	750.00	766.67	783.33	800.00	816.67
5000	833.33	850.00	866.67	883.33	900.00	916.67	933.33	950.00	966.67	983.33
6000	1000.00	1016.67	1033.33	1050.00	1066.67	1083.33	1100.00	1116.67	1133.33	1150.00
7000	1166.67	1183.33	1200.00	1216.67	1233.33	1250.00	1266.67	1283.33	1300.00	1316.67
8000	1333.33	1350.00	1366.67	1383.33	1400.00	1416.67	1433.33	1450.00	1466.67	1483.33
9000	1500.00	1516.67	1533.33	1550.00	1566.67	1583.33	1600.00	1616.67	1633.33	1650.00
10000	1666.67	1683.33	1700.00	1716.67	1733.33	1750.00	1766.67	1783.33	1800.00	1816.67
11000	1833.33	1850.00	1866.67	1883.33	1900.00	1916.67	1933.33	1950.00	1966.67	1983.33
12000	2000.00	2016.67	2033.33	2050.00	2066.67	2083.33	2100.00	2116.67	2133.33	2150.00
13000	2166.67	2183.33	2200.00	2216.67	2233.33	2250.00	2266.67	2283.33	2300.00	2316.67
14000	2333.33	2350.00	2366.67	2383.33	2400.00	2416.67	2433.33	2450.00	2466.67	2483.33
15000	2500.00	2516.67	2533.33	2550.00	2566.67	2583.33	2600.00	2616.67	<b>26</b> 33.33	2650.00
16000	2666.67	2683.33	2700.00	2716.67	2733.33	2750.00	2766.67	2783.33	2800.00	2816.67
17000	2833.33	2850.00	2866.67	2883.33	2900.00	2916.67	2933.33	2950.00	2966.67	2983.33
18000	3000.00	3016.67	3033.33	3050.00	3066.67	3083.33	3100.00	3116.67	3133.33	3150.00
19000	3166.67	3183.33	3200.00	3216.67	3233.33	3250.00	3266.67	3283.33	3300.00	3316.67
20000	3333.33	3350.00	3366.67	3383.33	3400.00	3416.67	3433.33	3450.00	3466.67	3483.33
21000	3500.00	3516.67	3533.33	3550.00	3566.67	3583.33	3600.00	3616.67	3633.33	3650.00
22000	3666.67	3683.33	3700.00	3716.67	3733.33	3750.00	3766.67	3783.33	3800.00	3816.67
23000	3833.33	3850.00	3866.67	3883.33	3900.00	3916.67	3933.33	3950.00	3966.67	3983.33
24000	4000.00	4016.67	4033.33	4050.00	4066.67	4083.33	4100.00	4116.67	4133.33	4150.00
25000	4166.67	4183.33	4200.00	4216.67	4233.33	4250.00	4266.67	4283.33	4300.00	4316.67
26000	4333.33	4350.00	4366.67	4383.33	4400.00	4416.67	4433.33	4450.00	4466.67	4483.33

### XI. CONVERSION OF PARIS OR FRENCH FEET INTO METRES.

1 Paris Foot = 0.32483943 Metres.

French Feet.					Hune	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
1000	000.00 324.84				l .	162.42	194.90			
2000	649.68		1			487.26 812.10	519.74 844.58			617.1
3000	974.52						1	1	1	1
4000	1299.36			1396.81	1429.29			1526.75	1	
5000	1624.20	1656.68	1689.16	1721.65	1754.13	1786.62	1819.10	1851.58	1884.07	1916.
6000	1949.04					2111.46				
7000	2273.88	2306.36	2338.84	2371.33	2403.81	2436.30	2468.78	2501.26	2533.75	2566.
8000	2598.72	2631.20	2663.68	2696.17	2728.65	2761.14	2793.62	2826.10	2858.59	2891.
9000	2923.55	2956.04	2988.52	3021.01	3053.49	3085.97	3118.46	3150.94	3183.43	3215.
10000	i .					3410.81				
11000	3573.23			1		3735.65				
12000	3	3930.56		1	ł.		i .	ł .	4157.94	
13000			1	i .		4385.33	1			r .
14000	4547.75	4580.24	4612.72	4645.10	4677.59	4710.07	4742.56	4775.04	4807.52	4840.
15000	4872.59	4905.08	4937.56	4970.04	5002.53	5035.01	5067.49	5099.98	5132.46	5164.
16000						5359.85				
17000	5522.27	5554.75	5587.24	5619.72	5652.21	5684.69	5717.17	5749.66	5782.14	5814.
18000	5847.11	5879.59	5912.08	5944.56	5977.05	6009.53	6042.01	6074.50	6106.98	6139.
19000	6171.95	6204.43	6236.92	6269.40	6301.88	6334.37	6366.85	6399.34	6431.82	6464.
20000	6496.79	6529.27	6561.76	6594.24	6626.72	6659.21	6691.69	6724.18	6756.66	6789.
21000	6821.63	6854.11	6886.60	6919.08	6951.56	6984.05	7016.53	7049.02	7081.50	7113.
22000	7146.47	7178.95	7211.44	7243.92	7276.40	7308.89	7341.37	7373.86	7406.34	7438.
23000	7471.31			7568.76	7601.24	7633.73	7666.21	7698.69	7731.18	7763.6
24000	7796.15	7828.63	7861.11	7893.60	7926.08	7958.57	7991.05	8023.53	8056.02	8088.
25000						8283.41			1	
26000						8608.24				
27000	S770.66	8803.15	8835.63	8868.12	8900.60	8933.08	8965.57	8998.05	9030.54	9063.0
Tens.					Un	its.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.0000	0.3248	0.6497	0.9745	1.2994	1.6242	1.9490	2.2739	2.5987	2.923
10 20	3.2484 6.4968	$\frac{3.5732}{6.8216}$	3.8981	4.2229	4.5478 7.7961	4.8726 8.1210	5.1974 8.4458	5.5223 8.7707	5.8471 9.0955	6.171 9.420
30						8.1210				
40						14.6178				
50	16.2420	16.5668	16.8916	17.2165	17.5413	17.8662	18.1910	18.5158	18.8407	19.165
60						21.1146				
70	22.7388	23.0636	23.3884	23.7133	24.0381	24.3630	24.6878	25.0126	25.3375	25.662
80	25.9872	26.3120	26.6368	26.9617	27.2865	27.6114	27.9362	28.2610	28.5859	28.910
90	20 2255	20 560 1	20 8852	20 2101	20 52 10	30.8597	21 18 16	31 5001	21 82 12	29 150

1 French Foot = 1.06576527 English Feet.

				1 French	u root = .	1.06576527	Engust Fe	et.											
Table   Tabl	French Feet.					Hund	lreds.												
0	Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900								
1000										1 -	Eng. fee								
2000							1	1		}	i								
3000		ll .	1		1														
\$\begin{array}{c c c c c c c c c c c c c c c c c c c					3		1			ţ	1								
5000		l l		1			1												
6000         6394.6         6501.2         6607.7         6714.3         6820.9         6927.5         7034.1         7140.6         7247.2         7333           7000         7460.4         7566.9         7673.5         7780.1         7856.7         7993.2         8099.8         8206.4         8313.0         8419           8000         8526.1         8632.7         8739.3         8845.9         8952.4         9059.0         9165.6         9272.2         9378.7         948.7           9000         9591.9         9698.5         9803.0         9911.6         10012.4         1023.3         1037.9         1044.5         1053.3         1037.9         1044.5         1052.1         1100.1         10657.7         10764.2         10570.8         1097.4         11084.0         1124.5         1022.1         11403.7         11510.3         11616.6         1204.1         1249.7         1226.3         12362.9         12468.5         12576.0         12682         1266.8         15773.3         1533.2         1310.9         12256.3         12362.9         12468.5         12576.0         12682         1266.8         15773.3         1536.0         1660.8         15775.5         1868.6         1566.8         15775.3         18641.8	4000	4263.1	4369.6	4476.2	4582.8	4689.4	4795.9	4902.5	5009.1	5115.7	5222								
\$\begin{array}{c c c c c c c c c c c c c c c c c c c	5000	5328.8	5435.4	5542.0	5648.6	5755.1	5861.7	5968.3	6074.9	6181.4	6288.								
8000	6000	6394.6	6501.2	6607.7	6714.3	6820.9	6927.5	7034.1	7140.6	7247.2	7353.								
9000	7000	7460.4	7566.9	7673.5	7780.1	7886.7	7993.2	8099.8	8206.4	8313.0	8419.								
10000	8000	8526.1	8632.7	8739.3	8845.9	8952.4	9059.0	9165.6	9272.2	9378.7	9485.								
11000	9000	9591.9	9698.5	9805.0	9911.6	10018.2	10124.8	10231.3	10337.9	10444.5	10551.								
11000	10000	10657.7	10764.2	10870.8	10977.4	11084.0	11190.5	11297.1	11403.7	11510.3	11616.								
12000		11					9	1											
13000		Į I					i .	1			1								
14000		<b>{</b>							l										
17050			1		Į.					}									
17050	15000	15086 5	16009 1	16100 6	16306.2	16.119.8	16519.1	16625 9	16732 5	16839.1	169.15								
17000		1			1		1												
19183.8   19290.4   19396.9   19503.5   19610.1   19716.7   19823.2   19929.8   20036.4   20143   20400   20349.5   20356.1   20462.7   20569.3   20675.8   20782.4   20889.0   20995.6   21102.2   21208   21000   22381.1   22487.7   22594.2   22700.8   22807.4   22914.0   23020.5   23127.1   23233.7   23340   22000   23446.8   23553.4   23660.0   23766.6   23873.1   23979.7   24086.3   24192.9   24299.5   244000   25578.4   25684.9   25791.5   25898.1   26004.7   26111.3   26217.8   26324.4   26431.0   26537   266000   27709.9   27816.5   27923.1   28029.6   28136.2   28242.8   28349.4   28455.9   28562.5   28669.2   27000   28775.7   28882.2   28988.8   29095.4   29202.0   29308.5   29415.1   29521.7   29628.3   29734   29202.0   29308.5   29415.1   29521.7   29628.3   29436.1   29436.1   29436.1   29436.1   29436.		1			1														
19000   20249.5   20356.1   20462.7   20569.3   20675.8   20782.4   20889.0   20995.6   21102.2   21208				1			§		1										
21000							1		i .										
21000	20000	01915 9	21 (21 0	91599 5	91695 A	21741 6	018 (8 9	220218	20161 2	22167 0	99974								
22000		[]	1	1			1												
23000		ll .	1				1			1									
24000   25578.4   25684.9   25791.5   25898.1   26004.7   26111.3   26217.8   26324.4   26431.0   26537   25000   26644.1   26750.7   26857.3   26963.9   27070.4   27177.0   27283.6   27390.2   27496.7   27603   26000   27709.9   27816.5   27923.1   28029.6   28136.2   28242.8   28349.4   28455.9   28562.5   28669   27000   28775.7   28882.2   28988.8   29095.4   29202.0   29308.5   29415.1   29521.7   29628.3   29734      Tens.		11	į.		1	1				l .									
26000   27709.9   27816.5   27923.1   28029.6   28136.2   28242.8   28349.4   28455.9   28562.5   28669   27000   28775.7   28882.2   28988.8   29095.4   29202.0   29308.5   29415.1   29521.7   29628.3   29734   29			1		l .														
26000   27709.9   27816.5   27923.1   28029.6   28136.2   28242.8   28349.4   28455.9   28562.5   28669   27000   28775.7   28882.2   28988.8   29095.4   29202.0   29308.5   29415.1   29521.7   29628.3   29734   29	25000	200441	00000 0	0.00== 0	20000	0000	02122 0	0#000 C	27200 2	22 100 2	0=000								
27000         28775.7         28882.2         28988.8         29095.4         29202.0         29308.5         29415.1         29521.7         29628.3         29734           Units.           Units.           Eng. feet.          colspan="8" td=""><td></td><td></td><td></td><td></td><td>1</td><td>1</td><td></td><td></td><td></td><td></td><td></td></th>	<td></td> <td></td> <td></td> <td></td> <td>1</td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td>												1	1					
Tens.    Description																			
Co.         1.         2.         3.         4.         5.         6.         7.         8.         9.           0         0.000         1.066         2.132         3.197         4.263         5.329         6.395         7.460         8.526         9.5           10         10.658         11.723         12.789         13.855         14.921         15.986         17.052         18.118         19.184         20.22           20         21.315         22.381         23.447         24.513         25.578         26.644         27.710         28.776         29.841         30.99           30         31.973         33.039         34.104         35.170         36.236         37.302         38.368         39.433         40.499         41.56           40         42.631         43.696         44.762         45.828         46.894         47.959         49.025         50.091         51.157         52.23           50         53.288         54.354         55.420         56.486         57.551         58.617         59.683         60.749         61.814         62.88           60         63.946         65.012         66.077         67.143         68.209         69.275<	27000	1 20110.1	20002.2	29900.0	25055.4			23413.1	20021.1	2002010	23104								
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Tens.					Un	uts.				1								
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.	1.	2.	3.	4.	5.	6.	7.	8.	9.								
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					_				-	-	Eng fee								
20     21.315     22.381     23.447     24.513     25.578     26.644     27.710     28.776     29.841     30.90       30     31.973     33.039     34.104     35.170     36.236     37.302     38.368     39.433     40.499     41.56       40     42.631     43.696     44.762     45.828     46.894     47.959     49.025     50.091     51.157     52.23       50     53.288     54.354     55.420     56.486     57.551     58.617     59.683     60.749     61.814     62.88       60     63.946     65.012     66.077     67.143     68.209     69.275     70.341     71.406     72.472     73.53       70     74.604     75.669     76.735     77.801     78.867     79.932     80.998     82.064     83.130     84.16       80     85.261     86.327     87.393     88.459     89.524     90.590     91.656     92.722     93.787     94.83		11	ì				1												
30     31.973     33.039     34.104     35.170     36.236     37.302     38.368     39.433     40.499     41.56       40     42.631     43.696     44.762     45.828     46.894     47.959     49.025     50.091     51.157     52.23       50     53.288     54.354     55.420     56.486     57.551     58.617     59.683     60.749     61.814     62.88       60     63.946     65.012     66.077     67.143     68.209     69.275     70.341     71.406     72.472     73.53       70     74.604     75.669     76.735     77.801     78.867     79.932     80.998     82.064     83.130     84.19       80     85.261     86.327     87.393     88.459     89.524     90.590     91.656     92.722     93.787     94.83			1							1									
40     42.631     43.696     44.762     45.828     46.894     47.959     49.025     50.091     51.157     52.23       50     53.288     54.354     55.420     56.486     57.551     58.617     59.683     60.749     61.814     62.88       60     63.946     65.012     66.077     67.143     68.209     69.275     70.341     71.406     72.472     73.53       70     74.604     75.669     76.735     77.801     78.867     79.932     80.998     82.064     83.130     84.19       80     85.261     86.327     87.393     88.459     89.524     90.590     91.656     92.722     93.787     94.83		11	l .			f	ı												
50     53.288     54.354     55.420     56.486     57.551     58.617     59.683     60.749     61.814     62.88       60     63.946     65.012     66.077     67.143     68.209     69.275     70.341     71.406     72.472     73.53       70     74.604     75.669     76.735     77.801     78.867     79.932     80.998     82.064     83.130     84.19       80     85.261     86.327     87.393     88.459     89.524     90.590     91.656     92.722     93.787     94.83						1	1				1								
60     63.946     65.012     66.077     67.143     68.209     69.275     70.341     71.406     72.472     73.53       70     74.604     75.669     76.735     77.801     78.867     79.932     80.998     82.064     83.130     84.19       80     85.261     86.327     87.393     88.459     89.524     90.590     91.656     92.722     93.787     94.83	40	42.631	43.696	44.762	45.828	46.891	47.959	49.025	50.091	91.157	52.22								
70   74.604   75.669   76.735   77.801   78.867   79.932   80.998   82.064   83.130   84.15   85.261   86.327   87.393   83.459   89.524   90.590   91.656   92.722   93.787   94.83	50	53.288	54.354	55.420	56.486	57.551	58.617	59.683	i e		62.88								
80   85.261   86.327   87.393   88.459   89.524   90.590   91.656   92.722   93.787   94.83	60	63.946	65.012	66.077	67.143	68.209	69.275	70.341	71.406	72.472	73.53								
		{	75.669	76.735		78.867	79.932	80.998	82.064	83.130	84.19								
	80	85.261	86.327	87.393	83.459	89.524	90.590	91.656	92.722	93.787	94.85								
	90	95.919	96.985	98.050		100.182	101.248	102.313	103.379	104.445	105.51								

1 French Foot = 1.0657034 American Foot.

French Feet.					Hun	dreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Am. Feet	Am.Feet	Am. Feet.	1	1	Am. Feet.	Am. Feet.	Am. Feet.	1	Am.Feet
0	0.0	106.6		319.7			639.4	746.0	852.6	959.1
1000	1065.7		1	1	1	1	1	1811.7		1
2000	2131.4	2238.0		1		2664.3	2770.8	2877.4		
3000	3197.1	3303.7	1			3730.0	3836.5		4049.7	4156.2
4000	4262.8	4369.4	4476.0	4582.5	4689.1	4795.7	4902.2	5008.8	5115.4	5221.9
5000	5328.5	5435.1	5541.7	5648.2	5754.8	5861.4	5967.9	6074.5	6181.1	6287.7
6000	6394.2	6500.8	6607.4	6713.9	6820.5	6927.1	7033.6	7140.2	7246.8	7353.4
7000	7459.9	7566.5	7673.1	7779.6	7886.2	7992.8	8099.3	8205.9	8312.5	8419.
8000	8525.6	8632.2	8738.8	8845.3	8951.9	9058.5	9165.1	9271.6	9378.2	9484.8
9000	9591.3	9697.9	9804.5	9911.0	10017.6	10124.2	10230.8	10337.3	10443.9	10550.5
10000	10657.0	10763.6	10870.2	10976.7	11083.3	11189.9	11296.5	11403.0	11509.6	11616.5
11000	11722.7	11829.3	11935.9	1	12149.0		12362.2		12575.3	12681.
12000	12788.4	12895.0	13001.6	13108.2	13214.7	13321.3	13427.9	13534.4		
13000	13854.1	13960.7	14067.3	14173.9		14387.0	14493.6	J	14706.7	
14000	14919.9	15026.4	1	15239.6		15452.7	15559.3	15665.8		
15000	15985.6	16092.1	  16198.7	16305.3	16411.8	16518.4	16625.0	16731.5	16838.1	16944.
16000	17051.3	17157.8	17264.4	17371.0	17477.5	17584.1	17690.7	17797.2	17903.8	18010.
17000	18117.0	18223.5	18330.1	18436.7	18543.2	18649.8	18756.4	18863.0	18969.5	19076.
18000	19182.7	19289.2	19395.8	19502.4	19608.9	19715.5	19822.1	19928.7	20035.2	20141.8
19000	20248.4	20354.9	20461.5	20568.1	20674.6	20781.2	20887.8	20994.4	21100.9	21207.
20000	21314.1	21420.6	21527.2	21633.8	21740.4	21846.9	21953.5	22060.1	22166.6	22273.5
21000	22379.S	22486.3	22592.9	22699.5	22806.1	22912.6	23019.2	23125.8	23232.3	23338.
22000	23445.5	23552.0	23658.6	23765.2	23871.8	23978.3	24084.9	24191.5	24298.0	24404.0
23000	24511.2	24617.8	24724.3	24830.9		25044.0		25257.2	25363.7	25470.
24000		25683.5			26003.2					
25000	26642.6	26749.2	26855.7	26962.3	27068.9	27175.4	27282.0	27388.6	27495.2	27601.
26000	27708.3	27814.9	27921.4	28028.0	28134.6	28241.1	28347.7	28454.3	28560.9	28667.
27000	28774.0	28880.6	28987.1	29093.7	29200.3	29306.8	29413.4	29520.0	29626.6	29733.
28000	29839.7	29946.3	30052.8	30159.4	30266.0	30372.6	30479.1	30585.7	30692.3	30799.8
					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Am. Feet.		Am Feet	Am.Feet.	Am Feet	Am Feet.	Am.Feet.	Am Feet.	Am Feet	Am. Feet
0	0.00	1.07	2.13	3.20	4.26	5.33	6.39	7.46	8.53	9.59
10	10.66	11.72	12.79	13.85	14.92	15.99	17.05	18.12	19.18	20.25
20	21.31	22.38	23.45	24.51	25.58	26.64	27.71	28.77	29.84	30.91
30	31.97	33.04	34.10	35.17	36.23	37.30	38.37	39.43	40.50	41.56
40	42.63	43.69	44.76	45.83	46.89	47.96	49.02	50.09	51.15	52.22
50	53.29	54.35	55.42	56.48	57.55	58.61	59.68	60.75	61.81	62.88
60	63.94	65.01	66.07	67.14	68.21	69.27	70.34	71.40	72.47	73.53
- 11	74.60	75.66	76.73	77.80	78.86	79.93	80.99	82.06	83.12	84.19
76										
76 80	85.26	86.32	87.39	88.45	89.52	90.58	91.65	92.72	93.78	94.85

## ENGLISH YARDS AND FEET

### INTO DIFFERENT MEASURES OF LENGTH.

XIV. CONVERSION OF ENGLISH YARDS INTO FRENCH TOISES.

1 English Yard = 0.4691465 Toise.

English Yards					Hund	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.
0	0.00	46.91	93.83	140.74	187.66	234.57	281.49	328.40	375.32	422.23
1000	469.15	516.06	562.98	609.89	656.80	703.72	750.63	797.55	844.46	891.38
2000	938.29	985.21	1032-12	1079.04	1125.95	1172.87	1219.78	1266.70	1313.61	1360.52
3000	1407.44	1454.35	1501.27	1548.18	1595.10	1642.01	1688.93	1735.84	1782.76	1829.67
4000	1876.59	1923.50	1970.41	2017.33	2064.24	2111.16	2158.07	2204.99	2251.90	2298.82
5000	2345.73	2392.65	2439.56	2486.48	2533.39	2580.31	2627.22	2674.13	2721.05	2767.96
6000	2814.88	2861.79	2908.71	2955.62	3002.54	3049.45	3096.37	3143.28	3190.20	3237.11
7000	3284.02	3330.94	3377.85	3424.77	3471.68	3518.60	3565.51	3612.43	3659.34	3706.26
8000	3753.17	3800.09	3847.00	3893.92	3940.83	3987.74	4034.66	4081.57	4128.49	4175.40
9000	4222.32	4269.23	4316.15	4363.06	4409.98	4456.89	4503.81	4550.72	4597.63	4644.55

#### XV. CONVERSION OF ENGLISH YARDS INTO METRES.

1 English Yard = 0.91438348 Metre.

English Yards,					Huno	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	91.44	182.88	274.32	365.75	457.19	548.63	640.07	731.51	822.95
1000	914.38	1005.82	1097.26	1188.70	1280.14	1371.58	1463.01	1554.45	1645.89	1737.33
2000	1828.77	1920.21	2011.64	2103.08	2194.52	2285.96	2377.40	2468.84	2560.27	2651.71
3000	2743.15	2834.59	2926.03	3017.47	3108.90	3200.34	3291.78	3383.22	3474.66	3566.10
4000	3657.53	3748.97	3840.41	3931.85	4023.29	4114.73	4206.16	4297.60	4389.04	4480.48
5000	4571.92	4663.36	4754.79	4846.23	4937.67	5029.11	5120.55	5211.99	5303.42	5394.86
6000	5486.30	5577.74	5669.18	5760.62	5852.05	5943.49	6034.93	6126.37	6217.81	6309.25
7000	6400.68	6492.12	6583.56	6675.00	6766.44	6857.88	6949.31	7040.75	7132.19	7223.63
8000	7315.07	7406.51	7497.94	7589.38	7680.82	7772.26	7863.70	7955.14	8046.57	8138.01
9000	8229.45	8320.89	8412.33	8503.77	8595.20	8686.64	8778.08	8869.52	S960.96	9052.40

### XVI. CONVERSION OF ENGLISH FEET INTO METRES.

 $1 \; English \; Foot = 0.30479449 \; Metre.$ 

English					Hund	reds.				
Feet. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0		30.4794	60.9589		121.918	152.397	182.877		243.836	
1000	1		365.763		426.712			518.151		
2000	1	640.068	670.548	701.027	731.507	761.986	792.466	822.945		883.90
3000 4000	1	944.863 1249.66		1310.62	1036.30 1341.10	1066.78 1371.58	1097.26 1402.05	1	1158.22 1463.01	
5000	1523.97	1554.45	1584.93	1615.41	1645.89	1676.37	1706.85	1737.33	1767.81	1798.5
6000	1828.77	1859.25	1889.73	1920.21	1950.68	1981.16	2011.64	2042.12	2072.60	2103.0
7000	2133.56	2164.04	2194.52	2225.00	2255.48	2285.96	2316.44	2346.92	2377.40	2407.8
8000	2438.36	2468.84	2499.31	2529.79	2560.27	2590.75	2621.23	2651.71	2682.19	2712.0
9000	2743.15	2773.63	2804.11	2834.59	2865.07	2895.55	2926.03	2956.51	2986.99	3017.
10000	3047.94	3078.42	3108.90	3139.38	3169.86	3200.34	3230.82	3261.30	3291.78	3322.
11000	3352.74	3383.22	3413.70	3444.18	3474.66	3505.14	3535.62	3566.10	3596.57	3627.
12000	3657.53	3688.01	3718.49	3748.97	3779.45	3809.93	3840.41	3870.89	3901.37	3931.
13000	3962.33	3992.81	4023.29	4053.77	4084.25	4114.73	4145.21	4175.68	4206.16	4236.
14000	4267.12	4297.60	4228.08	4358.56	4389.04	4419.52	4450.00	4480.48	4510.96	4541.
15000	4571.92	4602.40	4632.88	4663.36	4693.84	4724.31	4754.79	4785.27	4815.75	4846.
16000	4876.71	4907.19	4937.67	4968.15	4998.63	5029.11	5059.59	5090.07	5120.55	5151.
17000	5181.51	5211.99	5242.47	5272.94	5303.42		(	5394.86	5425.34	5455.
18000	1			5577.74				5699.66		ļ
19000		5821.57		5882.53	5913.01	5943.49	5973.97		6034.93	
20000	l I	6126.37		6187.33			6278.77	1	6339.73	
21000 22000		6431.16 6735.96		6492.12 6796.92	6522.60 $6827.40$	6553.08 6857.88	1	6614.04 6918.83		
23000	7010 27	7040.75	7071.23	7101.71	7132.19	7162.67	7193.15	7223.63	7254.11	7284.
24000		7345.55		7406.51				7528.42		
25000	1	7650.34		7711.30				7833.22		
26000	ll.	7955.14		\$	8046.57			8138.01	1	
27000	8229.45	8259.93	8290.41	8320.89	8351.37	8381.85	8412.33	8442.81	8473.29	8503.
28000	8534.25	8564.73	8595.20	8625.68	8656.16	8686.64	8717.12	8747.60	8778.08	8808.
					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
0		0.30479		0.91438		1.52397		1	2.43836	
10	3.04794	3.35274	3.65753	3.96233	4.26712	4.57192	4.87671	5.18151	5.48630	5.791
20					7.31507					
30					10.3630					
40	12.1918	12.4966	12.8014	13.1062	13.4110	13.7158	14.0205	14.3253	14.6301	14.93
50					16.4589					
60					19.5068					
70					22.5548					
80					25.6027					
90	27.4315	27.7363	28.0411	28.3459	28.6507	28.9555	29.2603	29.5651	29.8699	30.17

D

1 English Foot = 0.9382929 Paris Foot.

English Feet.					Hund	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.				Par. Feet	Par. Feet.
0	0.000	93.8	187.7	281.5	375.3	469.1	563.0	656.8	750.6	844.5
1000	938.3	1032.1	1126.0	1219.8	1313.6	1407.4		1	1688.9	1782.8
2000	1876.6	1970.4	2064.2	2158.1	2251.9	2345.7	2439.6		2627.2	2721.0
3000	2814.9	2908.7	3002.5	3096.4	3190.2		1		3565.5	3659.3
4000	3753.2	3847.0	3940.8	4034.7	4128.5	4222.3	4316.1	4410.0	4503.8	4597.6
5000	4691.5	4785.3	4879.1	4973.0	5066.8	5160.6	5254.4	5348.3	5442.1	5535.9
6000	5629.8	5723.6	5817.4	5911.2	6005.1	6098.9	6192.7	6286.6	6380.4	6474.2
7000	6568.0	6661.9	6755.7	6849.5	6943.4	7037.2	7131.0	7224.9	7318.7	7412.5
8000	7506.3	7600.2	7694.0	7787.8	7881.7	7975.5	8069.3	8163.1	8257.0	8350.8
9000	8444.6	8538.5	8632.3	8726.1	8820.0	8913.8	9007.6	9101.4	9195.3	9289.1
10000	9382.9	9476.8	9570.6	9664.4	9758.2		9945.9			10227.4
11000	10321.2	10415.0	10508.9	10602.7	1	10790.4		10978.0		1
12000	11259.5		11447.2	11541.0	11634.8	11728.7	11822.5	11916.3	12010.1	12104.0
13000	12197.8	12291.6	12385.5	12479.3	12573.1	12667.0	12760.8	12854.6	12948.4	13042.3
14000	13136.1	13229.9	13323.8	13417.6	13511.4	13605.2	13699.1	13792.9	13886.7	13980.6
15000	14074.4	14168.2	14262.0	14355.9	14449.7	14543.5	14637.4	14731.2	14825.0	14918.9
16000	15012.7	15106.5	15200.3	15294.2	15388.0	15481.8	15575.7	15669.5	15763.3	15857.1
17000	15951.0	16044.8	16138.6		16326.3	1	16514.0		16701.6	
18000	16889.3		17076.9		17264.6	17358.4	17452.2	17546.1	17639.9	17733.7
19000		17921.4	18015.2			18296.7	1		18578.2	
20000	18765.9	18859.7	18953.5	19047.3	19141.2	19235.0	19328.8	19422.7	19516.5	19610.3
21000	19704.1		19891.8	19985.6	20079.5	20173.3	20267.1	20361.0	20454.8	20548.6
22000	20642.4	20736.3	20830.1	20923.9	21017.8	21111.6	21205.4	21299.2	21393.1	21486.9
23000	21580.7	21674.6	21768.4	21862.2	21956.0	22049.9	22143.7	22237.5	22331.4	22425.2
24000	22519.0	22612.9	22706.7	22800.5	22894.3	22988.2	23082.0	23175.8	23269.7	23363.5
. 25000	23457.3	23551.1	23645.0	23738.8	23832.6	23926.5	24020.3	24114.1	24208.0	24301.8
26000	24395.6	24489.4	24583.3	24677.1	24770.9	24864.8	24958.6	25052.4	25146.2	25240.1
27000	25333.9	25427.7	25521.6	25615.4	25709.2	25803.1	25896.9	25990.7	26084.5	26178.4
28000	26272.2	26366.0	26459.9	26553. <b>7</b>	26647.5	26741.3	26835.2	26929.0	27022.8	27116.7
					Un	its.				
Tens.	· O.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par, Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par, Feet.	Par. Feet.	Par, Feet.	Par. Feet.
0	0.00	0.94	1.88	2.81	3.75	4.69	5.63	6.57	7.51	8.44
10	9.38	10.32	11.26	12.20	13.14	14.07	15.01	15.95	16.89	17.83
20	18.77	19.70	20.64	21.58	22.52	23.46	24.40	25.33	26.27	27.21
30	28.15	29.09	30.03	30.96	31.90	32.84	33.78	34.72	35.66	36.59
40	37.53	38.47	39.41	40.35	41.28	42.22	43.16	44.10	45.04	45.98
50	46.91	47.85	48.79	49.73	50.67	51.61	52.54	53.48	54.42	55.36
60	56.30	57.24	58.17	59.11	60.05	60.99	61.93	62.87	63.80	64.74
70	65.68	66.62	67.56	68.50	69.43	70.37	71.31	72.25	73.19	74.13
80	75.06	76.00	76.94	77.88	78.82	79.75	80.69	81.63	82.57	83.51
90	84.45	85.38	86.32	87.26	88.20	89.14	90.08	91.01	91.95	92.89

135

D

1 English Foot = 0.99994197 American Foot.

					Hund	lreds.				
Eng. Feet. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Am Feet	Am. Feet.	Am. Feet.	Am Feet.	Am.Feet.	Am Feet	Am Feet.	Am.Feet.	Am Feet.	Am. Feet.
0	0.00	99.99	199.99	299.98	399.98	499.97	599.97	699.96	799.95	899.95
1000	999.94	1099.94	1199.93	1299.92	1399.92	1499.91	1599.91	1699.90	1799.90	1899.89
2000	1999.88	2099.88	2199.87	2299.87	2399.86	2499.85	2599.85	2699.84	2799.84	2899.83
3000	2999.83	3099.82	3199.81	3299.81	3399.80	3499.80	3599.79	3699.79	3799.78	3899.77
4000	3999.77	4099.76	4199.76	4299.75	4399.74	4499.74	4599.73	4699.73	4799.72	4899.72
5000	4000 71	5000 70	5100 70	5200 CO	5399.69	5 100 GS	5500 69	5699.67	5700 CC	5000 CC
6000	1				6399.63			6699.61		
7000					7399.57			7699.55		
8000	ì	8099.53						8699.50		
9000					9399.45					
0000	0000140	5055.41	3133.41	3233.40	3933.43	040040	3033.44		0100.40	0000140
10000	9999.42	10099.4	10199.4	10299.4	10399.4	10499.4	10599.4	10699.4	10799.4	10899.4
11000	10999.4	11099.4	11199.4	11299.3	11399.3	11499.3	11599.3	11699.3	11799.3	11899.3
12000	11999.3	12099.3	12199.3	12299.3	12399.3	12499.3	12599.3	12699.3	12799.3	12899.2
13000	12999.2	13099.2	13199.2	13299.2	13399.2	13499.2	13599.2	13699.2	13799.2	13899.2
14000	13999.2	14099.2	14199.2	14299.2	14399.2	14499.2	14599.2	14699.1	14799.1	14899.1
15000	14999.1	15099.1	15199.1	15299.1	15399.1	15499.1	15599.1	15699.1	15799.1	15899.1

The following Table of Differences between English and American Feet, for every hundred feet, will make it easy to convert English into American Feet, or American into English Feet, by adding to, or subtracting from, the number of feet to be converted, which is contained in the first column, the numbers found in the other columns.

XIX. DIFFERENCES BETWEEN ENGLISH AND AMERICAN FEET.

To obtain English Feet add. To obtain American Feet subtract.

10000 American Feet = 10000.5803 English Feet.

Number of Feet.			Hundreds	ı.		Number of Feet.			Hundreds		
Thou- sands.	0.	200.	400.	600.	800.	Thou- sands.	0.	200.	400.	600.	800.
	Diff feet	Diff.feet	Diff feet.	Diff.feet.	Diff feet		Diff.fcet.	Diff.feet	Diff.feet	Diff feet.	Diff.feet
0	±0.000	+0.012	+0.023	±0.035	+0.046	15000	±0.870	±0.882	±0.894	±0.905	±0.917
1000	0.058	0.070	0.082	0.093	0.105	16000	0.928	0.940	0.952	0.963	0.975
2000	0.116	0.128	0.139	0.151	0.162	17000	0.987	0.998	1.010	1.021	1.033
3000	0.174	0.186	0.197	0.209	0.221	18000	1.045	1.056	1.068	1.079	1.091
4000	0.232	0.244	0.255	0.267	0.279	19000	1.103	1.114	1.126	1.137	1.149
5000	0.290	0.302	0.313	0.325	0.337	20000	1.161	1.172	1.184	1.195	1.207
6000	0.348	0.360	0.371	0.383	0.395	21000	1.219	1.230	1.242	1.253	1.265
7000	0.406	0.418	0.429	0.441	0.453	22000	1.277	1.288	1.300	1.311	1.323
8000	0.464	0.476	0.487	0.499	0.511	23000	1.335	1.346	1.358	1.370	1.381
9000	0.522	0.534	0.546	0.557	0.569	24000	1.393	1.404	1.416	1.428	1.439
10000	0.580	0.592	0.604	0.615	0.627	25000	1.451	1.462	1.474	1.486	1.497
11000	0.638	0.650	0.662	0.673	0.685	26000	1.509	1.520	1.532	1.544	1.555
12000	0.696	0.708	0.720	0.731	0.743	27000	1.567	1.578	1.590	1.602	1.613
13000	0.754	0.766	0.778	0.789	0.801	28000	1.625	1.636	1.648	1.660	1.671
14000	0.812	0.824	0.836	0.847	0.859	29000	1.683	1.694	1.606	1.718	1.729

## AMERICAN YARDS AND FEET

#### INTO DIFFERENT MEASURES OF LENGTH

#### XX. CONVERSION OF AMERICAN YARDS INTO FRENCH TOISES.

1 American Yard = 0.4691737 Toise.

American Yards					Hune	lreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Torses.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	"oises.
0	0.20	45.92	93.83	140.75	187.67	234.59	281.50	328.42	375.34	422.26
1000	469.17	516.09	563.01	609.93	656.84	703.76	750.68	797.60	844.51	891.43
2000	938.35	985.26	1032-18	1079.10	1126.02	1172.93	1219.85	1266.77	1313.69	1360.60
3000	1407.52	1454.44	1501.36	1548.27	1595.19	1642.11	1689.02	1735.94	1782.86	1829.78
4000	1876.69	1923.61	1970.53	2017.45	2064.36	2111.28	2158.20	2205.12	2252.03	2298.95
5000	2345.87	2392.79	2439.70	2486.62	2533.54	2580.45	2627.37	2674.29	2721.21	2768.12
6000	2815.04	2861.96	2908.88	2955.79	3002.71	3049.63	3096.55	3143.46	3190.38	3237.30
7000	3284.22	3331.13	3378.05	3424.97	3471.88	3518.80	3565.72	3612.64	3659.55	3706.47
8000	3753.39	3800.31	3847.22	3894.14	3941.06	3987.98	4034.89	4081.81	4128.73	4175.65
9000	4222.56	4269.48	4316.40	4363.31	4410.23	4457.15	4504.07	4550.98	4597.90	4644.82

#### XXI. CONVERSION OF AMERICAN YARDS INTO METRES.

1 American Yard = 0.91443655 Metre.

American Yards,					Hune	ireds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	91.44	182.89	274.33	365.77	457.22	548.66	640.11	731.55	822.99
1000	914.44	1005.88	1097.32	1188.77	1280.21	1371.65	1463.10	1554.54	1645.99	1737.43
2000	1828.87	1920.32	2011.76	2103.20	2194.65	2286.09	2377.54	2468.98	2560.42	2651.87
3000	2743.31	2834.75	2926.20	3017.64	3109.08	3200.53	3291.97	3383.42	3474.86	3566.30
4000	3657.75	3749.19	3840.63	3932.08	4023.52	4114.96	4206.41	4297.85	4389.30	4480.74
5000	1579 18	4663.63	1755.07	1846.51	1937.96	5029.40	5120.84	5212.29	5303.73	5395.18
6000		5578.06								
7000		6492.50								
8000		7406.94								
9000	8229 93	-								

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#### XXII. CONVERSION OF AMERICAN FEET INTO METRES.

1 American Foot = 0.30481218 Metre.

Amer. Feet.					Huno	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
1000	0.00	30.48	60.96	1		152.41	1			
2000	304.81 609.62	335.29 640.11	365.77 670.59			457.22 762.03	1	1		1
3000	914.44	944.92			1036.36		192.31			
4000	1219.25	1249.73				1371.65		1432.62		
5000	1524.06	1554.54	1585.02	1615.50	1645.99	1676.47	1706.95	1737.43	1767.91	1798.3
6000	1828.87	1859.35	1889.84	1910.32	1940.80	1971.28	2001.76	2032.24	2062.72	2093.2
7000	2123.69	2154.17	2184.65	2225.13	2255.61	2286.09	2316.57	2347.05	2377.54	2408.0
8000	2438.50	2468.98	2499.46	2529.94	2560.42	2590.90	2621.38	2651.87	2682.35	2712.8
9000	2743.31	2773.79	2804.27	2834.75	2865.23	2895.72	2926.20	2956.68	2987.16	3017.6
10000			ž.	3139.57	3170.05	3200.53	3231.01	3261.49	3291.97	3322.4
11000	3352.93	3383.42	3413.90	3444.38	3474.86	3505.34	3535.82	3566.30	3596.78	3627.2
12000		3688.23	3718.71	3749.19	3779.67	3810.15				3932.0
13000	3962.56	3993.04	4023.52	4054.00	4084.48					4236.8
14000	4267.37	4297.85	4328.33	4358.81	4389.30	4419.78	4450.26	4480.74	4511.22	4541.7
15000	4572.18	4602.66	4633.15	4663.63	4694.11	4724.59	4755.07	4785.55	4816.03	4846.5
16000				4968.44				5090.36	}	i
17000	1	5212.29	1	1	5303.73			5395.18	ŧ	
18000		5517.10	1	1	5608.54		5669.51	5699.99	5730.47	5760.9
19000	5791.43	5821.91	5852.39	5882.88	5913.36	5943.84	5974.32	6004.80	6035.28	6065.7
20000	6096.24	6126.72	6157.21	6187.69	6218.17	6248.65	6279.13	6309.61	6340.09	6370.5
21000	6401.06	6431.54	6462.02	6492.50	6522.98	6553.46	6583.94	6614.42	6644.91	6675.3
22000	6705.87	6736.35	6766.83	6797.31	6827.79	6858.27	6888.76	6919.24	6949.72	6980.2
23000	7010.68	7041.16	7071.64	7102.12	7132.61	7163.09	7193.57	7224.05	7254.53	7285.0
24000	7315.49	7345.97	7376.45	7406.94	7437.42	7467.90	7498.38	7528.86	7559.34	7589.8
25000	7620.30	7650.79	7681.27	7711.75	7742.23	7772.71	7803.19	7833.67	7864.15	7894.6
26000	7925.12	7955.60	7986.08	8016.56	8047.04	8077.52	8108.00	8138.49	8168.97	8199.4
27000	8229.93	8260.41	8290.89	8321.37	8351.85	8382.33	8412.82	8443.30	8473.78	8504.2
28000	8534.74	8565.22	8595.70	8626.18	8656.67	8687.15	8717.63	8748.11	8778.59	8809.0
Tens.				,	Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.0000	0.3048	0.6096	0.9144	1.2192	1.5241	1.8289	2.1337	2.4385	2.743
10	3.0481	3.3529	3.6577	3.9626	4.2674	4.5722	4.8770	5.1818	5.4866	5.791
20	6.0962	6.4011	6.7059	7.0107			7.9251			
30 40						10.6684 13.7165				
-										
50 60						16.7647				
UU	18.2887					19.7128				
l i	01 0000	07 8 42 0	01 0 . 0 . 1	00 00	00 8800	00 0000	00 10-0	00 4=0=1	OD MMF.	0 4 000
70 80	21.2369					$\frac{22.8609}{25.9090}$				

1 American Foot = 0.93834737 Paris Foot.

Amer. Feet.				<del></del>	Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. Feet.			Par. Feet.	1	Par.Feet.	Par. Feet.			Par. Feet.
0	0.0	93.8	187.7	281.5	375.3	469.2	563.0	656.8	750.7	844.5
1000	938.3		1126.0			ì	1501.4	1595.2	1	1782.9
2000	1876.7	1970.5	2064.4	2158.2	2252.0	2345.9	2439.7	2533.5	1	2721.2
3000	2815.0	2908.9	3002.7	3096.5	3190.4	3284.2	3378.1	3471.9		3659.6
4000	3753.4	3847.2	3941.1	4034.9	4128.7	4222.6	4316.4	4410.2	4504.1	4597.9
5000	4691.7	4785.6	4879.4	4973.2	5067.1	5160.9	5254.7	5348.6	5442.4	5536.2
6000	5630.1	5723.9	5817.8	5911.6	6005.4	6099.3		6286.9		6474.6
7000	6568.4		6756.1	6849.9		7037.6	7131.4			7412.9
8000	7506.8	7600.6	7694.4	7788.3	7882.1	7976.0	8069.8	8163.6	8257.5	8351.3
9000	8445.1	8539.0	8632.8	8726.6	8820.5	8914.3	9008.1	9102.0	9195.8	9289.6
10000	0000 =	0.488 0	0577.1	0.005.0	02500	0070.0	0046 =	700/0.0	101040	10000 0
10000	9383.5		1		1	9852.6				11166.3
11000 12000						10791.0 11729.3	}			
13000	1	12292.3	•	]	t .	12667.7			1	
14000	1	13230.7		ì		13606.0		1	13887.5	13981.4
14000	15150.5	1020011	10024.0	10410.4	10012.2	13000.0	1000000	10100.1	10001.0	10001.1
15000	14075.2	14169.0	14262.9	14356.7	14450.5	14544.4	14638.2	14732.1	14825.9	14919.7
16000	15013.6	15107.4	15201.2	15295.1	15388.9	15482.7	15576.6	15670.4	15764.2	15858.1
17000	15951.9	16045.7	16139.6	16233.4	16327.2	16421.1	16514.9	16608.7	16702.6	16796.4
18000	16890.3	16984.1	17077.9	17171.8	17265.6	17359.4	17453.3	17547.1	17640.9	17734.8
19000	17828.6	17922.4	18016.3	18110.1	18203.9	18297.8	18391.6	18485.4	18579.3	18673.1
00000	10766.0	10000 0	1005 + 6	10040 4	101 (0.0	10000 1	10000 0	10.400.0	10517 0	10611 5
20000 21000	Į.			1		19236.1 20174.5				
22000	1	1				21112.8				
23000			1			22051.2				
24000						22989.5				
24000	2202010	22011.2	2210,010	2200110	22000.1	22000.0	2000000	2011112	20211.0	2000110
25000	23458.7	23552.5	23646.4	23740.2	23834.0	23927.9	24021.7	24115.5	24209.4	24303.2
26000	24397.0	24490.9	24584.7	24678.5	24772.4	24866.2	24960.0	25053.9	25147.7	25241.5
27000	25335.4	25429.2	25523.0	25616.9	25710.7	25804.5	25898.4	25992.2	26086.1	26179.9
<b>2</b> 8000	26273.7	26367.6	26461.4	26555.2	26649.1	26742.9	26836.7	26930.6	27024.4	27118.2
					Un	its.				
Tens.		•	0	9	4			) psy	e e	0
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par Feet.	Par. Feet.	Par.Feet.		Par.Feet.	Par Feet.	Par.Feet.	Par.Feet	Par Feet	Par.Feet
0	0.00	0.94	1.88	2.82	3.75	4.69	5.63	6.57	7.51	8.45
10	9.38	10.32	11.26	12.20	13.14	14.08	15.01	15.95	16.89	17.83
20	18.77	19.71	20.64	21.58	22.52	23.46	24.40	25.34	26.27	27.21
30 40	28.15 37.53	29.09 38.47	30.03 39.41	30.97 40.35	31.90 41.29	32.84 $42.23$	33.78 43.16	34.72 44.10	35.66 45.04	36.60 45.98
40	91.00	90.41	99.41	40.00	41.43	42.20	45.10	44.10	49.04	49.95
50	46.92	47.86	48.79	49.73	50.67	51.61	52.55	53.49	54.42	55.36
60	56.30	57.24	58.18	59.12	60.05	60.99	61.93	62.87	63.81	64.75
70	65.68	66.62	67.56	68.50	69.44	70.38	71.31	72.25	73.19	74.13
80	75.07	76.01	76.94	77.88	78.82	79.76	80.70	81.64	82.57	83.51
90	84.45	85.39	86.33	87.27	88.20	89.14	90.08	91.02	91.96	92.90

## KLAFTER AND FEET OF VIENNA

#### INTO DIFFERENT MEASURES OF LENGTH.

1 KLAFTER OF VIENNA = 6 FEET OF VIENNA = 0.9730317 Tolse DU PÉROU.

From this value are derived the equations used in computing the following tables.

XXIV. CONVERSION OF KLAFTER OF VIENNA INTO FRENCH TOISES.  $1 \; {\rm Klafter} = 0.9730317 \; {\rm Toise}.$ 

Klafter of Vienna.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.
0	0.00	97.30	194.61	291.91	389.21	486.52	583.82	681.12	778.43	875.73
1000	973.03	1070.33	1167.64	1264.94	1362.24	1459.55	1556.85	1654.15	1751.46	1848.76
2000	1946.06	2043.37	2140.67	2237.97	2335.28	2432.58	2529.88	2627.19	2724.49	2821.79
3000	2919.10	3016.40	3113.70	3211.00	3308.31	3405.61	3502.91	3600.22	3697.52	3794.82
4000	3892.13	3989.43	4086.73	4184.04	4281.34	4378.64	4475.95	4573.25	4670.55	4767.86
5000	4865.16	4962.46	5059.76	5157.07	5254.37	5351.67	5448.98	5546.28	5643.58	5740.89
Klafter.					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.
0	0.000	0.973	1.946	2.919	3.892	4.865	5.838	6.811	7.784	8.757
10	9.730	10.703	11.676	12.649	13.622	14.595	15.569	16.542	17.515	18.488
20	19.461	20.434	21.407	22.380	23.353	24.326	25.299	26.272	27.245	28.218
30	29.191	30.164	31.137	32.110	33.083	34.056	35.029	36.002	36.975	37.948
40	38.921	39.894	40.867	41.840	42.813	43.786	44.759	45.732	46.706	47.679
50	48.652	49.625	50.598	51.571	52.544	53.517	54.490	55.463	56.436	57.409
60	58.382	59.355	60.328	61.301	62.274	63.247	64.220	65.193	66.166	67.139
70	68.112	69.085	70.058	71.031	72.004	72.977	73.950	74.923	75.896	76.870
80	77.843	78.816	79.789	80.762	81.735	82.708	83.681	84.654	85.627	86.600
90	87.573	88.546	89.519	90.492	91.465	92.438	93.411	94.384	95.357	96.330

Klafter of Vienna.					Hune	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	.Metres.	Metres.	Metres.
0	0.00						1137.88			
1000	1	1	}		2655.06	2844.71	3034.36	3224.01	3413.65	3603.3
2000	3792.95	3982.60	4172.24	4361.89	4551.54	1	4930.83	!		
3000		1	6068.72				6827.31	4		
4000	7585.90	7775.54	7965.19	8154.84	8344.49	8534.13	8723.78	8913.43	9103.08	9292.7
Klafter.					Un	its.			•	
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.000	1.896	3.793	5.689	7.586	9.482	11.379	13.275	15.172	17.06
10	18.965	20.861	22.758	24.654	26.551	28.447	30.344	32.240	34.136	36.03
20	37.929	39.826	41.722	43.619	45.515	47.412	49.308	51.205	53.101	54.99
30	56.894	58.791	60.687	62.584	64.480	66.377	68.273	70.170		73.96
40	75.859	77.755	79.652	81.548	83.445	85.341	87.238	89.134	91.031	92.92
50	94.824	96.720	98.617	100.513	102.409	104.306	106.203	108.099	109.995	111.89
60	113.788	115.685	117.581	119.478	121.374	123.271	125.167	127.064	128.960	130.85
70	132.753	134.650	136.546	138.443	140.339	142.236	144.132	146.029	147.925	149.82
	II	159 614	155 511	157.407	159.304	161,200	163.097	164.993	166.890	168.78
80	151.718	199.014	1100.011	101.401						
90	170.683	172.579	174.476 F KLAF	176.372 TER OF	178.269 VIENN	180.165 A INTO	182.062 PARIS		1	
90 XXVI.	170.683	172.579	174.476 F KLAF	176.372 TER OF	178.269	180.165 A INTO	182.062 PARIS		1	-
90 XXVI.	170.683	172.579	174.476 F KLAF	176.372 TER OF	VIENN 002 Paris of	180.165 A INTO	182.062 PARIS		1	EET.
30 XXVI.	170.683 CONVER	172.579 SION O	F KLAF	TER OF = 5.83819	178.269 VIENN 002 Paris of Hund	A INTO r French F	PARIS eet.	700.	800.	900.
30 XXVI.	170.683 CONVER	172.579 sion o	174.476 F KLAF 1 Klafter	176.372 TER OF = 5.83819 300. Par. Feet.	VIENN 002 Paris of Hund 400. Par.Feet.	A INTO r French Flreds.  500. Par.Feet.	PARIS eet.	700.	SOO. Par.Feet.	900.
80 XXVI.  Klafter of Vienna. Thousands.	0. Par.Feet. 0.00	172.579 ssion o  100. Par.Feet. 583.82	F KLAF 1 Klafter 200. Par.Feet.	176.372 TER OF = 5.83819 300. Par. Feet. 1751.46	178.269 VIENN 002 Paris of Hund 400. Par.Feet. 2335.28	A INTO r French F dreds.  500. Par.Feet. 2919.10 8757.29	PARIS eet.  600. Par.Feet. 3502.91 9341.10	760. Par.Feet. 4086.73 9924.92	800. Par.Feet. 4670.55	900. Par.Feet 5254.3 11092.
90  XXVI.  Klafter of Vienna. Thousands.	0. Par.Feet. 0.00 5833.19 11676.4	172.579 asion o asion o Par.Feet. 583.82 6422.01 12260.2	174.476  F KLAF 1 Klafter  200.  Par.Feet. 1167.64 7005.S3. 12844.0	176.372  TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8	178.269 VIENN 002 Paris of Hund  400. Par.Feet. 2335.28 8173.47 14011.7	A INTO r French F dreds.  500. Par.Feet. 2919.10 8757.29	PARIS eet.  600.  Par.Feet. 3502.91	760. Par.Feet. 4086.73 9924.92	800. Par.Feet. 4670.55	900. Par.Feet 5254.3 11092.
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000	0.00 753 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	172.579 asion o asion	174.476  F KLAF  1 Klafter  200.  Par.Feet. 1167.64 7005.83 12844.0 18682.2	TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0	VIENN 02 Paris of Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8	A INTO r French F dreds.  500.  Par.Feet. 2919.10 8757.29 14595.5 20433.7	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5	760.  Par.Feet. 4086.73 9924.92 15763.1 21601.3	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1	900. Par.Feet 5254.3 11092. 16930. 22768.
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000	0.00 753 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	172.579 asion o asion	174.476  F KLAF  1 Klafter  200.  Par.Feet. 1167.64 7005.83 12844.0 18682.2	TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0	178.269 VIENN 002 Paris of Hund  400. Par.Feet. 2335.28 8173.47 14011.7	A INTO r French F dreds.  500.  Par.Feet. 2919.10 8757.29 14595.5 20433.7	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5	760.  Par.Feet. 4086.73 9924.92 15763.1 21601.3	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1	900. Par.Feet 5254.3 11092 16930.3 22768.3
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000 4000	0.00 753 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	172.579 asion o asion	174.476  F KLAF  1 Klafter  200.  Par.Feet. 1167.64 7005.83 12844.0 18682.2	TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0	VIENN 02 Paris of Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8	A INTO r French F lreds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5	760.  Par.Feet. 4086.73 9924.92 15763.1 21601.3	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1	900. Par.Feet 5254.3' 11092 16930 22768
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000	0.00 753 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	172.579 asion o asion	174.476  F KLAF  1 Klafter  200.  Par.Feet. 1167.64 7005.83 12844.0 18682.2	TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0	VIENN 1002 Paris of Hund 1400.  Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0	A INTO r French F lreds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5	760.  Par.Feet. 4086.73 9924.92 15763.1 21601.3	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1	900. Par.Feet 5254.3 11092 16930.3 22768.3
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000 4000  Klafter.	0.000 5838.19 11676.4 17514.6 23352.8	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	174.476  F KLAF 1 Klafter  200.  Par.Feet. 1167.64 7005.93. 12843.0 18682.2 24520.4	176.372 TER OF = 5.83810  300. Par.Feet. 1751.46 17589.65 13427.8 19266.0 25104.2	178.269 VIENN 002 Paris of Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni	180.165 A INTO r French F lreds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 tts.	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3	900. Par.Feet 5254.3 11092. 16930. 22768. 28607.
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000 4000  Klafter.	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	174.476  F KLAF 1 Klafter  200.  Par.Feet. 1167.64 7005.83. 12844.0 18682.2 24520.4	176.372 TER OF = 5.83819  300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2	VIENN 002 Paris of Hund 400.  Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0	180.165 A INTO r French F lreds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 tts.	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3	900. Par.Feet 5254.3 11092. 16930. 22768. 28607.
90  XXVI.  Klafter of Vienna. Thonsands.  0 1000 2000 3000 4000  Klafter. Tens.	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8  0. Par.Feet.	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	174.476  F KLAF 1 Klafter  200. Par.Feet. 1167.64 7005.83. 12844.0 18682.2 24520.4	176.372 TER OF = 5.83819 300. Par.Feet. 1751.46 7589.65 13427.8 19266.0 25104.2	VIENN 1002 Paris of Hund 1400.  Par. Feet. 2335.28 8173.47 14011.7 19849.8 25658.0 Uni	180.165 A INTO r French F lreds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 ts.  7ar.Feet.	PARIS eet.  600. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5	800. Par. Feet. 4670.55, 10508.7 16346.9 22185.1 28023.3	900.  Par.Feet 5254.3 11092. 16930. 22768. 28607.  Par.Feet 52.54
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000 4000  Klafter. Tens.	0. Par.Feet. 0.00 5838.19 117514.6 23352.8  0. Par.Feet. 0.00	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	200. Par.Feet. 1167.64 7005.83 12844.0 18682.2 24520.4  Par.Feet. 11.68	176.372 TER OF = 5.83819  300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2  3. Par. Feet. 17.51	VIENN 1002 Paris of Hund 1400.  Par.Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni  Par.Feet. 23.35	A INTO r French F dreds.  500.  Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9  ts.  Par.Feet. 29.19	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5	800. Par. Feet. 4670.55, 10508.7 16346.9 22185.1 28023.3 Par. Feet. 46.71	900. Par.Feet 5254.3 11092. 16930. 22768. 28607.  Par.Feet 52.54 110.93
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000 4000  Klafter. Tens.	0. Par.Feet. 0.00 5838.19 11654.4 17514.6 23352.8  0. Par.Feet. 0.00 58.38	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	174.476  F KLAF 1 Klafter  200. Par.Feet. 1167.64 7005.83. 12844.0 18682.2 24520.4  Par.Feet. 11.68 70.06	176.372 TER OF = 5.83813  300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2  Par. Feet. 17.51 75.90	VIENN 002 Paris of Hund 400.  Par. Feet. 2335.28 8173.47 19849.8 25688.0 Uni  Par. Feet. 23.35 81.73	A INTO r French F dreds.  500.  Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 ts.  Par.Feet. 29.19 87.57	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7  Par.Feet. 35.03 93.41	760.  Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5  Par.Feet. 40.87 99.25	Par. Feet. 46.71 105.09 163.47	900.  Par.Feet 5254.3 11092. 16930. 22768. 28607.  Par.Feet 52.54 110.93 169.31
90  XXVI.  Klafter of Vienna. Thousands.  0 1000 2000 3000 4000  Klafter. Tens.  0 10 20	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8  Par.Feet. 0.00 58.38 116.76	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	200. Par.Feet. 1167.64 7005.83 12844.0 18682.2 24520.4  Par.Feet. 11.68 70.06 128.44	176.372 TER OF = 5.83813  300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2  A. Par. Feet. 17.51 75.90 134.28	178.269 VIENN 002 Paris of Hund 400. Par.Feet. 2335.28 8173.47 19849.8 25688.0 Uni Par.Feet. 23.35 81.73 140.12	A INTO r French F dreds.  500.  Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 ts.  Par.Feet. 29.19 87.57 145.95	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7  6.  Par.Feet. 35.03 93.41 151.79	760.  Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5  Par.Feet. 40.87 99.25 157.63	Par. Feet. 46.71 105.09	900. Par.Fee 5254.3 11092. 16930. 22768. 28607.  Par.Fee 52.54 110.93 169.31 227.69
90  XXVI.  Klafter of Vienna. Thonsands.  0 1000 2000 3000 4000  Klafter. Tens.  0 10 20 30 40	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8  0. Par.Feet. 0.00 58.38 116.76 175.15 233.53	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6  Par.Feet. 5.84 64.22 122.60 180.98 239.37	200. Par.Feet. 1167.64 7005.83. 12844.0 18682.2 24520.4  2. Par.Feet. 11.68 70.06 128.44 186.82 245.20	TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2  Par. Feet. 17.51 75.90 134.28 192.66 251.04	178.269 VIENN 002 Paris of Hund  400.  Par.Feet. 2335.28 8173.47 19849.8 25688.0  Uni  4.  Par.Feet. 23.35 81.73 140.12 198.50 256.88	A INTO r French F dreds.  500.  Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 ts.  Par.Feet. 29.19 87.57 145.95 204.34 262.72	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7  6.  Par.Feet. 35.03 93.41 151.79 210.17 268.56	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5  Par.Feet. 40.87 99.25 157.63 216.01 274.39	Par. Feet. 46.71 105.09 163.47 221.85 280.23	900. Par.Feet 5254.3 11092. 16930. 22768. 28607.  Par.Feet 52.54 110.93 169.31 227.69 286.07
90  XXVI.  Klafter of Vienna. Thonsands.  0 1000 2000 3000 4000  Klafter. Tens.  0 10 20 30 40 40 40 40 50	0.00 5838.19 11676.4 17514.6 23352.8  0.00 58.38 116.76 1175.15 233.53	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6  Par.Feet. 5.84 64.22 122.60 180.98 239.37 297.75	200. Par.Feet. 1167-64 7005-93. 12844.0 18682.2 24520.4  Par.Feet. 11.68 70.06 128.44 186.82 245.20 303.59	176.372  TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2  Par. Feet. 17.51 75.90 134.28 192.66 251.04 309.42	178.269 VIENN 002 Paris of Hunde 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni Par.Feet. 23.35 81.73 140.12 198.50 256.88 315.26	180.165 A INTO r French F treds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 ts.  Par.Feet. 29.19 87.57 145.95 204.34 262.72 321.10	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7  6.  Par.Feet. 35.03 93.41 151.79 210.17 268.56	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5  Par.Feet. 40.87 99.25 157.63 216.01 274.39 332.78	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47 221.85 280.23 338.62	900. Par.Feet 5254.3 11092. 16930. 22768. 28607.  Par.Feet 52.54 110.98 169.31 227.69 286.07
90  XXVI.  Klafter of Vienna. Thonsands.  0 1000 2000 3000 4000  Klafter. Tens.  0 10 20 30 40 50 60	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8  0. Par.Feet. 0.00 58.38 116.76 175.13 233.53 291.91 350.29	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6  Par.Feet. 5.84 64.22 122.60 180.98 239.37 297.75 356.13	200. Par.Feet. 1167-64 7005-93. 12844.0 18682.2 24520.4  Par.Feet. 11.68 70.06 128.44 186.82 245.20 303.59 361.97	176.372  TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2  Par. Feet. 17.51 75.90 134.28 192.66 251.04 309.42 367.81	178.269 VIENN 002 Paris of Hunde 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par.Feet. 23.35 81.73 140.12 198.50 256.88 315.26 373.64	180.165 A INTO r French F treds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 ts.  5. Par.Feet. 29.19 87.57 145.95 204.34 262.72 321.10 379.48	PARIS eet.  GOO.  Par.Feet. 35.02.91 9341.10 15179.3 21017.5 26855.7  G.  Par.Feet. 35.03 93.41 151.79 210.17 268.56 326.94 385.32	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5  Par.Feet. 40.87 99.25 157.63 216.01 274.39 332.78 391.16	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47 221.85 280.23 338.62 397.00	900.  Par.Feet 5254.3 11092. 16930. 22768. 28607.  Par.Feet 52.54 110.93 1297.69 286.07
90  XXVI.  Klafter of Vienna. Thonsands.  0 1000 2000 3000 4000  Klafter. Tens.  0 10 20 30 40 40 40 40 50	0.00 5838.19 11676.4 17514.6 23352.8  0.00 58.38 116.76 1175.15 233.53	172.579  SION O  Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6  Par.Feet. 5.84 64.22 122.60 180.98 239.37 297.75	200. Par.Feet. 1167-64 7005-93. 12844.0 18682.2 24520.4  Par.Feet. 11.68 70.06 128.44 186.82 245.20 303.59	176.372  TER OF = 5.83819  300.  Par. Feet. 1751.46 7589.65 13427.8 19266.0 25104.2  Par. Feet. 17.51 75.90 134.28 192.66 251.04 309.42	178.269 VIENN 002 Paris of Hunde 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni Par.Feet. 23.35 81.73 140.12 198.50 256.88 315.26	180.165 A INTO r French F treds.  500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 ts.  Par.Feet. 29.19 87.57 145.95 204.34 262.72 321.10	PARIS eet.  600.  Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7  6.  Par.Feet. 35.03 93.41 151.79 210.17 268.56	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5  Par.Feet. 40.87 99.25 157.63 216.01 274.39 332.78	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47 221.85 280.23 338.62	900. Par.Feet 5254.3 11092.16930.2 22768.2

1 Klafter = 6.2221403 English Feet.

Klafter of					Hund	lreds.				
Vienna. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng feet
0	0.00	622.21	1244.43	1866.64	2488.86	3111.07	3733.28	4355.50	4977.71	5599.93
1000	6222.14	6844.35	7466.57	8088.78	8711.00	9333.21	9955.42	10577.6	11199.9	11822.
2000	12444.3	13066.5	13688.7	14310.9	14933.1	15555.4	16177.6	16799.8	17422.0	18044.
3000						21777.5				
4000	24888.6	25510.8	26133.0	26755.2	27377.4	27999.6	28621.8	29244.1	29866.3	30488.
Klafter.					Un	its.				
Tens.	0.	1.	2.	3,	4.	5.	6.	7.	8.	9.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet
0	0.00	6.22	12.44	18.67	24.89	31.11	37.33	43.55	49.78	56.00
10	62.22	68.44	74.67	80.89	87.11	93.33	99.55	105.78	112.00	118.22
20	124.44	130.66	136.89	143.11	149.33	155.55	161.78	168.00	174.22	180.44
30	186.66	192.89	199.11	205.33	211.55	217.77	224.00	230.22	236.44	242.66
40	248.59	255.11	261.33	267.55	273.77	280.00	286.22	292.44	298.66	304.88
50	311.11	317.33	323.55	329.77	336.00	342.22	348.44	354.66	360.88	367.11
60	5 <b>7</b> 3.33	379.55	385.77	391.99	398.22	404.44	410.66	416.88	423.11	429.33
70	435.55	441.77	447.99	454.22	460.44	466.66	472.88	479.10	485.33	491.55
80	497.77	503.99	510.22	516.44	522.66	528.S8	535.10	541.33	547.55	553.77
90	559.99	566.21	572.44	578.66	584.88	591.10	597.33	603.55	609.77	615.99

#### XXVIII. CONVERSION OF FEET OF VIENNA INTO METRES.

1 Foot of Vienna = 0.3160790 Metre.

Feet of					Hund	lreds.				
Vienna. Thonsands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	31.61	63.22	94.82	126.43	158.04	159.65	221.26	252.86	284.47
1900	316.08	347.69	379.29	410.90	442.51	474.12	505.73	537.33	568.94	600.55
2000	632.16	663.77	695.37	726.98	758.59	790.20	821.81	853.41	885.02	916.63
3000	948.24	979.84	1011.45	1043.06	1074.67	1106.28	1137.88	1169.49	1201.10	1232.71
4000	1264.32	1295.92	1327.53	1359.14	1390.75	1422.36	1453.96	1485.57	1517.18	1548.79
5000	1580.40	1612.00	1643.61	1675.22	1706.83	1738.43	1770.04	1801.65	1833.26	1864.87
6000	1896.47	1928.08	1959.69	1991.30	2022.91	2054.51	2086.12	2117.73	2149.34	2180.95
7000	2212.55	2244.16	2275.77	2307.38	2338.98	2370.59	2402.20	2433.81	2465.42	2497.02
8000	2528.63	2560.24	2591.85	2623.46	2655.06	2686.67	2718.28	2749.89	2781.50	2813.10
9000	2844.71	2876.32	2907.93	2939.53	2971.14	3002.75	3034.36	3065.97	3097.57	3129.18
10000	3160.79	   3192.40	3224.01	3255.61	3287.02	3318.83	3350.44	3382.05	3413.65	3445.26
11000	ll .				3603.30				1	
12000	3792.95	3824.56	3856.16	3887.77	3919.38	3950.99	3982.60	4014.20	4045.81	4077.42
13000	4109.03	4140.64	4172.24	4203.85	4235.46	4267.07	4298.67	4330.28	4361.89	4393.50
14000	4425.11	4456.71	4488.32	4519.93	4551.54	4583.15	4614.75	4646.34	4677.97	4709.58
15000	4741.19	4772.79	4804.40	4836.01	4867.62	4899.22	4930.83	4962.44	4994.05	5025.66

1 Foot of Vienna = 0.9730317 Paris Foot.

Feet of Vienna.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet
0	0.0	97.30	19.46	29.19	38.92	48.65	58.38	68.11	77.84	87.57
1000	973.0	1070.3	1167.6	1264.9	1362.2	1459.5	1556.9	1654.2	1251.5	1848.8
2000	1946.1	2043.4	2140.7	3238.0	2335.3	2432.6	2530.0	2627.2	2724 5	2821.8
3000	2919.1	3016.4	3113.7	3211.0	3308.3	3405.6	3502.9	3600.2	3697.5	3794.8
4000	3892.1	3989.4	4086.7	4184.0	4281.3	4378.6	4475.9	4573.2	4670.6	4767.9
5000	4865.2	4962.5	5059.8	5157.1	5254.4	5351.7	5449.0	5546.3	5643.6	5740.9
6000	5838.2	5935.5	6032.8	6130.1	6227.4	6324.7	6422.0	6519.3	6616.6	6713.9
7000	6811.2	6908.5	7005.8	7103.1	7200.4	7297.7	7395.0	7492.3	7589.6	7687.0
8000	7784.3	7881.6	7978.9	8076.2	8173.5	8270.8	8368.1	8465.4	8562.7	8660.0
9000	8757.3	8854.6	8951.9	9049.2	9146.5	9243.8	9341.1	9438.4	9535.7	9633.0
10000	9730.3	9827.6	9924.9	10022.2	10119.5	10216.S	10314.1	10411.4	10508.7	10606.0
11000	10703.3	10300.7	10898.0	10995.3	11092.6	11189.9	11287.2	11384.5	11481.8	11579.1
12000	11676.4	11773.7	11871.0	11968.3	12065.6	12162.9	12260.2	12357.5	12454.8	12552.
13000	12649.4	12746.7	12844.0	12941.3	13038.6	13135.9	13233.2	13330.5	13427.8	13525.1
14000	13622.4	13719.7	13817.1	13914.3	14011.7	14109.0	14206.3	14303.6	14400.9	14498.2
15000	14595.5	14692.8	14790.1	14887.4	14984.7	15082.0	15179.3	15276.6	15373.9	15471.2
16000	15568.5	15665.8	15763.1	15860.4	15957.7	16055.0	16152.3	16249.6	16346.9	16444.2

#### XXX. CONVERSION OF FEET OF VIENNA INTO ENGLISH FEET AND DECIMALS.

1 Foot of Vienna = 1.0370234 English Foot.

Feet of Vienna.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.
0	0.0	103.7	207.4	311.1	414.8					933.3
1000	1037.0	1140.7	1244.4	1348.1	1451.S	1555.5	1659.2	1762.9	1866.6	1970.3
2000	2074.0	2177.7	2281.5	2385.2	2488.9	2592.6	2696.3	2800.0	2903.7	3007.4
3000	3111.1	3214.8	3318.5	3422.2	3525.9	3629.6	3733.3	3837.0	3940.7	4044.4
4000	4148.1	4251.8	4355.5	4459.2	4562.9	4666.6	4770.3	4874.0	4977.7	5081.4
5000	5185.1	5288.8	5292.5	5496.2	5599.9	5703.6	5807.3	5911.0	6014.7	6118.4
6000	6222.1	6325.8	6429.5	6533.2	6636.9	6740.7	6844.4	6948.1	7051.8	7155.5
7000	7259.2	7362.9	7466.6	7570.3	7674.0	7777.7	7881.4	7985.1	8088.8	8192.5
8000	8296.2	8399.9	8503.6	8607.3	8711.0	8814.7	8918.4	9022.1	9125.8	9229.5
9000	9333.2	9436.9	9540.6	9644.3	9748.0	9851.7	9955.4	10059.1	10162.8	10266.5
10000	10370.2	10473.9	10577.6	10681.3	10785.0	10888.7	10992.4	11096.2	11199.9	11303.6
11000	11407.3	11511.0	11614.7	11718.4	11822.1	11925.8	12029.5	12133.2	12236.9	12340.6
12000					12859.1				13273.9	
13000	13481.3	13585.0	13688.7	13792.4	13896.1	13999.8				
14000					14933.1				15347.9	
15000	15555.4	15659.1	15762.8	15866.5	15970.2	16073.9				
16000	16592.4									

## RHINE OR PRUSSIAN FEET

#### INTO DIFFERENT MEASURES OF LENGTH.

The Rhine Foot is used in Physical Geography, though not so extensively as the French or Paris Foot, in the northwestern part of Germany, Denmark, and Holland. Its legal value in the Prussian system of weights and measures is 139.13 French or Paris Lines, from which are derived the equations used in computing the following tables.

XXXI. CONVERSION OF RHINE OR PRUSSIAN FEET INTO FRENCH TOISES.

1 Rhine Foot = 0.1610301 Toise.

Rhine Feet					Hun	dreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Torses.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.	Toises.
0	0.00	16.10	32.21	48.31	64.41	80.52	96.62	112.72	128.82	144.93
1000	161.03	177.13	193.24	209.34	225.44	241.55	257.65	273.75	289.85	305.96
2000	322.06	338.16	354.27	370.37	386.47	402.58	418.68	434.78	450.88	466.99
3000	483.09	499.19	515.30	531.40	547.50	563.61	579.71	595.81	611.91	628.02
4000	634.12	650.22	666.33	692.43	608.53	724.64	740.74	756.84	772.94	789.05
5000	805.15	821.25	837.36	853.46	869.56	885.67	901.77	917.87	933.97	950.08
6000	966.18	982.28	998.39	1014.49	1030.59	1046.70	1062.80	1078.90	1095.00	1111.11
7000	1127.21	1143.31			1191.62					
8000					1352.65					
9000					1513.68					

1 Rhine Foot = 0.31385350 Metre.

Rhine Feet.				RI	hine Feet.	Hundreds	3.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	31.39	62.77	94.16	125.54	156.93	188.31	219.70	251.08	282.47
1000	313.85	345.24	376.62	408.01	439.39	470.78	502.17	533.55	564.94	596.32
2000	627.71	659.09	690.48	721.86	753.25	784.63	816.02	847.40	878.79	910.18
3000	941.56	972.95	1004.33	1035.72	1067.10	1098.49	1129.87	1161.26	1192.64	1224.03
4000	1255.41	1286.80	1318.18	1349.57	1380.96	1412.34	1443.73	1475.11	1506.50	1537.88
5000	1569.27	1600.65	1632.04	1663.42	1694.81	1726.19	1757.58	1788.97	1820.35	1851.74
6000	1883.12	1914.51	1945.89	1977.28	2008.66	2040.05	2071.43	2102.82	2134.20	2165.59
7000	2196.97	2228.36	2259.75	2291.13	2322.52	2353.90	2385.29	2416.67	2448.06	2479.44
8000	2510.83	2542.21	2573.60	2604.98	2636.37	2667.76	2699.14	2730.53	2761.91	2793.30
9000	2824.68	2856.07	2887.45	2918.84	2950.22	2981.61	3012.99	3044.38	3075.76	3107.15

# XXXIII. OF RHINE OR PRUSSIAN FEET 1NTO FRENCH FEET AND DECIMALS. 1 Rhine Foot = 0.96618056 French Foot.

	1									
Rhine Feet.				R	hine Feet.	Hundred	ls.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Fr. Feet.	Fr Feet.	Fr Feet	Fr. Feet.	Fr.Feet	Fr Feet.	Fr.Feet.	Fr.Feet.	Fr Feet.	Fr. Feet.
0	0.00	96.62	193.24	289.85	386.47	483.09	579.71	676.33	772.94	869.56
1000	966.18	1062.80	1159.42	1256.03	1352.65	1449.27	1545.89	1642.51	1739.13	1835.74
2000	1932.36	2028.98	2125.60	2222.22	2318.83	2415.45	2512.07	2608.69	2705.31	2801.92
3000	2898.54	2995.16	3091.78	3188.40	3285.01	3381.63	3478.25	3574.87	3671.49	3768.10
4000	3864.72	3961.34	4057.96	4154.58	4251.19	4347.81	4444.43	4541.05	4637.67	4734.28
								~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		
5000						5313.99			1	
6000	5797.08	5893.70	5990.32	6086.94	6183.56	6280.17	6376.79	6473.41	6570.03	6666.65
7000	6763.26	6859.88	6956.50	7053.12	7149.74	7246.35	7342.97	7439.59	7536.21	7632.83
8000	7729.44	7826.06	7922.68	8019.30	8115.92	8212.53	8309.15	8405.77	8502.39	8599.01
9000	8695.63	8792.24	8888.86	8985.48	9082.10	9178.72	9275.33	9371.95	9468.57	9565.19

#### XXXIV. OF RHINE OR PRUSSIAN FEET INTO ENGLISH FEET AND DECIMALS. $1 \ {\rm Rhine\ Foot} = 1\,0297217 \ {\rm English\ Foot}.$

Rhine Feet.				R	hine Feet.	Hundred	ls.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.
0	0.00	102.97	205.94	308.92	411.89	514.86	617.83	720.81	823.78	926.75
1000	1029.72	1132.69	1235.67	1338.64	1441.61	1544.58	1647.55	1750.53	1853.50	1956.47
2000	2059.44	2162.42	2265.39	2368.36	2471.33	2574.30	2677.28	2780.25	2883.22	2986.19
3000	3089.17	3192.14	3295.11	3398.08	3501.05	3604.03	3707.00	3809.97	3912.94	4015.92
4000	4118.89	4221.86	4324.83	4427.80	4530.78	4633.75	4736.72	4839.69	4942.66	5045.64
5000	5148.61	5 <b>2</b> 51.58	5354.55	5457.53	5560.50	5663.47	5766.44	5869.41	5972.39	6075.36
6000	6178.33	6281.30	6384.28	6487.25	6590.22	6693.19	6796.16	6899.14	7002.11	7105.08
7000	7208.05	7311.02	7414.00	7516.97	7619.94	7722.91	7825.89	7928.86	8031.83	8134.80
8000	8237.77	8340.75	8443.72	8546.69	8649.66	8752.64	8855.61	8958.58	9061.55	9164.52
9000	9267.50	9370.47	9473.44	9576.41	9679.38	9782.36	9885.33	9988.30	10091.3	10194.2

## SPANISH OR MEXICAN VARAS AND FEET

INTO DIFFERENT MEASURES OF LENGTH.

XXXV. CONVERSION OF SPANISH OR MEXICAN VARAS INTO METRES.

1 Vara = 0.847965 Metre.

Varas.		Hundreds.												
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.				
	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.				
0	0.00	84.80	169.59	254.39	339.19	423.98	508.78	593.58	678.37	763.17				
1000	847.96	932.76	1017.56	1102.35	1187.15	1271.95	1356.74	1441.54	1526.34	1611.13				
2000	1695.93	1780.73	1865.52	1950.32	2035.12	2119.91	2204.71	2289.51	2374.30	2459.10				
3000	2543.89	2628.69	2713.49	2798.28	2883.08	2967.88	3052.67	3137.47	3222.27	3307.06				
4000	3391.86	3476.66	3561.45	3646.25	3731.05	3815.84	3900.64	3985.44	4070.23	4155.03				
5000	4239.82	4324.62	4409.42	4494.21	4579.01	4663.81	4748.60	4833.40	4918.20	5002.99				
6000	5087.79	5172.59	5257.38	5342.18	5426.98	5511.77	5596.57	5681.37	5766.16	5850.96				
7000	5935.75	6020.55	6105.35	6190.14	6274.94	6359.74	6444.53	6529.33	6614.13	6698.92				
8000	6783.72	6868.52	6953.31	7038.11	7122.91	7207.70	7292.50	7377.30	7462.09	7546.89				
9000	7631.68	7716.48	7801.28	7886.07	7970.87	8055.67	8140.46	8225.26	8310.06	8394.85				

XXXVI. OF SPANISH OR MEXICAN VARAS INTO ENGLISH FEET AND DECIMALS.

1 Vara = 2.78209 English Feet.

Varas.		Hundreds.													
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.					
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet					
0	0.0		556.4	1		-		_	_	2503.9					
1000	2782.1	3060.3	3338.5	3616.7	3894.9	4173.1	4451.3	4729.6	5007.8	5286.0					
2000	5564.2	5842.4	6120.6	6398.8	6677.0	6955.2	7233.4	7511.6	7789.9	8068.1					
3000	8346.3	8624.5	8902.7	9180.9	9459.1	9737.3	10015.5	10293.7	10571.9	10850.2					
4000	11128.4	11406.6	11684.8	11963.0	12241.2	12519.4	12797.6	13075.8	13354.0	13632.2					
5000	13910.4	14188.7	14466.9	14745.1	15023.3	15301.5	15579.7	15857.9	16136.1	16414.3					
6000	16692.5	16970.7	17249.0	17527.2	17805.4	18083.6	18361.8	18640.0	18918.2	19196.4					
7000	19474.6	19752.8	20031.0	20309.3	20587.5	20865.7	21143.9	21422.1	21700.3	21978.5					
8000	22256.7	22534.9	22813.1	23091.3	23369.6	23647.8	23926.0	24204.2	24482.4	24760.6					
9000	25038.8	25317.0	25595.2	25873.4	26151.6	26429.9	26708.1	26986.3	27164.5	27442.7					

### XXXVII. CONVERSION OF CASTILIAN FEET INTO METRES.

1 Castilian Foot = 0.282655 Metre.

Castilian Feet.	Hundreds.										
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.	
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	
0	0.00	28.27	56.53	84.80	113.06	141.33	169.59	197.86	226.12	254.39	
1000	282.65	310.92	339.19	367.45	395.72	423.98	452.25	480.51	508.78	537.04	
2000	565.31	593.58	621.84	650.11	678.37	706.64	734.90	763.17	791.43	819.70	
3000	847.96	876.23	904.50	932.76	961.03	989.29	1017.56	1045.82	1074.09	1102.35	
4000	1130.62	1158.89	1187.15	1215.42	1243.68	1271.95	1300.21	1328.48	1356.74	1385.01	
5000	1413.27	1441.54	1469.81	1498.07	1526.34	1554.60	1582.87	1611.13	1639.40	1667.66	
6000	1695.93	1724.20	1752.46	1780.73	1808.99	1837.26	1865.52	1893.79	1922.05	1950.32	
7000	1978.58	2006.85	2035.12	2063.38	2091.65	2119.91	2148.18	2176.44	2204.71	2232.97	
8000	2261.24	2289.51	2317.77	2346.04	2374.30	2402.57	2430.83	2459.10	2487.36	2515.63	
9000	2543.89	2572.16	2600.43	2628.69	2656.96	2685.22	2713.49	2741.75	2770.02	2798.28	

#### XXXVIII. CONVERSION OF CASTILIAN FEET INTO PARIS OR FRENCH FEET. 1 Castilian Foot = 0 870138 Paris Foot.

Castilian Feet.					Hun	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par.Feet.	Par Feet	Par.Feet.	Par Feet.	Par Feet.	Par. Feet.	Par.Feet.	Par Feet.	Par.Feet.	Par.Feet.
0	0.00	87.01	174.03	261.04	348.06	435.07	522.08	609.10	696.11	783.12
1000	870.14	957.15	1044.17	1131.18	1218.19	1305.21	1392.22	1479.23	1566.25	1653.26
2000	1740.28	1827.29	1914.30	2001.32	2088.33	2175.35	2262.36	2349.37	2436.39	2523.40
3000	2610.41	2697.43	2784.44	2871.46	2958.47	3045.48	3132.50	3219.51	3306.52	3393.54
4000	3480.55	3567.57	3654.58	3741.59	3828.61	3915.62	4002.64	4089.65	4176.66	4263.68
5000	4350.69	4437.70	4524.72	4611.73	4698.75	4785.76	4872.77	4959.79	5046.80	5133.82
6000	5220.83	5307.84	5394.86	5481.87	5568.88	5655.90	5742.91	5829.93	5916.94	6003.95
7000	6090.97	6177.98	6265.00	6352.01	6439.02	6526.04	6613.05	6700.06	6787.08	6874.09
8000	6961.11	7048.12	7135.13	7222.15	7309.16	7396.17	7483.19	7570.20	7657.22	7744.23
9000	7831.24	7918.26	8005.27	8092.29	8179.30	8266.31	8353.33	8440.34	8527.35	8614.37

#### XXXIX. CONVERSION OF CASTILIAN FEET INTO AMERICAN FEET. 1 Castilian Foot = 0.927309 American Foot.

Castilian Feet.		Hundreds.											
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
	Am. Feet	Am Feet.	Am. Feet.	Am. Feet.	Am.Feet.	Am. Feet.	Am. Feet.	Am Feet	Am. Fcet	Am. Feet.			
0	0.00	92.73	185.46	278.19	370.92	463.65	556.39	649.12	741.85	834.58			
1000	927.31	1020.04	1112.77	1205.50	1298.23	1390.96	1483.69	1576.43	1669.16	1761.89			
2000	1854.62	1947.35	2040.08	2132.81	2225.54	2318.27	2411.00	2503.74	2596.47	2689.20			
3000	2781.93	2874.66	2967.39	3060.12	3152.85	3245.58	3338.31	3431.04	3523.78	3616.51			
4000	3709.24	3801.97	3894.70	3987.43	4080.16	4172.89	4265.62	4358.35	4451.08	4543.82			
5000	4636.55	4729.28	4822.01	4914.74	5007.47	5100.20	5192.93	5285.66	5378.39	5471.12			
6000	5563.86	5656.59	5749.32	5842.05	5934.78	6027.51	6120.24	6212.97	6305.70	6398.43			
7000	6491.17	6583.90	6676.63	6769.36	6862.09	6954.82	7047.55	7140.28	7233.01	7325.74			
8000	7418.47	7511.21	7603.94	7696.67	7789.40	7882.13	7974.86	8067.59	8160.32	8253.05			
9000	8345.78	8438.51	8531.25	8623.98	8716.71	8809.44	8902.17	8994.90	9087.63	9180.36			

The length of the Spanish Vara, and of the Spanish or Castilian foot, used in the late Spanish Colonies of Mexico and South America, owing, no doubt, to the imperfection of the local standards, shows considerable variations from the value on which the preceding tables are based.

A careful comparison of the standard Vara, brought from Mexico by Major Turnbull, and deposited in the United States Office of Weights and Measures, (see above p. 113,) gave for its length 32.9682 American inches = 2.7473333 American feet = 2.7474928 English feet = 0.8374206 metre.

From a series of altitudes published in Mexico, by Cortina, in Castilian feet, and by Orbegozo in metres and Castilian feet, Jul. Schmidt derives the following value of the Vara and of the Castilian foot, used by these authors (see Petermann's *Mittheil*. 1857, p. 371): One Vara = 2.573296 Paris feet = 0.8358065 metre; and one Castilian foot = 0.857764 Paris foot = 0.91417 English foot.

According to Colonel J. Ondarza, one of the authors of the new official Map of Bolivia, the Bolivian government has declared the legal value of the Spanish Vara to be in the ratio of 100 metres = 118 Varas = 354 Spanish feet, which value has been adopted by him in publishing his measured altitudes.

XXXVIII' MEXICO. — CONVERSION OF CASTILIAN FEET INTO METRES, PARIS AND ENGLISH FEET.

Mexican or	Aceordin	ng to Turnbull's	Standara.	According	g to Schmidt, fro	m Cortina.
Castilian Feet.	Metres.	Paris Feet.	English Feet.	Metres.	Paris Feet.	English Feet
1000	279.14	859.30	915.83	278.64	857.76	914.17
2000	558.28	1718.60	1831.66	557.27	1715.53	1828.34
3000	837.42	2577.89	2747.49	835.91	2573.29	2742.51
4000	1116.56	3437.19	3663.32	1114.54	3431.06	3656.68
5000	1395.70	4296.49	4579.15	1393.18	4288.82	4570.85
6000	1674.84	5155.79	5494.99	1671.81	5146.58	5485.02
7000	1953.98	6015.08	6410.82	1950.45	6004.35	6399.19
8000	2233.12	6874.38	7326.65	2229.08	6862.11	7313.36
9000	2512.26	7733.68	8242.48	2507.72	7719.88	8227.53

XXXIX'. BOLIVIA. — CONVERSION OF SPANISH VARA AND SPANISH FEET.

1 Spanish foot = 0 2824859 metre = 0.8696171 Paris foot, = 0.9268078 English foot.

Bolivian or Spanish Feet.	Metres.	Paris Feet.	English Feet.	Metres.	Spanish Varas.	Spanish Feet.
1000	282.49	869.62	926.81	1000	1180	* 3540
2000	564.97	1739.23	1853.61	2000	2360	7080
3000	847.46	2608.85	2780.42	3000	3540	10620
4000	1129.94	3478.47	3707.23	4000	4720	14160
5000	1412.43	4348.09	4634.04	5000	5900	17700
6000	1691.92	5217.70	5560.85	6000	7080	21240
7000	1977.40	6087.32	6487.65	7000	8260	24780
8000	2259.89	6956.94	7414.46	8000	9440	25320
9000	2542.37	7826.55	8341.27	9000	10620	31860

## FRACTIONAL PARTS OF A TOISE AND OF A FOOT

INTO EACH OTHER.

XL. CONVERSION OF INCHES INTO DUODECIMAL LINES.

1 Inch = 12 Lines.

Inches.		Inches. Units.												
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.				
0	0	12	24	36	48	60	72	84	96	108				
10	120	132	144	156	168	180	192	204	216	228				
20	240	252	264	276	288	300	312	324	336	348				
30	360	372	384	396	408	420	432	444	456	468				
40	480	492	504	516	528	540	552	564	576	588				
50	600	612	624	636	648	660	672	684	696	708				
60	720	732	744	756	768	780	792	804	816	828				
70	840	852	864	876	888	900	912	924	936	948				
80	960	972	984	996	1008	1020	1032	1044	1056	1068				
90	1080	1092	1104	1116	1128	1140	1152	1164	1176	1188				
100	1200	1212	1224	1236	1248	1260	1272	1284	1296	1308				

XLI. CONVERSION OF DECIMALS OF A TOISE INTO FEET AND INCHES.

1 Toise = 6 Feet = 72 Inches = 864 Lines.

Toises.					Hundredths	of a Toise		_		
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	ft in lin.	ft. in. lin.	ft. in. lin	ft. in. lin.	ft. in lin.	ft. in. lin.	ft. in. lin.	ft. in. lin. f	t. in. lin.	ft. in, lin.
0.0	0.0.0,00	0. 0. 8,64	0. 1. 5,28	0. 2. 1,92	0. 2.10,56	0. 3.7,20	0. 4. 3,84	0.5. 0,48	0. 5. 9,12	0. 6. 5,76
0.1	0.7.2,40	0. 7.11,04	0. 8. 7,68	0. 9. 4,32	0.10. 0,96	0.10.9,60	0.11. 6,24	1.0. 2,88	0.11,52	1. 1. 8,16
0.2	1.2.4,80	1. 3. 1,44	1. 3.10,08	1. 4. 6,72	1. 5. 3,36	1. 6.0,00	1. 6. 8,64	1.7. 5,28	l. 8. 1,92	1. 8.10,56
0.3	1.9.7,20	1.10. 3,84	1.11. 0,48	1.11. 9,12	2. 0. 5,76	2. 1.2,40	2. 1.11,04	2.2. 7,68	2. 3. 4,32	2. 4. 0,96
0.4	2.4.9,60	2. 5. 6,24	2. 6. 2,88	2. 6.11,52	2. 7. 8,16	2. 8.4,80	2. 9. 1,44	2.9.10,08	2.10. 6,72	2.11. 3,36
0.5	3.0.0,00	3. 0. 8,64	3. 1. 5,28	3. 2. 1,92	3. 2.10,56	3. 3.7,20	3. 4. 3.84	3.5. 0.48 8	3. 5. 9.12	3, 6, 5,76
			3. 8. 7,68							
			4. 3.10,08							
0.8			4.11. 0,48							
0.9			5. 6. 2,88							

Feet.				]	Hundredth	s of a Foot				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
0.0	0.00	0.12	0.24	0.36	0.48	0.60	0.72	0.84	0.96	1.08
0.1	1.20	1.32	1.44	1.56	1.68	1.80	1.92	2.04	2.16	2.28
0.2	2.40	2.52	2.64	2.76	2.88	3.00	3.12	3.24	3.36	3.48
0.3	3.60	3.72	3.84	3.96	4.08	4.20	4.32	4.44	4.56	4.68
0.4	4.80	4.92	5.04	5.16	5.28	5.40	5.52	5.64	5.76	5.88
0.5	6.00	6.12	6.24	6.36	6.48	6.60	6.72	6.84	6.96	7.08
0.6	7.20	7.32	7.44	7.56	7.68	7.80	7.92	8.04	8.16	8.28
0.7	8.40	8.52	8.64	8.76	8.88	9.00	9.12	9.24	9.36	9.48
0.8	9.60	9.72	9.84	9.96	10.08	10.20	10.32	10.44	10.56	10.68
0.9	10.80	10.92	11.04	11.16	11.28	11.40	11.52	11.64	11.76	11.88

XLIII. CONVERSION OF DECIMALS OF A FOOT INTO INCHES AND DUODECIMAL LINES.

Feet.				1	Iundredths	of a Foo	t.			
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	In. Line.	In. Line.	In. Line.	In. Line.	In, Line.	In Line	In. Line	In. Line.	In. Line	In. Line.
0.0	0.0,00	0. 1,44	0. 2,88	0. 4,32	0. 5,76	0.7,20	0. 8,64	0.10,08	0.11,52	1. 0,96
0.1	1.2,40	1. 3,84	1. 5,28	1. 6,72	1. 8,16	1.9,60	1.11,04	2. 0,48	2. 1,92	2. 3,36
0.2	2.4,80	2. 6,24	2. 7,68	2. 9,12	2.10,56	3.0,00	3. 1,44	3. 2,88	3. 4,32	3. 5,76
0.3	3.7,20	3. 8,64	3.10,08	3.11,52	4. 0,96	4.2,40	4. 3,84	4. 5,28	4. 6,72	4. 8,16
0.4	4 9,60	4.11,04	5. 0,48	5. 1,92	5, 3,36	5.4,80	5. 6,24	5. 7,68	5. 9,12	5.10,56
0.5	6.0,00	6. 1,44	6. 2,88	6. 4,32	6. 5,76	6.7,20	6. 8,64	6.10,08	6.11,52	7. 0,96
0.6	7.2,40	7. 3,84	7. 5,28	7. 6,72	7. 8,16	7.9,60	7.11,04	8. 0,48	8. 1,92	8. 3,36
0.7	8.4,80	8. 6,24	8. 7,68	8. 9,12	8.10,56	9.0,00	9. 1,44	9. 2,88	9. 4,32	9. 5,76
0.8	9.7,20	9. 8,64	9.10,08	9.11,52	10. 0,96	10.2,40	10. 3,84	10. 5,28	10. 6,72	10. 8,16
0.9	10.9,60	10.11,04	11. 0,48	11. 1,92	11. 3,36	11.4,80	11. 6,24	11. 7,68	11. 9,12	11.10,56

XLIV. CONVERSION OF INCHES AND DUODECIMAL LINES INTO DECIMALS OF A FOOT.

1 Inch = 0.08333 of a Foot. 1 Line = 0.006944 of a Foot.

						Li	nes.					
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.
	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.
0	0.0000	0.0069	0.0139	0.0208	0.0278	0.0347	0.0417	0.0486	0.0556	0.0625	0.0694	0.0764
1	0.0833	0.0903	0.0972	0.1042	0.1111	0.1181	0.1250	0.1319	0.1389	0.1458	0.1528	0.1597
2	0.1667	0.1736	0.1806	0.1875	0.1944	0.2014	0.2083	0.2153	0.2222	0.2292	0.2361	0.2431
3	0.2500	0.2569	0.2639	0.2708	0.2778	0.2847	0.2917	0.2986	0.3056	0.3125	0.3194	0.3264
4	0.3333	0.3403	0.3472	0.3542	0.3611	0.3681	0.3750	0.3819	0.3889	0.3958	0.4028	0.4097
5	0.4167	0.4236	0.4306	0.4375	0.4444	0.4514	0.4583	0.4653	0.4722	0.4792	0.4861	0.4931
							1	-				
6	[0.5000]	0.5069	0.5139	0.5208	0.5278	0.5347	0.5417	0.5486	0.5556	0.5625	0.5694	0.5764
7	0.5833	0.5903	0.5972	0.6042	0.6111	0.6181	0.6250	0.6319	0.6389	0.6458	0.6528	0.6597
8	0.6667	0.6736	0.6806	0.6875	0.6944	0.7014	0.7083	0.7153	0.7222	0.7292	0.7361	0.7431
9	0.7500	0.7569	0.7639	0.7708	0.7778	0.7847	0.7917	0.7986	0.8056	0.8125	0.8194	0.8264
10	0.8333	0.8403	0.8472	0.8542	0.8611	0.8681	0.8750	0.8819	0.8889	0.8958	0.9028	0.9097
11	0.9167	0.9236	0.9306	0.9375	0.9444	0.9514	0.9583	0.9653	0.9722	0.9792	0.9861	0.9931

# METEOROLOGICAL TABLES.

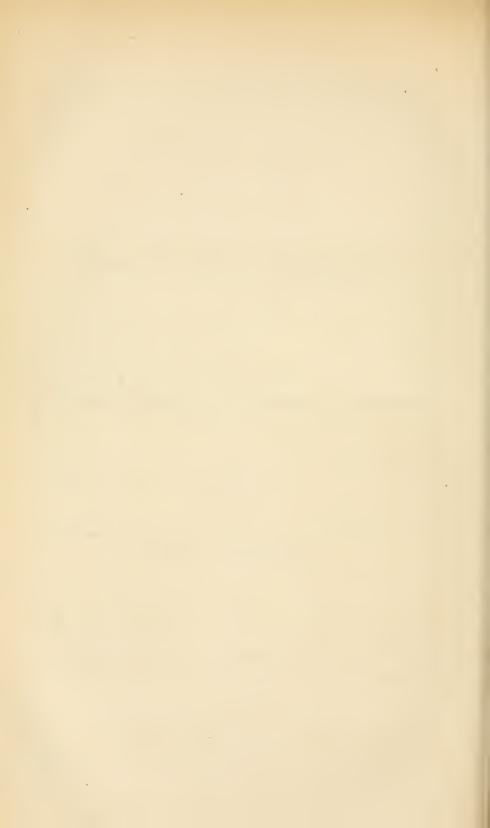
V.

# METEOROLOGICAL CORRECTIONS,

OR

## TABLES

FOR CORRECTING SERIES OF OBSERVATIONS FOR THE PERIODIC AND NON-PERIODIC VARIATIONS.



# CONTENTS.

[The figures refer to the folio at the bottom of the page.—The letters near them mean, D. = calculated by Dove; Gl. = Glaisher; G. = Guyot; L. = Lefroy. For the letters before the latitudes, see page 12.]

## Temperature.

### Hourly Corrections for Periodic Variations.

#### NORTH AMERICA.

Station.				Latitude.	Scale.		Page.				
Гав	LE I.	Washington, District Columbia,	B 1.	38 54 N.	Reau.	D.	15				
66	II.	Philadelphia, Girard College,	A'3.	39 58 N.	Reau.	D.	15				
66	III.	Philadelphia, Girard College,	A'3.	39 58 N.	Fahr.	G.	16				
66	IV.	Frankfort Arsenal, Penn.,	C.	39 57 N.	Reau.	D.	17				
66	v.	Frankfort Arsenal, Penn.,	C.	39 57 N.	Fahr.	D.	18				
66	VI.	Toronto, Canada West,	В.	43 40 N.	Fahr.	D.	19				
66	VII.	Toronto, Canada West,	В.	43 40 N.	Reau.	D.	20				
46	VIII.	Toronto, Canada West,	A'6.	43 40 N.	Fahr.	L.	21				
"	IX.	Toronto, Canada West,	A'6.	43 40 N.	Reau.	D.	22				
66	X.	Montreal, Canada East,	A'1.	45 30 N.	Fahr.	G.	22				
"	XI.	Sitka, Russian America,	A'5.	57 3 N.	Reau.	D.	23				
"	XII.	Boothia Felix, Arctic America,	A.	69 59 N.	Reau.	D.	24				
"	XIII.	Lake Athabasca, Arctic America,	C.	59 N.	Fahr.	L.	25				
66	XIV.	Melville Island, Arctic America,	C.	74 47 N.	Reau.	D.	25				
46	XV.	Hecla Cove, Spitzbergen,	C.	79 55 N.	Reau.	D.	25				
Appendix.											
64	V'.	Amherst College, Mass.,	A'1.	42 22 N.	Fahr.	D.	28				
SOUTH AMERICA.											
66	XVI.	Rio Janeiro, Brazil,	C.	22 54 S.	Fahr.	D.	26				
64	XVII.	Rio Janeiro, Brazil,	C.	22 54 S.	Reau.	D.	27				

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		ASIA. Station.	Latitude.	Scale.	р	age.
Тав	LE XVIII.	Trevandrum, India,	A. 8 31 N.	Fahr.	D.	31
LAB.	XIX.	Trevandrum, India,	A. 8 31 N.	Reau.	D.	32
6	XX.	Madras, India,	A. 13 4 N.	Fahr.	D.	33
46	XXI.	Madras, India,	A. 13 4 N. A. 13 4 N.	Reau.	D.	34
66	XXII.	Bombay, India,	A. 18 56 N.	Fahr.	D.	35
66	XXIII.	Bombay, India,	A. 18 56 N.	Reau.	D.	36
44	XXIII.	Madras, India,	A'5. 13 4 N.	Reau.	D.	37
66	XXV.	Bombay, India,	A'4. 18 56 N.	Reau.	D.	37
66	XXVI.	Calcutta, India,	A'2. 22 33 N.	Reau.	D.	38
46	XXVII.	Tiflis, Georgia,	A'4. 41 41 N.	Reau.	D.	39
66	XXVIII.	Peking, China,	A'4. 39 54 N.	Reau.	D.	39
66	XXIX.	Nertchinsk, Siberia,	A'6. 51 18 N.	Reau.	D.	40
66	XXX.	Nertchinsk, Siberia,	A. 51 18 N.	Reau.	D.	41
44	XXXI.	Barnaul, Siberia,	A. 53 20 N.	Fahr.	D.	42
4.6	XXXII.	Barnaul, Siberia,	A. 53 20 N.	Reau.	D.	43
66	XXXIII.	Barnaul, Siberia,	A'6. 53 20 N.	Reau.	D.	44
	212121111	Damaui, Siberia,	11 0. 00 20 IV.	meau.	ν.	7.7
		EUROPE.				
66	XXXIV.	Rome, Italy,	C. 41 54 N.	Reau.	D.	47
44	XXXV.	Padua, Italy,	C. 45 24 N.	Reau.	D.	48
66	XXXVI.	Geneva, Switzerland,	C 10. 46 12 N.	Reau.	D.	49
66	XXXVII.	Geneva, Switzerland,	C'4. 46 12 N.	Reau.	D.	49
66	XXXVIII.	St. Bernard, Switzerland,	C 10. 45 52 N.	Reau.	D.	50
66	XXXIX.	St. Bernard, Switzerland,	C'4. 45 52 N.	Reau.	D.	50
44	XL.	Kremsmünster, Austria,	C. 48 3 N.	Reau.	D.	51
66	XLI.	Salzburg, Austria,	A'6. 47 48 N.	Reau.	D.	52
66	XLII.	Munich, Bavaria,	A'6. 48 9 N.	Reau.	D.	52
66	XLIII.	Prague, Bohemia,	A'10. 50 5 N.	Reau.	D.	53
46	XLIV.	Prague, Bohemia,	A. 50 5 N.	Reau.	D.	54
44	XLV.	Plymouth, England,	C. 50 22 N.	Fahr.	D.	55
46	XLVI.	Plymouth, England,	C. 50 22 N.	Reau.	D.	56
44	XLVII.	Brussels, Belgium,	B. 50 51 N.	Reau.	D.	57
44	XLVIII.	Brussels, Belgium,	B'. 50 51 N.	Reau.	D.	58
44	XLIX.	Schwerin, Germany,	B'3. 53 36 N.	Reau.	D.	58
44	L.	Mühlhausen, Prussia,	C. 51 13 N.	Reau.	D.	59
66	LI.	Utrecht, Holland,	A'2. 52 5 N.	Reau.	D.	60
46	LII.	Greenwich, England,	B'7. 51 29 N.	Reau.	D.	60
"	LIII.	Greenwich, England,	B. 51 29 N.	Reau.	D.	61
46	LIV.	Greenwich, England,	B. 51 29 N.	Fahr.	Gl.	62
"	LV.	Halle, Prussia,	C. 51 30 N.	Reau.	D.	63
	LVI.	Göttingen, Hanover,	C. 51 32 N.	Reau.	D.	64
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		Station.		Latitude.	Scale.		Page.
TABLE	E LVII.	Berlin, Prussia,	A.	52 30 N.	Reau.	D.	65
"	LVIII.		Α.	52 5 N.	Reau.	D.	66
66	LIX.	Stettin, Germany,	A'.	53 25 N.	Reau.	D.	67
66	LX.	Apenrade, Sleswick,	C.	55 3 N.	Reau.	D.	68
66	LXI.	Leith, Scotland,	A.	55 59 N.	Fahr.	D.	69
"	· LXII.	Leith, Scotland,	A.	55 59 N.	Reau.	D.	70
66	LXIII.	Makerstoun, Scotland,	A′3.	55 36 N.	Reau.	D.	71
66	LXIV.	Dublin, Ireland,	B'4.	53 23 N.	Reau.	D.	71
66	LXV.	Catharinenburg, Russia,	A.	56 50 N.	Reau.	D.	72
66	LXVI.	Catharinenburg, Russia,	A'6.	56 50 N.	Reau.	D.	73
66	LXVII.	St. Petersburg, Russia,	A'10.		· Reau.	D.	73
46	LXVIII.	Helsingfors, Finland,	A'3.	60 10 N.	Reau.	" D.	74
66	LXIX.	St. Petersburg, Russia,	A.	59 56 N.	Reau.	D.	75
66	LXX.	Helsingfors, Finland,	C.	60 10 N.	Reau.	D.	76
66	LXXI.	Christiania, Norway,	C.	59 55 N.	Reau.	D.	77
"	LXXII.	Drontheim, Norway,	C.	63 26 N.	Reau.	D.	78
66	LXXIII.	Strait of Kara, Russia,	A	70 37 N.	Reau.	D.	79
46	LXXIV.	Matoschkin Schar, Novaia Zemlia,	A.	73 N.	Reau.	D.	80
66	LXXV.	Bossekop, Norway,	C.	69 58 N.	Reau.	D.	81
66	LXXV'.	Bossekop, Norway,	C.	69 58 N.	Centig.	G.	81
		AFRICA AND AUSTRA	гта				
					T)	T.	0.5
66	LXXVI.	St. Helena, Africa,	A'5.	15 55 S.	Reau.	D.	85
66	LXXVII.	Cape of Good Hope, Africa,	A'5.	33 56 S.	Reau.	D.	85
46	LXXVIII.	Hobarton, Tasmania,	A's.	42 53 S.	Reau.	D.	. 86
							•
		Monthly Corrections for Non-perio	odic V	ariations.			
		Station.		Latitude.	Scale.		Page.
TABL	E LXXIX.	Madras, India,		13 4 N.	Reau.	D.	90
46	LXXX.	Palermo, Sicily,		38 7 N.	Reau.	D.	91
"	LXXXI.	Milan, Italy,		45 28 N.	Reau.	D.	92
66	LXXXII.	Geneva, Switzerland,		46 12 N.	Reau.	D.	94
66	LXXXIII.	Vienna, South Germany,		48 13 N.	Reau.	D.	96
66	LXXXIV.	Ratisbon, South Germany,		49 1 N.	Reau.	D.	97
66	LXXXV.	Stuttgard, South Germany,		48 46 N.	Reau.	D.	99
66	LXXXVI.	Carlsruhe, South Germany		49 1 N.	Reau.	D.	100
دد	LXXXVII.	Berlin, North Germany,		52 30 N.	Reau.	D.	102
"	LXXXVIII.	Copenhagen, Denmark,		55 41 N.	Reau.	D.	105
66	LXXXIX.	Paris, France,		48 50 N.	Reau.	D.	107
66	XC.	Zwanenburg, Holland,		52 23 N.	Reau.	D.	108
"	XCI.	London, England,		51 30 N.	Reau.	D.	110
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		Station.	Latitude.			Page.
TABL	E XCII.	Kinfauns Castle, Scotland,	56 24 N.	Reau.	Đ.	112
66	XCIII.	Torneå, Finland,	65 50 N.	Reau.	D.	112
66	XCIV.	Albany, N. Y., North America,	42 39 N.	Reau.	D.	113
66	XCV.	Salem, Mass., North America,	42 31 N.	Reau.	D.	114
66	XCVI.	Reikiavik, Iceland,	64 8 N.	Reau.	D.	115
66	XCVII.	Godthaab, Greenland,	64 10 N.	Reau.	D.	115

# Force of Vapor and Relative Humidity.

### Hourly Corrections for Periodic Variations.

66	XCVIII.	Greenwich, England, Force of Vapor, by Glaisher,		119
66	XCIX.	Greenwich, England, Relative Humidity, by Glaisher,		120

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### METEOROLOGICAL CORRECTIONS.

One of the prominent objects of a prolonged series of meteorological observations is to determine the mean condition of the atmosphere, during a given interval of time, such as a day, a month, or a year, as to its temperature, moisture, and barometric pressure. In order to furnish the true means of these elements, free from the periodic changes which depend upon the daily course of the sun and upon the seasons, the observations ought to be made at equal intervals of time, and be so often repeated as actually to represent the sum of the variations which took place during the stated time. It is generally admitted that observations taken at every one of the twenty-four hours of the day give means which do not sensibly differ from the means which would be obtained from a still larger number of observations during the same time; so that means derived from hourly observations may be considered as the true daily, monthly, and annual means of the year in which the observations were taken.

However, as the means of a given month, or year, will generally be found somewhat to differ from those of another year, at the same place, from causes which are not of a periodic nature, it is obvious that the absolute means can only be derived from the means of a series of years, in which the differences arising from these non-periodic variations may be considered as sufficiently balancing each other.

Hourly observations can be expected only from a very few stations, favored with peculiar arrangements for the purpose. By far the larger number of observers must necessarily confine themselves to three or four observations a day. The means, therefore, deduced from such a set of observations, generally differ from the true means which would be given by hourly observations, by a quantity which varies with the hours selected for the observations. If that quantity, however, is known by having been previously determined for every hour, or set of hours, by a long series

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#### METEOROLOGICAL CORRECTIONS.

of hourly observations taken at some station in a similar climatic situation, it is evident that, whatever be the hours at which observations are taken, the means derived from them can always be reduced to the true means by correcting them for that difference.

The following tables furnish such corrections, both for periodic and non-periodic variations of temperature, and for stations situated in various latitudes. They give the quantities which must be added to, or subtracted from, the hourly means, in order to obtain the true means of the day, of the month, and of the year.

Two tables of the same description, for moisture, which may be considered as specimens of the kind, close the set.

Two other tables, for correcting the mean barometric pressures, are found at the end of the Hypsometrical Tables, pp. 92, 93.

# CORRECTIONS FOR TEMPERATURE.

HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

### TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY, OF THE MONTH, AND OF THE YEAR.



### HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

CORRECTIONS TO BE APPLIED TO THE MEANS OF THE HOURS OF OBSERVATION, OR SETS OF HOURS, IN ORDER TO OBTAIN THE TRUE MEAN TEMPERATURES OF THE RESPECTIVE DAYS, MONTHS, AND OF THE YEAR.

The following set contains all the tables for correcting the means of observations on atmospheric temperature for the effect of diurnal variation which have been published by Dove, together with a few others of the same description. Dove's tables are found in two papers, published in the Memoirs of the Royal Academy of Berlin for 1846 and for 1856, and in the first Report on the Observations of the Meteoro-

logical Institute of Prussia, Berlin, 1851.

In the first paper are twenty-nine tables, in Reaumur's scale, nine of which have been republished, in Fahrenheit's scale, in the *Proceedings of the British Association* for 1847, and will also be found below. In that series the corrections have been formed by finding first the differences between the hourly and the true means, and then computing the observations by Bessel's formula, in order to eliminate the accidental irregularities due to the shortness of the period during which the observations were taken. Calling x the horary angle reckoned from noon, Bessel's formula is

$$tx = u + u' \sin(x + U') + u'' \sin(2x + U'') + u''' \sin(3x + U''').$$

The stations at which hourly observations were made are Trevandrum, Madras, Bombay, Salzuflen, Prague, St. Petersburg, Catharinenburg, Barnaul, Nertchinsk, Matoschkin-Schar, Strait of Kara, and Boothia Felix. Bi-hourly observations were taken at Brussels, Greenwich, and Toronto; in all others the night observations are wanting, and were obtained by interpolation. Moreover, in several stations the number of observations was small, at Madras even only thirty-six days. The tables of that series may be readily distinguished from those belonging to the same stations in the second, by their containing the corrections for several sets of hours, which are not found in the tables of the other.

In Dove's second series, and in all other tables, the corrections given are simply the differences, with reverse signs, between the hourly and the true means, excepting, however, the stations of Toronto, in which the corrections were computed, by Bessel's formula, by Colonel Sabine; of Prague, by Jelineck; of Salzburg, and those of

Geneva and St. Bernard, by Plantamour.

The observations from which these tables are derived were made hourly at Hobarton during 8 years; at the Cape of Good Hope, for  $5\frac{1}{4}$  years; St. Helena, 5 years; Madras, 5 years; Bombay, 4 years; Calcutta,  $1\frac{1}{2}$  years; Toronto, 6 years; Philadelphia, 3 years; Makerstoun, 3 years; Utrecht,  $1\frac{3}{4}$  years; Prague,  $10\frac{1}{2}$  years; Munich, 7 years; Salzburg, 6 years; St. Petersburg, 10 years; Catherinenburg, 6 years; Barnaul, 5 years; Tiflis, 4 years; Nertchinsk, 6 years; Peking, 4 years; Sitka, 5 years. In the following stations the observations were bi-hourly:—Washington, for  $1\frac{1}{2}$  years; Greenwich, 7 years; Dublin, 4 years; Brussels, 9 years; Geneva and St. Bernard, 4 years; Schwerin, 3 years.

The observations made in England, and in her colonies, are found in the various government publications. Those of the Russian stations are taken from the Annuaire Météorologique et Magnétique des Ingénieurs des Mines, and in the Annales de

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l'Observatoire Physique Central de Russie. The observations made at Prague, Munich, Geneva, with those at St. Bernard, Makerstoun, Greenwich, Brussels, and Washington, were published by their respective Observatories; those of Utrecht, by Buys-Ballot; of Dublin, by Lloyd, in his Notes on the Meteorology of Ireland; those of Schwerin were communicated in manuscript by Dippe; the observations at Melville Island are published in No. 42 of the Parliamentary papers for 1854; and those at Bossekop, by Martins and Bravais, in the Voyage de la Commission Scientifique du Nord.

The tables of this second series being mostly deduced from longer series of observations than those in the first, when the same station is found in both, the table in the

second is generally to be preferred.

Glaisher's table for Greenwich has been taken from the *Greenwich Observations*. Captain Lefroy kindly furnished the tables for Toronto and Lake Athabasea. To him the author is also indebted for the observations made at Montreal by Mr. McCord, from which Table X. was computed. Table III., for Philadelphia, was deduced by the writer from the observations made at Girard College under the direction of Prof. A. D. Bache.

In order to facilitate the selection of the tables, they are marked in the table of

contents with capitals, which have the following signification: -

Observed Means.

A and B mean that the tables have been derived from hourly and bi-hourly observations, and have been computed by Bessel's formula; C, that the tables contain values obtained by interpolation.

A', B', and C' indicate the tables based respectively on hourly and bi-hourly or partly interpolated observations, which give simply the differences between the hourly

and the true means.

The figures added to the letters indicate the number of years during which the observations used in forming the table were carried on. The stations are arranged, in each continent, in the order of their latitude.

#### Use of the Tables.

In order to reduce meteorological means obtained from any set of hours to the true means, the table best suited to the purpose must first be selected. The diurnal variation changing with the seasons, the latitude, the altitude, and the distance from the sea-shore, the station which comes nearest, in all these respects, to the station the observations of which are to be corrected, must be adopted.

Suppose the thermometer has been observed at Baltimore, during the month of January, at 7 A. M., 1 P. M., and 7 P. M., and the monthly means of these hours to be respectively 27°, 35°, and 31° Fahrenheit. We take Table III., Philadelphia, it being the nearest in latitude and climatic situation. We find the correction for the

Corrections.

hours 7, 1, and 7, and we have

For 7 A. M. 
$$27^{\circ}$$
  $+3^{\circ}.63 = 30^{\circ}.63$   
For 1 P. M.  $35^{\circ}$   $-3^{\circ}.87 = 31^{\circ}.13$   
For 7 P. M.  $31^{\circ}$   $-1^{\circ}.13 = 29^{\circ}.87$   
Sums,  $93^{\circ}$   $-1^{\circ}.37 = 91^{\circ}.63$   
Means,  $31^{\circ}$   $-0^{\circ}.46 = 30^{\circ}.54$  True Mean for January.

True Means.

It is obvious that the corrections can be applied, either separately to each hour, as is done above, or collectively, in taking the mean of the three hourly corrections and applying it to the mean of the three observations, as in the last line, which is the more convenient method. Therefore, in order to find the correction for any set of hours, it suffices to take the mean of the corrections given in the table for the hours composing the set. The true daily means can be found in the same way, and the true yearly means can be derived from the corrected monthly means, or by applying the corrections given in the last column.

E

# HOURLY CORRECTIONS

FOR

# PERIODIC VARIATIONS.

NORTH AMERICA. - SOUTH AMERICA.



North America. — Washington. Lat. 38° 54' N. Long. 77° 3' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M. 0 12'	1.15	1.26	1.60	1.95	2.33	2.87	2.94	2.31	2.39	1.73	0.85	0.96	1.86
2 12'	1.28	1.86	2.14	2.40	3.15	3.21	3.25	3.07	2.75	2.27	1.34	1.12	2.32
4 12'	1.45	2.18	2.67	2.75	3.56	3.64	3.83	3.49	3.15	2.89	1.92	1.54	2.76
6 12'	1.88	2.32	2.76	2.59	2.20	2.23	2.12	2.81	3.02	3.19	2.18	1.81	2.43
8 12'	1.48	1.76	1.68	1.05	0.32	-0.16	0.09	0.28	1.04	1.69	1.88	1.68	1.07
10 12'	-0.18	-0.58	-0.88	-0.76	-1.24	-1.82	-1.32	-1.81	-1.31	-1.25	-0.17	-0.15	-0.96
7 75 0 70/	3 45	200	0.00	2.20	0.04	0.00	0.55	0.0=	0.00	0.00	1.00	1	0.00
P.M. 0 12'													1
2 12'	-2.60	-3.15	-3.35	-3.41	-3.57	-3.84	-3.49	-3.83	-3.74	-3.64	-2.44	-2.50	-3.30
4 12'	-2.32	-3.05	-3.20	-3.51	-3.66	-4.29	-4.16	-3.59	-3.65	-3.29	-2.08	-2.19	-3.25
6 12'	-0.76	-1.25	-1.73	-2.18	-2.44	-1.60	-2.24	-1.74	-1.88	-1.84	-1.59	-1.01	-1.69
8 12'	-0.23	0.02	-0.05	0.06	0.27	0.44	-0.21	-0.26	-0.23	0.18	-0.22	-0.26	-0.04
10 12'	0.33	0.69	0.76	1.42	1.67	2.04	1.26	1.79	1.41	0.98	0.23	0.43	1.08
										<u> </u>			
Means.	1.32	1.52	6.26	9.02	12.64	18.34	19.29	17.78	16.04	7.47	5.20	1.63	

II.

N. AMERICA.—PHILADELPHIA. Lat. 39° 58' N. Long. 75° 11' W. Gr.—Dove.

Degrees of Reaumur.

						81000 01	recount						
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.64	1.27	1.33	1,81	2.06	2.34	2.10	1.94	2.12	1.70	1.31	0.62	1.60
1	0.94	1.48	1.61	2.20	2.32	2.63	2.45	2.19	2.04	1.87	1.22	0.81	1.81
2	1.00	1.67	1.85	2.58	2.64	2.86	2.69	2.41	2.22	2.18	1.43	0.98	2.04
3	1.13	1.95	2.00	2.76	2.96	3.20	2.88	2.44	2.43	2.36	1.50	1.12	2.23
4	1.24	2.05	2.08	2.97	3.27	3.40	3.04	2.74	2.56	2.58	1.74	1.28	2.41
5	1.36	2.13	2.50	3.06	3.32	3.28	3.11	2.89	2.68	2.78	1.83	1.38	2.53
6	1.50	2.24	2.44	2.84	2.63	2.54	2.56	2.64	2.65	2.95	1.89	1.44	2.36
7	1.60	2.28	2.24	2.15	1.68	1.45	1.53	1.84	1.92	2.40	1.88	1.36	1.86
8	1.40	1.46	1.26	1.17	0.65	0.40	0.54	0.67	0.78	1.08	1.21	1.14	0.98
9	0.78	0.57	0.35	0.23	-0.39	-0.52	-0.36	-0.20	-0.18	-0.15	0.26	0.52	0.08
10	0.02	-0.39	-0.46	-0.71	-1.06	-1.23	-1.00	-1.05	-1.08	-1.17	-0.56	-0.22	-0.74
11	-0.68	-1.20	-1.38	-1.54	-1.74	-1.93	-1.74	-1.84	-1.90	-1.96	-1.27	-0.92	-1.50
Noon.	-1.21	-1.77	-1.97	-2.16	-2.24	-2.51	-2.26	-2.34	-2.45	-2.61	-1.77	-1.28	-2.05
1	-1.73	-2.36	-2.45	-2.86	-2.71	-3.06	-2.66	-2.67	-2.88	-3.14	-2.26	-1.63	-2.53
2	-2.04	-2.66	-2.74	-3.29	-3.11	-3.32	-2.97	-3.01	-3.22	-3.45	-2.52	-1.84	-2.85
3	-2.10	-2.82	-3.07	-3.42	-3.36	-3.40	-3.15	-3.11	-3.26	-3.45	<b>-2.4</b> 8	-1.85	-2.96
4	-1.98	-2.69	-2.99	-3.44	-3.46	-3.44	-3.06	-2.98	-3.17	-3.33	-2.24	-1.63	-2.87
5	-1.30	-2.18	-2.52	-3.14	-3.26	-3.05	-2.94	-2.70	-2.77	-2.46	-1.46	-1.10	-2.41
6	-0.91	-1.37	-1.60	-2.49	-2.46	-2.47	-2.30	-2.03	-1.77		-0.82	-0.64	
7	-0.51	-0.80	-0.88	-1.23	-1.28	-1.38	-1.44	-1.02	-0.76	-0.52	-0.33	-0.31	-0.87
8	-0.20	-0.21	-0.20	-0.29		0.06	0.03	0.01	0.28	0.18			-0.05
9	0.07	0.11	0.90	0.35	0.65	0.82	0.57	0.60	0.81	0.65	0.29	0.09	0.49
10	0.33	0.48	0.77	0.93	1.24	1.37	1.08	1.09	1.33	1.24	0.45	0.27	0.88
11	0.56	0.75	0.96	1.44	1.74	1.91	1.55	1.44	1.64	1.63	0.79	0.40	1.23
Mean.	0.30	1.12	5.18	8.75	12.18	16.22	18.19	17.52	14.66	8.72	3.67	0.58	

NORTH AMERICA. — PHILADELPHIA. Lat. 39° 58 N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — GUYOT.

Degrees	of	Fahren	heit.
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Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight	1.47	2.90	2.90	4.13	4.68	5.28	4.70	4.37	4.47	3.80	2.70	1.40	3.57
1	2.13	3.37	3.63	4.88	5.25	5.93	5.57	4.93	4.60	4.17	2.73	1.83	4.08
2	2.20	3.57	4.17	5.88	5.95	6.45	6.10	5.43	5.00	4.87	3.20	2.20	4.59
3	2.57	4.43	4.50	6.28	6.68	7.23	6.53	5.50	5.47	5.27	3.37	2.53	5 03
4	2.80	4.67	4.70	6.75	7.38	7.68	6.90	6.17	5.77	5.77	3.90	2.87	5.45
5	3.07	4.83	5.63	6.95	7.48	7.40	7.03	6.50	6.03	6.23	4.10	3.10	5.70
6	3.40	5.10	5.50	6.45	5.93	5.73	5.80	5.93	5.97	6.60	4.23	3.23	5.32
7	3.63	5.17	5.03	4.90	3.80	3.28	3.50	4.13	4.33	5.37	4.20	3.07	4.20
8	3.17	3.33	2.80	2.50	1.48	0.90	1.27	1.50	1.93	2.40	2.70	2.57	2.16
9	1.77	1.33	0.80	0.58	-0.85	-1.15	-0.77	-0.43	-0.40	-0.37	0.57	1.17	0.19
10	0.07	-0.83	-1.03	-1.53	-2.38	-2.75	-2.20	-2.37	-2.43	-2.67	-1.27	-0.50	-1.66
11	-1.40	-2.63	-3.10	-3.40	-3.90	-4.33	-3.87	-4.13	-4.27	-4.43	-2.87	-2.07	-3.37
										1			
Noon.	-2.70	-3.93	-4.43	-4.72	-5.03	-5.63	-5.03	-5.27	-5.50	-5.90	-4.00	-2.87	-4.58
1	-3.87	-5.27	-5.50	-6.38	-6.08	-6.88	-5.93	-6.00	-6.47	-7.10	-5.10	-3.67	-5.69
2	-4.57	-5.97	-6.17	-7.12	-6.98	-7.45	-6.63	<b>-6.</b> 83	-7.20	-7.80	-5.67	-4.13	-6.40
3	-4.70	-6.30	-6.90	<b>-7.</b> 63	-7.55	<b>-7.63</b>	<b>-7.0</b> 3	-7.00	-7.33	-7.80	-5.60	-4.17	-6.64
4	-4.43	-6.00	<b>-6.7</b> 3	-7.65	-7.78	-7.73	<b>-6</b> .83	-6.70	<b>-7.13</b>	<b>-7.5</b> 3	-5.07	-3.67	-6.44
5	-2.90	-4.87	-5.67	-7.00	-7.33	-6.85	-6.57	-6.07	-6.23	-5.57	-3.30	-2.47	-5.40
6	-2.03	-3.03	-3.60	-5.55	-5.53	-5.55	-5.13	-4.57	-3.97	-3.03	-1.87	-1.43	-3.77
7	-1.13	-1.77	-1.97	-2.70	-2.88	-3.10	-3.20	-2.30	-1.70	-1.20	-0.77	-0.70	-1.95
8				-0.60				1	1		1		-0.11
9	0.17								1	ł	1		
10	0.77	1.13	1			1			3.00			1	2.00
11	1.27	1.73	2.17	3.30	3.93	4.30	3.53	3.23	3.70	3.63	1.77	0.90	2.78
6, 6	0.69	1	1				1	1	1	1	1		li .
7, 7	1.25	ł	1					1		1			1
8, 8	1.37	1			1	1			1				1.04
9, 9	0.97	0.82	0.76	0.72	0.32	0.35	0.28	0.47	0.72	0.53	0.60	0.69	0.66
10, 10	0.42										-0.13		0.17
7, 2, 9						-0.77							
6, 2, 8	1.0	1	1			-0.52							
6, 2, 10	-0.13	0.09	0.53	0.74	0.58	0.46	0.55	0.52	0.59	0.52	-0.15	-0.10	0.44
6 0 0	1.00	0 ~0	1 40	9.0*	9 10	-2.42	_1 49	_1 69	_1 79	_1 41	_1 10	_0.79	-1.44
6, 2, 6													
7, 2													-1.09 -2.10
8, 2													-2.10 $-1.76$
8, 1	-0.35	-0.97	-1.30	-1.94	-2.30	-2.99	-2.33	-2.20	-2.03	2.00	1.20	-0.55	1.70
7, 1	_0.19	_0.03	_0.24	-0.74	_1 14	_1 90	_1 22	-0.94	-1.02	-0.82	-0.45	-0.30	-0.75
9, 12, 3, 9													
0, 12, 0, 9	-1.07	-2.16	7-2.40	-2.13	-2.99	-9.14	-4.00	-2:00	2.00	9.10	2.00	1.45	11 2.00

N. America. — Frankfort Arsenal. Lat. 39° 57′ N. Long. 75° 8′ W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	es of Re	aumui.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.34	1.46	1.75	1.87	2.60	3.41	3.07	2.69	2.63	2.40	1.18	1.34	2.15
2	1.51	1.73	2.13	2.33	3.05	3.73	3.51	3.04	3.05	2.67	1.27	1.50	2.46
3	1.82	1.98	2.56	2.88	3.43	3.92	3.83	3.32	3.49	2.94	1.41	1.66	2.77
4	2.13	2.23	2.90	3.29	3.57	3.84	3.84	3.36	3.73	3.13	1.51	1.80	2.94
5	2.31	2.46	2.95	3.31	3.32	3.36	3.40	2.99	3.54	3.12	1.73	1.87	2.86
6	2.25	2.35	2.62	2.83	2.65		2.52	2.21	2.84	2.82	1.38	1.80	2.39
7	1.88	2.01	1.91	1.94	1.66	1.26	1.34	1.15	1.71	2.19	1.06	1.52	1.64
8	1.22	1.33	0.94	0.85	0.57	-0.03	0.08	0.01	0 36	1.26	0.58	0.97	0.68
	0.04	0.00	0.05	0.00	0.45	1 20	1 00	1 00	0.00	0.10	0.00	0.10	0.04
9	0.34	0.30			i			-1.00			-0.02	0.18	
- 10	-0.62		1	-1.05		-2.11		-1.7S				-0.76	]
- 11	-1.54			-1.69								-1.70	!
Noon	-2.30	-2.60	-2.32	-2.22	-2.35	-3.17	-3.16	<b>-2.7</b> 8	-3.47	<b>-3.</b> 35	-1.96	-2.45	-2.68
1	-2.85	-3.01	_2 71	-2 79	-3.07	-3.51	-9 59	_3 16	-3.86	-4.05	-5 38	-2.87	-3.15
$\begin{vmatrix} & & 1 \\ 2 & \end{vmatrix}$		-3.18											
3		-2.93				-3.89					-2.34 $-2.40$		-3.41
4		-2.44											
4	-2.55	-2.44	-2.90	-9.00	-0.70	-3.75	-3.07	-5.42	-5.05	-5.00	-1.90	-1.94	-3.10
5	-1.90	-1.87	-2.50	-3.11	-3.20	-3.23	-3.00	-2.81	-2.84	-2.75	-1.52	-1.23	-2.50
6	1	-1.11				-2.33				-1.65		-0.55	
7		-0.46				-1.16			-0.48		0.14	0.01	-0.63
8	0.29		-0.06		-0.10		0.28	0.43	0.66	0.43	0.69	0.42	0.27
							0.20	0.10			0.00		0.2.
9	0.76	0.66	0.61	0.85	0.80	1.17	1.17	1.29	1.49	1.17	1.02	0.71	0.98
10	1.02	0.93	1.05	1.32	1.43	2.02	1.79	1.84	1.96	1.66	1.15	0 90	1.42
11	1.13	1.18	1.31	1.50	1.85	2.61	2.24	2.15	2.18	1.96	0.91	1.06	1.67
Midn	1.19	1.36	1.48	1.62	2.01	3.04	2.63	2.40	2.35	2.18	1.15	1.20	1.88
6. 6	0.56	0.62	0.42	0.30	0.17	0.07	0.26	0.19	0.56	0.58	0.41	0.62	0.40
7. 7	0.76	0.78	0.50	0.42	0.24	0.05	0.26	0.24	0.62	0.83	0.60	0.76	0.51
8.8	0.76	0.72	0.44	0.43	0.24	0.02	0.18	0.22	0.51	0.85	0.63	0.70	0.48
9. 9	0.55	0.48	0.27	0.33	0.18	-0.02	0.06	0.14	0.26	0.64	0.50	0.44	0.32
10.10	0.20	0.11	0.03	0.13	0.07	-0.05	-0.08	0.03	-0.05	0.26	0.23	0.07	0.08
	0.50	0.15	0.70	0.70	0.05	0.45	0	0.05	0.00	0.00	0.7	0.20	0.25
7. 2. 9	-0.13	-0.17	-0.16		-0.35			-0.35			-0.15	1	-0.27
6. 2. 8	-0.16			-0.11				-0.28					-0.25
6. 2.10	0.08	0.03	0.22	0.32	0.19	0.24	0.15	0.19	0.24	0.04		-0.06	0.14
6. 2. 6	-0.64	-0.65	-0.72	-0.86	-1.06	-1.21	-1.12	-1.03	-0.98	-1.06	-0.57	-0.55	-0.87
7. 2	-0.57	-0.59	-0.55	-0.63	-0.92	-1.26	-1 27	-1.17	-1.19	-1.00	-0.71	-0.69	-0.80
8. 2	1	-0.93	- 1										
8. 1		-0.93											
7. 1		-0.54											
7. 1	-0.49	-0.50	-0.42	-0.59	0.71	1.13	-1.12	-1.10	-1.03	-0.93	-0.00	-0.03	-0.70
9.12.3.9	-1.03	-1.14	-1.22	-1.28	-1.45	-1.77	-1.75	-1.53	-1.74	-1.57	-0.84	-1.03	-1.36
7. 2.2(9)	0.10	1	-0.03	3	1	-0.04		0.06	0.16		0.14	0.01	
											-		
Dail. ext.	-0.36	-0.36	-0.08	-0.12	-0.11	0.02	-0.05	-0.13	-0.17	-0.62	-0.41	-0.51	-0.24
				,									

N. AMERICA. — FRANKFORT ARSENAL. Lat. 39° 57' N. Long. 75° 8' W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Fal	irenheit						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
								٩					
Morn. 1	3.02	3.29	3.94	4.21	5.85	7.67	6.91	6.05		5.40	2.66	3.02	4.84
2	3.40	3.89	4.79	5.24	6.86	8.39	7.90		6.86	6.01	2.86	3.38	5.54
3	4.10	4.46	5.76	6.48	7.72	8.82	8.62	1	7.85	6.62	3.17	3.74	6.23
4	4.79	5.02	6.53	7.40	8.03	8.64	8.64	7.56	8.39	7.04	3.40	4.05	6.62
5	5.20	5.54	6.64	F 45	7.74	7.56	7.65	6.73	7.97	7.02	3.89	4.21	6.44
6	5.06	5.29	5.90	7.45 6.37	5.96	5.54	5.67	4.97	6.39	6.35	3.11	4.05	5.38
7	4.23	4.52	4.30	4.37	3.74	2.84	3.02		3.85	4.93	2.39	3.42	3.69
8	2.75	2.99	2.12	1.91	1.28	-0.07	0.18		0.81	2.84	1.31	2.18	1.53
Ü	2.10	2.00	2.12	1.51	1.20	0.01	0.10	0.02	0.01	2.01	1.07	2.10	1.00
9	0.77	0.68	-0.16	-0.45	-1.01	-2.70	-2.39	-2.25	-2.16	0.27	-0.05	0.41	-0.77
10	-1.40	-1.62	-2.25	-2.36	-2.90	-4.75	-4.41	-4.01	-4.64	-2.54	-1.58	-1.71	-2.86
11	-3.47	-3.98	-3.96	-3.80	-4.43	-6.17	-5.94	-5.27	-6.50	-5.24	-2.52	<b>-3.</b> S3	-4.59
Noon	-5.18	-5.85	-5.22	-5.00	-5.29	<b>-7.13</b>	-7.11	-6.26	-7.81	-7.54	-4.41	-5.51	-6.03
	0.45	0.70	0.30	0.75	0.05	m 00	0.00		0.00	0.17	- 00	0.10	<b>*</b> 00
1	-6.41				,		i	-7.11	)			1	
2								-7.83				-6.58	
3	1							-8.12		,	i	-5.72	
4	-5.69	-5.49	-6.64	-7.99	-8.33	-8.44	-8.26	<b>-7.7</b> 0	-5.17	-8.24	-4.41	-4.37	<b>-6.9</b> 8
5	-4.28	-4.21	-5.63	-7.00	<b>-7.</b> 20	-7.27	-6.75	-6.32	-6.39	-6.19	-3.42	-2.77	-5.63
6		-2.50						-4.12				-1.24	-3.60
7	-0.83		-2.07		-2.68		-1.87			-1.22	0.32	0.02	-1.42
8	0.65	0.27	-0.14		-0.23	0.16	0.63	0.97	1.49	0.97	1 55	0.95	0.61
9	1.71	1.48	1.37	1.91	1.80	2.63	2.63	2.90	3.35	2.63	2.30	1.60	2.21
10	2.30	2.09	2.36	1.97	3.22	4.55	4.03	4.14	4.41	3.74	2.59	2.03	3.20
11	2.54	2.66	2.95	3.38	4.16	5.87	5.04	4.84	4.91	4.41	2.05	2.39	3.76
Midn	2.68	3.06	3.33	3.65	4.52	6.84	5.92	5.40	5.29	4.91	2.59	2.10	4.23
0.0	1.00	7.40	0.0-	0.00	0.00	0.10	0.70	0.43	1.26	1 01	0.00	7.40	0.90
6. 6	1.26	1.40	0.95	0.68	0.38	0.16	0.59 0.59	0.45	1.40	1.31	0.92	1.40	1.15
7. 7 3. 8	1.71	1.76 1.62	1.13 0.99	$0.95 \\ 0.97$	$0.54 \\ 0.54$	0.05	0.59	0.50	1.40	1.87 1.91	1.35 1.42	1.71	1.13
9. 9	1.24	1.02	0.99	0.57	0.34	-0.05	0.14	0.32	0.59	1.44	1.13	0.99	0.72
10.10	0.45	0.25	0.07	0.74		-0.03	-0.18	0.07		0.59	0.52	0.33	0.12
10.10	0.49	0.20	0.07	0.20		0.11	0.10	0.01	0.11	0.00	0.04	0.10	0,10
7. 2. 9	-0.29	-0.38	-0.36	-0.29	-0.79	-1.01	-1.01	-0.79	-0.65	-0.74	-0.34	-0.50	-0.61
6. 2. 8	-0.36	-0.54	-0.39	-0.25	-0.72	-0.92	-0.81	-0.63	-0.43	-0.83	-0.36	-0.50	-0.56
6. 2.10	0.18	0.07	0.50	0.72	0.43	0.54	0.34	0.43	0.54	0.09	0.00	-0.14	0.32
6. 2. 6	-1.44	-1.46	-1.62	-1.94	-2.39	-2.72	-2.52	-2.32	-2.21	-2.39	-1.28	-1.24	-1.96
* 0	1.00	1.00			2.00	0.01	0.00	9.00	0.00	0.5	1.00	1	0.00
7. 2								-2.63					
8. 2								-3.92					
8. 1 7. 2	-1.85							-3.56					
1. 2	-1.10	-1.13	-0.95	-0.88	-1.60	-2.54	-2.52	-2.27	-2.43	-2.09	-1.49	-1.93	-1.71
9.12.3.9	-2.32	-2.57	-2.75	-2.88	-3.26	-3.98	-3.94	-3.44	-3.92	-3.53	-1.89	-2.32	-3.06
7. 2.2(9)	0.23		0.07		-0.16				0.36	0.09		0.02	0.09
` ′													
Dail.ext.	-0.81	-0.81	-0.18	-0.27	-0.25	0.04	-0.11	-0.29	-0.38	-1.39	-0.92	-1.15	-0.51

N. AMERICA. — TORONTO. Lat. 43° 39′ 35″ N. Long. 79° 21′ 30″ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degree		,						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.87	0.92	3.04	4,43	5.90	5.94	6.30	5.06	5.74	4.16	1.91	1.04	3.87
$\parallel$ 2	2.16	1.33	3.56	5.11	6.64	6.62	7.13	5.68	6.68	4.68	2.14	1.13	4.41
3	2.39	1.91	4.19	5.76	7.36	7.29	8.01	6.82	7.63	5.04	2.39	1.40	5.02
4			4.75	6.17	7.65	7.56	8.44	7.61	8.19	5.20	2.61	1.78	5.45
5	3.02	3.40	4.95	5.94	7.07	6.98	7.88	7.49	7.94	5.02	2.68	2.16	5.38
6	11		4.61	4.97	5.49	5.38		6.14	6.71	4.48	2.52	2.39	4.68
7	3.26	1	3.65	3.38	3.17	3.04	l .	1	4.52	3.44	2.05	2.27	3.33
8	11	1	i	1.42	0.68	0.43	i		i .	1.91	1.15	1.71	1.55
	2.12	9.40	2.12	1.42	0.00	0.40	0.52	0.00	1.70	1.91	1.19	1.71	1.55
9	1.58	2.33	0.00	0.50	1 51	_1 95	9.19	-2.09	_1.06	_0.05	-0.07	0.50	-0.36
11	11	1	l .		1		1	1	f	l .	ł .	l .	1
10	51				1			-4.14	L.	ŧ.	l .	-0.34	
11	-1.71	ł.	1	1	ı	1		-5.33		1	1		
Noon.	-3.11	-2.66	-4.55	-4.19	-5.00	-5.18	-5.90	-5.96	-7.25	-6.12	-3.78	-2.30	-4.66
									0.0			0	
1		-3.67											
2		-4.07											
3	11	-3.92											
4	-2.84	-3.38	-5.02	-6.48	-8.51	-8.08	-8.55	-7.81	-8.12	-5.18	-2.52	-2.23	-5.72
5	-2.14	-2.63	-4.03	-5.94	-7.76	-7.43	<b>-7.</b> 83	-6.95	-6.59	-3.53	-1.44	-1.71	-4.84
6	-1.62	-1.89	-2.75	-4.66	-5.83	-5.65	-5.94	-5.00	-4.43	-1.91	-0.45	-1.13	-3.44
7	-1.24	-1.24	-1.31	-2.81	-3.08	-3.04	-3.17	-2.25	-1.94	-0.50	0.32	-0.54	-1.73
8	-0.88	-0.68	0.05	-0.77	-0.16	-0.18	-0.18	0.65	0.43	0.65	0.86	0.02	-0.02
				1									
9	-0.43	-0.25	1.15	1.06	2.30	2.30	2.39	2.97	2.30	1.53	1.17	0.47	1.42
10			1.89	2.41	3.94	3.98	4.14	1	3.58	2.25	1.37	0.81	2.41
11	0.83		2.34	3.26	4.82	4.93	5.11	4.77	4.37	2.90	1.53	0.97	3.02
Midn.	11	1	2.66	3.85	5.33	5.45	5.64		1	3.56	1.71	1.01	3.42
Dialida.	1.42	0.00	2.00	0.00	0.00	0.10	0.01	1.01	0.00	0.00	1	1.01	0.15
6. 6	0.83	1.01	0.95	0.16	-0.18	0.14	0.11	0.56	1.13	1.28	1.04	0.63	0.61
16	III .		1			0.00	0.11		1.13	1.49			0.81
7. 7	1.01	1.27	1.17	1	-0.05	i .	i .			1.49	1.19	0.86	0.51
8.8	0.92	1.37	1.08	0.34	0.27	0.14	0.16	l .	1.10		1.01	0.86	
9. 9	0.59	0.99	0.72	0.29	0.41	0.23	0.14	0.45	0.63	0.74	0.56	0.63	0.54
10.10	0.07	0.36	0.14	0.16	0.43	0.27	0.07	0.09	-0.02	0.00	-0.05	0.23	0.14
	0.55		0.00	0.45		0 50		0.10	0 ==0	0 ===	0.00	0.0-	0.47
7. 2. 9		-0.11											
6. 2. 8	11	-0.27	1	1			i	-0.11					-0.43
6. 2.10	11	-0.02	0.27	0.54		0.83		l .		-0.18	)	0.11	0.38
6. 2. 6	-0.77	-0.68	-1.28	-1.82	-2.50	-2.39	-2.43	-1.98	-2.21	-1.55	-0.70	-0.54	-1.58
7. 2	11	-0.05	1		1						1	1	
8. 2	-0.63	-0.34	-1.80	-2.18	-3.24	-3.24	-3.49	-3.22	-3.56	-2.68	-1.51	-0.59	-2.21
8. 1	-0.59	-0.14	-1.62	-1.80	-2.66	-2.77	-3.04	-2.93	-3.29	-2.61	-1.58	-0.54	-1.96
7. 1	-0.32	0.16	-0.86	-0.81	-1.42	-1.46	-1.55	-1.42	-1.91	-1.85	-1.13	-0.25	-1.06
,													
9.12.3.9	-1.37	-1.15	-2.18	-2.50	-3.08	-3.13	-3.49	-3.20	-3.71	-2.79	-1.55	-0.92	-2.43
7. 2.2(9	. 11	-0.16			1					-0.18	0.07	1	0.05
	/												

N. AMERICA. — TORONTO. Lat. 43° 39′ 35″ N. Long. 79° 21′ 30″ W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the tru

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					20000	s of Ke							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.83	0.41	1.35	1.97	2.62	2.64	2.80	2.25	2.55	1.85	0.85	0.46	1.72
2	0.96	0.59	1.58	2.27	2.95	2.94	3.17	2.57	2.97	2.08	0.95	0.50	1.96
3	1.06	0.85	1.86	2.56	3.27	3.24	3.56	3.03	3.39	2.24	1.06	0.62	2.23
4	1.19	1.18	2.11	2.74	3.40	3.36	3.75	3 38	3.64	2.31	1.16	0.79	2.42
-	2020												
5	1.34	1.51	2.20	2.64	3.14	3.10	3.50	3.33	3.53	2.23	1.19	0.96	2.39
6	1.46	1.74	2.05	2.21	2.44	2.39	2.73	2.73	2.98	1.99	1.12	1.06	2.08
7	1.45	1.77	1.62	1.50	1.41	1.35	1.55	1.63	2.01	1.53	0.91	1.01	1.48
8	1.21	1.51	0.94	0.63	0.30	0.19	0.23	0.30	0.79	0.85	0.51	0.76	0.69
	1.21	1.01	0.54	0.00	0.00	0.10	0.20	0.00	0.,0	0.00	0.01	00	0.00
9	0.70	0.99	0.13	-0.22	-0.67	-0.82	-0.94	-0.93	-0.47	-0.02	-0.03	0.35	-0.16
10	-0.00	0.27	-0.71	-0.92			-1.78		-1.61		-0.65	1	
11	-0.76	-0.51	1						-2.54		-1.24		
1	1												
Noon	-1.38	-1.18	-2.02	-1.86	-2.22	-2.30	-2.02	2.00	-3.22	-2.72	-1.68	-1.02	-2.07
	_1 ~0	_1 69	-2.38	_9 99	_9 66	_2 64	_2 02	_2 80	-3.70	_3 16	-1.00	_1.99	_9 19
1	-1.73												
2	1		-2.54										
3	-1.57		-2.49										
4	-1.26	-1.50	-2.23	<b>-2.</b> 88	<b>-3.7</b> 8	<b>-3.</b> 59	-3.80	-3.47	-3.61	-2.30	-1.12	-0.99	-2.54
5	-0.95	-1.17	-1.79	-2.64	-3.45	-3.30	-3.48	-3.09	-2.93	-1.57	-0.64	-0.76	-2.15
6	1	-0.84							-1.97			-0.50	
7	1	-0.55							-0.86			-0.24	
8	l .	-0.30		-0.34						0.29	0.38		-0.01
	0.00							1					
9	-0.19	-0.11	0.51	0.47	1.02	1.02	1.06	1.32	1.02	0.68	0.52	0.21	0.63
10	0.07	0.05	0.84	1.07	1.75	1.77	1.84	1.92	1.59	1.00	0.61	0.36	1.07
11	0.37	0.17	1.04	1.45	2.14	2.19	2.27	2.12	1.94	1.29	0.68	0.43	1.34
Midn	0.63	0.28	1.18	1.71	2.37	2.42	2.53	2.15	2.22	1.58	0.76	0.45	1.52
6. 6	0.37	0.45	0.42	0.07	-0.08	-0.06	0.05	0.25	0.50	0.57	0.46	0.28	0.27
1	ll .		1	0.13	l .	1	1	0.32	1	0.66	1	0.38	0.36
7. 7	0.45	1				1	1	0.32	1	0.57	0.35	1	0.34
8.8	0.41	0.61	1	0.15		0.06	0.07			1		0.38	
9. 9	0.26	1	1	0.13			0.06	1	1	0.33		0.28	0.24
10.10	0.03	0.16	0.06	0.07	0.19	0.12	0.03	0.04	-0.01	0.00	-0.02	0.10	0.06
<b></b>	0.7-	0.00	0.14	_0.90	-0.95	_0.99	_0.24	_0.02	-0.31	_0.24	-0.14	_0.09	_0.18
7. 2. 9	11	-0.05	1		-0.25		-0.24	1	4	1		1	
6. 2. 8	JI	-0.12	1	-0.23		1			-0.26				1
6. 2.10	11	-0.01			1	0.37	1	1	1	-0.08	1		0.17
6. 2. 6	-0.34	[-0.30]	-0.57	-0.81	-1.11	-1.06	-1.08	-0.88	-0.98	-0.69	-0.31	-0.24	-0.70
				0.5-	0.00	0.00	0.00	0 ~-	0.0=	0.05	0.10	0.10	_0 =0
7. 2	-0.16	-0.02	-0.46	-0.53	-0.89	-0.86	-0.89	-0.77	-0.97	-0.85	-0.47	-0.13	0.03
8. 2	-0.28	-0.15	-0.80	-0.97	-1.44	-1.44	-1.55	-1.43	-1.58	-1.19	-0.67	-0.26	-0.98
8. 1	FI	-0.06	-0.72	-0.80	-1.18	-1.23	-1.35	-1.30	-1.46	-1.16	-0.70	-0.24	-0.87
7. 1	-0.14	0.07	-0.38	-0.36	-0.63	-0.65	-0.69	-0.63	-0.S5	-0.S2	-0.50	-0.11	-0.47
9.12.3.9	-0.61	-0.51	-0.97	-1 11	-1.37	-1.39	-1.55	-1.49	-1.65	-1.24	-0.69	-0.41	-1.08
7. 2.2(9)	11	-0.07	1	-0.03		ł .	1		I.	-0.08	1	1	1
1. 2.2(9)	-0.18	-0.07	0.03	-0.03	0.07	0.00	0.00	0.20	0.00	0.00	0.00	0.04	
Dail. ext.	-0.16	-0.02	-0.17	-0.07	-0.19	-0.12	-0.03	-0.08	-0.16	-0.46	-0.36	-0.11	-0.14
	1	1	1				-			1	-		

### VIII.

North America. — Toronto. Lat. 43° 40' N. Long. 79° 21' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Lefrox.

					Degre	ees of Fa	hrenhe	it.					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Year.
Midnight.	1.47	1.73	2.63	3.22	5.02	5.15	6.37	5.33	5.96	3.22	1.80	0.90	3.57
1	1.95	2.09	3.11	3.79	5.93		7.13	6.06	4.57	3.80	2.10		4.00
2	2.05	2.46	3.47	4.48	6.77	6.70	7.68	6.69	5.17	4.13	2.36	1.85	4.48
3	2.20	2.82	3.76	5.08	7.45	7.50	8.41	7.29	5.59	4.31	2.66	1.96	4.92
													1
4	2.28	3.20	4.07	5.38	7.93	8.06	9.03	7.63	6.18	4.64	2.85	2.04	5.27
5	2.46	3.62	4.35	5.75	7.83		9.02	7.89	6.77	4.77	2.76	2.07	5.43
6	1.83	4.23	4.75	5.48		1	5.92	6.57	6.17	4.71	2.52	2.39	4.60
7	1.94	4.34	3.93	3.22	2.43	2.41	2.38	3.28	3.68	3.94	2.52	2.55	3.05
8	1.66	3.29	1.89	1.09	0.06	0.10	-0.31	0.21	1.02	1.66	1.53	2.12	1.25
9	0.63		-0.25		1		-2.39		1		0.01	0.92	-0.82
10	-0.59			-2.45	1	-3.49	-3.98			-2.93	-1.41		-2.47
11	-1.70	-2.44		-3.85		-4.77	-5.49	-5.57	1	1	-2.44	-1.72	-3.77
Noon.	_9 (9	-3.56	_ ( 15	_1 86	_5 87	- 5 ee	6 79	6 20	-5.95	= 20	994	0 50	170
1		-3.30 $-4.49$				i .			-6.58	1		1	-4.76 $-5.43$
2	)	-4.45  -4.88			1	ļ		-7.11 -7.62			-3.74 $-3.82$		-5.43
3		-4.90		f .	1			<b>-7.98</b>		-5.85	-3.64	1	-5.82
	0.10	1.00	0.10	0.10			0.01	1.30	7.01	3.03	0.04	0.10	9.02
	0.00		4.05		- 1-	- 00	2 22				2.00		
4 5									-6.75				-5.47
6		-3.30 -1.87			-5.05			-5.39	-5.78 -3.16				-4.61 $-3.12$
7									-0.43				-3.12 $-1.22$
	0.40	-0.50	0.51	0.54	2.13	<b>3.00</b>	-5.20	-1.04	-0.40	-0.29	-0.10	-0.17	1.22
8	-0.12	-0.13	0.03	0.66	0.43	0.33	0.68	1.23	0.81	0.48		-0.12	0.38
9	0.07	0.52	1.00	1.78	2.31	2.44	2.99	2.70	1.90	1.25	0.44	0.18	1.46
10 11	0.44	1.06	1.63	2.59	3.29	3.80	4.24	3.73	2.94	1.97	0.78	0.47	2.24
11	0.77	1.00	2.01	3.07	4.20	4.76	5.21	4.54	3.61	2.68	1.13	0.59	2.85
		•											
6, 6	0.46	1.18	1.20	1.03	0.17	-0.26	-0.32	0.59	1.50	1.67	1.38	0.78	0.74
7, 7	0.77	1.67	1.51	1.14		-0.29	-0.45	0.82	1.62	1.84	1.18	1.04	0.91
8, 8	0.77	1.58	0.96	0.87	0.24	0.21	0.18	0.72	0.91	1.45	0.98	1.15	0.82
9, 9	0.35	0.77	0.37	0.38	0.10	0.31	0.30	0.22	0.19	0.10	0.22	0.55	0.32
10, 10	-0.07	0.05	-0.14	-0.07	-0.26	0.25	0.12	-0.22	-0.26	-0.18	-0.31	-0.03	-0.11
6, 2, 10	-0.31	0.14	0.36	0.64	0.52	0.66	0.63	0.89	0.72		-0.31		0.34
7, 2, 9	-0.40				-0.80		-0.96	-0.55	1		-0.29		-0.43
9, 12, 3, 9	-1.23				-3.22		-3.61	-3.48	-3.14				-2.48
Mari	25.00	99.70	20.70	11.00	59.00	60.6*	66.90	67.00	====	11.	20.70	05. 10	44.05
Mean.	20.52	23.70	29.79	41.99	92.92	60.67	00.39	00.86	07.55	44.14	36.18	27.40	44.37
	1				1				1				

# NORTH AMERICA. - TORONTO. Lat. 43° 40' N. Long. 79° 21' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.	Year.
Midn.	0.68	0.81	1.10	1.45	2.24	2.36	2.91	2.43	1.76	1.44	0.81	0.40	1.53
1	0.88	0.98	1.31	0.78	2.62	2.67	3.29	2.72	2.03	1.71	0.94	0.66	1.80
2	0.92	1.13	1.48	2.08	2.99	2.98	3.54	3.02	2.29	1.85	1.06	0.83	2.01
3	0.99	1.32	1.61	2.17	3.31	3.32	3.86	3.32	2.49	1.92	1.20	0.38	2.20
4	1.03	1.45	1.78	2.36	3.52	3.58	4.14	3.48	2.76	2.06	1.28	0.90	2.36
5	1.11	1.61	2.01	2.52	3.49	3.49	4.16	3.57	3.04	2.13	1.23	0.91	2.44
6	0.79	1.86	2.13	2.47	2.40	2.32	2.74	2.92	2.74	2.04	1.11	1.09	2.05
7	0.83	1.92	1.75	1.45	1.08	1.07	1.11	1.60	1.60	1.70	1.11	1.16	1.36
8	0.73	1.47	0.87	0.45	0.09	0.03	-0.05	0.15	0.38	0.70	0.64	0.97	0.56
9	0.30	0.44	-0.10	-0.43	-0.94	-0.81	-1.03	-0.96	-0.69	-0.49	-0.04	0.45	-0.36
10	-0.25	-0.45	-0.87	-1.11	-1.69	-1.55	-1.78	-1.84	-1.57	-1.35	-0.68	-0.20	-1.11
11	-0.77	-1.16	-1.41	-1.72	-2.20	-2.12	-2.47	-2.48	-2.20	-1.96	-1.13	-0.75	-1.70
Noon.	-1.12	-1.69	-1.87	-2.18	-2.62	-2.61	-3.05	-3.04	-2.64	-2.36	-1.48	-1.11	-2.15
1	-1.34	-2.07	-2.16	-2.60	-3.03	-2.93	-3.46	-3.25	-2.90	-2.55	-1.66	-1.42	-2.45
2	-1.46	-2.25	-2.41	-2.76	-3.18	-3.12	-3.84	-3.51	-3.08	-2.70	-1.69	-1.49	-2.62
3	-1.44	-2.24	-2.32	-2.80	-3.21	-3.29	-3.92	-3.66	-3.09	-2.60	-1.62	-1.38	-2.63
4	-1.21		-2.11	-2.62	-3.19	-3.40	-3.93	-3.60	-3.00	-2.28	-1.22	-1.09	-2.47
5	-0.77	-1.47	-1.78	-2.30	-3.02	-3.13	-3.72	-3.35	-2.57	-1.50	-0.68	-0.67	-2.08
6	-0.40	-0.82	-1.03	-1.50	-2.24	-2.55	-3.08	-2.51	-1.38	-0.59	-0.32	-0.36	-1.40
7	-0.17	-0.38	-0.38	-0.37	-0.96	-1.33	-1.54	-0.74	-0.18	-0.10	-0.06	-0.21	-0.53
8	-0.03	0.00	0.05	0.33	0.24	0.13	0.33	0.56	0.39	0.23	0.08	-0.04	0.19
9	0.06	0.28	0.50	0.81	1.02	1.09	1.38	1.26	0.85	0.57	0.20	0.07	0.67
10	0.23	0.53	0.79	1.16	1.45	1.69	1.93	1.72	1.32	0.90	0.36	0.20	1.02
11	0.37	0.76	1.08	1.38	1.86	2.12	2.45	2.07	1.60	1.20	0.52	0.25	1.31
Mean.	-2.97	<b>-3.</b> SS	-0.98	4.72	9.29	12.75	15.11	15.00	11.37	5.42	1.88	-2.03	

X.

North America. — Montreal. Lat.  $45^{\circ}$  30' N. Long.  $73^{\circ}$  22' E. Gr.

Degrees of Fahrenheit.

Hour.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year.
Midn.	4.00	3.89	2.83	1.36	1.68	1.10	1.28	1.31	2.52	4.55	5.25	4.39	2.85
2	5.39	4.34	4.01	1.59	1.00	2.36	2.69	2.88	4.37	6.95	7.42	7.17	4.20
4	6.34	5.60	4.84	1.81	1.38	2.88	3.36	5.56	7.09	6.95	7.18	7.57	4.96
6	5.99	4.59	4.83	1.36	1.32	3.54	3.90	5.22	5.56	6.61	5.55	5.46	4.50
8	2.79	2.19	2.52	0.78	0.92	3.10	3.22	3.30	3.44	3.06	0.88	0.60	2.24
10	-1.74	-1.48	-0.99	-0.41	0.21	-0.21	-0.81	-0.03	-0.79	-0.97	-1.75	-2.85	-0.93
Noon.	-5.63	-5.43	-1.22	-1.87	-1.22	-2.82	-3 50	-4.23	-5 01	-7.10	-5.17	-5.46	-4.30
2	1						1					-7.36	
4	-7.72	-6.70	-5.62	-2.52	-3.22	-3.88	-3.60	-5.96	-5.79	-8.35	-7.00	-7.51	-5.65
6	-5.63	-2.80	-2.79	-1.04	-1.30	-1.77	-1.50	-3.43	-3.88	-3.87	-5.02	-5.40	-3.20
8	-0.70	0.10	-0.25	0.03	0.02	-0.90	-0.59	-1.23	-0.81	-1.61	-1.10	-0.67	-0.65
10	1.99	2.39	1.42	1.18	0.89	0.17	0.22	-0.30	0.64	-1.87	2.47	2.64	1.30
Mean.	66.40	57.70	48.31	30.39	23.42	8.10	20.84	27.31	42.27	56.61	64.38	70.39	43.01

## NORTH AMERICA. - MONTREAL, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.

Degrees of Fahrenheit.

Hour.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year.
Tiour.	Aug.	- Sept.		Nov.	Dec.	Jau.		March.	April.	May.			- Tear.
A.M.1	5.03	4.92	2.53	1.16	0.88	1.43	1.61	4.38	3.12	4.85	4.55	5.07	3.30
3	5.99	5.20	3.61	1.58	1.79	1.30	2.72	5.18	5.14	6.51	5.10	6.80	4.25
5	6.44	5.43	4.45	2.08	2.21	1.87	3.95	6.84	6.54	6.56	6.30	7.76	5.05
7	2.10	3.47	3.61	2.01	2.08	1.98	5.22	7.07	3.84	3.56	4.72	3.04	3.56
9	-0.58	0.73	0.77	0.63	1.14	1.16	3.99	2.96	0.71	0.50	-0.02	0.22	1.02
11	-3.61	-2.20	-2.73	-1.35	-0.49	-1.08	-0.17	-2.51	-2.48	-2.79	-3.42	-3.21	-2.17
P.M.1	-6.61	-5.12	-5.41	-3.47	-2.38	-1.49	-4.80	-7.41	-1.93	-5.78	-5.97	-6.08	-4,95
			í					-9.03			1		
5	-5.47	-5.S3	-3.15	-1.19	-1.44	-0.63	-4.12	-6.48	-5.63	-6.62	-6.18	-6.53	-4.43
7	-1.45	-0.62	-1.00	-0.44	-0.70	-0.60	-1.23	-2.40	-2.93	-3.50	-3.17	-2.88	-1.74
9	1.58	1.32	0.32	0.13	-0.71	-0.66	-0.96	-0.75	0.44	0.61	1.58	1.17	0.34
11	3.10	3.02	2.47	1.48	0.22	0.61	0.24	1.78	2.06	2.52	3.55	3.39	2.02
	20.00										27.00		
Mean.	69.69	57.53	44.70	32.76	15.91	18.96	14.52	22.50	34.47	51.33	65.08	67.42	41.24

### XI.

NORTH AMERICA. — SITKA. Lat. 57° 3′ N. Long. 135° 18′ W. Gr. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Year.
Midn.	0.33	0.58	0.97	1.51	1.80	1.81	1.68	1.34	1.07	1.19	0.41	0.28	1.08
1	0.34	0.66	1.09	1.68	2.04	2.06	1.88	1.53	1.18	1.11	0.46	0.33	1.20
2	0.35	0.72	1.17	1.81	2.20	2.25	2.04	1.66	1.33	1.18	0.49	0.33	1.29
3	0.51	0.78	1.36	1.89	2.43	2.49	2.16	1.77	1.24	0.64	0.48	0.18	1.33
4	0.45	0.86	1.47	2.02	2.55	2.57	2.20	1.82	1.29	0.68	0.49	0.18	1.3
5	0.45	0.83	1.57	2.07	2.39	2.47	2.95	1.89	1.33	0.70	0.49	0.14	1.5
6	0.45	0.84	1.56	1.89	1.76	1.77	1.67	1.62	1.33	0.78	0.46	0.18	1.20
7	0.52	0.82	1.37	1.13	0.96	1.08	0.96	1.09	1.05	0.58	0.40	0.17	0.8
S	0.48	0.76	0.75	0.31	0.00	0.26	0.26	0.40	0.47	0.53	0.33	0.12	0.3
9	0.39	0.49	-0.08	-0.63	-0.82	-0.52	-0.58	-0.26	-0.17	0.12	0.23	0.10	-0.1
10	0.16	-0.03	-0.69	-1.12	-1.35	-1.28	-1.27	-0.95	-0.73	-0.28	0.00	-0.11	-0 6
11	-0.19	-0.60	-1.29	-1.68	-1.75	-1.70	-1.97	-1.57	-1.28	-0.75	-0.35	-0.11	-1.1
Noon.	-0.57	-1.05	-1.71	-2.13	-2.17	-2.11	-2.11	-2.04	-1.65	-1.14	-0.72	-0.32	-1.4
1	-0.83	-1.36	-1.74	-2.33	-2.35	-2.35	-2.25	-2.33	-1.56	-1.38	-0.84	-0.46	-1.6
2	-0.95	-1.44	-1.99	-2.28	-2.40	-2.42	-2.31	-2.16	-1.86	-1.42	-1.00	-0.50	-1.73
3	-0.95	-1.47	-1.94	-2.10	-2.28	-2.31	-2.13	-2.00	-1.72	-1.37	-0.94	-0.44	-1.6
4	-0.78	-1.20	-1.67	-1.91	-2.04	-2.09	-1.94	-1.76	-1.56	-1.13	-0.75	-0.32	-1.43
5	-0.50	-0.85	-1.17	-1.63	-1.73	-1.76	-1.65	-1.43	-1.24	-0.88	-0.45	-0.20	-1.15
6	-0.25	-0.45	-0.82	-1.13	-1.37	-1.48	-1.26	-1.02	-0.64	-0.50	-0.21	-0.10	-0.7
7	-0.15	-0.10	-0.29	-0.48	-0.76	-1.00	-0.81	-0.49	-0.28	-0.16	-0.04	-0.03	-0.38
8	-0.01	0.11	0.13	0.15	-0.23	-0.41	-0.22	0.12	0.19	0.06	0.07	0.01	0.0
9	0.15	0.30	0.44	0.70	0.48	0.27	0.33	0.66	0.52	0.21	0.22	0.12	0.3
10	0.23	0.37	0.64	1.07	1.02	0.97	0.99	0.96	0.76	0.30	0.29	0.19	0.63
11	0.31	0.48	0.84	1.28	1.57	1.46	1.38	1.19	0.90	0.95	0.43	0.22	0.9
Mean.	-1.39	-1.07	0.55	3.51	6.21	9.10	10.24	10.28	7.96	5.26	2.52	1.73	

ARCTIC AMERICA. — BOOTHIA FELIX. Lat. 69° 59' N. Long. 92° 1' W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Degrees of Reaumur.  Hours, Jan. Feb. March, April. May, June, July, Aug. Sept. Oct. Nov. Dec. Mean,													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.08	0.42	1.61	2.17	2.64	2.38	1.78	1.34	0.56	0.30	0.02	0.12	1.12
2	0.10	0.28	1.85	2.25	2.75	2.55	1.78	1.30	0.62	0.32	0.18	0.13	1.15
3	0.11	0.25	2.10	2.30	2.61	2.45	1.65	1.17	0.66	0.33	0.29	0.10	1.12
4	0.11	0.21	2.30	2.26	2.23	2.05	1.35	1.02	0.66		1	0.06	1
								1			1		
5	0.10	0.22	2.38	2.02	1.76	1.39	0.99	0.86	0.56	0.32	0.24	0.02	0.87
6	0.10		2.23	1.53		0.65	0.61	ł	0.46	1		-0.04	0.64
7	0.09	1	1.77	0.81	0.35		0.26	0.50	0.27	0.17		-0.07	0.37
71		1					1		1				
8	0.08	0.22	0.98	-0.06	-0.32	-0.58	-0.03	0.24	0.05	0.01	0.01	-0.10	0.04
9	0.06	0.05	-0.06	_0.08	0.05	0.00	_0.27	0.10	_0.19	0.20	-0.01	- 0.10	0.22
[1	0.00		-1.22										
10			l .	1			i	1	1		l .	1	
11		-0.58			1	ļ.		1					
Noon	-0.05	-0.87	-3.05	-2.86	-2.46	-2.02	-1.43	-1.16	-0.82	-0.69	-0.32	-0.12	-1.32
	.0.11	_1.00	_2 20	_9 00	_9.00	9 99	_1.70	_1.94	_0.09	_0.60	_0.20	_0.14	_1 477
1		-1.02	ì	1	i e		l .			Į.	-0.30	l .	
2		-0.98		ł			1	1					
3	)	-0.78			1	1							
4	-0.14	-0.46	-2.06	-2.18	-1.98	-1.98	-1.56	-1.18	-0.68	-0.18	0.06	-0.05	-1.03
5	-0.11	-0.14	-1.29	-1.50	-1.45	-1.36	-1.18	-1.01	-0.44	0.01	0.24	0.01	-0.69
6	-0.09	0.13	-0.57	-0.74	-0.88	-0.66	-0.78	-0.78	-0.17	0.14	0.31	0.07	-0.34
7	-0.06	0.32	0.01		-0.34			-0.50		0.22	0.36		-0.01
8	-0.05	0.43	0.44	0.78	0.20	0.51			0.26	0.25	0.38	0.11	0.27
	-0.05	0.40	0.44	0.10	0.20	0.51	0.07	0.10	0.20	0.20	0.00	0.11	0.27
9	-0.03	0.50	0.76	1.35	0.74	0.92	0.50	0.24	0.38	0.26	0.38	0.10	0.51
10	-0.02	0.51	0.99	1.74	1.28	1.26	0.90	0.66	0.44	0.26	0.35	0.10	0.71
11	0.02	0.52	1.19	1.95	1.82	1.63	1.20	1.01	0.48	0.26	0.28	0.09	0 37
Midn	0.05	0.49	1.38	2.08	2.30	2.04	1.59	1.25	0.51	0.28	0.15	0.12	1.02
Midn	0.03	0.45	1.00	2.00	2.30	2.04	1.55	1.20	0.51	0.25	0.15	0.12	1.02
6. 6	0.01	0.20	0.83	0.40	0.07	-0.01	_0.09	-0.01	0.15	0.21	0.09	0.02	0.15
7. 7	0.02	0.31	0.89	0.44		-0.03			0.18	0.20	0.17	0.02	0.18
8. 8													
11	0.02	0.33	0.71	0.36			0.02	0.04	0.16	0.13	0.20		0.16
9. 9	0.02	0.28	0.35	0.19			0.07	0.07	0.13	0.03			0.10
10.10	-0.00	0.13	-0.12	-0.04	-0.13	-0.04	0.10	0.09	0.01	-0.08	0.11	-0.00	0.00
7. 2. 9	_0.02	-0.06	-0.24	_0.2~	_0.50	_0.59	_0.97	_0.91	_0.10	-0.05	0.06	-0.03	_0.20
11			1										
6. 2. 8		-0.10										-0.02	
6. 2.10	,	-0.07		- 1				-0.01				-0.02	1
6. 2. 6	-0.04	-0.20	-0.53	-0.72	-0.84	-0.83	-0.68	-0.49	-0.22	-0.05	-0.00	-0.03	-0.39
7. 2	-0.09	_0.25	-0.75	_1.00	1.15	1.00	0.00	_0 44	0.24	0.00	_0.11	_0.10	-0.55
8. 2		-0.35	1	1	1	+							
[]		-0.38		- 1		- 1							
8. 1	1	-0.40		1				1				-0.12	-0.72
7. 1	-0.01	-0.37	-0.81	-1.11	-1.16	-1.19	-0.72	-0.42	-0.33	-0.26	-0.16	-0.11	-0.55
9.12.3.9	-0.04	-0.28	_1 90	_1.90	_1 25	_1.19	-0.77	-0.59	_0.25	_0.25	-0.01	_0.06	-0.61
7. 2.2(9)	-0.03							1					
1. 2.2(9)	-0.03	0.08	0.01	0.14	-0.21	-0.17	-0.15	-0.10	0.02	0.03	0.14	-0.00	-0.02
Dail. ext.	-0.02	-0.25	-0.50	-0.37	0.05	0.04	-0.04	-0.02	-0.11	-0.18	0.03	-0.01	-0.16
		0.20	0.00	0.01	0.00	0.04	0.04	0.02	0.14	0.10	0.00	0.01	0.10

N. AMERICA. — LAKE ATHABASCA. Lat. 59° N. Long. 111° W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Lefroy.

The corrections for April and May are derived from observations made at Fort Simpson, Lat. 620 N.

Degrees of Fabrenheit.

Hour.	April.	May.	October.	November.	December.	January.	February.
daily ext.	1.58	1.71	0.33	0.25	-0.17	0.77	1.19
6, 6	1.15	0.51	1.07	0.59	0.27	0.84	1.19
7, 7	1.50	0.16	0.76	0.54	0.30	0.58	1.31
8,8	1.72	0.18	0.69	0.55	0.62	0.95	1.27
9, 9	0.54	0.30	0.37	0.32	0.84	0.80	0.78
10, 10	-0.43	-0.08	-0.32	-0.06	0.34	0.12	0.31
11, 11	-1.68	-1.20	-0.57	-0.37	0.10	-0.62	-0.23
6, 2, 10	0.47	0.46	-0.31	-0.21	-0.22	-0.17	-0.05
7, 3, 11	0.46	0.59	-0.40	-0.16	0 17	0.06	-0.26
Mean.	32.48	44.56	21.44	9.76	0.40	-23.00	4.79

#### XIV.

Arctic America. — Melville Island. Lat. 74° 47' N. Long. 110° 48' W. Gr. — Dove.

Degrees of Reaumur.

			8				
Hour.	January.	February.	March.	October.	Hour.	November.	December.
A.M. 1	0.12	0.10	1.04	0.04	A.M. 2	-0.12	-0.09
3	0.18	0.05	1.22	0.12	4	-0.02	-0.06
5	0.07	0.25	0.90	0.24	6	0.00	0.11
7	0.11	0.29	0.57	0.20	8	-0.22	0.07
9	-0.13	-0.24	0.29	-0.15	10	-0.38	0.11
11	-0.35	-0.43	-1.33	-0.46	12	-0.41	0.24
P.M. 1	-0.22	-0.65	-1.72	-0.43	P.M. 2	-0.27	0.14
. 3	-0.25	-0.52	-1.00	0.22	-1	0.16	0.00
5	0.04	0.04	-0.43	-0.24	6	0.27	-0.12
7	0.04	0.24	0.06	-0.10	8	0.38	-0.26
9	0.11	0.35	0.33	0.11	10	0.36	-0.12
11	0.40	0.49	0.66	0.43	12	0.25	0.00
Mean.	-29.75	-27.58	-22.73	-14 32	Mean.	-18.65	-25.75

### XV.

Spitzbergen. — Hecla Cove. Lat. 79° 55′ N. Long. 16° 49′ E. Gr. — Dove.

Degrees of Reaumur.

Hour.	June.	July.	August.	Hour.	June.	July.	August.
A.M. 1	0.63	0.62	0.42	P.M. 1	-0.67	-0.67	-0.63
3	0.43	0.84	0.54	3	-0.58	-0.42	-0.58
5	0.26	0.51	0.53	5	-0.27	-0.44	-0.32
7	-0.12	-0.02	0.25	7	0.26	-0.17	-0.06
9	-0.29	-0.09	-0.09	9	0.21	0.06	0.14
11	-0.47	-0.49	-0.45	11	0.61	0.26	0.24
				Mean.	1.71	3.63	2.84

S. America. — Rio Janeiro. Lat. 22° 54′ S. Long. 43° 16′ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Hours, Jan. Feb. March. April. May. June. July. Aug. Sept. Oct. Nov. Dec. Mean.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.74	1.51	1.80	0.90	1.13	0.56	1.85	1.31	1.04	0.97	1.76	1	1.24
2	1.64	2.41	2.48	1.64	2.12	1.53	2.75	2.00	1.69	1.64	2.32	2.05	2.03
3	2.50	3.11	3.02	2.32	2.93	2.43	3.47	2.66	2.27	2.21	2.75	2.66	2.70
4	3.08	3.90	3.24	2.79	3.38	3.04	3.87	3.04	2.59	2.50	2.93	2.99	3.06
5	3.22	3.29	3.15	2.90	3.40	3.29	3.83	3.08	2.66	2.52	2 79	2.99	3.08
6	2.93	2.84	2.75	2.75	3.06	3.20	3.47	2.79	2.41	2.27	2.32	2.68	2.79
7	2.30	2.21	2.14	2.30	2.48	2.84	2.70	2.25	2.00	1.82	1.67	2.12	2.23
8	1.49	1.49	1.40	1.71	1.85	2.39	1.96	1.60	1.46	1.28	0.90	1.40	1.58
9	0.68	0.72	0.59	1.04	1.15	1.82	1.15	0.90	0.86	0.68	0.14	0.59	0.86
10	}	-0.05		0.32		1.13		1	i		-0.56		1
11	-0.77		-1.01	-0.45	-0.23	0.32				-0.59		-1.04	
1	l .	-1.64			-0.23 -0.99		-1.31	1	1		-1.80	l .	1
Noon.													
1		-2.30						-1.91					
2		-2.75											
3	-2.59	-2.88	-2.84	-2.66	-2.66								
4	-2.45	-2.70	-2.77	-2.57	<b>-2.7</b> 5	-3.04	-3.60	-2.93	-2.36	-2.12	-2.66	-2.59	-2.70
5	-2 05	-2.30	-2.50	-2.21	-2.54	-2.75	-3.47	-2.68	-2.00	-1.78	-2.25	-2.09	-2.39
6		-1.82											
7		-1.40											
8		-1.13											
9	-0.59	-0.92	-0.77	-0.72	-1.44	-1.26	-1.22	-0.70	-0.61	-0.61	-0.14	-0.38	-0.79
0		-0.63						-0.32	-0.41	-0.45	0.23	-0.16	-0.50
11	-0.41	-0.14				-0.86			-0.09		0.65	0.14	0.09
Midn	0.00		1.06	0.23		-0.29			0.38		1.15		0.47
				0.20		0.20							
6. 6	0.72	0.52	0.32	0.50	0.43	0.50	0.30	0.29	0.43	0.45	0.34	0.61	0.45
7. 7	0.63	0.41	0.25	0.52	0.29	0.54	0.16	0.29	0.45	0.41	0.29	0.56	0.41
8.8	0.38	0.18	0.09	0.38	0.09	0.50		0.25	0.32	0.27	0.16	0.41	0.25
9. 9	1	-0.11		-0.16			-0.05	0.11	0.14	0.05	0.00	0.11	0.05
10.10	-0.32	-0.34	-0.25	-0.11	-0.32	0.00	-0.14	-0.05	-0.11	-0.20	-0.18	-0.20	-0.18
7. 2. 9		-0.50											
6. 2. 8		-0.34						-0.32 -0.27					
6. 2.10		-0.34 -0.18	- 1										
6. 2. 6	-0.34	-0.59	-0.68	-0.47	-0.47	-0.50	-0.81	-0.63	-0.50	-0.43	-0.68	-0.54	-0.56
7. 2	1	-0.27						-0.11					
8. 2		-0.63		1				-0.45					
8. 1		-0.65						-0.16					
7. 1	0.16	-0.05	-0.09	0.18	0.38	0 59	-0.27	0.18	0.07	0.02	-0.34	-0.16	-0.11
9.12.3.9		-1.19								-0.86	-1.15	-1.13	-1.01
7. 2.2(9)		-0.61					-0.65	-0.41	-0.38	-0.38	-0.32	-0.36	-0.47
Dail. ext.	0.32	0.27	0.20	0.14	0.34	0.14	0.14	0.09	0.09	0.14	0.07	0.07	0.16

### XVII.

S. America. — Rio Janeiro. Lat. 22° 54' S. Long. 43° 16' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

						Degre	es of Re	eaumur.						
	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Morn. 1	0.33	0.67	0.80	0.40	0.50	0.25	0.82	0.58	0.46	0.43			0.55
	2	0.73	1.07	1.10	0.73	0.94	0.68	1.22	0.89	0.75	0.73			0.90
	3	1.11	1.38	1.34	1.03	1.30	1.08	1.54	1.18	1 01	0.98	1.22	1.18	1.20
	4	1.37	1.51	1.44	1.24	1.50	1.35	1.72	1.35	1.15	1.11	1.30	1.33	1.36
	5	1.43	1.46	1.40	1.29	1.51	1.46	1.70	1.37	1.18	1.12	1.24	1.33	1.37
1	6	1.30	1.26	1.22	1.22	1.36	1.42	1.54	1.24	1.07	1.01	1.03	1.19	1.24
	7	1.02	0.98	0.95	1.02	1.10	1.26	1.20	1.00	0.89	0.81	0.74	0.94	0.99
	8	0.66	0.66	0.62	0.76	0.82	1.06	0.87	0.71	0.65	0.57	0.40	0.62	0.70
	9	0.30	0.32	0.26	0.46	0.51	0.81	0.51	0.40	0.38	0.30	0.06	0.26	0.38
	10	-0.03	-0.02	-0.10	0.14	0.22	0.50	0.14	0.10	0.08	0.02	-0.25	-0.10	0.06
1	11	-0.34	-0.38	-0.45	-0.20	-0.10	0.14	-0.22	-0.22	-0.24	-0.26	-0.54	-0.46	-0.27
	Noon	-0.62	-0.73	-0.76	-0.54	-0.44	-0.29	-0.58	-0.53	-0.56	-0.54	-0.80	-0.81	-0.60
	1	-0.89	-1.02	-1.02	-0.86	-0.76	-0.74	-0.96	-0.85	-0.84	-0.79	-1.03	-1.08	-0.90
	2	1							-1.10		1	i i	t .	-1.12
۱	3		1					1		i .	1		-1.27	
	4											1	-1.15	
	5	_0 01	_1.02	_1 11	_0.08	_1 19	_1 99	_1.54	_1 10	_0.80	_0.70	_1 00	-0.93	_1.06
1	6	1									i	1	-0.66	
1	7								1			l .	-0.44	1 1
1	8	1										l .	-0.27	
1	0	0.02	0.00	-0.04	0.42	-0.14	0.05	0.02	-0.50	0.07	0.04	0.20	0.21	0.40
	9	-0.26	-0.41	-0.34	-0.32	-0.64	-0.56	-0.54	-0.31	-0.27	-0.27	-0.06	-0.17	-0.35
	10	-0.25	-0.28	-0.11	-0.23	-0.50	-0.50	-0.26	-0.14	-0.18	-0.20	0.10	-0.07	-0.22
	11	-0.18	-0.06	0.16	-0.11	-0.28	-0.38	0.04	-0.04	-0.04	-0.07	0.29	0.06	-0.04
	Midn	0.00	0.26	0.47	0.10	0.06	-0.13	0.41	0.27	0.17	0.14	0.51	0.29	0.21
Ì														
	6. 6	0.32	0.23	0.14	0.22	0.19	0.22	0.10	0.13	0.19	0.20	0.15	0 27	0.20
	7. 7	0.28	0.18	0.11	0.23	0.13	0.24	0.07	0.13	0.20	0.18	0.13	0.25	0.18
İ	8. 8	0.17	0.08	0.04	0.17	0.04	0.22	0.03	0.11	0.14	0.12	0.07	0.18	0.11
	9. 9	0.02	-0.05	-0.04	0.07	-0.07	0.13	-0.02	0.05	0.06	0.02	-0.00	0.05	0.02
	10.10	-0.14	-0.15	-0.11	-0.05	-0.14	-0.00	-0.06	-0.02	-0.05	-0.09	-0.08	-0.09	-0.08
	7. 2. 9	-0.10	-0.22	-0.19	-0.12	-0.19	-0.13	-0.21	-0.14	-0.14	-0.14	-0.17	-0.16	-0.16
	6. 2. 8	-0.03	-0.15	-0.17	-0.09	-0.13	-0.10	-0.19	-0.12	-0.11	-0.10	-0.14	-0.11	-0.12
	6. 2.10	-0.01	-0.08	-0.02	-0.03	-0.05	-0.06	-0.00	-0.00	-0.05	-0.05	-0.02	-0.04	-0.03
-	6. 2. 6												-0.24	
	7. 2	-0.03	-0.12	-0.12	-0.03	0.04	0.08	-0.04	-0.05	-0.08	-0.08	-0.22	-0.16	-0.07
-	8. 2		-0.28		-0.16								-0.32	
	8. 1	-0.12	-0.18	-0.20	-0.05	0.03	0.16	-0.05	-0.07	-0.10	-0.11	-0.32	-0.23	-0.10
-	7. 1	0.07	-0.02	-0.04	0 08	0.17	0.26					-0.15		0.05
-	9.12.3.9	-0.12	-0.59	_0.59	-0.40	-0.11	_0.24	-0.59	_0 (2	-0.20	_0.30	_0.51	-0.50	-0.45
	7. 2.2(9)	1											-0.36	- 6
	Dail.ext.	0.14	0.12	0.09	0.06	0.15	0.06	0.06	0.04	0.04	0.06	0.03	0.03	0.07
1	Dan. ext.	0.14	0.12	0.03	0.00	0.13	0.00	0.00	0.04	0.04	0.00	0.03	0.03	0.07

N. America. — Amherst College. — Lat. 42° 22' N. Long. 72° 30' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dewey.

Degrees of Fahrenheit.

Degrees of Fahrenheit.													
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Morn. 1	3.90	2.78	4.73	6.23	5.51	6.64	6.39	5.14	5.36	4.87	2.34	1.63	4.63
2	4.24	3.03	4.81	6.69	6.48	7.28	6.83	5.66	6.12	5.65	2.99	2.20	5.16
3	4.13	3.20	5.36	7.42	7.41	7.92	7.28	6.03	6.92	6.46	3.49	2.55	5.68
4	4.50	3.94	5.69	7.85	7.88	8.04	7.42	6.29	6.56	7.09	3.72	2.70	6.06
5	4.72	4.20	6.04	8.12	8.18	7.80	7.54	6.66	7.88	7.72	4.03	3.32	6.35
6	4.68	4.78	6.12	7.77	6.77	5.96	6.02	5.81	7.44	7.65	4.34	3.78	5.93
7 8	4.75	4.78	4.62	5.97	4.22	4.20	3.80	4.48	5.32	6.87	4.28	3.97	4.77
	3.83	3.78	2.08	3.04	1.62	1.40	1.09	1.96	2.52	4.31	2.68	4.13	2.70
9	1.46	1.45	-0.46	0.08	-0.60	-0.88	-0.87	-0.93	-0.56	0.83	0.34	2.40	0.19
	1	-0.85	-2.57	- 2.69		-3.12	-3.80	-3.04	-3.32	-2.24	-1.43	-0.55	11
\$ II	1	-2.72	-4.77	- 5.65	-5.12	-5.68	-6.43	-5.45	-6.04	-5.02	-3.01	-2.76	-4.73
Noon.	-6.32	-4.26	-6.38	<b>- 7.</b> 92	-6.75	-8.08	-8.50	-6.86	-8.16	-7.06	-5.01	-4.30	-6.63
	- 1	-5.35	-7.65	- 9.46		-9.36	-8.83	-8.23	-9.12	-8.24	-6.12	-6.14	-7.84
}		-6.06	-8.34	-10.42		-9.00		-7.86	1		1	-6.30	-8.26
1 11	1	-5.80	-8.11	- 9.81	-8.27	-8.60	-7.50	-7.67	-9.20	-9.24	-5.28	-5.60	-7.70
4 -	-5.84	-4.89	-7.23	- 8.61	-7.86	-7.84	-7.17	-6.23	-8.40	-8.24	-3.85	-3.76	-6.66
5 -	-3.32	-3.10	-5.65	- 7.04	-5.97	-6.00	-5.83	-5.26	-6.44	-5.65	-2.28	-2.03	-4.88
	- 1	-1.18	-3.46	- 4.50	-4.08	-4.20	-4.17	-2.82	-3.52		-0.85	-0.68	
7	0.24	-1.05	0.17	- 1.69	-2.38	-1.92	-1.54	-1.44	-1.47	-1.24	-0.64	-0.31	-1.11
8	0.64	-0.43	0.93	0.27	-0.19	0.04	0.98	0.33	0.11	0.13	0.08	0.20	0.26
								}					
1	1.50	0.28	1.89	1.77	1.66	1.96	3.05	1.59	1.99	1.16	0.80	0.69	1.53
10	2.01	0.57	3.29	3.31	2.73	3.20	3.79	3.02	3.53	1.90	1.16	1.20	2.48
	2.42	1.19	4.29	4.23	3.99	4.20	4.24	3.79	4.61	3.24	1.96	1.58	3.31
Midnight.	2.50	1.70	4.85	4.92	4.75	5.48	5.31	4.52	5.34	4.09	2.40	1.98	3.99
3, 9, 3, 9	-0.05	-0.22	-0.08	- 0.13	0.05	0.10	0.49	0.26	-0.21	-0.20	-0.16	-0.01	-0.01
	1.48	0.87	0.72	0.93	0.53	0.54	1.09	0.33	0.72	1.00	0.57	1.55	0.86
1 1	0.38	-0.14	0.36	0.31	0.81	0.04	0.00	-0.51	0.11	-0.17	-0.13	0.33	0.12
7, 2, 9	-0.48	-0.33	-0.61	- 0.89	-0.96	-0.95	-0.88	-0.60	-0.83	-0.42	-0.29	-0.55	-0.65
, , ,		-0.24	0.36	- 0.24	0.25	0.05	0.10	0.32	0.39	0.09	-0.16	-0.44	0.01
' '		-0.04	-0.14	- 0.38	-0.60	-0.53	-0.64	-0.12	-0.32	-0.17	-0.18	-0.38	-0.32
6664	0.21	-0.03	0.19	- 0.07	-0.18	-0.20	-0.49	0.14	0.04	0.28	0.09	-0.25	-0.07
	-0.09 -0.01	0.02 -0.18	0.13	0.00 - 0.23	-0.12 $-0.30$	-0.13 -0.22	-0.08	$0.20 \\ -0.05$	0.11 -0.12	0.07 $-0.02$	0.13 -0.02	0.17	0.03 $-0.11$
	0.01	-0.13	0.01	- 0.23	-0.30	-0.22	0.10	-0.03	-0.12	-0.02	-0.02	-0.24	-0.11
Mean. 2	22.94	28.57	34.81	48.54	56.92	61.60	71.61	67.44	59.80	50.46	34.80	29.28	47.23

The numbers without sign must be added; those with the sign — must be subtracted.

The above Table has been derived from one year of hourly observations made at Amherst College, Massachusetts, in 1839, under the direction of Professor Snell, and communicated by Professor Chester Dewey. It gives the simple differences of the monthly means of each hour from the monthly means of the twenty-four hours which are found in the last line.

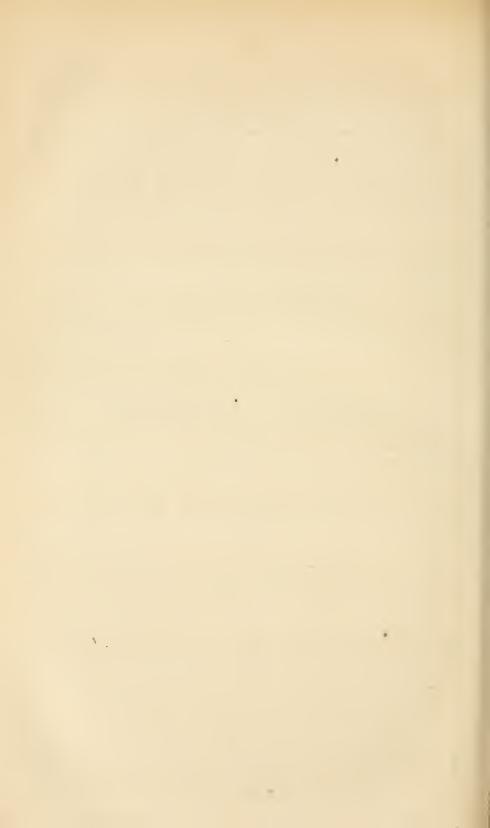
# HOURLY CORRECTIONS

FOR

# PERIODIC VARIATIONS.

ASIA.

E



### XVIII.

India. — Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Degrees of Fahrenheit.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	4.41	4.03	3.80	3.85	3.26	2.66	0.41	2.88	2.99	3.06	3.33	4.25	3.42
13	4.41	1	į.	1	1		1	1					
2 3	5.13	4.95	4.64	4.46	3.80	3.02	2.75	3.24	3.44	3.44	3.83	4.86	3.96
II .	6.03	6.12	5.67	5.15	4.39	3.47	3.17	3.74	3.98	3.92	4.46	5.67	4.66
4	6.95	7.31	6.64	5.74	4.82	3.80	3.58	4.21	4.48	4.34	5.04	6.50	5.29
5	7.56	8.15	7.13	5.81	4.82	3.83	3.76	4.41	4.61	4.46	5.22	6.93	5.56
6	7.34	8.01	6.73	5.11	4.14	3.35	3.49	4.07	4.14	4.01	4.73	6.57	5.15
7	6.01	6.59	5.20	3.53	2.81	2.34	2.68	3.06	3.02	2.88	3.40	5.11	3.89
8	3.56	3.92	2.66	1.22	0.95	0.90	1.35	1.49	1.26	1.13	1.40	2.70	1.87
9	0.41	0.50	-0.47	-1 42	_1 19	-0.71	_0.27	-0.45	-0.81	-0.99	-0.92	_0.29	-0.54
10	-2.84		-3.53					-2.41				1	
11	-5.51		-5.94	-5.76	i .	-3.53		-4.05				-5.58	-4.84
Noon	-7.25	i I	-7.36			1		-5.18					-6.01
TOOH	-7.23	-1.00	-1.50	-0.02	-9.55	-4.04	-4.02	-3.10	-3.34	02	-5.07	7.00	-0.01
1	1	-8.17						l	l .				-6.41
2	-7.76	<b>-7.</b> 83	<b>-7.</b> 22	)				-5.60					-6.14
3	-7.09	-6.98	-6.26					-5.04					-5.45
4	-6.17	-5.99	-5.06	-4.46	-3.94	-3.47	-3.51	-4.10	-3.80	-3.53	-4.12	-5.67	-4.48
5	_5.15	-4.88	-3.83	-3.11	-2.88	-2.52	-2.52	-2.90	-2.59	-2.32	-3.15	-4.61	-8.38
6		-3.74		-1.71				-1.58		1			-2.16
7		-2.45		-0.34		-0.32			-0.11	0.00			-0.90
8		-1.04		0.92	0.63	0.70	0.68	0.90	0.92	0.97	1	-0.32	0.32
9	0.68	0.38	1.06	1.91	1.53	1.46	1.40	1.76	1.69	1.71	1.42	1.19	1.35
10	2.05	1.64	1.96	2.61	2.16	1.96	1.85	2.30	2.18	2.25	2.21	2.43	2.14
11	3.08	2.57	2.63	3.06	2.57	2.23	2.09	2.54	2.48	2.57	2.68	3.26	2.66
Midn	3.83	3.31	3.17	3.42	2.88	2.41	2.23	2.68	2.70	2.81	2.99	3.80	3.02
6. 6	1.71	2.14	2.09	1.71	1.24	0.97	1.04	1.24	1.42	1.46	1.35	1.60	1.51
7. 7	1.76	2.07	1.96	1.60	1.17	1.01	1.19	1.40	1.44	1.44	1.28	1.62	1.49
8.8	1.33	1.44	1.31	1.06	0.79	0.79	1.01	1.19	1.08	1.06	0.88	1.19	1.10
9. 9	0.54	0.43	0.29	0.25	0.20	0.36	0.56	0.65	0.43	0.36	0.25	0.45	0.41
10.10	-0.41	-0.65	-0.79	-0.63		-0.18		-0.07	-0.34	-0.41	-0.45	-0.40	-0.41
7. 2. 9	-0.36	-0.29	-0.32	-0.38	-0.34	-0.27	-0.23	-0.27	-0.29	-0.32	-0.27	-0.32	-0.32
6. 2. 8	-0.45	-0.29	-0.18	-0.18				-0.20	-0.18	<b>-0.1</b> S	-0.16	-0.34	-0.23
6. 2.10	0.54	0.61	0.50	0.38	0.32	0.23	0.18	0.25	0.25	0.25	0.45	0.59	0.38
6. 2. 6	-1.44	-1.19	-1.01	-1.06	-0.97	-0.90	-0.90	-1.04	-0.92	-0.88	-0.97	-1.35	-1.06
7. 2	_0.99	-0.63	-1.01	_1 59	_1 28	-1.15	_1.06	_1.28	_1 31	-1.32	-1.10	-1.08	-1.13
8. 2		-1.96											
8. 1	1	-2.14		l .		1	1	1		į.	i e		-2.27
7. 1		-0.79											-1.26
				1	2.30								
9.12.3.9	-3.31	-3.42	-3.26	-2.99	-2.43	-1.96	-1.87	-2.23	-2.39	-2.41	-2.54	-3.17	-2.66
7. 2.2(9)	-0.11	-0.11	0.02	0.20	0.14	0.16	0.18	0.25	0.20	0.20	0.16	0.07	0.11
	L			<u> </u>	l	I	1	1	l			I	

#### XIX.

India. — Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degre	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.96	1.79	1.69	1.71	1.45	1.18	1.07	1.28	1.33	1.36	1.48	1.89	1.52
2	2.28	2.20	2.06	1.98	1.69	1.34	1.22	1.44	1.53	1.53	1.70	2.16	1.76
3	2.68	2.72	2.52	2.29	1.95	1.54	1.41	1.66	1.77	1.74	1.98	2.52	2.07
4	3.09	3.25	2.95	2.55	2.14	1.69	1.59	1.87	1.90	1.93	2.24	2.89	2.35
5	3.36	3.62	3.17		1	1.70		1.96	2.05			(	1
6	3.26	3.56	1			1.49		1.81	1.84	1.78	2.10		1
7	2.67	2.93	2.31	1.57	1	1.04	1.19	1.36	1.34	1.28	1.51	2.27	1.73
8	1.58	1.74	1.18	0.54	0.42	0.40	0.60	0.66	0.56	0.50	0.62	1.20	0.83
9	0.18	0.22									-0.41		
10	}.				1	1				1	-1.38		
11					1					1	-2.11		
Noon	-3.22	-3.37	-3.27	-3.03	-2.37	-1.93	-1.92	-2.30	-2.46	-2.54	-2.52	-3.11	-2.67
1	-3.52	-3.63	-3.43	-3.13	-2.49	-2.08	-2.13	-2.53	-2.61	-2.64	-2.62	-3.33	-2.85
2	-3.45	-3.48	-3.21	-2.93	-2.39	-2.05	-2.12	-2.49	-2.49	-2.46	-2.49	-3.22	-2.73
3	-3.15	-3.10	-2.78	-2.51	-2.13	-1.86	-1.91	-2.24	-2.16	-2.07	-2.20	-2.92	-2.42
4			1		1					J	-1.83		
5	1 1	-2.17								ł	-1.40		1
6	-1.74	-1.66	-1.14	-0.76	-0.75	-0.63	-0.62	-0.70	-0.58	-0.49	-0.90	-1.49	-0.96
7	-1.11	-1.09	-0.58	-0.15	-0.22	-0.14	-0.13	-0.12	-0.05	0.00	-0.36	-0.84	-0.40
8	-0.41	-0.46	-0.03	0.41	0.28	0.31	0.30	0.40	0.41	0.43	0.17	-0.14	0.14
9	0.30	0.17	0.47	0.85	ł I	0.65	0.62	0.78	0.75		0.63	0.53	0.60
10	0.91	0 73	0.87	1.16	0.96	0.87	0.82	1.02	0.97	1.00	0.98	1.08	0.95
11	1.37	1.14	1.17	1.36	1.14	0.99	0.93	1.13	1.10	1.14	1.19	1.45	1.18
Midn	1.70	1.47	1.41	1.52	1.28	1.07	0.99	1.19	1.20	1.25	1.33	1.69	1.34
6. 6	0.76	0.95	0.93	0.76	1	0.43	0.46	0.55	0.63	0.65	0.60	0.71	0.67
7. 7	0.78	0 92	0.87	0.71	0.52	0.45	0.53	0.62	0.64	0.64	0.57	0.72	0.66
8.8	0.59	0-64	0.58	0.47	0.35	0.35	0.45	0.53	0.48	0.47	0.39	0.53	0.49
9. 9	0.24	0.19	0.13	0.11	0.09	0.16	0.25	0.29	0.19	0.16	0.11	0.20	0.18
10.10	-0.18	-0.29	-0.35	-0.28	-0.20	-0.08	-0.01	-0.03	-0.15	-0.18	-0.20	-0.18	-0.18
7. 2. 9	-0.16	-0.13	-0.14	-0.17	-0.15	-0.12	-0.10	-0.12	-0.13	-0.14	-0.12	-0.14	-0.14
6. 2. 8	-0.20	-0.13	-0.08	-0.08	-0.09	-0.08	-0.09	-0.09	-0.08	-0.08	-0.07	-0.15	-0.10
6. 2.10	0 24	0.27	0.22	0.17	0.14	0.10	0.08	0.11	0.11	0.11	0.20	0.26	0.17
6. 2. 6	1		1		-0.43	- 1	1	-0.46			-0.43		
7. 2	-0.39												
11											-0.49		
8. 2		1					1	1			-0.94		11
8. 1	-0.97		1	- 1	1					j	-1.00		
7. 1	-0.43	-0.35	-0.56	-0.78	-0.62	-0.52	-0.47	-0.59	-0.64	-0.68	-0.56	-0.53	-0.56
9.12.3.9	-1.47	-1.52	-1.45	-1.33	-1.08	-0.87	-0.83	-0.99	-1.06	-1.07	-1.13	-1.41	-1.18
7. 2.2(9)	-0.05		0.01	0.09	0.06	0.07	0.08	0.11	0.09	0.09	0.07	0.03	0.05
											- 1	1	- 11

# India. - Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

							ahrenhe						
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	2.05	2.54	2.25	3.65	2.74	3.03	2.90	2.86	2.34	1.84	2.05	1.89	2.50
1	2.54	1	2.23		3.31	3.50		3.01	2.70	2.27	1	2.25	2.87
2	2.96	1	3.60	3.57	3.72	3.86	3.55	3.39	3.10	2.79	3.03	2.63	3 35
3	3.33		4.25	4.07	4.07	4.27	3.93	3.69	3.55	3.12	3.50	2.96	3.77
	0.00	- 00	4 70				4.07	0.00					
5	3.62	5.06	4.79	4.40	4.45	4.68	4.31	3.98	3.95	3.46	3.91	3.19	4.15
6	3.81	5.49	5.24 5.11	4.45 3.78	4.68 3.86	4.95 4.21	4.31	4.34	4.23 3.82	3.71	4.23	3.60	4.45
7	2.43	3.33	2.54	1.78	2.07	2.51	2.92	2.79	2.43	1.80	2.00	2.38	2.41
	2.40	0.00	2.04	1	2.0.	2.01	1.02	2	2.40	1.00	2.00	2.00	2.41
8	-0.04	0.29		-0.18		0.38	1.06	0.99	0.72	1	-0.56	0.00	0.23
9		-1.93						-0.90		-1.26	1	-1.73	-1.72
10	il .	-3.60			-4.68	-3.67	-2.67	-2.74	-2.96	-2.34		-3.05	
11	-4.02	-4.81	-4.81	<b>-4.</b> S3	-5.75	-5.02	-4.25	-4.16	-4.54	-3.17	-4.09	-3.62	-4.42
Noon.	-4.43	-5.06	-5.35	-5.66	-5.87	-5.85	-5.51	-5.28	-5.04	-3.76	-4.31	-3.93	-5.01
1	-4.40	-5.35	-5.42	-5.53	-5.64	-6.05	-6.07	-5.75	-5.04	-3.73	-4.25	-3.86	-5.09
2		-5.30			-4.99		-6.02	-5.40	-4.66		-3.73	-3.60	-4.75
3	-3.46	-4.85	-4.27	-4.07	-4.00	-4.61	-4.92	-4.59	<b>-3.7</b> 3	-3.03	-3.05	-2.88	-3.95
4	-2.41	-3.64	-3.10	-2.65	-2.45	-3.57	-3.73	-3.44	-2.56	-2.38	-1.98	-2.04	-2.83
5	-1.19	-2.27	-1.66	-1.03	-1.01	-1.91	-2.18	-1.84	-1.44	-1.26	-0.88	-1.01	-1.47
6	-0.38	-1.10	-0.52	0.20	0.11	-0.58	-0.81	-0.70	-0.52	-0.63	-0.25	-0.38	-0.46
7	0.09	-0.36	0.17	0.83	0.76	0.36	0.16	0.13	0.07	-0.18	0.09	0.00	0.18
			]										
8	0.54	0.27	0.58	0.99	1.19	0.97	0.83	0.74	0.47	0.16	0.47	0.34	0.63
9	0.94	0.81	0.97	1.57	1.57	1.42	1.35	1.17	0.99	0.49	0.74	0.67	1.06
10	1.39	1.33	1.39	1.89	1.96	2.11	1.87	1.64	1.39	0.90	1.08	1.03	1.50
11	1.84	1.87	1.84	2.25	2.34	2.41	2.29	2.14	1.89	1.28	1.46	1.44	1.92
		2.25	2.26	- 00	7.00	7.05	1 45	7.05	7.05	7.00	7.00	7 07	
6, 6	1.83	2.27	2.29	1.99	1.98	1.81	1.75	1.65	1.65	1.32	1.90	1.67	1.84
7, 7	1.26	1.48	1.35 0.37	1.30	0.54	1.43 0.67	1.54 0.94	1.46	1.25	0.81	1.04	1.19	1.29
8, 8	0.25 $-0.54$	$0.28 \\ -0.56$	-0.46	0.40 $-0.42$	-0.43	-0.15	0.94	$0.81 \\ 0.13$	0.59 -0.06		-0.04 $-0.87$	$0.17 \\ -0.53$	0.43 -0.33
9, 9	-0.54	0.50	0.40	0.42	0.40	0.19	0.29	0.10	0.00	0.00	0.01	0.00	0.00
	0.00				7.00	0.70	0.40	0 75	0 ==0	0.70	1.00		0.05
10, 10		-1.13						-0.55					-0.93
7, 1	!	-1.01		,	-1.78	-1.77	-1.57		)	-0.86		-0.74	-1.33
7, 2, 9	-0.26 $0.43$	0.39	0.49	-0.53 $0.24$	$-0.45 \\ 0.28$	$-0.59 \\ 0.21$	-0.58 0.05	-0.48 0.10	-0.41 0.18	$\begin{array}{c} -0.42 \\ 0.21 \end{array}$	$-0.33 \\ 0.47$	-0.18 $0.39$	0.30
6, 2, 10	0.43		0.50	0.24	0.20	0.21		-0.10			0.47		
Mean.	76.77	78.25	82.24	85.73	87.10	87.01	86.22	84.51	83.50	81.18	78.53	76.75	

### XXI.

# India. - Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
						-							
Morn. 1	1.41	1.22	1.32	1.06	1.26	1.15				1		i .	1.17
2	1.79	1.64	1.42	1.36	1.59	1.42	1.09	1	1	1.46	1.32	1	1.46
3	2.14	2.10	1.50	1.76	1.94	1.70	1.26			1.70			1.73
4	2.38	2.42	1.58	2.10	2.17	1.90	1.42	1.66	1.70	1.88	1.90	1.93	1.92
5	2.42	2.43	1.61	2.20	2.18	1.95	1.42	1.45	1.62	1.88	2.02	2.17	1.95
6	2.22	2.05	1.48	1.91	1.86	1.77	1.33	1.10		1.64	1.81	2.25	1.73
7	1.76	1.30	1.14	1.24	1.19	1.30	1.12	0.75	1.02	1.14	1.27	2.00	1.27
8	1.05	0.36	0.54	0.30	0.27	0.70	0.78	0.46	0.47	0.40	0.50	1.32	0.60
9	0.15	-0.59	-0.23	-0.71	-0.75	-0.06	0.35	0.16	-0.23	-0.46	-0.35	0.27	-0.20
10	-0.82		1					-0.18	1	5		-0.94	
11	i	-1.94						-0.62					
Noon	1	-2.23			1		f	6		1		-2.76	)
1	-2.90	-2.34	-2.10	-2.34	-2.48	-2.20	-2.13	-1.57	-2.47	-2.17	-2.25	-2.98	-2.33
2		-2.30							1				ł I
3		-2.12						1	ĺ				
4	1	-1.81						-1.43	ì	\$		-1.65	
5	-1.47	-1.34	-0.83	-1.00	-0.65	-1.28	-1.44	-0.94	-0.50	-0.70	-1.10	-1.13	-1.03
6	-0.81	-0.78	-0.58					-0.46				-0.72	
7	-0.26			0.04	0.02			-0.14	0.18	Į.		-0.39	-0.13
8	0.13			0.49	0.26	0.12		-0.04	0.27	0.06	1	-0.06	
9	0.38	0.62	0.42	0.71	0.45	0.42	0.86	-0.06	0.33	0.26	0.64	0.30	0.44
10	0.58	0.77	0.60	0.90	0.61	0.63	0.91	-0.06	0.44	0.46	0.81	0.66	0.61
11	0.79	0.84	0.91	0.91	0.78	0.79	0.87		0.66	0.67	0.83	0.99	0.76
Midn	1.06	0.96	1.16	0.92	0.98	0.94	0.84	0.47	0.95	0.91	0.89	1.22	0.94
6. 6	0.71	0.64	0.45	0.72	0.80	0.50	0.34	0.32	0.67	0.63	0 62	0.77	0.60
7. 7	0.75	0.56	0.40	0.64	0.61	0.50	0.60	0.31	0.60	0.50	0.57	0.81	0.57
8. 8	0.59	0.33	0.23	0.40	0.27	0.41	0.70	0.21	0.37	0.23	0.43	0.63	0 40
9. 9	0.27	0.02	0.10	-0.00	-0.15	0.18	0.61	0.05	0.05	-0.10	0.15	0.29	0.12
10.10	-0.12	-0.31	-0.22	-0.33	-0.53	-0.10	-0.35	-0.12	-0.29	-0.40	-0.15	-0.14	-0.20
7. 2. 9	-0.28	-0.13	-0.11	-0.06	-0.16	-0.17	-0.16	-0.38	-0.31	-0.17	-0.09	-0.15	-0.18
6. 2. 8	-0.21	0.02	-0.16	0.09				-0.25			-0.01	-0.19	-0.11
6. 2.10	-0.06	0.17	0.07	0.22	0.11	0.05	<b>-0.0</b> 8	-0.26	-0.15	0.06	0.15	0.05	0.03
6. 2. 6	-0.52	-0.34	-0.33	-0.24	-0.18	-0.42	-0.60	-0.39	-0.31	-0.22	-0.32	-0.41	-0.36
7. 2	-0.61	-0.50	-0.37	-0.45	-0.47	-0.47	-0.68	-0.54	-0.63	-0.32	-0.46	-0.38	-0.50
8. 2	1	-0.97		- 1									-0.83
8. 1		-0.99											-0.87
7. 1	-0.57	-0.52	-0.48	-0.55	-0.65	-0.45	-0.51	-0.41	-0.73	-0.52	-0.49	-0.49	-0 53
9.12.3.9	-1.16	-1.08	-0.85	-1.05	-1.13	-0.01	-0.70	-0.70	-0.99	-0.97	-0.95	-1.11	-0.97
7. 2.2(9)	-0.11	0.06	0.03		-0.01			-0.30				-0.04	
Dail.ext.	-0.28	0.05	-0.25	-0.08	-0.20	-0.15	-0.53	-0.08	-0.39	-0.15	-0.12	-0.37	-0.19

### XXII.

## India. — Bombay. Lat. 18° 56′ N. Long. 72° 54′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Hours.         Jan.         Feb.         March.         April.         May.         June.         July.         Aug.         Sept.         Oct.         Nov.         Dec.         Mea           Morn. 1         1.49         1.40         0.99         1.13         1.42         1.15         0.79         0.97         0.86         1.49         2.03         1.55         1.2           2         1.80         1.69         1.33         1.51         1.78         1.40         0.88         1.13         0.97         1.87         2.18         1.87         1.5           3         2.27         2.21         1.91         2.05         2.14         1.69         0.90         1.24         1.24         2.32         2.45         2.41         1.9           4         2.86         2.84         2.59         2.48         2.32         1.91         0.90         1.31         1.53         2.75         2.81         3.11         2.2           5         3.47         3.40         3.04         2.61         2.23         1.96         0.86         1.31         1.71         2.95         3.11         3.78         2.5           4         3.83         3.62         3.06
2     1.80     1.69     1.33     1.51     1.78     1.40     0.88     1.13     0.97     1.87     2.18     1.87     1.53     4     2.86     2.84     2.59     2.48     2.32     1.91     0.90     1.24     1.24     2.32     2.45     2.41     1.94     4     2.86     2.84     2.59     2.48     2.32     1.91     0.90     1.31     1.53     2.75     2.81     3.11     2.2     3.11     3.78     2.5     3.47     3.40     3.04     2.61     2.23     1.96     0.86     1.31     1.71     2.95     3.11     3.78     2.5     4     3.83     3.62     3.06     2.34     1.80     1.80     0.79     1.24     1.67     2.79     3.15     4.16     2.5     4.16     4.16     2.5     4.16     2.5     4.16     2.5     4.16     2.5     4.16     2.5     4.16     2.5     4.16     2.5     4.16     4.16     2.5     4.16     2.5     4.16     4.16     2.5     4.16     4.16     2.5     4.16     4.16     2.5     4.16     4.16     2.5     4.16     4.16     2.5     4.16     4.16     2.5     4.16     4.16     2.5     4.16     4.16     2.5     4.16     4
2
3
4       2.86       2.84       2.59       2.48       2.32       1.91       0.90       1.31       1.53       2.75       2.81       3.11       2.22         5       3.47       3.40       3.04       2.61       2.23       1.96       0.86       1.31       1.71       2.95       3.11       3.78       2.5         4       3.83       3.62       3.06       2.34       1.80       1.80       0.79       1.24       1.67       2.79       3.15       4.16       2.5         7       3.69       3.33       2.54       1.67       1.15       1.42       0.65       1.04       1.22       2.21       2.79       4.01       2.1         8       2.97       2.48       1.58       0.77       0.36       0.88       0.38       0.74       0.79       1.28       1.91       3.24       1.4         9       1.69       1.22       0.38       -0.14       -0.41       0.23       0.00       0.32       0.09       0.16       0.63       1.87       0.5         10       0.07       -0.23       -0.77       -0.90       -1.06       -0.43       -0.52       -0.20       -0.65       -0.95       -0.83
5 3.47 3.40 3.04 2.61 2.23 1.96 0.86 1.31 1.71 2.95 3.11 3.78 2.55 4 3.69 3.33 2.54 1.67 1.15 1.42 0.65 1.04 1.22 2.21 2.79 4.01 2.18 2.97 2.48 1.58 0.77 0.36 0.88 0.38 0.74 0.79 1.28 1.91 3.24 1.44 0.99 1.69 1.22 0.38 -0.14 -0.41 0.23 0.00 0.32 0.09 0.16 0.63 1.87 0.5 1.04 0.07 -0.23 -0.77 -0.90 -1.06 -0.43 -0.52 -0.20 -0.65 -0.95 -0.83 0.16 -0.5 1.1 1 -1.55 -1.55 -1.67 -1.49 -1.55 -6.08 -6.08 -0.79 -1.28 -1.91 -2.21 -1.60 -1.4 1.20 -1.20 -1.4 1.20 -1.4 1.20 -1.4 1.20 -1.4 1.20 -1.4 1.20 -1.4 1.20 -1
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$ \begin{vmatrix} 4 &   -3.42 &   -3.42 &   -2.72 &   -2.50 &   -2.09 &   -2.25 &   -0.92 &   -1.69 &   -1.87 &   -2.66 &   -3.33 &   -4.12 &   -2.88$
5   -2.84   -2.95   -2.34   -2.07   -1.64   -1.78   -0.38   -1.24   -1.37   -2.14   -2.61   -3.38   -2.07   -2.
6   -2.18   -2.27   -1.71   -1.37   -1.04   -1.15   0.09   -0.72   -0.74   -1.46   -1.78   -2.45   -1.46
7   -1.49   -1.44   -0.88   -0.54   -0.38   -0.47   0.38   -0.23   0.05   -0.72   -0.88   -1.46   -0.66
8   -0.79   -0.56   -0.07   0.23   0.18   0.14   0.50   0.16   0.47   -0.02   0.00   -0.52   -0.00
$9 \begin{vmatrix} -0.11 & 0.23 & 0.56 & 0.72 & 0.59 & 0.54 & 0.54 & 1.43 & 0.86 & 0.52 & 0.77 & 0.29 & 0.49 & 0.54 & 0.$
Midn   1.24   1.26   0.92   0.95   1.15   0.99   0.70   0.83   0.88   1.26   1.91   1.37   1.
6. 6 0.81 0.68 0.68 0.50 0.38 0.34 0.43 0.25 0.45 0.68 0.70 0.86 0.
7. 7   1.10   0.95   0.83   0.56   0.38   0.47   0.52   0.41   0.63   0.74   0.95   1.28   0.56   0.38   0.47   0.52   0.41   0.63   0.74   0.95   1.28   0.56   0.38   0.47   0.52   0.41   0.63   0.74   0.95   1.28   0.56   0.38   0.47   0.52   0.41   0.63   0.74   0.95   1.28   0.56   0.38   0.47   0.52   0.41   0.63   0.74   0.95   0.83   0.47   0.52   0.41   0.63   0.74   0.95   0.83   0.47   0.52   0.41   0.63   0.74   0.95   0.83   0.47   0.52   0.41   0.63   0.74   0.95   0.83   0.47   0.95   0.83   0.9
8. 8   1.08   0.97   0.77   0.50   0.27   0.50   0.45   0.45   0.63   0.63   0.95   1.35   0.63   0.95   1.35   0.63   0.95   1.35   0.95   0.95   1.35   0.9
9. 9   0.79   0.72   0.47   0.29   0.09   0.38   0.27   0.36   0.47   0.34   0.70   1.08   0.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$
3310 0.21 0.23 0.01 0.00 0.11 0.10 0.12 0.13 0.03 0.02
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
6. 2.10   0.11   0.27   0.38   0.25   0.09   0.07   -0.16   -0.07   0.14   0.18   0.14   0.14   0.
6. 2. 6   -0.79   -0.74   -0.50   -0.52   -0.52   -0.59   -0.29   -0.50   -0.45   -0.61   -0.90   -0.97   -0.
7. 2   -0.16   -0.14   -0.16   -0.43   -0.61   -0.50   -0.56   -0.50   -0.52   -0.47   -0.65   -0.29   -0.
8. 2   -0.52   -0.56   -0.63   -0.88   -0.99   -0.77   -0.70   -0.63   -0.74   -0.92   -1.08   -0.68   -0.
8. 1   -0.36   -0.41   -0.54   -0.79   -0.92   -0.63   -0.72   -0.52   -0.68   -0.86   -1.01   -0.43   -0.
7. 1   0.00   0.02   -0.07   -0.29   -0.54   -0.36   -0.59   -0.38   -0.45   -0.41   -0.56   -0.05   -0.
$ \begin{vmatrix} 9.12.3.9 & -1.25 & -1.22 & -1.06 & -0.99 & -1.01 & -0.83 & -0.61 & -0.65 & -0.77 & -1.24 & -1.44 & -1.37 & -1. \end{vmatrix} $
$ \begin{vmatrix} 7 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 &$

### XXIII.

# India. - Bombay. Lat. 18° 56' N. Long. 72° 54' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

	0.56 0.68 0.85 1.01 1.13 1.12 0.95 0.64 0.22 -0.23 -0.66 -1.00
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.68 0.85 1.01 1.13 1.12 0.95 0.64 0.22 -0.23 -0 66
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.68 0.85 1.01 1.13 1.12 0.95 0.64 0.22 -0.23 -0 66
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.85 1.01 1.13 1.12 0.95 0.64 0.22 -0.23 -0 66
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.01 1.13 1.12 0.95 0.64 0.22 -0.23 -0 66
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.13 1.12 0.95 0.64 0.22 -0.23 -0 66
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.12 0.95 0.64 0.22 -0.23 -0 66
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.12 0.95 0.64 0.22 -0.23 -0 66
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.95 0.64 0.22 -0.23 -0.66
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.64 0.22 -0.23 -0.66
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.22 -0.23 -0 66
$ \begin{vmatrix} 10 &   0.03 &   -0.10 &   -0.34 &   -0.40 &   -0.47 &   -0.19 &   -0.23 &   -0.09 &   -0.29 &   -0.42 &   -0.37 &   0.07 &   -0.69 &   -0.69 &   -0.69 &   -0.69 &   -0.48 &   -0.48 &   -0.35 &   -0.57 &   -0.85 &   -0.98 &   -0.71 &   -0.69 &   -0.48 $	-0.23 -0 66
11   -0.69   -0.69   -0.74   -0.66   -0.69   -0.48   -0.48   -0.35   -0.57   -0.85   -0.98   -0.71   -	-0 66
Noon   -1.27   -1.16   -1.02   -0.85   -0.86   -0.73   -0.69   -0.60   -0.80   -1.15   -1.46   -1.37	-1.00
	2.00
1 1 2 2 4 1 4 2 1 7 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.00
1   -1.64   -1.46   -1.18   -1.00   -0.98   -0.94   -0.81   -0.79   -0.94   -1.33   -1.74   -1.82   -1.74   -1.	
2   -1.77   -1.60   -1.26   -1.11   -1.04   -1.07   -0.79   -0.89   -1.00   -1.39   -1.81   -2.04   -1.07   -1.08   -1.	
3   -1.71   -1.62   -1.27   -1.16   -1.03   -1.09   -0.64   -0.88   -0.96   -1.33   -1.71   -2.02	
4   -1.52   -1.52   -1.21   -1.11   -0.93   -1.00   -0.41   -0.75   -0.83   -1.18   -1.48   -1.83	-1.19
5   -1.26   -1.31   -1.04   -0.92   -0.73   -0.79   -0.17   -0.55   -0.61   -0.95   -1.16   -1.50	-0.92
6   -0.97   -1.01   -0.76   -0.61   -0.46   -0.51   0.04   -0.32   -0.33   -0.65   -0.79   -1.09   -	
	-0.30
8   -0.35   -0.25   0.03   0.10   0.08   0.06   0.22   0.07   0.21   -0.01   0.   -0.23	
9   -0.05   0.10   0.25   0.32   0.26   0.24   0.24   0.19   0.38   0.23   0.34   0.13	0.22
10   0.21   0.36   0.40   0.41   0.37   0.35   0.24   0.26   0.44   0.39   0.60   0.38	0.37
11   0.41   0.49   0.43   0.41   0.44   0.40   0.27   0.32   0.43   0.48   0.76   0.53	0.45
Midn   0.55   0.56   0.41   0.42   0.51   0.44   0.31   0.37   0.39   0.56   0.85   0.61	0.50
6. 6   0.36   0.30   0.30   0.22   0.17   0.15   0.19   0.11   0.20   0.30   0.31   0.38	0.25
	0.23
$ \begin{vmatrix} 7 & 7 & 0.49 & 0.42 & 0.37 & 0.25 & 0.17 & 0.21 & 0.23 & 0.18 & 0.28 & 0.33 & 0.42 & 0.57 \\ 8 & 8 & 0.48 & 0.43 & 0.34 & 0.22 & 0.12 & 0.22 & 0.20 & 0.20 & 0.28 & 0.28 & 0.42 & 0.60 \\ \end{vmatrix} $	0.33
$ \begin{vmatrix} 8 & 8 & & 0.48 & 0.43 & 0.34 & 0.22 & 0.12 & 0.22 & 0.20 & 0.20 & 0.28 & 0.28 & 0.42 & 0.60 \\ 9 & 9 & & 0.35 & 0.32 & 0.21 & 0.13 & 0.04 & 0.17 & 0.12 & 0.16 & 0.21 & 0.15 & 0.31 & 0.48 \\ \end{vmatrix} $	0.32
$ \begin{vmatrix} 9 & 9 & 0.03 & 0.02 & 0.21 & 0.13 & 0.04 & 0.17 & 0.12 & 0.16 & 0.21 & 0.13 & 0.04 \\ 10.10 & 0.12 & 0.13 & 0.03 & 0.00 & -0.05 & 0.08 & 0.01 & 0.09 & 0.08 & -0.02 & 0.11 & 0.23 \\ \end{vmatrix} $	0.07
0.12 0.10 0.00 0.00 0.01 0.00 0.02 0.11 0.23	0.01
7. 2. 9   -0.06   -0.01   0.04   -0.02   -0.09   -0.07   -0.09   -0.08   -0.03   -0.06   -0.08   -0.04   -	-0.05
	-0.07
6. 2.10   0.05   0.12   0.17   0.11   0.04   0.03   -0.07   -0.03   0.06   0.08   0.06   0.06	0.06
6. 2 6   -0.35   -0.33   -0.22   -0.23   -0.23   -0.26   -0.13   -0.22   -0.20   -0.27   -0.40   -0.43   -0.43	-0.27
	0.10
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
8. 2	
8. 1   -0.16   -0.18   -0.24   -0.33   -0.41   -0.28   -0.32   -0.23   -0.30   -0.38   -0.45   -0.19	
7. 1   0.00   0.01   -0.03   -0.13   -0.24   -0.16   -0.26   -0.17   -0.20   -0.18   -0.25   -0.02	0.14
$ \begin{vmatrix} 9.12.2.9 &   -0.57 &   -0.54 &   -0.47 &   -0.44 &   -0.45 &   -0.37 &   -0.27 &   -0.29 &   -0.34 &   -0.55 &   -0.64 &   -0.61 & $	-0.46
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.02
Dail.ext.   -0.04   -0.01   0.05   0.01   0.00   -0.11   -0.21   -0.16   -0.12   -0.04   -0.21   -0.10   -0.10	

### XXIV.

### India. - Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.91	1.13	1.00	1.62	1.22	1.35	1.19	1.27	1.04	0.82	0.91	0.84	1.11
1	1.13	1.45	1.29	1.37	1.47	1.56	1.38	1.34	1.20	1.01	1.13	1.00	1.28
2	1.32	1.76	1.60	1.59	1.65	1.72	1.58	1.51	1.38	1.24	1.35	1.17	1.49
3	1.43	2.01	1.88	1.81	1.81	1.90	1.75	1.64	1.58	1.39	1.56	1.32	1.68
4	1.61	2.25	2.13	1.96	1.98	2.08	1.92	1.77	1.76	1.54	1.74	1.42	1.85
5	1.74	2.44	2.33	1.98	2.08	2.20	2.07	1.93	1.88	1.65	1.88	1.60	1.98
6	1.80	2.51	2.27	1.68	1.72	1.87	1.92	1.81	1.70	1.46	1.80	1.66	1.85
7	1.08	1.48	1.13	0.79	0.92	1.12	1.30	1.24	1.08	0.80	1.89	1.06	1.07
8	-0.02	0.13	0.07	-0.08	-0.05	0.17	0.47	0.44	0.32	0.06	-0.25	0.00	0.10
9	-0.90	<b>-0.</b> 86	-0.84	-1.07	-1.08	-0.77	-0.34	-0.40	-0.50		-1.11	-0.77	-0.77
10	-1.45	-1,60	-1.63	-1.84	-2.08	-1.63	-1.19	-1.22	-1.32	-1.04		-1.36	-1.49
11	-1.79	-2.14	-2.14	-2.15	-2.56	-2.23	-1.89	-1.85	-2.02	-1.41	-1.82	-1.61	-1.47
Noon.	-1.97	-2.25	-2.38	-2.52	-2.61	-2.60	-2.45	-2.35	-2.24	-1.67	-1.92	-1.75	-2.23
1	-1.96	-2.33	-2.41	-2.46	-2.51	-2.69	-2.70	-2.56	-2.24	-1.66	-1.89	-1.72	
2	-1.84	-2.36	-2.22	-2.20	-2.22	-2.53	-2.67	-2.40	-2.07	-1.58	-1.66	-1.60	-2.11
3	-1.54	-2.16	-1.90	-1.81	-1.78	-2.05	i	-2.04			1	-1.28	
4	-1.07	-1.62	-1.38	-1.18	-1.09	-1.59		-1.53	Į.				-1.26
5	-0.53	-1.01	-0.74	-0.46	-0.45	-0.85	-0.97	-0.82	-0.64	-0.56	-0.39	-0.45	-0.66
6	-0.17	-0.49	-7.23	0.09	0.05	-0.26	-0.36	-0.31	-0.23	-0.28	-0.11	-0.17	-0.21
7	0.04	-0.16	0.07	0.37	0.34	0.16	0.07	0.06	0.03	-0.08	0.04	0.00	0.08
8	0.24	0.12	026	0.44	0.53	0.43	0.37	0.33	0.21	0.07	0.21	0.15	0.28
9	0.42	0.36	0.43	0.70	0.70	0.63	0.60	0.52	0.44	0.22	0.33	0.30	0.47
10	0.62	0.59	0.61	0.84	0.87	0.94	0.83	0.73	0.62	0.40	0.48	0.46	0.67
11	0.82	0.83	0.82	1.00	1.04	1.07	1.02	0.95	0.84	0.57	0.65	0.64	0.85
Mean,	19.90	20.56	22.33	23.88	24.49	24.45	24.10	23.34	22.89	21.86	20.68	19.89	

### XXV.

India. — Bombay. Lt. 18° 56′ N. Long. 72° 54′ E. Greenw. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.76	1.68	1.43	1.40	\.30	0.80	0.57	0.59	0.92	1.36	1.74	1.93	1.29
1	1.91	1.88	1.65	1.54	140	0.89	0.65	0.64	0.98	1.52	1.80	2.00	1.40
2	2.04	2.04	1.80	1.75	154	0.88	0.63	1.16	1.09	1.62	1.97	2.18	1.56
3	2.18	2.22	1.90	1.92	1.9	0.94	0.65	0.81	1.18	1.74	2.11	2.28	1.63
4	2.39	2.44	2.26	2.02	1.8.	1.04	0.76	0.82	1.25	1.89	2.23	2.41	1.78
5	2.65	2.68	2.42	2.26	1.92	1.09	0.83	0.90	1.25	1.96	2.40	2.62	1.92
6	2.88	2.88	2.60	2.20	1.65	1.03	0.84	0.84	1.21	2.00	2.55	2.66	1.94
7	2.53	2.37	1.61	0.76	0.44	\60	0.55	0.51	0.61	1.02	1.47	2.08	1.21
8	0.72	0.48	-1.04	-0.62	-0.51	-001	0.02	0.08	-0.20	-0.31	-0.12	0.20	-0.11
9	-1.04	-1.05	-1.49	-1.53	-1.30	-0.6	-0.46	-0.45	-0.84	-1.53	-1.40	-1.00	-1.05
10	-2.40	-2.29	-2.28	-2.00	-1.73	-0.7	-0.74	-0.76	-1.32	-2.17	-2.38	-2.14	-1.75
11	-3.08	-2.98	-2.54	-2.20	-2.08	-1.18	-1.07	-1.12	-1.51	-2.38	-3.18	-2.94	-2.19

#### XXV.

### INDIA. - BOMBAY, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Pec.	Year.
Noon.	-3.40	-3.29	-2.52	-2.44	-2.32	-1.40	-1.09	-1.34	-1.72	-2.39	-3.26	-3.32	-2.37
1	-3.02	-3.12	-2.67	-2.53	-2.28	-1.50	-1.12	-1.35	-1.77	-2.22	-2.96	-3.35	-2.32
2	-2.78	-2.89	-2.56	-2.32	-2.14	-1.52	-0.97	-1.35	-1.55	-2.09	-2.55	-2.97	-2.14
3	-2.38	-2.54	-2.25	-2.05	-1.85	-1.31	-0.85	-1.09	-1.37	-1.79	-2.22	-2.59	-1.86
-4	-1.96	-2.07	-1.72	-1.49	-1.36	-0.89	-0.63	-0.76	-0.95	-1.38	-1.55	-2.03	-1.40
5	-1.30	-1.41	-1.08	-0.96	-0.83	-0.49	-0.36	-0.34	-0.36	-0.61	-0.67	-1.09	-0.79
6	-0.61	-0.44	-0.16	0.00	0.09	-0.02	0.03	0.13	0.14	0.01	-0.14	-0.52	-0.13
7	-0.28	-0.07	0.19	0.43	0.63	0.22	0.21	0.26	0.28	0.30	0.09	-0.23	0.17
8	0.00	0.23	0.48	0.66	0.87	0.39	0.28	0.34	0.44	0.53	0.36	0.10	0.39
9	0.58	0.63	0.80	0.83	0.92	0.44	0.36	0.41	0.58	0.76	085	0.75	0.66
10	1.16	1.15	1.04	1.09	0.95	0.52	0.41	0.52	0.78	0.96	1.32	1.35	0.94
11	1.47	1.48	1.20	1.24	1.17	0.71	0.48	0.56	0.89	1.18	1.58	1.65	1.13
Mean.	18.38	19.30	21.00	22.50	23.43	22.35	21.67	21.45	21.42	22.08	21.28	19.54	

### XXVI.

India. — Calcutta. Lat. 22° 33′ 5″ N. Long. 88° 19′ 2″ E. Greenw. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Year.
Midn.	1.86	1.69	2.06	1.60	1.90	1.12	0.69	0.69	0.71	100	1.24	1.51	1.34
1	2.24	2.00	2.37	1.96	2.06	1.12	0.80	0.78	0.76	1.17	1.47	1.77	1.54
2	2.53	2.22	2.62	2.18	2.21	1.16	0.91	0.85	0.84	1.26	1.69	2.00	1.71
3	2.80	2.44	2.84	2.27	2.32	1.29	1.02	0.92	0.93	1.26	1.82	2.31	1.85
4	3.06	2.71	3.08	2.40	2.41	1.29	1.11	0.96	1.04	1.46	2.00	2.40	1.99
5	3.33	2.89	3.28	2.47	2.50	1.34	1.24	1.07	1.1€	1.53	2.22	2.66	2.14
6	3.53	3.11	3.42	2.53	2.41	1.34	1.24	1.12	1.6	1.62	2.36	2.80	2.22
7	3.71	3.24	3.42	2.22	1.90	1.03	0.96	0.89	093	0.86	2.31	2.93	2.03
8	2.73	2.20	1.97	1.18	0.81	0.45	0.42	0.32	6.27	0.31	0.93	1.68	1.11
9	0.91	0.71	. 0.46	0.11	-0.34	-0.13	-0.16	-0.22	-J.24	-0.47	-0.13	0.35	0.07
10	-0.78	-0.62	-0.98	-0.44	-1.39	-0.66	-0.69	-0.33	-0.73	-0.58	-1.02	-0.76	-0.75
11	-2.09	-1.64	-2.14	-1.82	-2.14	-1.15	-1.13	-1.08	-1.16	-1.60	-1.91	-1.S7	-1.64
Noon.	-3.31	-2.62	-3.16	-2.67	-2.76	-1.60	-1.51	-1.5	-1.40	-1.94	-2.44	-2.80	-2.31
1	-4.14	-3.28	-3.87	-3.09	-3.12	-1.68	-1.58	-1.5	-1.44	-2.05	-2.80	-3.29	-2.66
2	-4.52	-3.64	-4.25	-3.47	-3.32	-1.73	-1.29	-130	-1.63	-2.12	-3.07	-3.69	-2.88
3	-4.65	<b>-</b> 3.87	-4.40	-3.62	-3.43	-1.92	-1.24	1			-2.98	1 3	-2.84
4	-3.78	-3.69	-4.23		-3.10	,		3 i	-0.91				-2.41
5	-3.07	-3.13	-3.36	-2.73	-2.43	-1.20	-0.64	-0.68	-0.56	-0.92	-1.60	-2.18	-I.SS
6	-1.87	-1.91	-1.96	-1.42	-1.23	-0.57	-0.31	-0.31	-0.16	-0.25	-0.76	-1.34	-1.01
7	-0.96	-0.93	-0.78	-0.31	-0.14	-0.11	-0.0	-0.09	0.04	0.13	-0.22	-0.63	-0.34
8	-0.20	-0.22	0.00	0.40	0.68	0.20	0.0	0.25	0.22	0.42	0.27	-0.05	0.17
9	0.42	0.38	0.73	0.89	1.08	0.49	022	0.45	0.33	0.60	0.62	0.44	0.55
10	0.95	0.80	1.22	1.20	1.46	0.63	1.36	0.56	0.47	0.75	1.07	0.93	0.87
11	1.37	1.20	1.66	1.54	1.64	0.74	0.49	0.65	0.60	0.88	1.16	1.20	1.09
Mean.	15.49	17.57	21.19	22.51	24.01	23.29	22.68	22.86	22.42	21.73	18.88	16.36	

### XXVII.

### Asia. — Tiflis. Lat. 41° 41' N. Long. 45° 17' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

		1			1							1	1
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.87	1.01	1.54	1.81	1.95	2.38	2.43	2.22	1.60	1.38	0.99	0.80	1.58
1	1.02	1.15	1.80	2.10	2.28	2.67	2.79	2.52	1.81	1.64	1.16	0.94	1.82
2	1.17	1.33	2.02	2.40	2.58	2.94	3.13	2.82	2.08	1.88	1.37	1.04	2.06
3	1.32	1.47	2.23	2.64	2.84	3.22	3.49	3.13	2.29	2.11	1.59	1.14	2.28
4	1.46	1.57	2.39	2.94	3.14	3.43	3.73	3.44	2.59	2.39	1.73	1.25	2.51
5	1.60	1.69	2.58	3.12	3.09	3.09	3.55	3.59	2.74	2.62	1.85	1.35	2.57
6	1.76	1.75	2.63	2.89	2.39	2.35	2.77	3.06	2.63	2.77	1.99	1.40	2.37
7	1.87	1.75	2.14	2.19	1.53	1.28	1.50	2.16	1.99	2.38	1.85	1.42	1.84
8	1.40	1.23	1.23	0.99	0.53	0.35	0.70	1.05	1.07	1.52	1.44	1.19	1.06
9	0.05	0.50	0.16	-0.22	-0.51	-0.65	-0.32	-0.21	-0.03	0.30	0.54	0.49	0.01
10	-0.41	-0.46	-0.94	-1.20	-1.41	-1.66	-1.35	-1.32	-1.15	-0.47	-0.46	-0.19	-0.92
11	-1.17	-1.33	-1.85	-2.06	-2.19	-2.40	-2.27	-2.20	-2.01	-1.77	-1.31	-1.11	-1.81
Noon.	-1.91	-1.94	-2.64	-2.77	-2.89	-2.42	-2.99	-2.89	-2.67	-2.53	-2.07	-1.76	-2.46
1	-2.37	-2.45	-3.12	-3.29	-3.21	-3.42	-3.53	-3.60	-3.17	-3.07	-2.50	-2.21	-3.00
2	-2.59	-2.65	-3.25	-3.37	-3.34	-3.50	-3.68	-3.85	-3.41	-3.56	-2.81	-2.38	-3.20
3	-2.33	-2.58	-3.21	-3.41	-3.25	-3.51	-3.82	-3.98	-3.37	-3.41	-2.55	-2.08	-3.12
4	-1.78	-2.07	-2.78	-3.20	-2.97	-3.39	-3.82	-3.72	-2.95	-2.81	-1.87	-1.43	-2.73
5	-0.99	-1.24	-2.08	-2.46	-2.65	-2.86	-3.47	-3.20	-1.53	-1.85	-1.27	-0.90	-2.04
6	-0.57	-0.60	-1.11	-1.56	-1.47	-1.81	-2.36	-2.01	-1.18	-1.17	-0.73	-0.49	-1.26
7	-0.17	-0.19	-0.48	-0.69	-0.45	-0.63	-0.86	-0.85	-0.46	-0.50	-0.35	-0.13	-0.48
-8	0.15	0.19	0.12	-0.02	0.26	0.23	0.13	-0.02	0.18	0.11	-0.02	0.19	0.12
9	0.33	0.44	0.51	0.64	0.83	0.92	0.87	0.72	0.61	0.50	0.24	0.36	0.58
10	0.55	0.65	0.91	1.05	1.28	1.51	1.44	1.33	1.00	0.81	0.48	0.53	0.96
11	0.69	0.89	1.25	1.45	1.63	1.95	1.96	1.80	1.32	1.10	0.76	0.68	1.29
Mean.	-0.20	3.00	5.64	9.99	13.54	16.10	19.01	19.43	15.03	11.40	5.07	2.45	

### XXVIII.

China. — Peking. Lat. 39° 54′ N. Long. 116° 26′ E. Greenw. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June	July.	Aug	Sept.	Oct.	Nov	Dec	Year
Midn.	1.16	1.70	1.83	1.75	2.19	2.24	1.61	1.49	1.69	1.64	1.19	1.25	1.64
1	1.47	2.07	2.19	2.26	2.76	2.73	1.89	1.80	2.04	2.05	1.47	1.39	2.01
2	1.66	2.35	2.78	2.67	3.20	3.12	2.23	2.04	2.32	2.37	1.68	1.65	2.34
3	1.93	2.55	2.93	3.18	3.72	3.47	2.50	2.31	2.55	2.62	1.88	1.83	2.62
4	2.13	2.81	3.27	3.57	4.13	3.82	2.74	2.54	2.97	2.92	2.01	2.46	2.95
5	2.41	2.94	3.57	3.89	4.30	3.88	2.78	2.71	3.10	3.19	2.20	2.10	3.09
6	2.58	3.15	3.65	3.81	3.37	2.86	2.10	2.46	2.96	3.43	2.32	2.18	2.91
7	2.63	3.21	3.19	2.91	2.30	1.95	1.34	1.65	2.10	2.98	2.30	2.29	2.40
8	2.23	2.37	1.84	1.65	1.19	1.07	0.52	0.76	0.87	1.68	1.39	1.73	1.44
9	0.77	0.70	0.49	0.34	0.00	0.03	-0.12	-0.20	-0.24	0.15	0.19	0.31	0.20
10	-0.57	-0.65	-0.81	-0.79	-1.20	-1.06	-0.97	-1.09	-1.36	-1.05	-0.84	-0.97	-0.95
11	-1.35	-1.90	-1.93	-2.03	-1.24	-2.17	-1.71	-1.67	-2.17	-2.18	-1.74	-1.96	-1.84

#### XXVIII.

### CHINA. — PEKING, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-2.83	-2.80	-2.95	-2.92	-3.05	-2.92	-2.24	-2.02	-2.77	-3.03	-2.39	-2.64	-2.71
1	-3.01	-3.54	-3.54	-3.59	-3.74	-3.55	-2.65	-2.64	-3.10	-3.65	-2.87	-3.18	-3.25
2	-3.37	-3.84	-4.03	-3.98	-4.08	-3.97	-2.88	-2.90	-3.38	-3.96	-3.07	-3.41	-3.57
3	-3.40	-3.94	-4.12	-4.06	-4.24	-4.00	-2.85	-2.94	-3.44	-3.97	-2.88	-2.74	-3.55
4	-2.88	-3.65	-3.92	-3.86	-4.03	-3.74	-2.74	-2.79	-3.06	-2.43	-2.23	-2.50	-3.15
5	-1.79	-2.83	-3.21	-3.24	-3.65	-3.31	-2.36	-2.20	-2.34	-2.34	-1.18	-1.34	-2.48
6	-0.97	-1.79	-2.20	-2.34	-3.04	-2.44	-1.76	-1.45	-1.18	-1.12	-0.59	-0.64	-1.63
7						1		1				-0.26	
8	-0.02	-0.27	-0.30	-0.33	-0.19	-0.11	0.12	0.08	0.09	-0.02	0.01	0.18	-0.06
9	0.30	0.26	0.26	0.24	0.59	0.59	0.63	0.51	0.57	0.42	0.30	0.54	0.43
10	0.57	0.73	0.83	0.84	1.15	1.14	1.04	0.83	0.97	0.86	0.59	0.77	0.86
11	0.90	1.20	1.30	1.28	1.67	1.65	1.35	1.18	1.32	1.00	0.81	1.01	1.22
Mean.	-3.57	-2.04	3.42	9.66	15.83	19.61	21.27	19.30	15.68	9.61	1.79	-2.44	

### XXIX.

Siberia. — Nertchinsk. Lat. 51° 18' N. Long. 117° 20' E. Gr. — Dove.

Degrees of Reaumur.													
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.78	1.38	1.92	2.53	3.10	3.13	2.63	2.51	2.12	1.66	0.96	0.75	1.96
1	1.06	1.61	2.25	2.95	3.71	3.55	3.00	2.87	2.58	1.98	1.22	0.94	2.31
2	1.24	1.84	2.65	3.36	4.20	3.98	3.34	3.25	2.93	2.27	1.42	1.16	2.64
3	1.45	2.15	3.02	3.75	4.78	4.32	3.64	3.57	3.28	2.57	1.70	1.33	2.96
4	1.70	2.40	3.38	4.09	5.04	4.29	3.86	3.79	3.62	2.80	1.91	1.45	3.19
5	1.93	2.72	3.70	4.15	3.97	3.27	3.17	3.68	3.97	3.00	2.06	1.63	3.10
6	2.08	2.94	3.89	2.96	2.31	2.03	1.99	2.61	3.63	3.16	2.15	1.76	2.63
7	2.26	3.00	2.88	1.43	0.82	0.74	1.01	1.31	2.07	2.46	2.35	1.95	1.86
8	2.20	1.82	1.36	0.19	-0.53	-0.45	-1.28	0.11	0.66	0.84	1.61	1.98	0.71
9	0.56	-0.20	-0.12	-1.32	-1.77	-1.59	-1.25	-1.08	-0.72	-0.69	-0.03	0.62	-0.63
10	-0.96	-1.27	-1.71	-2.35	-2.73	-2.52	-2.13	-2.10	-1.99	-1.82	-1.17	-0.89	-1.80
11	-1.90	-2.34	-2.61	-3.08	-3.34	-3.17	-2.79	-2.91	-2.94	-2.78	-2.12	-1.85	-2.65
Noon.	-2.70	-3.16	-3.43	-3.70	-3.82	-3.62	-3.28	-3.49	-3.71	-3.41	-2.84	-2.58	-3.31
1	-3.06	-3.75	-3.96	-4.01	-4.08	-3.80	-3.58	-3.76	-4.09	-3.75	-3.09	-2.85	-3.65
2	-3.00	-3.80	-4.23	-4.08	-4.10	-3.73	-3.66	-3.92	-4.20	-3.66	-2.97	-2.52	-3.66
3	-2.50	-3.47	-4.03	-3.84	-3.99	-3.59	-3.48	-3.79	-3.86	-3.26	-2.27	-1.87	-3.33
1	-1.54	-2.73	-3.53	-3.48	-3.55	-3.24	-3.02	-3.21	-3.34	-2.43	-1.34	-0.96	-2.70
5	-0.71	-1.61	-2.75	-2.85	-3.02	-3.73	-2.38	-2.56	-2.48	-1.42	-0.87	-0.43	-1.98
6	-0.28	-0.63	-1.71	-1.97	-2.27	-2.06	-1.73	-1.68	-1.22	-0.50	-0.10	-0.17	-1.20
7	0.02	0.01	-0.34	-0.34	-0.93	-0.93	-0.82	-0.66	-0.49	-0.24	-0.17	-0.70	-0.47
8	0.13	0.39	0.24	0.61	0.27	0.97	0.37	0.41	0.34	0.30	0.06	0.08	0.29
9	0.27	0.63	0.66	1.19	1.34	1.32	1.24	1.30	0.89	0.64	0.34	0.22	0.84
10	0.43	0.86	1.06	1.72	1.92	2.02	1.78	1.70	1.30	1.01	0.54	0.43	1.23
11	0.57	1.16	1.47	2.17	2.63	2.63	2.29	2.14	1.71	1.31	0.75	0.56	1.62
Mean.	-21.94	-17.84	-8.35	0.01	7.51	1.78	13.91	11.91	6.55	-1.80	-13.44	-21.36	

### XXX.

Siberia. - Nertchinsk. Lat. 51° 18' N. Long. 119° 21' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn, I	0.91	1.42	2.07	2.69	4.07	4.29	3.07	3.00	2.16	2.31	0.76	0.66	2.28
2	1.00	1.68	2.57	3.29	4.69	4.71	3.46	3.48	2.96	2.79	0.96	0.74	2.69
3	1.15	2.08	3.16	3.78	5.08	4.90	3.75	3.89	3.27	3.26	1.26	0.84	3.04
4	1.42	2.52	3.63	3.97	4.98	4.70	3.76	4.04	3.81	3.61	1.66	1.07	3.26
	7 -0	0.04	0.00	0.00		0.00	0.0=	0.70	0.04	0.00	0.00		2 20
5	1.78	2.84	3.73	3.69	4.24	3.96	3.37	3.72	3.94	3.66		1.41	3.20
6	2.07 $2.06$	2.80	3.28	2.88	2.86	2.67	2.54	2.89	3.15	3.30		1.75	2.71
7 8	1.60	2.28	2.31	1.63	1.07	0.99	1.37	1.62	2.38	2.47	2.18	1.87 1.59	1.85 0.66
°	1.00	1.28	0.99	0.10	<b>-0.7</b> 8	-0.79	0.06	0.15	0.87	1.24	1.58	1.99	0.00
9	0.65	-0.05	-0.41	-1.26	-2,33	-2.34	-1.19	-1.25	-0.70	-0.23	0.55	0.87	-0.64
10	-0.59	•				-3.41		1	1			-0.17	-1.80
11				-3.22				-3.15				-1.23	
Noon	Į.			-3.64				-3.61	i			-2.01	-3.34
1								i				-2.30	1
2	-2.56	-3.27	-3.74	-3.65	-4.18	-3.92	-3.72	-3.88	-4.00	-4.20	-2.50	-2.08	-3.48
3	-1.89	-2.76	-3.65	-3.33	-4.03	-3.77	-3.62	-3.75	-3.54	-3.77	-1.87	-1.54	-3.13
4	-1.14	-2.12	-3.31	-2.84	<b>-</b> 3.69	-3.54	-3.29	-3.40	-3.24	-3.08	-1.17	-0.92	-2.65
_ [	0 = 0								2 00				0.00
5											l .	-0.47	-2.03
6	i	-0.81							1	ĺ	l .	-0.25	-1.31
7		-0.21	-0.77		-0.92	-1.23		-0.80		-0.54	i i	-0.23	-0.60
8	-0.04	0.31	0.18	0.20	0.26	0.00	0.20	0.24	0.17	0.17	-0.25	-0.24	0.12
9	0.09	0.74	0.90	0.82	1.29	1.21	1.06	1.11	0.97	0.74	0.05	-0.17	0.73
10	0.31	1.02	1.34	1.29	2.11	2.25	1.51	1.74	1.17	1.18	0.20	0.02	1.18
11	0.57	1.19	1.56	1.71	2.78	3.09	2.23	2.19	1.73	1.54	0.39	0.28	1.61
Midn	0.78	1.29	1.76	2.15	3.41	3.75	2.65	2.57	1.88	1.90	0.58	0.52	1.94
			11.0	2.10	0.11	3.10							
6.6	0.00	7.00	0 ===	0 ===	0.00	0.70	0.90	0.50	0.00	0.0*	1.01	0.75	0.70
6. 6	0.92	1.00	0.75	0.75	0.39	0.19	0.36 0.28	0.52	0 80 0.76	0.97 0.97	1.03	0.75	0.63
8.8	0.98	1.04 0.80	0.77	0.53	-0.26	-0.12	0.28	0.41	0.78	0.57	0.77	0.67	0.39
9. 9	0.78	0.34	0.58		-0.20	-0.56	-0.06	-0.07	0.32	0.71	0.30	0.35	0.05
10.10	-0.14	-0.20				-0.58			-0.29	-0.26		-0.07	-0.31
10.10	-0.14	-0.20	-0.10	-0.57	0.05	-0.30	0.24	0.02	0.20	0.20	0.20	0.01	0.01
7. 2. 9	-0.14	-0.08	-0.18	-0.40	-0.61	-0.57	-0.43	-0.38	-0.22	-0.33	-0.09	-0.13	-0.30
6. 2. 8				-0.19								-0.19	-0.22
6. 2.10	-0.06	ì	0.29			0.33	0.11	0.25	0.11	0.09	0.00	-0.01	0.14
6. 2. 6	-0.24	-0.43	-0.75	-0.72	-1.13	-1.18	-1.00	-0.95	-0.80	-0.75	-0.16	-0.19	-0.69
~ 0	0.47	0.61	0.07	0.0*	1 50	1 59	111	1 11	_0 66	_0 00	_0 22	-0.22	_0.85
7. 2 8. 2			ł			-1.53 $-2.26$						-0.22 $-0.71$	
8. 1												-0.71 -0.36	
7. 1												-0.11	
	0.20	0.00	0.72	1.01	1.00	1.41	1.10	1.10	0.01			,,,,	
9.12.3.9	-0.48	-1.00	-1.38	-1.75	-2.43	-2.36	-1.83	-1.87	-1.57	-1.48	-0.46	-0.25	-1.41
7. 2.2(9)	-0.08	1 -				-0.13						-0.14	
) 1												0.00	0.74
Dail.ext.	-0.40	<b>-0.3</b> 3	-0.01	-0.11	0.43	0.39	0.02	0.08	-0.03	-0.30	-0.26	-0.22	-0.14

### XXXI.

Siberia. — Barnaul. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degre	es of Fa	птеппе	U					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Mean.
										- 00			
Morn. 1	2.54	1.85	4.70			7.83	l .	7.11	5.45	3.06	2.48	1.82	4 95
2	2.81	2.14	5.47	6.30	10.19	8.87	9.77	8.35	6.50	3.78	2.97	2.00	5.76
3	2.70	2.48	6.28	7.07	10.96	9.59	10.69	9.52	7.65	4.52	3.35	2.07	6.41
4	2.39	2.81	7.02	7.45	10.76	9.14	10.67	10.15	8.48	5.15	3.71	2.18	6.66
5	2.07	3.13	7.43	7.09	9.32	7.58	9.50	9.77	8.60	5.47	4.01	2.45	6.37
6	1.96	3.33	9.38	5.87	6.68	5.45	7.18	8.12	5.58	5.29	4.16	2.79	5.65
7	2.00	3.20	5.90	3.87	3.38	2.50	4.05	5.36	2.70	4.46	3.96	2.99	3.94
8	1.93	2.59	3.71	1.37	-0.11	-0.18	0.70	1.96		2.97	3.15	2.70	1.96
9	1.53	1.37	0.86	-1.28	-3.02	-2.48	-2.32	-1.44	-0.56	0.99	1.64	1.73	-0.25
10	0.45	1			-5.06		ł		l .	-1.22	1	0.11	
11	-1.22			1	-6.35	,		1		-3.31	1	-1.76	
Noon	1	-4 03		1			ł	1		-5.00			-
Noon	5.00	4.00	-0.03	-7.04	-1.20	-1.01	-1.52	-1.51	-1.99	3,00	-4.40	-0.42	-0.01
1	-4.59	-5.13	-7 97	-8.35	-8.03	-8.39	-8.42	-8.96	-8.96	-6.05	-5.58	-4.39	-7.07
2		-5.38			-8.78				1	1			
3		-4.77			-9.41		) .	-9.88	ř .	,	1	2	1
4		-3.56											
			0.01	1.01	0.00				1.02		0.00		0.10
5	-2.25	-2.14	-5.65	-5.58	-8.66	-6.32	-8.35	-8.28	-6.26	-4.05	-2.57	-1.60	5.15
6	-0.90	-0.83	-6.46	-3.35	-6.82	-4.39	-6.48	-6.19	-4.25	-2.75	-1.55	-0.83	-3.74
7	0.02	0.09	-2.61	-1.04	-4.16	-1.94	-4.01	-3.51	-207	-1.49	-0.86	-0.43	-1.82
8	0.47	0.63	-0.97		-1.31	0.11				-0.36			
9	0.70	0.92	0.63	2.61	1.46	1.80	1.24	1.80	1.76	0.54	0.00	0.00	1.13
10	0.95	1.10	2.00	3.62	3.78	3.49	3.38	3.67	2.99	1.28	0.52	0.38	2.27
11	1.42	1.28	3.13	4.25	5.69	4.75	5.20	4.97	3.85	1.87	1.15	0.92	3.22
Midn	2.03	1.55	3.98	4.82	7.36	6.26	6.82	6.03	4.59	2.45	1.85	1.44	4.10
0.0	0 -		7 40	- 00	0.0=	0 - 1	0.04	0.00	* 00	1.00	1 01	0.00	0.0=
6. 6	0.54	1.24	1.46		-0.07	0.54	0.34	0.97	1.69	1.28	1.31	0 99	0.97
7. 7	1.01	1.64	1.64		-0.41	0.27	0.02	0.92	1.76	1.49	1.55	1 28	1.06
8.8	1.24	1.62	1.37		-0.72	-0.05	-0.29	0.65	1.35	1.31	1.37	1.24	0.86
9. 9	1.10	1.15	0.74		-0.79	-0.34		0.18	0.59	0.77	0.83	0.86	0.43
10.10	0.70	0.38	-0.09	-0.07	-0.63	-0.56	-0.65	-0.34	-0.34	0.05	0.07	0.25	-0.11
m 9 6	0.00	0.10	0.50	0	1.07	1.40	1.00	0.00	0.00	0	0.50	0.50	0.01
7. 2. 9		-0.43											
6. 2. 8		-0.47			-1.13								
6. 2.10	1	-0.32	1.06		0.56	0 05	0.47	0.72	0.47		-0.34		0.16
6. 2. 6	-1.10	-0.97	-1.76	-2.07	-2.97	-2.57	-2.81	-2.57	-1.94	-1.28	-1.04	0 83	-1.S5
7. 2	-1.64	-1.09	-1.16	-2.42	-2.70	-3.14	-2,56	-2.14	-1.83	-0 97	-0.88	-0.75	-1.77
8. 2		-1.40											
8. 1		-1.27											
7. 1	1	-0.97			ı	1		i .	1				
			1.04		_ 00		,13	1.00	2.00				
9.12.3 9	-1.45	-1.62	-3.29	-3.60	-4.55	-4.23	-4.55	-4.37	-3.92	-2.39	-1.96	-1.37	-3.11
7. 2.2(9)	-0.47	-0.09	-0.27	0.09	-0.63	-0.68	-0.65	-0.18	-0.05	-0.23	-0.45	-0.38	-0.34
Dail. ext.	-1.24	-1.04	0.59	-0.63	0.74	0.34	0.56	0.14	-0 32	-0.47	-0 79	-0.74	-0.41
<u> </u>	1		1	I	I								

### XXXII.

Siberia. — Barnaul. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degre	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.13	0.82	2.09	2.44	3.92	3.48	3.72	3.16	2.42	1.36	1.10	0.81	2.20
2	1.25	0.95	2.43	2.80	4.53	3.94	4.34	3.71	2.89	1.68	1.32	0.89	2.56
3	1.20	1.10	2.79	3.14	4.87	4.26	4.73	4.23	3.40	2.01	1.49	0.92	2.85
4	1.06	1.25	3.12	3.31	4.78	4.06	4.74	4.51	3.77	2.29	1.65	0.97	2.96
5	0.92	1 00	3.30	3.15		0.05	4.22	4.34	0.00	2.43	1.78	1.09	2.83
6	0.92	1.39	4.17	2.61	$\begin{vmatrix} 4.14 \\ 2.97 \end{vmatrix}$	3.37	3.19	3.61	3.82	1	1.85	1	2.53
7	0.89	1.48 1.42	2.62	1.72	1.50	2.42 1.11	1.80	2.38	3.40 2.48	1.98	1.76		1.75
8	0.88	1	1.65	0.61	-0.05	ì	0.31	0.87	1.20	1.32	1.40	I .	0.87
	0.00	1.10	1.00	0.01	0.00	0.00	0.01	0.07	1.20	1.02	1.40	1.20	0.0.
9	0.68	0.61	0.38	-0.57	-1.34	-1.10	-1.03	-0.64	-0.25	0.44	0.73	0.77	-0.11
10	0.20	-0.16	-0.97	-1.66	-2.25	-2.05	-2.08	-1.92	-1.63	-0.54	-0.18	0.05	-1.10
11	-0.54	-1.02	-2.18	-2.57	-2.82	-2.66	-2.82	-2.88	-2.76	-1.47	-1.16	-0.78	-1.97
Noon	-1.37	-1.79	-3.06	-3.26	-3.20	-3.25	-3.34	-3.54	-3.55	-2.22	-1.99	-1.52	-2.67
	200	0.00	0.54	0 ~1	0.55	9.70	0 ***	9.00	0.00	9.00	9.40	1.0-	9.74
1	i	1	1							4	1	-1.95	k I
2 3		1	-3.65	1					1	1		-1.99 -1.68	1 1
4	1	1	1	1	1				Ì	1		-1.08 $-1.19$	1
4	-1.03	-1.55	-5.04	-5.20	-4.22	-5.50	-4.10	-4.22	-3.47	-2.52	-1.71	-1.19	-2.01
5	-1.00	-0.95	-2.51	-2.48	-3.85	-2.81	-3.71	-3.68	-2.78	-1.80	-1.14	-0.71	-2.29
6	-0.40	-0.37	-2.87	-1.49	-3.03	-1.95	-2.88	-2.75	-1.89	-1.22	-0.69	-0.37	-1.66
7	0.01	0.04	-1.16	-0.46	-1.85	-0.86	-1.78	-1.56	-0.92	-0.66	-0.38	-0.19	-0.81
8	0.21	0.28	-0.43	0.46	-0.58	0.05	-0.58	-0.30	0.01	-0.16	-0.18	-0.10	-0.11
9	0.31	0.41	0.28	1.16	ł	0.80	0.55	0.80	0.78	0.24	0.00		0.50
10	0.42	0.49	0.89	1.61	1.68	1.55	1.50	1.63	1.33	0.57	0.23	0.17	1.01
11	0.63	0.57	1.39	1.89	2.53	2.11	2.31	2.21	1.71	0.83	0.51	0.41	1.43
Midn	0.90	0.69	1.77	2.14	3.27	2.78	3.03	2.68	2.04	1.09	0.82	0.64	1.82
6. 6	0.24	0.55	0.65	0.56	-0.03	0.24	0.15	0.43	0.75	0.57	0.58	0.44	0.43
7. 7	0.45	0.73	0.73		-0.18	0.12	0.01	0.41	0.78	0.66	0.69	0.57	0.47
8. 8	0.55	0.72	0.61		-0.32	-0.02		0.29	0.60	0.58	0.61	0.55	0.38
9. 9	0.49	0.51	0.33		-0.35	-0.15		0.08	0.26	0.34	0.37	0.38	0.19
10.10	0.31	0.17	-0.04	-0.03	-0.28	-0.25	-0.29	-0.15	-0.15	0.02	0.03	0.11	-0.05
			0.5	0.00	0.70		0.7	0.00	0.5	0.0		0.0	0.00
7. 2. 9	-0.38							-0.37		-0.21		-0.22	-0.36
6. 2. 8		-0.21						-0.32					-0.31
6. 2.10	1	-0.14	0.47	0.12	0.25	0.02		0.32	0.21		-0.15		0.07
6. 2. 6	-0.62	-0.43	-0.78	-0.92	-1.32	-1.14	-1.25	-1.14	-0.86	-0.57	-0.46	-0.37	-0.82
7. 2	-0.73	-0.49	-0.52	-1.80	-1.20	-1.40	-1.14	-0.95	-0.81	-0.43	-0.39	-0.33	-0.79
8. 2	1											-0.40	1 1
8. 1										i		-0.38	1
7. 1	-0.58	-0.43	-0.46	-1.00	-1.04	-1.31	-0.97	-0.80	-0.75	-0.36	-0.36	-0.31	-0.70
9.12.3.9			1									-0.61	
7. 2.2(9)	-0.21	-0.04	-0.12	0.04	-0.28	-0.30	-0.29	-0.08	-0.02	-0.10	-0.20	-0.17	-0.15
Dail.ext.	-0.55	-0.46	0.26	-0.28	0.33	0.15	0.25	0.06	-0.14	-0.21	_0.35	-0.33	-0.18
Dan.ext.	-0.00	0.40	0.20	0.20	0.00	0.19	0.40	0.00	0.14	0.21	-0.55	0.00	0.10

### XXXIII.

Siberia. — Barnaul. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — DOVE.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0.99	1.98	2.43	2.65	3.70	3.75	3.48	3.10	2.80	1.99	1.06	0.77	2.39
Midn.	1.15	2.21	2.45	3.03	4.11	4.30	4.07	3.50	3.20	2.24	1.22	0.77	2.72
1	1.15	2.36	3.13	3.24	4.11	4.83	4.49	3.90	3.63	2.50	1.39	0.95	3.00
2	1.41	2.47	3.34	3.49	4.47	4.95	4.49	4.29	3.92	2.69	1.46	1.01	3.21
3 4	1.56	2.56	3.61	3.59	4.72	4.93	4.40	4.23	4.11	2.89	1.51	1.07	3.18
5	1.55	2.68	3.70	2.78	2.85	3.12	3.34	3.60	3.90	2.91	1.57	1.10	2.76
Э	1.55	2.03	3.70	2.10	2.00	5.12	9.94	3.00	5.90	2.91	1.97	1.10	2.10
6	1.61	2.69	2.90	1.58	1.44	1.75	1.88	2.29	3.06	2.68	1.59	1.09	2.05
7	1.53	2.30	1.63	0.46	0.28	0.49	0.50	0.85	1.54	1.84	1.50	1.18	1.17
8	0.94	1.15	0.13	-0.69	-0.80	-0.65	-0.54	-0.51	-0.08	0.87	0.95	0.93	0.14
9	0.27	-0.47	-1.35	-1.80	-1.94	-1.78	-1.81	-1.79	-1.62	-0.73	-0.03	0.11	-1.08
10	-0.79	-1.90	-2.36	-2.68	-2.71	-2.75	-2.70	-2.80	-2.84	-1.96	-1.12	-0.83	-2.12
11	-1.69	-2.95	-3.31	-3.27	-3.39	-3.39	-3.44	-3.41	-3.75	-2.81	-1.93	-1.62	-2.91
	205	2.00	0 0							2.10		201	
Noon.							}	-3.81					-3.44
1	-2.61					-4.19			-4.41		-2.57	-2.12	-3.66
2	-2.39					-4.34		i	-4.34				-3.60
3	-1.88					-4.19	ļ	1	-4.11				-3.22
4		-2.30				-3.57		i .	-3.21				-2.56
5	-0.S1	-1.30	-1.69	-1.82	-3.09	-3.04	-3.07	-2.78	-2.29	-1.49	-0.71	-0.53	-1.89
6	-0.41	-0.56	-0.84	-0.62	-1.92	-2.19	-2.09	-1.54	-1.05	-0.72	-0.33	-0.28	-1.05
7	-0.20	0.09	0.35	0.27	-0.46	-0.84	-0.69	-0.20	-0.17	-0.08	-0.03	-0.02	-0.17
8	0.12	0.69	0.39	0.99	0.77	0.51	0.52	0.67	0.60	0.31	0.23	0.19	0.50
9	0.32	1.08	0.88	1.50	1.64	1.48	1.42	1.46	1.26	0.82	0.42	0.39	1.06
10	0.73	1.47	1.46	2.02	2.42	2.31	2.22	2.04	1.85	1.29	0.58	0.58	1.58
11	0.78	1.76	1.92	2.35	3.11	3.05	2.88	2.58	2.36	1.68	0.83	0.75	2.00
Mean.	-14.71	-13.47	-5.47	1.77	7.78	13.62	14.98	12.76	7.53	1.58	-8.36	-13.07	4.94

The numbers without sign must be added; those with the sign — must be subtracted.

# HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

EUROPE.



### XXXIV.

## Italy. - Rome. Lat. 41° 54' N. Long. 12° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Mours.   Dan.   Feb.   March.   April.   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Mean.						Degree	s of Rea	aumur.						
2	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
2						n)								
1.14   1.58   1.96   2.31   2.56   3.02   2.99   3.00   2.38   2.12   1.53   1.19   2.15     4	Morn. 1	0.90	1.08	1.22	1.55	1.88	2.44	2.17	2.20	1.63	1.50	1.15	0.93	1.55
1.36	2	0.99	1.26	1.50	1.84	2.10	2.59	2.41	2.49	1.91	1.75	1.29	1.02	1.76
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	1.14	1.58	1.96	2.31	2.56	3.02	2.99	3.00	2.38	2.12	1.53	1.19	2.15
6   1.77   2.52   2.76   2.92   3.04   3.36   3.81   3.53   3.17   3.10   2.42   1.87   2.86   7   1.74   2.33   2.24   2.25   2.19   2.38   2.82   2.62   2.58   2.58   2.32   2.33   1.83   2.34   1.40   1.73   1.29   1.15   0.93   0.98   1.27   1.22   1.51   2.05   1.82   1.47   1.40   9   0.72   0.78   0.10   -0.15   -0.47   -0.51   -0.44   -0.35   -0.15   0.56   0.93   0.78   0.20   10   -0.24   -0.38   -1.08   -1.39   -1.68   -1.75   -1.89   -1.78   -1.23   -0.58   -0.22   -0.15   -1.03   11   -1.27   -1.54   -2.06   -2.36   -2.53   -2.59   -2.87   -2.84   -2.41   -2.00   -1.41   -1.14   -2.09   1.15   -2.69   -3.07   -3.02   -3.27   -3.23   -3.40   -3.61   -3.81   -3.70   -3.82   -3.00   -2.52   -3.26   -2.78   -3.25   -2.44   -3.32   -3.38   -3.37   -3.70   -3.76   -3.92   -3.80   -3.99   -3.16   -2.66   -2.66   -3.33   -3.70   -3.76   -3.92   -3.80   -3.99   -3.16   -2.66   -2.66   -3.33   -3.70   -3.76   -3.82   -3.01   -2.66   -3.69   -2.84   -2.41   -2.09   -2.64   -1.83   -2.51   -2.45   -2.72   -3.14   -4.05   -3.88   -3.62   -3.11   -3.04   -2.41   -1.95   -2.89   -3.61   -2.66   -3.34   -3.44   -3.53   -3.84   -4.15   -3.85   -3.62   -3.11   -3.04   -2.41   -1.95   -2.89   -3.60   -3.99   -3.66   -3.65   -3.44   -3.35   -3.64   -4.85   -3.85   -3.62   -3.11   -3.04   -2.41   -1.95   -2.89   -3.69   -3.99   -3.66   -3.65   -3.44   -3.35   -3.65   -3.25   -2.44   -3.26   -3.15   -3.65   -3.65   -3.15   -3.65   -3.65   -3.25   -3.24   -3.26   -3.15   -3.65   -3.65   -3.25   -3.24   -3.25	4	1.36	1.99	2.46	2.80	3.06	3.51	3.68	3.54	2.91	2.58	1.87	1.43	2.60
6   1.77   2.52   2.76   2.92   3.04   3.36   3.81   3.53   3.17   3.10   2.42   1.87   2.86   7   1.74   2.33   2.24   2.25   2.19   2.38   2.82   2.62   2.58   2.58   2.32   2.33   1.83   2.34   1.40   1.73   1.29   1.15   0.93   0.98   1.27   1.22   1.51   2.05   1.82   1.47   1.40   9   0.72   0.78   0.10   -0.15   -0.47   -0.51   -0.44   -0.35   -0.15   0.56   0.93   0.78   0.20   10   -0.24   -0.38   -1.08   -1.39   -1.68   -1.75   -1.89   -1.78   -1.23   -0.58   -0.22   -0.15   -1.03   11   -1.27   -1.54   -2.06   -2.36   -2.53   -2.59   -2.87   -2.84   -2.41   -2.00   -1.41   -1.14   -2.09   1.15   -2.69   -3.07   -3.02   -3.27   -3.23   -3.40   -3.61   -3.81   -3.70   -3.82   -3.00   -2.52   -3.26   -2.78   -3.25   -2.44   -3.32   -3.38   -3.37   -3.70   -3.76   -3.92   -3.80   -3.99   -3.16   -2.66   -2.66   -3.33   -3.70   -3.76   -3.92   -3.80   -3.99   -3.16   -2.66   -2.66   -3.33   -3.70   -3.76   -3.82   -3.01   -2.66   -3.69   -2.84   -2.41   -2.09   -2.64   -1.83   -2.51   -2.45   -2.72   -3.14   -4.05   -3.88   -3.62   -3.11   -3.04   -2.41   -1.95   -2.89   -3.61   -2.66   -3.34   -3.44   -3.53   -3.84   -4.15   -3.85   -3.62   -3.11   -3.04   -2.41   -1.95   -2.89   -3.60   -3.99   -3.66   -3.65   -3.44   -3.35   -3.64   -4.85   -3.85   -3.62   -3.11   -3.04   -2.41   -1.95   -2.89   -3.69   -3.99   -3.66   -3.65   -3.44   -3.35   -3.65   -3.25   -2.44   -3.26   -3.15   -3.65   -3.65   -3.15   -3.65   -3.65   -3.25   -3.24   -3.26   -3.15   -3.65   -3.65   -3.25   -3.24   -3.25														
Total   Tota	5	1.60	2.36	2.80	3.07	3 30	3.71	4.06	3.79					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	1.77	2.52	2.76	2.92	3.04	3.36	3.81	3.53	3.17	3.10			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	1.74	2.33	2.24	2.25	2.19	2.38	2.82	2.62	2.58	2.82	2.33	1.83	2.34
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	1.40	1.73	1.29	1.15	0.93	0.98	1.27	1.22	1.51	2.05	1.82	1.47	1.40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.70	0.40	0.10	0.15	_0 17	_0.51	_0.11	_0.95	0.15	0.86	0.03	0.78	0.20
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1			l .	l	1	1	1						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		1											
1	1 .	ì	1		1	i .	)							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Noon	-2.15	-2.49	-2.71	-2.98	-5.01	-3.08	-3.38	-9.49	-5.24	-9.14	2.09	1.00	A+04
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	-2.69	-3.07	-3.02	-3.27	-3.23	-3.40	-3.61	-3.81	-3.70	-3.82	-3.00	-2.52	-3.26
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	t I	1									1			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				1		1	1		1					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1		1											-2.89
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	*	1.00	2.01	2.40	2	0.11	1.00	0.00	0.02	0.11	0.01			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	-1.11	-1.81	-1.89	-2.15	-2.70	-3.70	-3.53	-3.05	-2.38	-2.21	-1.76	-1.35	-2.30
8         0.39         0.25         0.26         0.30         0.29         0.13         0.08         0.21         0.38         0.19         0.05         0.17         0.23           9         0.59         0.67         0.78         0.94         1.22         1.46         1.33         1.22         1.05         0.71         0.46         0.46         0.91           10         0.71         0.99         1.07         1.31         1.76         2.29         2.10         1.86         1.43         1.05         0.76         0.66         0.66         1.33           Midn         0.84         1.02         1.15         1.44         1.93         2.57         2.33         2.11         1.54         1.24         0.95         0.79         1.49           Midn         0.84         1.02         1.15         1.44         1.93         2.57         2.33         2.11         1.54         1.24         0.95         0.79         0.79         1.49           Midn         0.86         0.66         0.57         0.28         0.57         0.68         0.85         0.89         0.67         0.56         0.67           8. 8         0.89         0.99	6	-0.45	-1.05	-1.20	-1.39	-1.91	-2.79	-2.67	-2.18	-1.48	-1.32	-1.09	-0.75	-1.52
8       0.39       0.25       0.26       0.30       0.29       0.13       0.08       0.21       0.38       0.19       0.05       0.17       0.23         9       0.59       0.67       0.78       0.94       1.22       1.46       1.33       1.22       1.05       0.71       0.46       0.46       0.91         10       0.71       0.90       1.07       1.31       1.76       2.29       2.10       1.86       1.43       1.05       0.76       0.66       0.66         11       0.78       0.99       1.15       1.44       1.93       2.57       2.33       2.11       1.54       1.24       0.95       0.79       1.49         Midn       0.84       1.02       1.15       1.44       1.93       2.57       2.33       2.11       1.54       1.24       0.95       0.79       1.49         Midn       0.84       1.02       1.14       1.93       2.57       2.33       2.11       1.54       1.24       0.95       0.79       1.49         Midn       0.85       0.89       0.67       0.68       0.85       0.89       0.67       0.56       0.67         0.91       <	7	0.05	-0.34	-0.11	-0.53	-0.84	-1.42	-1.38	-1.01	-0.51	-0.50	-0.48	-0.24	-0.64
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	0.39	0.25	0.26	0.30	0.29	0.13	0.08	0.21	0.38	0.19	0.05	0.17	0.23
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.59	0.67	0.78	0.94	1.22	1.46	1.33	1.22	1.05	0.71			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	0 71	0.90	1.07	1.31	1.76	2 29	2.10	1.86	1.43	1.05			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	0.78	0.99	1.15	1.44	1.93	2.57	2.33	2.11	1.54	1.24	0.95	0.79	1.49
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Midn	0.84	1.02	1.15	1.46	1.88	2.51	2.24	2.14	1.55	1.36	1.06	0.86	1.51
$\begin{array}{cccccccccccccccccccccccccccccccccccc$														
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			٥ ،	0 ==0	0 ==0		0.00	0 ==	0.00	0.05	0.00	0.67	0.56	0.67
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1			1					1		l .		1	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1					i .	1			1	1	4	1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1					1					1	1	1	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1				1	í							i .	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.10	0.24	0.26	-0.01	-0.04	0.04	0.27	0.10	0.04	0.10	0.23	0.27	0.26	0.15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7 2 0	-0.15	-0.00	-0.01	-0.02	0.09	0.05	0.13	-0.03	-0.06	-0.15	-0.12	-0.12	-0.05
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	1		1	ļ.			l .	)			1	l .	1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	1							l .		1	1		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1	1				1	1	1				1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0. 2. 6	-0.49	-0.59	-0.49	-0.58	-0.73	-1.04	-0.07	0.00	-0.70	0.14	0.01	0.01	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7. 2	-0.52	-0.46	-0.40	-0.52	-0.56	-0.66	-0.47	-0.65	-0.61	-0.59	-0.42	-0.42	-0.52
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						,								
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1				,								-0.53	-0.93
$ \begin{vmatrix} 9.12.3.9 \\ 7. & 2.2(9) \end{vmatrix} \begin{vmatrix} -0.82 \\ 0.04 \end{vmatrix} \begin{vmatrix} -1.02 \\ 0.11 \end{vmatrix} \begin{vmatrix} -1.17 \\ 0.19 \end{vmatrix} \begin{vmatrix} -1.32 \\ 0.21 \end{vmatrix} \begin{vmatrix} -1.39 \\ 0.21 \end{vmatrix} \begin{vmatrix} -1.53 \\ 0.33 \end{vmatrix} \begin{vmatrix} -1.53 \\ 0.40 \end{vmatrix} \begin{vmatrix} -1.60 \\ 0.43 \end{vmatrix} \begin{vmatrix} -1.62 \\ 0.29 \end{vmatrix} \begin{vmatrix} -1.41 \\ 0.29 \end{vmatrix} \begin{vmatrix} -1.32 \\ 0.06 \end{vmatrix} \begin{vmatrix} -0.98 \\ 0.02 \end{vmatrix} \begin{vmatrix} -0.80 \\ 0.02 \end{vmatrix} \begin{vmatrix} -1.25 \\ 0.19 \end{vmatrix} $	1									-0.56	-0.50	-0.34	-0.35	-0.46
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							i				į.		1	
71 2.2(0) 0.01 0.11 0.03	9.12.3.9	-0.82	-1.02	-1.17				Į.				1		
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	7. 2.2(9)	0.04	0.11	0.19	0.21	0.33	0.40	0.43	0.29	0.22	0.06	0.02	0.02	0.19
Dail.ext.   -0.51   -0.37   -0.12   -0.11   -0.01   -0.17   0.09   -0.07   -0.25   -0.45   -0.37   -0.40   -0.25	72 11	0.7-	0.00	0.10	0.77	0.03	0.15	0.00	0.0~	0.00	_0.45	_0.9*	_0.40	-0.25
	Dail.ext.	-0.51	-0.37	-0.12	-0.11	-0.01	-0.17	0.09	-0.07	1-0.28	-0.45	-0.57	-0.40	-0.20

### XXXV.

# Italy. — Padua. Lat. 45° 24' N. Long. 11° 52' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						es of Ite							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.58	0.57	0.89	1.23	2.43	2.21	2.86	2.27	1.59	0.86	1.04	0.83	1.45
2	0.58	0.81	1.20	1.49	2.70	2.40	3.20	2.70	1.85	1.03	1.16	0.96	1.67
3	0.76	0.97	1.42	1.66	3.00	1		1	1			1	
4	0.79	1.13	1.68	1.97	3.14	2.71	1	1	2.34	1	1		
								0.11		1.00	1.00	1.00	2.00
5	1.06	1.31	1.89	2.26	2.97	2.39	3.34	3.44	2.66	1.58	1.42	1.12	2.12
6	1.13	1.46	2.06	2.22	1.96	1.22	2.07	2.93	2.54	1 54	1.49	1.16	1.82
7	1.25	1.58	1.86	1.82	0.66	1	1		1.78	1.37		1	ł .
8	1.07	1.42	0.66	1.03	-0.23	-0.65	-0.25	0.58	0.79	0.81	0.97	ł.	į.
9	0.70	0.82	0.61	0.18	-1.07	-1.24	-1.63	-1.65	-0.58	0.18	0.02	0.33	-0.28
10	1							-1.90				-0.26	1
11		-0.62						-2.38					
Noon		-1.24						-2.97				-1.50	1
1,0011	0.00		1.02	2121		2.02	0.10	2.3.	2.11	1.41	2.02	1.00	1.04
1	-1.38	-1.45	-1.54	-1.68	-2.88	-2.61	-3.53	-3.34	-2.54	-1.74	-2.42	-1.90	-2.25
2								-3.73					
3								-3.81					
4								-3.23					
5													
11								-2.49				-0.74	
6								-1.34				-0.33	1
7								-0.32				-0.15	-0.36
8	-0.07	-0.42	-0.43	-0.47	-0.14	0.38	1.01	0.50	-0.10	0.05	0.33	0.04	0.06
9	0.05	-0.14	-0.10	-0.11	1.11	1.38	1.54	1.01	0.23	0.26	0.49	0.26	0.50
10	0.18	0.09	0.24	0.27	1.44	1.72	1.67	1.36	0.58	0.52	0.72	0.46	0.77
11	0.29	0.31	0.48	0.60	1.75	1.86	2.14	1.78	0.84	0.68	0.86	0.59	1.02
Midn	0.37	0.49	0.72	0.85	2.02	2.10	2.43	2.23	1.36	0.78	0.94	0.70	1.25
I IIIIIII	0.07	0.10	0	0.00	2.02	2.10	2.40	2.20	1.00	0.70	0.04	0.70	1.25
6. 6	0.27	0.34	0.52	0.36	0.38	0.11	0.33	0.80	0.86	0.50	0.67	0.42	0.46
7. 7	0.47	0.48	0.57	0.35	0.20	-0.02	0.05	0.75	0.80	0.62	0.55	0.54	0.47
8.8	0.50	0.50	0.12	0.28	-0.19	-0.14	0.38	0.54	0.35	0.43	0.65	0.52	0.33
9. 9	0.38	0.34	0.26	0.04	0.02	0.07	-0.05	-0.32	-0.18	0.22	0.26	0.30	0.11
10.10	0.14	0.01	-0.30	-0.08	-0.13	0.03	-0.31	-0.27	-0.23	0.01	-0.05	0.10	-0.09
7. 2. 9	-0.07	-0.06	0.01	-0.07	-0.39	-0.39	-0.55	-0.30	-0.28	-0.13	-0.16	-0.19	-0.21
6. 2. 8								-0.10					
6. 2.10	-0.07		0.19	0.19			-0.00		0.09		-0.11		0.05
6. 2. 6	l 1	-0.32	1			1			1	-0.34			-0.51
	-0.13							-0 96	i				]
8. 2		1							,				
8. 1								-1.58					
7. 1	-0.16 $-0.07$	$\begin{array}{c c} -0.02 \\ 0.07 \end{array}$	0.14					-1.38					
						- 1		-0.76		ļ	1		
11 4 . 1	-0.42	1						-1.86			ſ		- 11
7. 2.2(9)	-0.04	-0.08	-0.02	-0.0s	-0.02	0.06	-0.03	0.03	-0.15	-0.03	-0.00	<b>-0.0</b> S	-0.04
Dail.ext.	-0.13	-0.04	0.08	0.06	0.10	0.05	0.02	-0.19	-0.11	-0.23	-0.49	-0.42	-0.16

#### XXXVI.

## Switzerland. — Geneva. Lat. 46° 12' N. Long. 6° 9' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.50	0.68	1.38	1.68	2.16	2.77	2.54	2.38	1.86	1.44	0.80	0.48	1.56
1	0.62	0.83	1.88	2.14	2.72	3.32	3.19	3.08	2.41	1.71	0.97	0.54	1.95
2	0.74	1.01	2.34	2.53	3.16	3.68	3.70	3.68	2.93	1.95	1.14	0.61	2.29
3	0.83	1.22	2.70	2.76	3.40	3.74	3.89	4.03	3.34	2.14	1.30	0.70	2.50
4	0.92	1.46	2.89	2.78	3.34	3.50	3.80	4.00	3.49	2.22	1.43	0.81	2.55
5	0.98	1.66	2.83	2.54	2.93	2.88	3.26	3.52	3.30	2.14	1.51	0.91	2.37
0	0.50	1.00	2.00	₩.0 x	2.35	2.00	0.20	0.02	0.00	2.11	1.01	0.01	2.01
6	1.02	1.75	2.49	2.03	2.22	2.03	2.39	2.65	2.72	1.85	1.48	0.97	1.97
7	0.97	1.66	1.90	1.33	1.28	1.05	1.38	1.54	1.84	1.34	1.26	0.92	1.37
8	0.78	1.33	1.09	0.50	0.27	0.08	0.26	0.37	0.78	0.65	0.84	0.70	0.64
9	0.46	0.74	0.17	-0.34	-0.69	-0.82	-0.71	-0.70	-0.30	-0.15	0.23	0.34	-0.16
10	-0.02	-0.01	-0.77	-1.10	-1.51	-1.57	-1.53	-1.58	-1.26	-0.98	-0.47	-0.16	-0.91
11	-0.57	-0.80	-1.61	-1.75	-2.17	-2.18	-2.24	-2.29	-2.06	-1.70	-1.14	-0.67	-1.60
	1.00	7 40	2.20	0.00	0.00	2 =0	0.74	9.0-	9.00	0.00	1.00	1.10	0.14
Noon.						4.	1	-2.85			1	-1.10	-2.14 $-2.51$
1 2								-3.29		1		-1.37 $-1.41$	
3							1	-3.58					-2.66
4		-2.10						-3.65				$\begin{bmatrix} -1.26 \\ -0.97 \end{bmatrix}$	-2.61
5							1	-3.43	1			-0.97 -0.64	
Э	-0.79	-1.37	-2.10	-1.97	-2.32	-2.78	-2.90	-2.92	-2.57	-1.59	-0.99	-0.04	-1.91
6	-0.46	-0.94	-1.59	-1.46	-1.70	-2.11	-2.22	-2.18	-1.91	-1.06	-0.62	-0.32	-1.38
7	-0.20	-0.51	-1.06	-0.90	-1.00	-1.29	-1.40	-1.31	-1.16	-0.53	-0.30	-0.07	-0.81
8	-0.01	-0.14	-0.54	-0.34	-0.29	-0.42	-0.49	-0.46	-0.42	-0.02	-0.03	0.11	-0.26
9	0.12	0.14	0.05	0.20	0.38	0.47	0.34	0.32	0.26	0.42	0.20	0.24	0.26
10	0.25	0.37	0.42	0.70	0.91	1.30	1.10	1.02	0.83	0.82	0.42	0.34	0.71
11	0.37	0.54	0.90	1.20	1.51	2.07	1.87	1.70	1.35	1.15	0.62	0.41	1.14
Mean	-0.53	1.24	3.41	6.77	10.37	13.31	14.30	13.58	11.46	7.48	3.76	0.58	

### XXXVII.

SWITZERLAND. — GENEVA. Lat. 46° 12′ N. Long. 6° 9′ E. Gr. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.45	0.69	1.26	1.44	1.54	1.98	2.12	1.63	1.44	0.94	0.50	0.59	1.21
2	0.70	0.96	2.21	2.62	2.60	3.20	3.18	2.83	2.72	1.46	0.73	0.66	1.99
4	1.01	1.33	2.91	3.36	3.11	3.55	3.82	3.51	3.26	1.90	1.02	0.80	2.46
6	1.19	1.49	2.70	2.87	2.26	2.38	2.47	2.82	2.79	1.74	1.13	0.97	2.07
8	1.22	1.22	1.42	0.74	0.27	0.13	0.22	0.49	0.72	0.94	0.90	0.95	0.77
10	-0.02	-0.25	-0.68	-1.70	-1.30	-1.34	-1.25	-1.01	-1.10	-0.73	-0.26	-0.14	-0.73
	0.00								2.00	1.00	1 10	7.00	7.07
Noon.	1							-2.34					
2	-1.69	-1.70	-2.82	-2.94	-2.97	-3.09	-3.11	-3.17	-3.03	-2.35	-1.55	-1.46	-2.49
4	-1.30	-1.61	-2.70	-2.94	-2.46	-2.87	-2.89	-3.04	-2.86	-1.53	-1.19	-1.05	-2.20
6	-0.54	-0.90	-1.79	-2.06	-1.40	-1.89	-2.24	-2.04	-1.74	-0.88	-0.45	-0.43	-1.36
8	-0.09	-0.21	-0.89	-0.70	-0.10	-0.25	-0.58	-0.38	-0.38	-0.08	0.03	0.10	-0.29
10	0.20	0.28	0.34	0.40	0.86	0.78	0.78	0.69	0.57	0.47	0.29	0.18	0.49
ľ													
Mean.	1.20	0.47	2.28	6.81	9.48	12.82	14.43	13.74	10.66	7.73	3.30	0.12	

### XXXVIII.

SWITZERLAND. - St. BERNARD. Lat. 45° 52' N. Long. 9° 22' E. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.48	0.81	1.34	1.96	2.10	1.72	1.62	1.30	0.76	1.02	0.59	0.31	1.17
1	0.63	0.91	1.58	2.22	2.45	1.99	1.93	1.53	0.97	1.17	0.66	0.33	1.36
2	0.81	1.09	1.82	2.40	2.73	2.15	2.14	1.82	1.17	1.30	0.78	0.40	1.55
3	0.99	1.26	1.98	2.46	2.81	2.24	2.24	1.94	1.34	1.36	0.89	0.50	1.67
4	1.08	1.38	2.02	2.34	2.67	2.14	2.17	1.91	1.41	1.34	0.98	0.52	1.66
5	1.08	1.34	1.84	2.00	2.28	1.88	1.90	1.70	1.35	1.19	0.98	0.66	1.52
6	0.91	1.14	1.42	1.45	1.72	1.42	1.44	1.34	1.14	0.92	0.86	0.62	1.20
7	0.60	0.74	0.79	0.70	0.81	0.81	0.82	0.76	0.77	0.83	0.61	0.50	0.73
s	0.17	0.18	0.00	-0.16	-0.08	0.09	0.10	0.12	0.29	0.06	0.26	0.26	0.11
9	-0.31	-0.48	-0.85	-1.06	-1.10	-0.66	-0.66	-0.53	-0.26	-0.46	-0.22	-0.06	-0.55
10	-0.78	-1.13	-1.63	-1.86	-1.94	-1.36	-1.34	-1.13	-0.78	-0.94	-0.68	-0.41	-1.16
11	-1.14	-1.66	-2.23	-2.50	-2.58	-1.95	-1.90	-1.60	-1.22	-1.33	-1.09	-0.71	-1.66
Noon.	-1.34	-1.98	-2.58	-2.87	-2.96	-2.34	-2.26	-1.90	-1.51	-1.58	-1.36	-0.94	-1.97
1	-1.38	-2.04	-2.62	-2.98	-3.06	-2.51	-2.40	-2.02	-1.62	-1.66	-1.47	-1.03	-2.07
2	-1.24	-1.86	-2.38	-2.78	-2.89	-2.44	-2.33	-1.94	-1.56	-1.59	-1.39	-0.99	-1.95
3	-0.98	-1.47	-1.92	-2.36	-2.51	-2.21	-2.08	-1.74	-1.35	-1.38	-1.16	-0.82	-1.66
4	-0.65	-0.97	-1.34	-1.79	-1.98	-1.80	-1.70	-1.42	-1.05	-1.07	-0.83	-0.57	-1.26
5	-0.32	-0.43	-0.73	-1.17	-1.40	-1.32	-1.26	-1.06	-0.70	-0.72	-0.46	-0.27	-0.82
6	-0.05	0.04	-0.19	-0.54	-0.81	-0.80	-0.80	-0.70	-0.38	-0.36	-0.10	0.00	-0.39
7	0.14	0.39	0.25	0.04	-0.25	-0.28	-0.34	-0.34	-0.11	-0.03	0.19	0.21	-0.01
8	0.25	0.60	0.56	0.54	0.27	0.20	0.09	0.00	0.10	0.24	0.38	0.34	0.30
9	0.30	0.69	0.78	0.96	0.76	0.63	0.50	0.32	0.27	0.47	0.49	0.38	0.55
10	0.34	0.72	0.96	1.33	1.22	1.02	0.89	0.64	0.42	0.67	0.53	0.38	0.76
11	0.38	0.74	1.14	1.66	1.68	1.40	1.26	0.97	0.58	0.85	0.55	0.33	0.96
Mean.	-8.26	-6.62	-5.72	-2.97	0.74	3.55	4.82	4.32	2.40	-0.91	-3.95	-5.86	

### XXXIX.

Switzerland. — St. Bernard. Lat. 45° 52′ N. Long. 9° 22′ E. Gr. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.34	0.55	0.75	1.19	1.26	1.39	1.02	1.08	0.81	0.66	0.33	0.28	0.80
2	0.52	0.78	1.14	1.64	1.75	1.88	1.62	1.53	1.16	0.94	0.42	0.27	1.14
4	0.82	1.06	1.50	1.84	1.91	1.98	1.82	1.71	1.34	1.17	0.65	0.42	1.35
6	0.65	0.86	1.20	1.50	1.53	1.46	1.46	1.27	0.98	0.88	0.50	0.32	1.05
8	0.48	0.26	0.14	-0.08	-0.25	0.01	0.22	0.16	0.08	0.28	0.27	0.15	0.14
10	-0.35	-0.91	-1.06	-1.26	-1.39	-1.18	-1.11	-0.94	-0.86	-0.68	-0.54	-0.23	-0.88
Noon.	7 10	1 00		2									
1									i		-1.26	-0.91	-1.65
2	-1.37	-1.55	-1.89	-2.12	-2.12	-2.23	-2.01	-1.97	-1.54	-1.52	-1.23	-1.22	-1.73
4	-0.42	-0.71	-1.14	-1.55	-1.47	-1.65	-1.49	-1.30	-0.88	-0.86	-0.37	-0.02	-0.99
6	0.09	0.17	0.09	-0.26	-0.35	-0.71	-0.57	-0.46	-0.26	-0.07	0.08	0.22	-0.17
8	0.25	0.44	0.49	0.49	0.50	0.35	0.30	0.26	0.26	0.22	0.70	0.30	0.38
10	0.37	0.55	0.55	0.71	0.76	0.64	0.56	0.43	0.46	0.43	0.40	0.40	0.52
Mean.	-6.03	-8.83	-6.66	-3.01	-0.42	2.71	4.82	4.70	2.07	-0.36	-5.46	-6.18	

### XL.

Austria. — Kremsmünster. Lat. 48° 3′ N. Long. 14° 7′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of Re	eaumur.						
Hours,	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
N 1	0.58	0.90	1.05	1.14	2.30	2.77	1.00	1 04	1.52	1.90	0.61	0.40	1.00
Morn. 1	0.66		1.30	1.14	Į.	(	1.86 2.16	1.94 2.26	1	1		0.40	1.36 1.60
3	0.71	1.07	1.57	1.63		3.14	2.35	2.50		1		1	1.76
4	0.78	1.12	1.80	1.88	2.78	2.90	2.34	2.54	1	1.97	1		1.83
	0.04	7.70	7.00			2 22		2.00			,		
5 6	0.84 0.88		1.90 1.82	1.99 1.88	2.44 1.86	2.32 $1.54$	2.08 1.54	2.30 1.80	$\begin{vmatrix} 2.60 \\ 2.34 \end{vmatrix}$	1.98 1.91			1.75
7	0.84		1.50	1.41	1.11	0.68	0.94	1.11	1.81		$0.93 \\ 0.92$	1	1.52 1.15
8	0.67		0.96	0.87	0.31		0.23	0.35	1.09	1.21	0.80		0.66
9	0.35		0.30				-0.42		0.28		0.51	0.38	0.10
10	-0.10	$\begin{vmatrix} 0.01 \\ -0.72 \end{vmatrix}$					-0.95						-0.56
Noon	ll e	-0.72 $-1.37$									-0.47		-1.08
110011							ľ						
1		-1.78											
2		-1.90											
3		-1.69											
4	-0.86	-1.32	-1.79	-1.89	-2.51	-2.49	-2.22	-2.34	-2.52	-2.17	-1.01	-0.66	-1.98
5	-0.59	-0.92	-1.48	-1.60	-2.15	-2.16	-1.88	-2.00	-2.18	-1.69	-0.68	-0.35	-1.47
6		-0.57		-1.18	-1.62	-1.66	-1.38	-1.49	-1.66	-1.14	-0.41		
7	Į.	-0.36					-0.76					0.02	-0.62
8	-0.04	-0.19	-0.23	-0.17	-0.34	-0.35	-0.15	-0.24	-0.46	-0.26	-0.11	0.09	-0.20
9	0.07	-0.02	0.13	0.28	0.28	0.34	0.38	0.30	0.05	0.06	-0.02	0.12	0.16
10	0.20	0.18	0.42	0.61	0.84	1.02	0.82	0.76	0.46	0.34	0.11	0.18	0.49
11	0.34	0.46	0.63	0.82	1.36	1.68	1.19	1.15	0.80	0.63	0.27	0.25	0.80
Midn	0.47	0.70	0.83	0.97	1.85	2.27	1.52	1.53	1.14	0.94	0.46	0.34	1.08
6. 6	0.27	0.34	0.37	0.35	0.12	-0.06	0.08	0.16	0.34	0.39	0.26	0.22	0.24
7. 7	0.33	0.45	0.43	0.37		-0.18	0.09	0.13	0.38	0.48	0.35	0.29	0.27
8.8	0.32	0.44	0.37	0.35	-0.02	-0.10	0.04	0.06	0.32	0.48	0.35	0.24	0.24
9. 9	0.21	0.33	0.22	0.21		-0.26	-0.02	-0.04	0.17	0.34	0.25	0.25	0.13
10.10	0.05	0.10	0.01	0.02	-0.13	-0.20	-0.07	-0.11	-0.03	0.11	0.09	0.12	0.00
7. 2. 9	-0.12	-0.22	-0.13	-0.12	-0.41	-0.52	-0.31	-0.32	-0.23	-0.28	-0.17	-0.16	-0.25
6. 2. 8	-0.14	-0.28											
6. 2.10	-0.06		0.07	0.14		-0.01	0.03	0.06				-0.12	
6. 2. 6	-0.24	-0.41	-0.43	-0.45	-0.79	-0.90	-0.70	-0.69	-0.63	-0.94	-0.36	-0.15	-0.56
7. 2	-0.21	-0.32	-0.26	-0.33	-0.76	-0.95	-0.66	-0.63	-0.38	-0.45	-0.24	-0.25	-0.45
8. 2		-0.42											
8. 1	-0.28	-0.36	-0.47	-0.53	-1.06	-1.14	-0.91	-0.93	-0.60	-0.52	-0.25	-0.24	-0.61
7. 1	-0.19	-0.26	-0.20	-0.26	-0.66	-0.87	-0.56	-0.55	-0.24	-0.31	-0.19	-0.22	-0.38
9.12.3.9	-0.42	-0.60	-0.78	-0.82	-1.23	-1.33	-1.03	-1.10	-1.03	-0.87	-0.11	-0.31	-0.83
7. 2.2(9)	-0.07	-0.17	-0.07	-0.02	-0.24	-0.31	-0.15	-0.17	-0.14	-0.19	-0.13	-0.07	-0.14
` '				1									
Dail. ext.	-0.19	-0.32	-0.06	-0.04	0.09	0.36	0.01	0.04	-0.03	<b>-0.2</b> 8	-0.24	-0.25	-0.08

#### XLI.

## Austria. - Salzburg. Lat. 47° 48' N. Long. 13° 1' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.54	0.70	1.06	1.31	2.03	2.07	1.87	1.57	1.21	1.02	0.48	0.42	1.19
1	0.59	0.79	1.29	1.58	2.37	2.27	2.13	1.81	1.45	1.15	0.65	0.50	1.38
2	0.72	0.97	0.51	1.79	2.64	2.56	2.36	2.05	1.61	1.27	0.81	0.59	1.49
3	0.82	1.08	1.75	2.04	2.90	2.73	2.64	2.24	1.87	1.41	0.88	0.70	1.75
4	0.96	1.09	1.89	2.21	3.10	2.82	2.62	2.23	2.04	1.52	0.91	0.69	1.84
5	1.03	1.28	2.01	2.37	3.10	2.75	2.59	2.24	2.14	1.72	1.03	0.81	1.92
6	1.06	1.34	2.14	2.28	2.76	2.45	2.31	0.00	0.10	1 ~~	7.00	0.0*	1.0**
11	1.09	1.36	2.14	1.86	1.89	1.53	1	2.26	2.18	1.77	1.03	0.87	1.87
7 8	1.12	1.24					1	1.74	1.94	1.74	1.06	0.94	1.57
9	0.91	0.75	1.58 0.76	1.06	0.84 $-0.10$	0.63	0.67	0.89	1.15	1.26	1.07	1.00	1.04
10	0.31	0.75				-0.25	0.20	0.04	0.33	0.48	0.64	0.74	0.39
[]	-0.26	_			-0.92		-0.97	-0.76		-0.35	0.06	0.21	-0.39
11	-0.20	-0.62	-0.96	-1.39	-1.80	-1.87	-1.63	-1.40	-1.25	-1.17	-0.62	-0.35	-1.11
Noon	-0.90	-1.19	-1.75	-1.99	-2.36	-2.90	-2.14	-2.13	-2.00	-1.84	-1.25	-0.93	-1.78
1	-1.47	-1.68	-2.26	-2.48	-2.82	-2.84	-2.59	-2.59	-1.48	-2.39	-1.68	-1.47	-2.15
2	-1.70	-1.96	-2.55	-2.74	-3.08	-3.03	-2.77	-2.73	-2.71	-2.55	-1.85	-1.64	-2.44
3	-1.68	-2.04	-2.61	-2.74	-3.21	-3.04	-2.90	-2.75	-2.67	-2.51	-1.75	-1.55	-2.45
4	-1.40	-1.80	-2.55	-2.60	-3.27	-3.00	-2.90	-2.85	-2.56	-2.21	-1.37	-1.19	-2.31
5	-1.00	-1.46	-2.26	-2.10	-2.97	-2.64	-2.64	-2.46	-2.09	-1.63	-0.85	-0.72	-1.90
6	-0.60	-0.76	-1.51	-1.52	-2.27	-2.10	-2.05	-1.78	-1.31	-0.83	-0.35	-0.42	-1.29
7	-0.31				-1.43	-1.21		-0.85	-0.48	-0.29	-0.10	-0.15	-0.65
8			-0.16			-0.13		0.06	0.15	0.16	0.11	0.04	-0.06
9	-0.04	0.20	0.17	0.51	0.48	0.71	0.67	0.70	0.50	0.48	0.24	0.17	0.40
10	0.12	0.43	0.46	0.81	1.03	1.41	1.22	1.09	0.78	0.76	0.34	0.33	0.73
11	0.28	0.53	0.76	1.08	1.50	1.70	1.56	1.38	0.76	1.03	0.52	0.41	0.96
Mean.	-2 71	1.14	2.49	6.90	10.42	13.22	13.93	13.66	10.30	7.37	1.52	1.63	

### XLII.

Germany. — Munich. Lat. 48° 9' N. Long. 11° 37' E. Greenw. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn	0.71	0.92	1.54	2.27	2.58	2.49	2.84	2.37	2.17	1.53	0.91	0.46	1.73
1	0.90	1.04	1.83	2.37	3.02	3.06	3.27	2.64	2.33	1.59	0.87	0.58	1.96
2	0.97	1.18	2.04	2.62	3.30	3.39	3.56	2.94	2.61	1.67	0.94	0.67	2.16
3	1.04	1.30	2.16	2.89	3.61	3.66	3.80	3.19	2.81	1.78	1.00	0.77	2.33
4	1.03	1.33	2.25	3.12	3.85	3.82	4.05	3.41	2.98	1.91	1.04	0.85	2.47
5	1.07	1.43	2.37	3.29	3.69	3.25	3.71	3.50	3.16	2.01	1.12	0.92	2.46
6	1.14	. 1.52	2.56	2.93	2.61	2 11	2.41	2.79	3.08	2.14	1 13	0 99	2.12
7	1.17	1.55	2.17	1.80	1.21	0.77	0.93	1.48	2.22	1.84	1.13	0.97	1.44
8	1.10	1.14	1.14	0.36	-0.07	-0.35	-0.28	0.18	0.59	0.99	0.75	0.88	0.54
9	0.46	0.36	-0.11	-0.79	-1.00	-1.21	-1.25	-1.05	-0.74	-0.24	0.06	0.41	-0.42
10	-0.72	-0.61	-1.18	-1.S0	-1.99	-1.96	-2.12	-1.88	-1.70	-1.34	-0.79	-0.42	-1.38
11	-1.06	-1.46	-2.04	-2.39	-2.59	-2.69	-2.66	-2.58	-2.61	-2.19	-1.49	-0.97	-2.06

### XLII.

### GERMANY. - MUNICH, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jau.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon	-1.70	-1.93	-2.67	-2.99	-3.28	-2.98	-3.14	-3.09	-3.18	-2.69	-1.94	-1.02	-2.55
1	-2.08	-2.31	-3.01	-3.27	-3.59	-3.41	-3.48	-3.55	-3.58	-3.08	-2.23	-1.83	-2.95
2	-2.15	-2.40	-3.24	-3.60	-3.77	-3.79	-3.75	-3.72	-3.74	-3.15	-2.05	-1.85	-3.10
3	-1.83	-2.15	-3.17	-3.45	-3.77	-3.54	-3.83	-3.58	-3.56	-2.87	-1.75	-1.43	-2.91
4	-1.08	-1.67	-2.64	-3.18	-3.41	-3.34	-3.49	-3.30	-3.24	-2.27	-1.02	-0.76	-2.45
5	-0.46	-0.95	-1.93	-2.51	-2.87	-2.80	-3.07	-2.76	-2.56	-1.27	-0.43	-0.34	-1.83
6	0.16	0.27	0.04	1.50	0.05	1.04	0.00	1.01	1 00	0.11	0.10	0.10	7.00
1												-0.13	
7	0.04	-0.07	-0.20	-0.36	-0.74	-0.84	-2.99	-0.47	-0.30	0.08	0.20	0.06	-0.47
8	0.23	0.22	0.28	0.40	0.41	0.61	0.40	0.55	0.37	0.56	0.44	0.14	0.38
9	0.39	0.45	0.55	0.91	1.13	1.35	1.20	1.15	0.93	0.88	0.57	0.23	0.81
10	0.49	0.59	1.02	1.31	1.65	1.86	1.87	1.60	1.40	1.14	0.74	0.33	1.17
11	0.61	0.77	1.33	1.69	2.18	2.28	2.41	2.06	1.80	1.34	0.85	0.40	1.48
Mean.	-2.15	-0.12	0.75	5.57	9.29	12.74	13.65	12.93	9.45	6.28	1.55	-1.28	

XLIII.

Bohemia. — Prague. Lat. 50° 5′ N. Long. 14° 25′ E. Greenw. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug	Sept	Oct.	Nov.	Dec.	Year.
Midn	0.30	0.52	1.03	1.47	1.70	1.68	1.72	1.17	1.23	0.84	0.36	0.25	1.02
1	0.40	0.60	1.14	1.68	1.97	1.97	2.05	1.78	1.49	1.02	0.45	0.32	1.24
2	0.50	0.71	1.29	1.95	2.25	2.23	2.34	2.10	1.72	1.19	0.54	0.39	1.43
3	0.55	0.83	1.44	2.17	2.46	2.47	2.60	2.38	1.96	1.31	0.61	0.50	1.61
4	0.65	0.89	1.60	2.39	2.75	2.71	2.91	2.63	2,19	1.49	0.70	0.56	1.79
5	0.71	0.99	1.72	2.64	2.96	2.86	3.07	2.88	2.43	1.65	0.77	0.65	1.94
6	0.77	1.00	1.81	2.75	2.96	2.71	2.92	2.93	2.61	1.73	0.82	0.72	1.98
7	0.68	0.99	1.53	2.32	2.11	1.88	2.13	2.34	2.29	1.65	0.79	0.73	1.62
8	0.73	0.88	1.28	1.29	0.98	0.82	1.02	1.30	1.62	1.29	0.66	0.70	1.05
9	0.62	0.57	0.63	0.32	0.06	-0.14	0.17	0.21	0.60	0.70	0.41	0.54	0.39
10	0.26	0.15	-0.11	-0.53	-0.91	-0.93	-0.95	-0.77	-0.51	-0.10	-0.12	0.17	-0.36
11	-0.16	-0.45	-0.77	-1.51	-1.60	-1.58	-1.62	-1.50	-1.46	-0.86	-0.46	-0.22	-1.02
Noon.	-0.60	-0.92	-1.37	-2.09	-2.16	-2.08	-2.16	-2.18	-2.02	-1.53	-0.86	-0.65	-1.55
1	-0.93							-2.61				1	-1.95
2	-1.10	-1.50	-2.20	-2.74	-2.80	-2.73	-2.83	-2.89	-2.84	-2.31	-1.25	-1.07	-2.19
3	-1.11	-1.51	-2.29	-2.88	-2.90	-2.79	-2.93	-3.01	-2.96	-2.32	-1.28	-0.99	-2.25
4	-0.93	-1.35	-2.20	-2.76	-2.82	-2.71	-2 92	-2.85	-2.78	-2.10	-0.87	-0.79	-2.09
5	-0.68	-0.97	-1.S3	-2.46	-2.53	-2.56	-2.83	-2.66	-2.35	-1.58	-0.62	-0.55	-1.80
6	-0.44	-0.61	-1.26	-1.91	-2.17	-2.10	-2.36	-2.11	-1.64	-1.01	-0.36	-0.37	-1.36
7	-0.31	-0.32	-0.70	-1.12	-1.49	-1.37	-1.59	-1.23	-0.87	-0.51	-0.19	-0.21	-0.83
s	-0.23	-0.06	-0.24	-0.33	-0.51	-0.39	-0.58	-0.34	-0.24	-0.10	0.01	-0.19	-0.27
9	0.01	0.12	0.09	0.20	0.27	0.30	0.22	0.20	0.27	0.23	0.16	0.06	0.18
10	0.10	0.26	0.40	0.72	0.80	0.91	0.90	0.81	0.74	0.51	0.29	0.16	0.55
11	0.19	0.39	0.66	1.12	1.24	1.28	1.32	1.20	1.08	0.85	0.43	0.25	0.83
Mean.	-1.69	0.64	2.20	7.27	11.27	14.47	15.66	15.01	11.52	7.94	3.02	-0.12	

### XLIV.

## Bohemia. — Prague. Lat. 50° 5′ N. Long. 14° 24′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.45	1	0.86	1.73	1.47	1.90	1.93	1.59	1.46	1.06		0.45	1.20
2	0.52	0.88	1.05	2.06	1.77	2.22	2.24	1.85	1.69	1.18	0.79	0.52	1.40
3	0.54	0.98	1.24	2 45	2.08	2.62	2.36	2.04	1.85	1.23	0.82	0.54	1.56
4	0.53	1.06	1.42	2.82	2.31	3.02	2.27	2.10	1.95	1.24	0.78	0.55	1.67
5	0.50	1.14	1.55	3.02	2.35	3.22	2.01	2.01	1.97	1.22	0.78	0.60	1.70
6	0.49	1.15	1.60	2.92	2.12	3.03	1.62	1.76	1.90	1.19	0.80	0.70	1.61
7	0.47	1.09	1.51	2.43	1.62	2.40	1.16	1.36	1.69	1.10	0.77	0.80	1.37
8	0.42	0.91	1.24	1.59	0.92	1.40	0.66	0.83	1.28	0.90	0.69	0.82	0.97
													1
9	0.29	0.55	0.77	0.53	0.15	0.24	0.10	0.19	0.64	0.51	0.42	0.67	0.42
10	0.08	-1.01	0.16	-0.56	-0.57	-0.85	-0.52	-0.51	-0.20	-0.07	-0.02	0.31	-0.31
11	1	-1.19	(	-1.52		1	ł .			1			-0.95
Noon	-0.52	-1.10	-1.16	-2.25	-1.60	-2.23	-1.84	-1.86	-2.00	-1.47	-1.10	-0.70	-1.49
	0.80	1 ""	1.00	0.74	1.03	0	0.05	9.00	9.00	1.00	1.40	1.00	1.01
1	1		l .			1						-1.08	
2		1		-3.00							1	-1.23	1
3		Į.		-3.08		1		1				$\begin{bmatrix} -1.13 \\ -0.87 \end{bmatrix}$	
4	-0.71	-1.39	-1.75	-2.97	-2.20	-2.90	-2.30	-2.25	-2.51	-1.05	-1.05	-0.07	-1.88
5	-0.51	-1.05	-1.45	-2.65	-2.08	-2.86	-1.86	-1.75	-1.70	-1.14	-0.67	-0.56	-1.52
6		4	t		,			ļ.			1	-0.31	
7			1	-1.42					l .	-0.17	1	-0.17	1
8			}	-0.64						ł	{	-0.11	}
	1												
9	0.02	0.11	0.10	0.11	0.03	0.06	0.19	0.30	0.26	0.34	0.20		0.12
10	0.11	1.35	0.18	0.71	0.52	0.81	0.61	0.65	0.57	0.51	0.32	0.01	0.53
11	0.22	1.10	0.42	1.15	0.89	1.32	1.05	0.97	0.87	0.70	0.44	0.14	0.77
Midn	0.34	0 61	0.65	1.46	1.18	1.64	1.51	1.28	1.17	0.89	0.61	0.31	0.97
0.0	0.00	0.04	0.95	0.40	0.01	V 30	0.17	0.20	0.40	0.90	0.95	0.19	0.96
6. 6	0.09	0.24	$0.25 \\ 0.39$	0.40	0.21 $0.22$	$0.29 \\ 0.33$	$0.17 \\ 0.22$	$0.29 \\ 0.37$	0.42	0.29	$0.25 \\ 0.37$	0.13	0.26
7. 7 8. 8	0.15	0.35	0.39	0.30	0.22	0.33	0.22	0.36	0.60	0.47	0.39	0.35	0.36
9. 9	0.16	0.33	0.42	0.47	0.18	0.27	0.21	0.30	0.45	0.31	0.31	0.30	0.30
10.10	0.09		0.17		-0.03		0.04	0.07	0.18	0.42	0.15	0.16	0.27
10.10	0.03	0.17	0.11	0.00	0.00	0.02	0.04		0,10	0.22	0.10	3,13	0.11
7. 2. 9	-0.13	-0.17	-0.16	-0.15	-0.16	-0.10	-0.44	-0.30	-0.31	-0.26	-0.20	-0.17	-0.21
6. 2. 8	-0.15	-0.21	-0.23	-0.24	-0.19	-0.19	-0.43	-0.31	-0.36	-0.30	-0.23	-0.21	-0.25
6. 2.10	-0.09		-0.04		0.17			-0.05					0.01
6. 2. 6	-0.23	-0.40	-0.46	-0.74	-0.58	-0.73	-0.77	-0.66	-0.69	-0.54	-0.36	-0.28	-0.54
										0	0	0.00	0.50
7. 2	-0.21							1				-0.22	
8. 2												-0.21	
8. 1												-0.13	
7. 1	-0.15	-0.21	-0.06	-0.16	-0.15	-0.08	-0.61	-0.49	-0.47	-0.45	-0.35	-0.14	-0.28
9.12.3.9	-0.27	-0.52	-0.60	-1.17	-0.92	-1.21	-1.05	-0.98	-0.97	-0.68	-0.48	-0.31	-0.76
7. 2.2(9)												-0.14	
1. 2.2(0)	100	0.10	0.10	0.03	0.12	0.00	0.40	3,13		0.11	0.10		0.10
Dail. ext.	-0.17	-0.18	-0.16	-0.03	0.05	0.12	-0.15	-0.24	-0.46	-0.49	-0.38	0.21	-0.22
		1										-	

### XLV.

England. — Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

_						Degrees	of Fah	renheit.						
Ī	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean,
	Morn. 1	0.86	1.46	2 32	4.01	5.13	4.34	4.75	4.16	3.24	2.66	1.58	0.95	2.95
	2	0.90	1.67	2.63	4.43	5.94	4.82	5.38	4.79	3.60	2.79	1.69	0.86	3.29
1	3	0.99	1.87	3 02	4.91	6.62	5.13	5.69	5.45	4.03	3.02	1.80	0.74	3.60
I	4	1.15	2.12	3.31	5.13	6.75	5.00	5.58	5.76	4.34	3.31	1.96	0.81	3.76
1						1					i			
	5	1.37	2.36	3.40	4.91	6.03	4.57	4.82	5.42	4.25	3.51	2.09	1.04	3.65
11	6	1.53	2.48	3.08	3.98	4.37	2.79	3.35	4.21	3.62	3.38	2.14	1.31	3.02
	7	1.46	2 30	2.25	2.39	2.00	0.95	1.92	2.25	2.32	2.66	1.89	1.40	1.94
	8	1.10	1.67	0.97	0.29	-0.54	-1.01	-0.65	-0.11	0.50	1.26	1.24	1.13	0.50
		0.00	0.50	0.00	1.04	0.00	0.00	0 ==	9.20	-1.53	0.65	0.16	0.41	-1.15
I	9	0.36	0.59	1 1		-2.88 $-4.57$								
II	10	-0.61 -1.58		-2.25 -3.56								-2.43		
I	11	-2.32		-3.30 -4.43								-3.29		
		-2.52	-5.55	-4.40	-0.17	-0.12	-1.55	-9.90	-3.07	5.14	-9.40	-0.50	-2.45	-4.04
ľ	Noon. 1	-2.63	-3.85	-4.70	-6.37	-6.37	-5.02	-5.81	-5.96	-5.92	-5.51	-3.56	-2.70	-4.86
	2	-2.50		-4.43										
1	3			-3.74										
	4	-1.26	-2.07	-2.81	-4.14	-5.47	-4.03	-4.64	-4.52	-3.49	-2.45	-1.55	-1.10	-3.13
١	5	-0.59	-1.10	-1.76	-2.86	-4.32	-3.04	-3.47	-3.44			-0.77	1	-2.12
	6	-0.07	-0.38	-0.74	1	-2.68	-1.73	1	1		-0.45	-0.23		-1.06
	7	0.29	0.09	0.14	0.00	-0.81	-0.27	-0.38	0.47	1	0.23	0.07	0.34	
	8	0.50	0.36	0.86	1.26	0.99	0.74	1.10	1.06	1.37	0.79	0.25	0.52	0.81
		0.00			0.05	2.00	0.07	0.00	0.00	0.10	1 00	0.45	0.00	1.55
	9	0.63	0.56	1	2.25	2.36	2.21	2.27	2.23	)	1.33	1		
	10	0.72	0.77		2.93	3.29	2.93 $3.44$		2.97 3.40	1	1.85 2.23	0.77 1.08	0.88	
	11	0.79	0.99		3.35	3.89 4.46	3.87		3.71	2.99	2.48	1.05	1.01	1
	Midn	0.83	1.26	2.07	3.07	4.40	3.57	4.21	3.71	2.33	2.40	1.07	1.04	2.00
		0 ***			7.00	0.00	0.54	0.00	0.00	1.00	1.40	0.05	0.00	0.00
	6. 6	0.74					0.54 $0.34$	1		1		1		1
	7. 7 8. 8	0.88	1			1	0.34		1		1	1		
	9. 9	0.50	{			1	-0.14		ł		1		1	1
	10.10	0.07					$\begin{bmatrix} -0.25 \\ -0.47 \end{bmatrix}$		1			-0.20		
ı	10.10	0.01	-0.00	, -0.21	0.02	1 0.00	0.41	0.4.	0.00	1		0120		0.02
	7. 2. 9	-0.14	-0.27	-0.27	-0.45	-0.68	-0.59	-0.70	-0.41	-0.36	-0.29	-0.29	-0.11	-0.38
	6. 2. 8	И	6 -0.29											-0.25
	6. 2.10	11	-0.10		1		1					-0.11		
	6. 2. 6	-0.34	1-0.5	1 -0.70	-1.15	-1.55	-1.28	-1.46	-1.24	-0.92	-0.63	-0.43	-0.36	-0.88
	7. 2	_0.59	-0.70	1 10	1 50	_2 19	_1 09	_2.19	3 -1.79	-1.60	_1.10	0 69	-0.5	-1.35
	8. 2													-2.07
	8. 1													-2.21
	7. 1	11		9 -1.2		1	1	1				1	1	-1.46
	9.12.3.9	-0.83	3 -1.3	1 -1.87	7   -2.77	7 -4.20	-2.55	2 -2.81	-2.8	1 -2.43	-2.12	-1.28	-0.79	-2.07
	7. 2.2(9)	. 11	7 -0.0	1		1		1				-0.09	1	1
							1				1		1	1

### XLVI.

England. — Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
36 1	0.38	0.65	1.03	1.78	2.28	1.93	0 11	1.85	1.44	1.18	0.70	0.42	1.31
Morn. 1	0.38	0.00	1.03	1.75	2.28 $2.64$	2.14	2.11	2.13	1.60	1.18	0.75	0.42	1.46
3	0.44	0.83	1.34	2.18	2.94	2.28	2.53	2.42	1.79	1.34	0.80	0.33	1.60
4	0.51	0.94	1.47	2.28	3.00	2.22	2.48	2.56	1.93	1.47	0.87	0.36	1.67
_	0.07	1.05	1.51	2.18	2.68	0.00	0.14	0.47	1.89	1.50	0.93	0.46	1.00
5 6	0.61	1.10	1.37	1.77	1.94	$\frac{2.03}{1.24}$	2.14 1.49	2.41 1.87	1.61	1.56 1.50	0.95	0.46	1.62
7	0.65	1.02	1.00	1.06	0.89	0.42	0.63	1.00	1.03	1.18	0.84	0.62	0.86
8	0.49	0.74	0.43	0.13	-0.24	-0.45	-0.29	-0.05	0.22	0.56	0.55	0.50	0.22
	0.10	0.00	0.00	0.60	1.00	1 00	7.74	1.00	0.00	0.00	0.07	0.10	0.51
9	0.16		-0.28 -0.99						-0.68		0.07	0.18	-0.51 $-1.19$
11			-0.55 -1.58					1	-2.19			-0.74	
Noon	i		-1.97										
1		-1.71		-2.83									
2	-1.11		-1.97										
3 4		-0.92	-1.66 -1.25	-2.32 $-1.84$									
**	-0.50	-0.32	-1.20	-1.04	-2.40	-1.75	-2.00	_2.01	1.00	1.03	0.00	0.43	1.00
5	-0.26	-0.49	-0.78					-1.53		-0.59		-0.18	1
6	-0.03	-0.17	-0.33				-0.89			-0.20		}	-0.47
7	0.13	0.04	0.06	-0.00	-0.36	-0.12	-0.17	-0.21	0.16	0.10	0.03	0.15	1
8	0.22	0.16	0.38	0.56	0.44	0.33	0.49	0.47	0.61	0.35	0.11	0.23	0.36
9	0.28	0.25	0.60	1.00	1.05	0.98	1.01	0.99	0.94	0.59	0.21	0.32	0.69
10	0.32	0.34	0.75	1.30	1.46	1.30	1.38	1.32	1.15	0.82	0.34	0.39	0.91
11	0.35	0.44	0.84	1.49	1.73	1.53	1.63	1.51	1.26	0.99	0.48	0.45	1.06
Midn	0.37	0.56	0.92	1.63	1.98	1.72	1.87	1.65	1.33	1.10	0.61	0.46	1.18
6. 6	0.33	0.47	0.52	0.57	0.38	0.24	0.30	0.44	0.61	0.65	0.43	0.30	0.44
7. 7	0.39	0.53		0.53	0.27	0.15	0.23	0.40	0.60	0.64	0.44	0.39	0.42
8. 8	0.36	0.45	0.41	0.35	0.10	-0.06	0.10	0.21	0.42	0.46	0.33	0.37	0.29
9. 9	0.22	0.26	0.16	0.07	-0.12	-0.11	-0.07	-0.04	0.13	0.15	0.14	0.25	0.09
10.10	0.03	-0.02	-0.12	-0.23	-0.29	-0.21	-0.21	-0.28	-0.19	-0.19	-0.09	0.06	-0.14
7. 2. 9	-0.06	-0.12	-0.12	-0.20	-0.30	-0.26	-0.31	-0.18	-0.16	-0.13	-0.13	-0.05	-0.17
6. 2. 8	II.		-0.07	1		1			1		-0.12	1	) 1
6. 2.10	11	-0.07		0.14	0.19		0.10			1	-0.05	1	1
6. 2. 6	-0.15	-0.24	-0.31	-0.51	-0.69	-0.57	-0.65	-0.55	-0.41	-0.28	-0.19	-0.16	-0.39
7. 2	_0.99	_0.97	_0 10	_0.90	_0.0~	_0.90	_0.0~	-0.77	_0.71	_0 10	-0.30	-0.24	-0.60
8. 2			-0.42 $-0.77$										1
8. 1	ł J	1	-0.83				I .		1		1	1	1 [
7. 1	11		-0.55	1	)		1	1		ł .			1
0.10.5									Ì				
9.12.3.9	11		-0.83	į.	4	1	l .	1			-0.57	1	-0.92
7. 2.2(9)	0.03	-0.03	0.06	0.10	0.04	0.05	0.02	0.11	0.12	0.05	-0.04	0.04	0.05
Dail.ext.	-0.25	-0.31	-0.29	-0.28	0.09	0.03	-0.03	-0.05	-0.35	-0.45	-0.32	-0.29	-0.25
											-		

### XLVII.

Belgium. — Brussels. Lat. 50° 51′ N. Long. 4° 22′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. I	0.58	0.67	1.19	2.23	2.57	2.83	2.34	2.49	1.71	0.85	0.49	0.73	1.56
2	0.60	0.73	1.36	2.59	2.89	3.12	2.57	2.84	2.00	0.99	0.49	0.39	1.71
3	0.60	0.79	1.54	2.99	3.17	3.18	2.74	3.20	2.33	1.15	0.54	0.08	1.86
4	0.60	0.86	1.70	3.29	3.28	3.14	2.74	3.42	2.57	1.31	0.65	0.02	1.97
	0.62	0.92	1 *0	9.00	0.00	0.27	0.4**	0.00	0.50	1 40	0.75	0.25	1.93
5	0.64		1.79	3.29	3.06	2.71	2.47	3.32	2.58	1.40	0.77	0.25	1
6 7	0.61	0.97 $0.93$	1.74 1.50	2.86 $2.01$	$\frac{2.45}{1.52}$	2.00	1.88 1.06	2.82 1.94	2.28 1.67	1.35	0.85 $0.81$	0.03	1.71 1.27
8	0.46	0.33	1.03	0.86	0.44	0.16	0.15	0.82	0.82	0.68	0.58	0.97	0.64
	0.40	0.10	1.00	0.00	0.44	0.10	0.10	0.02	0.02	0.00	0.50	0.51	0.04
9	0.18	0.39	0.39	-0.35	-0.59	-0.61	-0.69	-0.34	-0.14	0.08	0.19	0.56	-0.08
10	-0.22	-0.13	-0.36	-1.42	-1.43	-1.35	-1.33	-1.37	-1.06	-0.60	-0.31	-0.13	-0.81
11	-0.65	-0.71	-1.11	-2.23	-2.06	-1.86	-1.77	-2.19	-1.86	-1.23	-0.80	-0.84	-1.44
Noon	-1.01	-1.23	-1.72	-2.77	-2.52	-2.27	-2.06	-2.81	-2.48	-1.71	-1.16	-1.29	-1.92
1	1	-1.57		-3.11		-2.65		ļ			1	-1.33	
2	-1.19						-2.51	5	1	-1.95	t .	1	-2.33
3		-1.49					ł .	-3.69	1			1	
4	-0.70	-1.14	-1.93	-3.18	-3.36	-3.16	-2.71	-3.53	-2.63	-1.31	-0.75	-0.26	-2.06
5	_0 20	-0.72	_1.51	-2.76	- 0.0*	_9 69	-9 47	_2 02	_2.05	_0.84	-0.45	-0.16	-1.68
6	i			-2.76 $-2.05$		ł.				1	1	-0.25	1
7	0.02		-0.55		-1.20	1		-1.15			1	-0.37	1
8	0.02	0.03		-0.16		1						-0.33	
	0.12	0.17	0.10	0.10	0.12	0.51	0.20	0.03	0.20	0.20	0.10	0.00	0.00
9	0.21	0.31	0.28	0.69	0.82	0.68	0.64	0.82	0.78	0.48	0.32	0.05	0.50
10	0.31	0.41	0.59	1.31	1.51	1.37	1.31	1.48	1.13	0.60	0.41	0.37	0.90
11	0.42	0.50	0.83	1.70	1.96	1.97	1.77	1.89	1.33	0.68	0.47	0.75	1.19
Midn	0.52	0.59	1.02	1.96	2.28	2.44	2.08	2.19	1.49	0.75	0.49	0.89	1.39
											0.00	0.00	0.00
6. 6	0.25	0.32	0.35	0.41		-0.09		0.31	0.49	0.48	0.33	0.20	0.26
7. 7	0.31	0.45	0.47	0.44		-0.09	1	0.39	0.59	0.55	0.42	0.30	0.33
8.8	0.29	0.46	0.47	0.35		-0.07		0.37	0.53	0.48	0.39	0.32	0.31
9. 9	0.20	0.35	0.34	0.17	0.12	i	-0.02	0.24	0.32	0.28	0.25	$0.25 \\ 0.12$	0.21   0.05
10.10	0.05	0.14	0.11	0.05	0.04	0.01	-0.01	0.05	0.03	0.00	0.00	0.12	0.00
7. 2. 9	-0.12	-0.14	-0.17	-0.20	-0.29	-0.40	-0.27	-0.27	-0.20	-0.12	-0.05	-0.04	-0.19
6. 2. 8	1	-0.17	1					-0.28				-0.24	
6. 2.10	1	-0.09	0.01	0.29	0.25	0.13	0.23	0.24	0.12	0.00		-0.00	0.09
6. 2. 6	1	-0.34	-0.53	1		-1.05		-0.98				-0.21	-0.60
7. 2	-0.29	-0.36	-0.40	-0.64	-0.85	-0.94	-0.73	-0.82	-0.69	-0.42	-0.23	-0.03	-0.53
8. 2	-0.37	-0.45	-0.63	-1.22	-1.39	-1.41	-1.18	-1.38	-1.12	-0.64	-0.35	-0.03	-0.85
8. 1				-1.13									
7. 1	-0.30	-0.32	-0.32	-0.55	-0.69	-0.78	-0.62	-0.67	-0.61	-0.43	-0.26	-0.18	-0.48
9.12.2.9	_0 40	_0.51	_0.00	-1.44	_1.49	_1.96	_1 20	-1.51	-1.91	-0.72	0.12	-0.34	-0.95
		1		-1.44	-0.01					0.03		-0.04	- 1
7. 2.2(9)	-0.04	-0.03	-0.06	0.03	-0.01	-0.13	-0.04	0.00	0.00	0.03	0.00	0.04	0.02
Dail.ext.	-0.28	-0.34	-0.25	-0.02	-0.06	-0.04	0.02	-0.14	-0.24	-0.28	-0.24	-0.18	-0.18
Dietacate		0.01											

### XLVIII.

Belgium. - Brussels. Lat. 50° 51' N. Long. 4° 22' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.30	0.60	1.09	1.72	2.27	2.46	2.20	1.88	1.52	0.92	0.51	0.30	1.31
2	0.56	0.82	1.39	2.19	3.00	2.82	2.77	2.44	2.03	1.20	0.77	0.47	1.70
4	0.64	0.97	1.66	2.64	3.32	3.53	3.14	2.76	2.38	1.44	0.83	0.62	1.99
6	0.66	1.03	1.83	2.43	2.44	2.27	2.30	2.44	2.47	1.56	0.93	0.63	1.75
8	0.67	0.84	1.02	0.76	0.49	0.41	0.32	0.68	1.03	0.96	0.79	0.63	0.72
9	0.36	0.33	0.21	-0.38	0.61	-0.61	-0.63	-0.39	-0.14	0.07	0.21	0.34	0.00
10	0.07	-0.09	-0.54	-1.18	-1.43	-1.32	-1.36	-1.26	-1.19	-0.78	-0.36	-0.08	-0.79
Noon.	-0.92	-1.27	-1.78	-2.42	-2.61	-2.47	-2.35	-2.47	-2.46	-1.87	-1.27	-0.83	-1.89
2	-1.15	-1.65	-2.30	-2.95	-3.22	-3.21	-2.92	-3.08	-3.04	-2.17	-1.42	-1.04	-2.35
4	-0.72	-1.19	-2.04	-2.63	-3.15	-3.18	-2.90	-2.93	-2.70	-1.61	-0.90	-0.65	-2.05
6	-0.21	-0.49	-0.94	-1.71	-2.44	-2.57	-2.38	-1.87	-1.21	-0.37	-0.28	-0.18	-1.22
8	-0.08	-0.05	-0.00	0.13	0.05	-0.16	-0.15	0.17	0.21	0.23	0.07	-0.03	0.03
9	0.13	0.17	0.31	0.63	0.76	0.80	0.79	0.76	0.64	0.43	0.24	0.07	0.48
10	0.20	0.30	0.58	1.04	1.25	1.45	1.39	1.27	1.01	0.54	0.38	0.14	0.80
Mean.	0.52	2.45	3.56	7.27	10.37	13.10	13.69	13.58	11.22	7.69	4.72	1.89	

### XLIX.

Germany. — Schwerin. Lat. 53° 36′ N. Long. 11° 30′ E. Gr. — Dove.

							1		1	1	1	1	1
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.05	0.49	0.92	1.66	1.97	2.10	2.12	1.92	1.70	0.87	0.21	0.16	1.18
2	0.08	0.69	1.20	2.17	2.44	2.69	2.72	2.41	2.19	1.14	0.24	0.34	1.53
4	0.27	0.83	1.43	2.53	2.96	2.97	2.96	2.62	2.54	1.51	0.42	0.48	1.79
6	0.35	0.86	1.62	2.67	2.07	1.80	1.94	2.13	2.70	1.67	0.62	0.48	1
8	0.59	1.19	1.24	,	0.56	0.25	0.12	0.32	0.95	1.21	0.70	0.63	0.78
10	0.17	0.18	-0.11	-0.97		-1.20	1				0.01	1	1
Noon.	-0.42	-0.97	-1.32	-2.34	-2.47	-2.36	-2.20	-2.29	-2.42	-1.80	-0.77	-0.43	-1.6
2	-0.61	-0.72	-2.21	-3.50	-3.38	-3.23	-3.26	-3.45	-3.58	-2.54	-0.91	-0.68	-2.42
4	-0.43	-1.22	-2.13	-2.86	-2.70	-2.62	-2.76	-2.76	-3.03	-1.85	-0.62	-0.62	-1.97
6	-0.02	-0.42	-0.95	-1.54	-1.62	-1.71	-1.70	-1.37	-1.32	-0.55	-0.23	-0.27	-0.98
8	-0.07	-0.07	-0.11	0.13	0.11	-0.02	0.08	0.34	0.26	0.16	0.02	-0.14	0.06
10	0.06	0.21	0.45	1.01	1.15	1.28	1.29	1.30	1.19	0.57	0.24	-0.02	0.78
Mean	-1.05	-2.00	1.18	5.26	8.45	12.19	13.50	13.02	10.42	7.48	1.42	-1.38	
mican.	1.00	2.00	1.10	0.20	0.40	12.10	10.00	10.02	10.12	1.10	1.12	1,00	

## PRUSSIA. — MÜHLHAUSEN. Lat. 51° 13' N. Long. 10° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.71	1.28	1.10	1.84	2.40	3.56	2.91	2.49	1.95	1.39	0.47	0.58	1.72
2	0.75	1.30	1.28	2.19	2.80	3.97	3.30	2.80	2.20	1.65	0.53	0.59	1.95
3	0.77	1.33	1.46	2.40	3.06	4.16	3.50	3.06	3.29	1.85	0.60	0.60	2.17
4	0.82	1.40	1.60	2.74	3.06	3.98	3.42	3.14	2.70	1.99	0.66	0.62	2.18
5	0.86	1.47	1.62	2.61	2.67	3.40	3.00	2.98	2.73	2.05	0.68	0.66	2.06
6	0.91	1.50	1.46	2.25	2.06	2.49	2.22	2.51	2.46	1.93	0.63	0.67	1.76
7	0.86	1.36	1.11	1.41	1.15	1.32	1.20	1.73	1.03	1.50	0.46	0.59	1.14
8	0.62	0.98	0.55	0.58	0.16	0.11	0.09	0.86	0.87	0.84	0.16	0.46	0.52
9	0.21		-0.02						-0.26			0.03	. 1
10		1	-0.70					1	1				
11		Į.	-1.30				t .		1			1	1
Noon	-1.38	-2.02	-1.76	-2.42	-2.44	-3.39	-2.94	-2.89	-3.14	-2.53	-1.09	-1.06	-2.26
1	_1 58	_2 38	-2.02	_2 80	-9 71	-2 86	-3 26	-3.29	_2 59	_2 82	_1 08	-1.15	_9.51
$\begin{vmatrix} & 1 \\ 2 \end{vmatrix}$	1		-2.02 $-2.07$					-3.46	į.	1		ł	1
3			-1.90							ì			1
4		4	-1.58						1		1		
	0.01	1.00	1.00	2.00	2.00	0.10	0.00	0.0.	2.00	1.00	8	0.00	2.00
5	-0.44	-1.02	-1.11	-1.95	<b>-2.</b> 19	-3.06	-2.52	-2.51	-1.89	-1.21	-0.14	-0.23	-1.52
6	-0.20	-0.54	-0.62	-1.20	-1.59	-2.10	-1.76	-1.76	-1.06	-0.58	0.02	-0.02	-0.95
7	-0.04	-0.17	-0.18	-0.47	-0.83	-1.02	-0.85	-0.90	-0.24	-0.03	0.06	0.12	-0.38
8	0.18	0.13	0.16	0.09	-0.08	0.05	0.03	-0.05	0.50	0.38	0.22	0.26	0.16
				0.50	0 70	- 0-				0.00			
9	0.27	0.41	0.45	0.53		1.01	0.81	0.71	0.99	0.70	0.26	0.32	0.59
10	0.37	0.66	0.64	0.89	1.10	1.76	1.46	1.24	1.35	0.91	0.34	0.40	0.93
11	0.53	0.89	0.78	1.14	1.56	2.42	2.01	1.78	1.58	1.10	0.38	0.47	1.22
Midn	0.64	1.08	0.94	1.58	1.98	3.05	3.29	2.16	1.75	1.26	0.42	0.54	1.56
6. 6	0.36	0.48	0.42	0.53	0.24	0.20	0.23	0.38	0.70	0.68	0.33	0.33	0.41
7. 7	0.41	0.60	0.47	0.47	0.16	0.15	0.18	0.42	0.40	0.74	0.26	0.36	0.38
8.8	0.40	0.56	0.36	0.34	0.04	0.08	0.06	0.41	0.69	0.61	0.19	0.36	0.34
9. 9	0.24	0.37	0.22	0.08	-0.09	-0.01	-0.08	0.18	0.37	0.34	0.02	0.18	0.15
10.10	-0.01	0.08	-0.03	-0.14	-0.20	-0.11	-0.18	-0.07	-0.03	-0.04	-0.14	-0.07	-0.0s
	0 -			0.0	0.5	0		0.5		0.55	0.00	0.0	
7. 2. 9	1		-0.17					-0.34					
6. 2. 8	-0.14		-0.15			-0.53					-0.01		
6. 2.10		-0.07	0.01	0.07	0.10		0.09			-0.05	}	-0.01	1
6. 2. 6	-0.27	-0.47	-0.41	-0.63	-0.80	-1.25	-0.99	-0.90	-0.71	-0.55	-0.08	-0.15	-0.60
7. 2	-0.33	-0.51	-0.48	-0.77	-0.86	-1.41	-1.11	-0.87	-1.26	-0.75	-0.22	-0.26	-0.74
8. 2		i	-0.76										1
8. 1		1	-0.74				1	-1.22				1	1 1
7. 1	)	1	-0.46	1		}		l .	1			1	1 1
9.12.3.9		1	-0.81	1		}	1	1			1		) [
7. 2.2(9)	-0.03	-0.05	-0.02	-0.12	-0.14	-0.20	-0.15	-0.08	-0.13	-0.02	0.02	0.03	-0.07
Dail.ext.	-0.34	-0.11	_0 22	-0.10	0.00	0.01	0.04	-0.16	-0.12	-0.47	-0.21	-0.24	-0.22
Dan. ext.	0.04	0.44	-0.25	0.10	0.09	0.01	0.04	0.10	0.10	0.47	0.21	0.24	0.22

## Holland. — Utrecht. Lat. 52° 5' N. Long. 5° 8' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.36	0.62	1.13	1.71	2.56	2.74	2.64	1.87	1.91	1.07	0.76	0.11	1.44
1	0.37	0.74	1.18	1.87	2.86	3.29	2.67	1.91	2.10	1.11	0.70	0.19	1.58
2	0.46	0.82	1.24	2.00	3.00	3.21	2.82	2.02	2.21	1.18	0.78	0.32	1.67
3	0.51	0.87	1.27	2.10	3.02	3.25	2.97	2.07	2.34	1.25	0.82	0.42	1.74
4	0.57	0.90	1.31	2.16	2.70	2.84	2.76	2.06	2.45	1.31	0.82	0.44	1.69
5	0.61	0.97	1.26	1.92	1.80	1.82	1.86	1.80	2.42	1.42	0.90	0.50	1.44
6	0.66	0.98	1.02	1.30	0.67	0.44	0.33	1.05	1.87	1.22	0.91	0.46	0.91
7	0.64	0.84	0.62	0.37	-0.38	-0.70	-0.77	0.04	0.72	0.39	0.78	0.38	0.24
S	0.50	0.56	-0.01	-0.40	-1.17	-1.50	-1.28	-0.68	-0.39	0.12	0.29	0.31	-0.30
9	0.13	-0.07	-0.53	-1.20	-1.68	-2.02	-1.69	-1.33	-1.12	-0.50	-0.22	0.14	-0.84
10	-0.26	-0.49	-1.05	-1.71	-2.06	-2.42	-2.02	-1.65	-1.79	-1.12	-0.71	-0.14	-1.29
11	-0.62	-0.97	-1.50	-2.16	-2.46	<b>-2.7</b> 8	-2.27	-1.87	-2.34	-1.68	-1.15	-0.33	-1.68
Noon.	-0.85	-1.34	-1.77	-2.41	-2.78	-2.94	-2.53	-2.16	-2.83	-1.98	-1.49	-0.62	-1.97
1	-0.98	-1.58	-1.88	-2.42	-2.94	-3.00	-2.61	-2.40	-3.07	-2.11	-1.62	-0.75	-2.11
2	-1.02	-1.54	-1.82	-2.42	-2.88	-2.94	-2.60	-2.30	-2.99	-1.99	-1.43	-0.66	-2.05
3	-0.81	-1.21	-1.54	-2.24	-2.58	-2.64	-1.58	-2.13	-2.68	-1.64	-1.08	-0.47	-1.72
4	-0.60	-0.89	-1.25	-1.82	-2.06	-2.20	-2.00	-1.79	-2.06	-1.10	-0.70	-0.23	-1.39
5	-0.35	-0.48	-0.75	-1.23	-1.42	-1.53	-1.62	-1.30	-1.34	-0.52	-0.42	-0.17	-0.93
6	-0.19	-0.21	-0.24	-0.47	-0.76	-0.74	-0.76	-0.61	-0.52	-0.11	-0.18	-0.10	-0.41
7	-0.05	-0.03	0.14	0.20	0.07	0.17	0.02	0.14	0.10	0.22	-0.02	-0.03	0.06
8	0.05	0.12	0.48	0.72	0.85	1.01	0.82	0.86	0.62	0.53	0.18	0.02	0.52
9	0.22	0.23	0.74	1.13	1.51	1.77	1.50	1.24	1.17	0.84	0.40	0.06	0.90
10	0.36	0.40	0.94	1.41	1.92	2.25	1.96	1.52	1.51	1.01	0.58	0.04	1.16
11	0.36	0.67	1.02	1.58	2.16	2.53	2.17	1.70	1.76	1.14	1.06	0.02	1.35
Mean	-2.83	4.18	3.20	7.14	10.55	12.95	13.75	12.90	10.87	6.88	4.65	0.76	

LII.

England. — Greenwich. Lat. 51° 28′ 38″ N. Long. 0° 0′. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M.1	0.44	0.75	1.44	2.32	2.72	3.24	2.73	2.49	2.05	1.34	0.67	0.47	1.72
3	0.62	0.94	1.66	2.66	3.04	3.70	3.11	2.82	2.40	1.42	0.80	0.56	1.98
5	0.75	1.06	1.92	2.84	2.84	3.25	2.91	2.89	2.58	1.54	0.87	0.56	2.00
7	0.86	1.08	1.60	1.31	0.75	0.80	0.88	1.22	1.65	1.26	0.88	0.60	1.07
9	0.41	0.24	-0.22	-0.82	-1.30	-1.52	-1.14	-1.14	-0.76	-0.30	0.11	0.24	-0.50
11	-0.74	-1.03	-1.90	-2.48	-2.60	-2.91	-2.67	-2.64	-2.57	-1.88	-1.06	-0.73	-1.93
P.M. 1	-1.25	-1.73	-2.62	-3.31	-3.36	-3.75	-3.17	-3.40	-3.28	-2.40	-1.64	-1.20	-2.59
3	-1.10	-1.59	-2.43	-3.08	-3.02	-3.60	-3.09	-3.20	-2.94	-2.04	-1.26	-0.85	-2.35
5	-0.36	-0.63	-1.33	-2.04	-2.05	-2.51	-2.24	-2.11	-1.65	-0.73	-0.38	-0.24	-1.37
7	0.03	0.05	0.09	-0.16	-0.29	-0.58	-0.50	-0.11	0.04	0.11	0.09	0.00	-0.10
9	0.10	0.32	0.71	0.99	1.20	1.40	1.13	1.22	0.89	0.63	0.40	0.21	0.77
11	0.23	0.54	1.11	1.77	2.06	2.52	2.08	1.96	1.60	1.07	0.53	0.37	1.33
Mean.	2.48	2.53	4.53	6.71	9.62	12.47	13.08	12.98	11.12	7.71	5.47	3.09	

LIII.

## England. — Greenwich. Lat. 51° 29' N. Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.38	0.68	1.29	2.21	2.72	3.13	2.61	2.61	1.89	1.28	0.60	0.40	1.65
2	0.63	0.82	1.44	2.31	2.85	3.30	2.71	2.68	2.06	1.45	0.75	0.52	1.79
3	0.83	0.95	1.62	2.44	2.91	3.41	2.74	2.78	2.22	1.56	0.88	0.59	1.91
4	0.93	1.02	1.82	2.54	2.85	3.40	2.71	2.86	2.34	1.60	0.95	0.62	1.97
5	0.93	1.03	1.95	2.46	2.60	3.14	2.53	2.81	2.35	1.56	0.95	0.62	1.91
6	0.84	0.97	1.93	2.17	2.08	2.52	2.11	2.48	2.15	1.42	0.89	0.60	1.68
7	0.71	0.84	1.66	1.56	1.25	1.53	1.38	1.77	1.67	1.15	0.75	0.57	1.24
8	0.53	0.61	1.11	0.66	0.20	0.28	0.40	0.72	0.88	0.71	0.52	0.48	0.59
9	0.30	0.26	0.30	-0.37	-0.92	-1.02	-0.71	-0.55	-0.13	0.09	0.19	0.28	-0.19
10	-0.01	1									1	-0.04	1
11	-0.39					ł				i .		-0.46	
Noon		-0.73 -1.27			<b>-3.</b> 13	ì		1				-0.37	
1,000	0.19	1.27	2.00	2.01	9.10	9.20	2.04	0.40	2.04	2.01	1.20	0.07	2.27
1	-1.12	-1.66	-2.79	-3.17	-3.26	-3.39	-3.04	-3.69	-3.28	-2.45	-1.59	-1.17	-2.55
2	-1.28	-1.81	-2.85	-3.14	-3.16	-3.34	-2.91	-3.63	-3.23	-2.48	-1.69	-1.25	-2.56
3					-2.90						1		
4			1							1		-0.76	-1.95
_	0.50	0 =0	7.40	1.0*	2.00	0.0*	0.90	0.00	1.00	1.01	0.50	0.90	1 15
5					-2.06				i .		-0.59	1	1
6	-0.22				-1.45						ł	-0.01	1
7	0.03	0.14			-0.71			-0.69		0.02	0.24		-0.34
8	0.11	0.37	0.30	0.17	0.11	-0.24	-0.19	0.24	0.29	0.32	0.41	0.26	0.18
9	0.08	0.46	0.65	0.84	0.92	0.81	0.64	1.11	0.77	0.52	0.44	0.23	0.62
10	0.03	0.48	0.89	1.42	1.62	1.74	1.41	1.81	1.17	0.69	0.41	0.19	0.99
11	0.04	0.49	1.05	1.81	2.16	2.42	2.01	2.27	1.47	0.87	0.40	0.20	1.27
Midn	0.16	0.56	1.17	2.03	2.51	2.86	2.40	2.51	1.70	1.08	0.46	0.28	1.48
Birdii	0.10	0.50	1011	2.00	2.01	2.00	2010		11,10	1,00	0110	0.20	1010
6. 6	0.31	0.36	0.59	0.42	0.31	0.21	0.27	0.46	0.62	0.50	0.39	0.30	0.40
7. 7	0.37	0.49	0.55	0.48	0.31	0.21	0.21	0.54	0.70	0.59	0.50	0.38	0.45
8.8	0.32	0.49	0.73	0.40	0.27	0.13	0.21	0.48	0.70	0.53	0.37	0.37	0.39
9. 9	0.32	0.49	0.48	0.42	0.00		-0.04	0.48	0.32	0.32	0.31	0.25	0.33
10.10	0.13	0.14	0.12	-0.00		-0.10		0.01	ì	0.02	0.08	0.07	-0.01
10.10	0.01	0.14	0.14	-0.00	-0.10	0.13	-0.10	0.01	0.00	0.02	0.00	0.01	0.01
7. 2. 9	-0.16	-0.17	-0.18	-0.25	-0.33	-0.33	-0.30	-0.25	-0.26	-0.27	-0.17	-0.15	-0.24
6. 2. 8					-0.32							-0.13	
6. 2.10	1	-0.12		0.15			-0.20			-0.12			0.04
6. 2. 6					-0.84			1					-0.59
	-	ļ											0.00
7. 2												-0.34	
8. 2	-0.38	-0.60	-0.87	-1.24	-1.48	-1.53	-1.26	-1.46	-1.18	-0.89	-0.59	-0.39	-0.99
8. 1												-0.35	
7. 1	-0.21	-0.41	-0.57	-0.81	-1.01	-0.93	-0.83	-0.96	-0.81	-0.65	-0.42	-0.30	-0.66
9.12.3.9	-0.41	-0.56	-0.99	-1.33	-1.51	-1.68	-1.42	-1.55	-1.29	-0.91	-0.53	-0.37	-1.05
7. 2.2(9)		-0.01	0.03		-0.02							-0.06	
Dail. ext.	-0.18	-0.30	-0.15						-0.47	-0.44	-0.37	-0.32	-0.30
Dan.ext.	-0.10	0.00	0.49	0.52	-0.10	0.01	0.10	0.42	0.47	0.44	0.01	0.02	0.50

LIV.

# England. — Greenwich. Lat. 51° 29' N. Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.—GLAISHER.

Degrees of Fahrenheit.

					Degrees	of Fah	renneit.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Midn	1.0	1.6	2.9	4.8	5.4	6.2	5.0	5.1	4.0	2.9	1.7	0.9	3.5
1	0.9	1.8	3.0	5.2	6.0	7.1	5.5	5.5	4.5	3.0	1.8	1.0	3.8
2	1.2	2.0	3.3	5.7	6.4	8.0	6.0	6.0	5.5	3.4	2.0	1.2	4.2
3	1.3	2.1	3.6	6.2	6.7	8.7	6.4	6.3	6.4	3.6	2.0	1.3	4.5
	1.0						0.0	0.5	0.0	0.0	0.1		4.0
4 5	1.6 1.8	$2.3 \\ 2.2$	3.9 4.0	6.6	6.7 6.3	9.3 8.8	6.6	6.5	6.6	3.8 3.8	$\frac{2.1}{2.0}$	1.4	4.8
6	1.9	2.3	3.9	6.0	4.8	6.4	4.5	5.5	5.3	3.5	1.9	1.4	3.9
7	1.9	2.3	3.6	4.3	2.6	3.0	2.5	3.3	4.0	2.8	1.7	1.5	2.8
•	1.9	2.1	5.0	4.5	2.0	3.0	2.0	9.9	4.0	2.0	1.7	1.0	2.5
8	1.5	1.6	2.5	2.0	0.5	0.0	0.0	0.9	2.1	1.6	1.0	1.3	1.2
9	1.0	0.7	0.2	-0.9	-2.0	-2.5	-2.0	-1.6	-0.4	0.0	0.4	0.9	-0.5
10	0.2	-0.5	-1.9	-3.2	-4.0	-4.5	-4.0	-3.5	-3.0	-2.0	-0.6	0.0	-2.2
11	-1.3	-2.1	-3.5	-5.3	-5.5	<b>-5.</b> 8	-5.4	-5.4	-5.0	-3.8	-2.0	-1.3	-3.9
Noon	-2.3	-3.2	-5.0	-6.8	-6.7	-7.3	-6.4	-6.5	-6.4	-5.1	-3.1	-2.1	-5.1
1	-2.9	-3.9	-5.8	<b>-7.</b> 9	-7.5	-8.1	-6.7	-7.5	-7.1	-5.5	-3.5	-2.4	-5.7
2	-3.0	-3.9	-5.8	-8.2	-7.7	-8.6	-6.7	-7.7	-7.1	-4.9	-3.6	-2.3	-5.8
3	-2.5	-3.6	-5.5	-7.7	<b>-7.</b> 3	-8.4	-6.5	-7.0	-6.6	-3.7	-3.0	-1.9	-5.3
4	-1.9	-2.8	-4.5	-6.7	-6.1	-7.4	-5.8	-5.5	-5.5	-2.8	-2.1	-1.3	-4.4
5	-1.1	-1.6	-3.3	-5.4	-4.8	-6.1	-4.9	-3.6	-4.2	-1.7	-1.2	-0.8	-3.2
6	-0.6	-0.6	-1.8	-3.5	-3.0	-4.5	-3.5	-2.0	-2.5	-0.8	-0.4	-0.4	-2.0
7	-0.3	0.3	-0.4	-1.1	-1.0	-2.4	-1.5	-0.5	-0.6	0.0	0.1	-0.1	-0.6
	0 =								- 0				0.0
8	0.1	0.6	0.9	0.7	0.9	0.0	0.3	1.0	1.0	0.7	0.6	0.2	0.6
9	0.4	1.0	1.7	2.0	2.3	1.8	1.9	2.4	1.8	1.3	1.0	0.4	1.5
10	0.6	1.3	2.3	3.2	3.5	3.6	3.3	3.3	2.7	1.9	1.3	0.5	2.3
11	0.7	1.5	2.6	4.1	4.5	5.0	4.2	4.3	3.4	2.4	1.5	0.8	2.9
6. 6	0.6	0.9	1.0	1.2	0.9	0.9	0.5	1.7	1.4	1.3	0.8	0.5	0.9
7. 7	0.8	1.2	1.6	1.6	0.8	0.3	0.5	1.4	1.7	1.4	0.9	0.7	1.1
8. 8	0.8	1.1	1.7	1.3	0.7	0.0	0.1	0.9	1.5	1.1	0.8	0.8	0.9
				6.5		0.0	0.0	0.1	0.=	0.0		0.0	0.5
9. 9	0.7	0.8	0.9	0.5	0.1	-0.3	-0.0	0.4	0.7	0.6	0.7	0.6	0.5
10.10	0.4	0.4	0.2	0.0	-0.2	-0.4	-0.4	-0.1	-0.1	-0.0	0.4	0.2	0.0
7. 2. 9	-0.2	-0.3	-0.2	-0.6	-0.9	-1.2	-0.8	-0.7	-0.4	-0.2	-0.3	-0.1	-0.5
6. 2. 8	-0.3	-0.3	-0.3	-0.5	-0.7	-0.7	-0.6	-0.4	-0.3	-0.2	-0.4	-0.2	-0.4
6. 2.10	-0.2	-0.1	0.1	0.3	0.2	0.5	0.4	0.3	0.3	0.2	-0.1	-0.1	0.1
6. 2. 6	-0.6	-0.7	-1.2	-1.9	-1.9	-2.2	-1.9	-1.4	-1.4	-0.7	-0.7	-0.4	-1.3
7. 2	0 -	0.0	1.1	1.0	-2.5	-2.8	-2.1	-2.2	-1.5	-1.0	-0.9	-0.4	-1.5
8. 2	-0.5 -0.7	-0.9	-1.1 -1.6	-1.9	-2.5 -3.6	-2.8 -4.3	-2.1 $-3.3$	-3.4	-1.5 $-2.5$	-1.0	-1.3	-0.5	-2.3
	$\begin{vmatrix} -0.7 \\ -0.7 \end{vmatrix}$	-1.1	1	-3.1 -2.9	-3.5	-4.0	-3.4	-3.3	-2.5	-1.9	-1.3	-0.5	-2.2
8. 1	-0.7 -0.5	-1.1	-1.6			-2.6	-3.4	-2.1	-2.5	-1.4	-0.9	-0.4	-1.5
7. 1	0.5	-0.9	-1.1	-1.8	-2.4	-2.0	-2.1	-2.1	-1.0	1.4	0.3	0.4	1.0
9.12.3.9	-0.8	-1.3	-2.1	-3.3	-3.4	-4.1	-3.2	-3.2	-2.9	-1.9	-1.2	-0.7	-2.4

LV.

## PRUSSIA. — HALLE. Lat. 51° 30' N. Long. 11° 57' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

,						Degre	es of Re	caumur.						
	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Morn. 1	0.53	1	1.36	1	1	3.91	3.72	3.32	1			1	
H	2	0.56	1.14	1.58	2.86	4.10	3.94	3.82	3.57	2.99	2.22	1	0.48	2.35
H	3	0.60	1	1.74	3.00	1	3.62	3.56	3.56		2.37		0.50	2.34
	4	0.66	1.34	1.82	2.94	3.10	2.95	2.97	3.27	3.02	2.41	1.03		2.17
H	5	0.72	1.36	1.72	2.62	2.18	2.09	2.14	2.64	2.62			1	1.82
i	6	0.72	1.30	1.42	1.98	1.30	1.18	1.24	1.90	1.97	1.90	1		1.37
ľ	7	0.65	1.10	0.94	1.07	0.32	0.25	0.23	0.84	0.98	1.32		0.55	0.75
	8	0.36	0.53	0.20	0.03	-0.56	-0.58	-0.57	-0.20	0.12	0.33	0.30	0.28	0.02
I	9	0.05	<b>-0.0</b> s	-0.66	-0.98	-1.34	-1.34	-1.30	-1.20	-1.14	-0.71	-0.31	-0.09	-0.76
l	10	-0.45	-0.76	-1.18	-1.86	-2.09	-2.01	-1.99	-2.10	-2.03	-1.66	-0.87	-0.54	-1.46
I	11	-0.82	-1.29	-1.73	-2.58	-2.66	-2.68	-2.65	-2.90	-2.72	-2.44	-1.35	-0.90	-2.06
	Noon	-1.09	-1.77	-2.06	-3.08	-3.14	-3.07	-3.16	-3.35	-3.11	-2.86	-1.66	-1.08	-2.45
I	1	-1.17	-2.02	-2.22	-3.32	-3.33	-3.35	-3.46	-3.53	-3.30	-3.01	-1.73	-1.09	-2.63
I	2	-1.06	-1.86	-2.10	-3.26	-3.37	-3.46	-3.54	-3.57	-3.27	-2.76	-1.52	-0.94	-2.56
I	3	-0.86	-1.49	-1.86	-2.90	-3.13	-3.23	-3.29	-3.30	-2.98	-2.32	-1.14	-0.74	-2.27
	4	-0.53	-1.01	-1.42	-2.39	-2.74	-2.74	-2.76	-2.84	-2.50	-1.81	-0.75	-0.42	-1.83
I	5	-0.30	-0.59	-0.91	-1.78	-2.24	-2.22	-2.16	-1.97	-1.83	-1.20	-0.40	-0.20	-1.32
H	6	-0.13	-0.29	-0.52	-0.96	-1.58	-1.50	-1.39	-1.38	-1.12	-0.69	-0.14	-0.03	-0.81
I	7	-0.00	-0.09	-0.06	-0.34	-0.86	-0.73	-0.55	-0.59	-0.38	-0.21	0.04	0.09	-0.31
	8	0.11	0.13	0.26	0.32	-0.10	0.07	0.26	0.15	0.29	0.25	0.21	0.22	-0.18
	9	0.21	0.30	0.59	0.88	0.68	0.90	1.09	0.90	0.87	0.68	0.39	0.34	0.65
I	10	0.31	0.46	0.79	1.33	1.64	1.81	1.87	1.61	1.42	1.12	0.59	0.37	1.11
	11	0.41	0.65	0.98	1.78	2.61	2.69	2.64	2.30	1.90	1.47	0.76	0.40	1.55
	Midn	0.48	0.83	1.16	2.17	3.43	3.42	3.29	2.86	2.33	1.77	0.89	0.43	1.92
	6. 6	0.21	0.39	0.41	0.42	-0.03	-0.07	-0.01	0.34	0.40	0.53	0.30	0.18	0.26
	7. 7	0.30	0.51	0.45	0.51	-0.14	-0.16	-0.08	0.26	0.43	0.61	0.39	0.28	0.28
	8. 8	0.33	0.51	0.44	0.37	-0.27	-0.24	-0.16	0.13	0.30	0.56	0.39	0.32	0.22
	9. 9	0.24	0.33	0.23	0.18	-0.33	-0.26	-0.16	-0.03	0.21	0.29	0.26	0.25	0.10
	10.10	0.13	0.11	-0.04	-0.05	-0.33	-0.22	-0.11	-0.15	-0.14	-0.02	0.04	0.13	-0.05
	7. 2. 9	-0.11	-0.20	-0.18	-0.34	-0.71	-0.70	-0.65	-0.49	-0.35	-0.29	-0.20	-0.10	-0.36
	6. 2. 8	-0.15	-0.25	-0.19	-0.35	-0.67	-0.66	-0.62	-0.49	-0.35	-0.32	-0.23	-0.15	-0.37
ı	6. 2.10		-0.12	0.03					-0.00				-0.07	
	6. 2. 6	-0.25	-0.42	-0.47	-0.83	-1.13	-1.16	-1.16	-0.95	-0.84	-0.65	-0.38	-0.25	-0.71
	7. 2		-0.36											
	8. 2		-0.46											
	8. 1	Į.	-0.34 -0.24		1				1	- 1				1,1
	7. 1		-0.24											
	9.12.3.9 7. 2.2(9)		-0.62 -0.12											
	Dail.ext.		-0.33			0.37	0.24	0.14					-0.26	Į.
1														زا

LVI.

## Hanover. — Göttingen. Lat. 51° 32' N. Long. 9° 56' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
M 1	0.90	1.13	1.58	2.24	3.31	3.43	3.56	3.35	2.31	1 50	0.60	0.00	0.00
Morn. 1	0.90	1.13	1.55	2.49	3.70	3.71	3.82	3.70	2.68	1.58 1.75	0.69	0.60	2.06 2.25
3	0.94	1.16	2.01	2.79	3.93	3.73	3.92	3.92	3.23	1.94	0.82	0.58	2.41
4	0.99	1.20	2.22	3.04	3.91	3.57	3.79	3.89	3.63	2.10	0.92	0.58	2.49
													2.10
5	1.15	1.26	2.29	3.08	3.55	3.10		3.52	3.62	2.15	1.00	0.62	2.39
6	1.12	1.20	2.10	2.73	2.62	2.22	2.59	2.79	3.50	1.99	1.08	0.66	2.05
7	1.13	1.14	1.77	2.24	1.78	1.21	1.40	1.69	2.62	1.58	0.94	0.65	
8	1.12	0.80	1.02	0.89	0.75	0.49	0.48	0.56	1.36	1.08	0.53	0.54	0.80
9	0.50	-0.08	-0.14	-0.16	-0.47	-0.55	-0.65	-0.68	-0.22	-0.21	0.10	0.30	-0.19
10	-0.37	ł		-1.32		ŀ	-2.22		1			-0.02	
11	-1.26			-2.30	-2.59		-2.74	-2.83		-1.74	Į.	-0.74	
Noon	-1.83	-2.17		-2.98	-3.30			-3.52			1	-1.12	1
1	1	-2.32				Į.		-3.82	1		į.	ř .	-2.95
2		-2.23				ì		-4.15				1	
3		<b>-1.98</b>		-3.48								-1.02	1
4	-1.23	-1.35	-2.45	-3.24	-3.07	-3.05	-3.82	-3.71	-3.62	-2.40	-0.90	-0.66	-2.56
5	-0.79	-0.59	-1.79	-2.64	-3.13	-3.09	-3.18	-3.15	-2.94	-1.74	-0.54	-0.36	-2.00
6	-0.33	-0.04		-1.86				-2.32				-0.14	1
7	-0.05	0.31	-0.26	-0.80	-1.44	-1.16	-1.30	-1.09	-0.87	-0.30	0.01	0.06	1
8	0.24	0.58	0.34	0.04	0.22	-0.15	0.03	0.13	0.05	0.24	0.17	0.20	0.14
		0.00	0 =0	0	0.00	0 =0	7.00	7.05	0 ==0	0 1111	0.00	0.00	0 70
9	0.40	0.82	0.78	0.77	0.88	0.79	1.09	1.05	0.78	0.71	0.30	0.30	0.72
10	0.57	0.94 1.01	1.05 1.30	1.30 1.75	1.59 $2.29$	$1.73 \\ 2.69$	1.87 2.62	1.62 $2.26$	1.28	1.02	0.42	0.40	1.15
Midn	0.71	1.07	1.54	2.11	2.29	3.01	3.18	2.20	2.00	1.35	$0.56 \\ 0.62$	0.44	1.56 $1.22$
Midn	0.00	1.07	1.04	2.11	2.02	3.01	3.10	2.00	2.00	1.44	0.02	0.00	1.22
6. 6	0.40	0.58	0.52	0.44	0.11	0.01	0.10	0.24	0.77	0.53	0.43	0.26	0.37
7. 7	0.54	0.73	0.76	0.72	0.17	0.03	0.05	0.30	0.88	0.64	0.48	0.36	0.47
8. 8	0.68	0.69	0.68	0.47	0.27	0.17	0.26	0.35	0.71	0.66	0.35	0.37	0.47
9. 9	0.45	0.37	0.32	0.31	0.21	0.12	0.22	0.19	0.28	0.25	0.20	0.30	0.27
10.10	0.10	0.03	-0.02	-0.01	0.03	0.07	-0.19	-0.11	-0.09	0.10	-0.00	0.19	0.01
7. 2. 9	-0.17	-0.09	-0.17	-0.18	-0.44	-0.68	-0.53	-0.47	-0.20	-0.23	-0.12	-0.11	-0.28
6. 2. 8		-0.15		-0.26					-0.15		-0.12		-0.30
6. 2.10	1	-0.03				-0.03	0.12	0.09	0.26		-0.03		0.04
6. 2. 6	-0.41	-0.36	-0.67	-0.90	-1.25	-1.34	-1.30	-1.23	-0.82	-0.64	-0.25	-0.25	-0.79
* 0	0.7	0.5-	0.01	0.00	1 10	1 12	7.0-	7.00	0.00	0 =0	0.00	0.03	0.00
7. 2 8. 2		-0.55						ł.					
8. 1	1	-0.72 $-0.76$				ł .			1				-1.14 -1.07
7. 1		-0.59				į.		)			,		1
	1010	100	0.02	0.01	1.02	1.20	2.10		0.00	2.00	0.02	0.00	-
9.12.3.9	-0.67	-0.85	-1.17	-1.46	-1.71	-1.72	-1.76	-1.80	-1.71	-1.21	-0.60	-0.39	-1.25
7. 2.2(9)	-0.03	0.14	0.07	0.06	-0.11	-0.31	-0.13	-0.09	0.05	0.01	-0.02	-0.01	-0.03
Deil aus	-0.11	_0.59	0.20	0.24	0.02	_0.15	0.00	0.19	0.90	_0.19	_0.26	_0 20	_0.20
Dail. ext.	-0.44	-0.53	-0.38	-0.24	-0.03	-0.15	-0.09	-0.12	-0.20	-0.42	-0.26	-0.33	-0.30

### LVII.

PRUSSIA. — BERLIN. Lat. 52° 30' N. Long. 13° 24' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degre		eaumur	•					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	0.34	0.59	0.90	1.78	2.21	2.15	1 70	1.50	1 50	0.05	0.44	0.34	1.21
1	0.43	0.59	1.13	2.22	3.23	2.15	1.78 2.52	1.52 2.53	1.50	0.95 1.48	0.44	0.34	1.67
2	0.49	0.73	1.38	2.56	3.83	3.38	3.06	3.05	2.41	1.45	0.68	0.43	2.02
3	0.54	1.09	1.64	2.41	4.00	3.46	3.28	3.15	2.76	2.31	0.03	0.46	2.15
,	0.04	1.03	1.04	2.41	4.00	9.40	3.20	3.13	2.10	2.01	0.73	0.40	2.10
													}
4	0.58	1.25	1.85	3.03	3.77	3.18	3.12	3.40	2.94	2.45	0.79	0.52	2.24
5	0.65	1.37	1.97	3.05	3.16	2.59	2.67	3.16	2.89	2.32	0.84	0.56	2.10
6	0.73	1.39	1.92	2.69	3.23	1.73	1.92	2.57	2.56	1.52	0.84	0.71	1.73
7	0.75	1.18	1.62	2.01	1.43	0.94	1.18	1.83	2.03	1.15	0.65	0.63	1.21
6	0.00	0.00	1,14	0.0.	0.10	0.43	0.44	0 ==	1.00	0.00	0 ~0	0.00	0.70
8 9	0.62	0.89	1.14	0.94			0.44	0.75		0.62	0.56	0.60	0.70
10	0.41	0.49							-0.09		1	0.38	0.00
11	1				-1.47		-1.15		-0.81	-0.81	-0.09	0.05	-0.66
11	-0.30	-0.66	-1.02	-1.78	-2.20	-1.72	-1.78	-2.07	-1.90	-1.46	-0.55	-0.36	-1.32
Noon.									-2.49				-1.77
1									-2.96				-2.11
2	-1.07	-1.73	-2.20	-2.98	-3.25	-2.72	-2.75	-3.17	-3.16	-2.23	-1.27	-0.96	-2.29
3	-1.03	-1.67	-2.28	-3.27	-3.34	-2.84	-2.82	-3.25	-3.19	-2.12	-1.20	-0.95	-2.32
4	-0.78	-1.46	-2.07	-3.11	-3.11	-2.72	-2.73	-3.14	-3.16	-1.75	-0.81	-0.73	-2.13
5									-2.34				-1.76
6							-2.16				-0.30		-1.36
7	-0.22									1	-0.11		-0.84
·													
	0.70	0.00	0.0=	201	0.0-	0.5*	0.00	0.00	0.70	0.00	0.00	0.00	0.00
8	15 1								-0.16		0.05		-0.27
9	0.06	$0.03 \\ 0.21$	$0.05 \\ 0.39$	0.40	0.13	0.31	0.38	0.84	0.36	-0.08	0.10	0.06	0.22
10	0.14			0.93	1.56		1.01	1.06	0.98	0.26	0.20	0.17	0.59
11	0.24	0.38	0.65	1.37	1.50	1.58	1.44	1.57	1.20	0.56	0.36	0.25	0.93
6, 6	0.17	0.32	0.40	0.20	-0.06	-0.31	_0.12	0.19	0.49	0.32	0.27	0.23	0.10
7, 7	0.17	0.36	0.49		-0.06		-0.12	0.19	0.49	0.32	0.27	0.23	0.10
7, 7 8, 8	0.27	0.35	0.49		-0.08		0.03	0.30	0.60	0.26	0.27	0.24	0.22
	0.23	0.35	0.30	0.30			0.03	0.23	-0.23	-0.06	0.28	0.29	0.13
9, 9	0.24	0.50	0.00	0.12	0.21	0.00	0.02	0.24	0.20	0.00	Giù.O	0.22	0.12
10, 10	0.17	0.06			<b>(</b>			1	-0.09			0.11	0.05
7, 1	-0.09		i		-0.79		-0.68						-0.42
7, 2, 9			1						-0.26				-0.26
6, 2, 10	-0.07	-0.04	0.04	0.21	-0.07	-0.01	0.06	0.15	0.13	-0.15	-0.08	-0.03	-0.07
D-21	0.56		2	0.50	0.25		0.00						
Daily ext.	-0.16	-0.17	-0.16	-0.11	0.33	0.31	0.23	0.08	-0.13	0.11	-0.22	-0.13	0.00
	1												

### LVIII.

Germany. — Salzuflen. Lat. 52° 5′ N. Long. 8° 40′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

<u></u>					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.00	1.10	1.05	2.11	2.41	2.57	2.05	1.71	2.12	1.24	0.90	0.31	1.46
Morn. 1	0.55	1.10	1.20	2.11	2.93	1	1	1	2.12	1			
3	0.60	į.	1.34	2.64	3.29	2.98	1	i		1		(	ł
4	0.62	1.26	1.38	2.62	3.37	2.86	1			1	1	1	
5	0.72	1.18	1.29	2.35	3.08	2.47		1	1	1.97	l .	0.83	1
6 7	0.62	1.01	1.06	1.80	2.41	1.83		1		1		0.79	3
8	0.51 0.31	0.75	$0.70 \\ 0.25$	$\begin{array}{ c c } 1.05 \\ 0.20 \end{array}$	$\begin{array}{ c c c } 1.45 \\ 0.38 \end{array}$	1.02 0.15	l .	1	1.34 0.30	I .	1	0.64	0.94 0.31
	0.51	0.41	0.20	0.20	0.50	0.19	-0.00	0.00	0.50	0.75	0.02	0.00	0.51
9	0.08	-0.03	-0.22	-0.63	-0.59	-0.67	-0.74	-0.54	-0.65	0.09	0.14	0.06	-0.31
10	ll .	-0.53							1	1	1	-0.24	-0.88
11	13	-1.02						1	1	1			t .
Noon	-0.91	-1.42	-1.39	-2.32	-2.31	-2.39	-1.90	-1.72	-2.41	-1.78	-1.18	-0.62	-1.70
1	-1.01	-1.68	-1.59	-2.54	-2.53	-2.72	-2.13	-2.03	-2.75	-2.09	-1.48	-0.64	-1.93
2	ll.	-1.74		,			1		Į.				
3	-0.79	-1.58	-1.56	-2.49	-2.72	-2.92	-2.36	-2.42	-2.90	-2.06	-1.46	-0.50	-1.98
4	-0.50	-1.29	-1.33	-2.21	-2.65	-2.71	-2.24	-2.30	-2.70	-1.76	-1.22	-0.41	-1.78
_	0.00	0.00	0.00	1 **	2.00	2 20	1 00	3 0=	3.05		0.00	0.05	7 10
5 6	4	-0.90				1		1			1		
7	0.01	-0.51 -0.17		-0.62		-0.86			-0.71	1	-0.65 $-0.44$		
8	0.08	0.11		-0.04				1	1	-0.11	1		
		0.11	0.10	0.01	0.00	0.00	0.00	0.21	0.12	0.11	0.51	0.2.	,0.00
9	0.14	0.34	0.45	0.48	0.04	0.62	0.70		0.81	1	-0.20	-0.21	0.34
10	0.21	0.55	0.63	0.94	0.68	1.22	1.26	-	1.30			-0.12	0.67
11	0.22	0.74	0.77	1.34	1.27	1.74	1.52	1.25	1.61	0.66	1	0.01	0.94
Midn	0.40	0.93	0.90	1.74	1.84	2.18	1.80	1.45	1.86	0.94	0.50	0.15	1.22
6. 6	0.26	0.25	0.25	0.29	0.24	0.11	0.05	0.13	0.32	0.43	0.36	0.24	0.24
7. 7	0.26	0.29	0.28	0.22	0.06	0.08	0.04	0.16	0.32	0.44	0.30	0.17	0.22
8. 8	0.20	0.26	0.22		-0.14	0.03	0.02	0.15	0.21	0.32	0.16	0.06	0.13
9. 9	0.11	0.16		-0.08	-0.28	-0.03	-0.02	0.09	0.08		-0.03	-0.08	0.02
10.10	-0.06	0.01	-0.03	-0.21	-0.37	-0.08	0.06	0.01	-0.09	-0.11	-0.21	-0.18	-0.11
7. 2. 9	-0.10	-0.22	-0.17	-0.36	-0.39	-0.42	-0.30	-0.27	-0.25	-0.22	-0.24	-0.05	-0.25
6. 2. 8		-0.21											
6. 2.10		-0.06	0.01	0.05	0.14	0.05	0.13			-0.00		0.03	0.04
6. 2. 6	-0.14	-0.41	-0.38	-0.67	-0.73	-0.90	-0.73	-0.68	-0.76	-0.44	-0.28	-0.04	-0.51
7. 2	-0.22	-0.50	_0.49	-0 -0	-0.67	0.05	_0.00	_0.70	_0 =0	_0.40	_0.90	0.00	_0.54
8. 2		-0.50 -0.67				j.							-0.54 -0.86
8. 1		-0.64		- 1		- 1				1			- 1
7. 1	1	-0.47	1			1							l l
9.12.3.9		-0.67											
7. 2.2(9)	-0.04	-0.08	-0.01	-0.15	-0.28	-0.16	-0.05	-0.02	0.02	-0.12	-0.23	-0.09	-0.10
Dail.ext.	-0.15	-0.24	-0.14	0.02	0.33	0.03	0.02	-0.08	-0.02	-0.10	0.04	0.10	-0.02
			0.11	0.02	0.00	0.00	0.02	0.001	0.02	0,10	330 I	- 5725	

### LIX.

# PRUSSIA. — STETTIN. Lat. 53° 25' N. Long. 14° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

					Degre	es of R	eaumur	•					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	0.26	0.54	0.98	1.66	2.21	2.21	1.83	1.93	1.53	0.88	0.50	0.39	1.24
1	0.38	0.59	1.17	1.91	2.66	2.46		2.24	1.61	1.01	0.44	0.46	1.43
2	0.43	0.70	1.30	2.15	3.03	2.84	2.62	2.54	1.87	1.13	0.47	0.50	1 63
3	0.49	0.88	1.41	2.39	3.39	3.10	2.95	2.83	2.11	1.24	0.51	0.56	1.99
4	0.53	0.89	1.51	2.60	3.58	3.08	3.07	3.08	2.33	1.33	0.55	0.61	1.92
5	0.57	0.97	1.63	2.67	3.45	2.78	2.85	3.10	2.46	1.40	0.58	0.64	1.92
6	0.55	0.94	1.62	2.40	2.78	2.12	2.21	2.78	2.45	1.42	0.60	0.56	1.70
7	0.46	0.83	1.37	1.70	1.63	1.17	1.31	2.02	1.98	1.25	0.52	0.46	. 1.23
8 9	0.36	0.66		0.66			1		1.11	0.79			0.59
li l	0.22	0.36						-0.26	1	0.16	0.13	0.23	-0.13
10 11	-0.04							-1.40			-0.22	1	-0 83
11	-0.36	-0.53	-1.06	-2.07	-2.62	-2.18	-1.96	-2.23	-1.96	-1.23	-0.60	-0.35	-1.43
Noon.	-0.63	-0.93	-1.59	-2.50	-3.09	-2.59	-2.46	-2.93	-2.58	-1.68	-0.90	-0.64	-1.88
1								-3.38					
$\frac{1}{2}$	-0.90	-1.39	-2.08	-2.94	-3.50	-2.99	-2.99	-3.50	-2.99	-2.06	-1.06	-0.94	-2.28
3								-3.38					
4								-3.03					
5								-2.40	-1.85	-0.99	-0.39	-0.48	-1.49
6								-1.68	-1.14			-0.30	
7	-0.11	-0.23	-0.40	-0.55	-0.89	-0.89	-0.93	-0.78	-0.52	-0.10	-0.00	-0.18	-0.46
8	0.01	-0.01	_0.02	0.10	-0.14	_0.14	-0.17	0.02	0.06	0.17	0.18	-0.06	0.00
9	0.03	0.16	0.32	0.68	0.73	0.73	0.48	0.02	0.60	0.17	0.30	0.07	0.31
10	0.20	0.30	0.61	1.10	1.30	1.30	1.03	1.20	1.00	0.58	0.43	0.22	0.77
11	0.25	0.42	0.79	1.42	1.76	1.76	1.47	1.60	1.31	0.74	0.50	0.32	1.03
						2000		1100		0	0.00		1100
6.0	0.15	0.24	0.36	0.74	0.50	0.70	0.00	0.55	0.0"	0.40	0.01	0.10	0.90
6, 6	0.13	0.30	0.30	$0.54 \\ 0.57$	$0.52 \\ 0.37$	0.19 0.14	0.29	$0.55 \\ 0.62$	0.65	0.48	$0.21 \\ 0.26$	0.13	0.36
8, 8	0.17	0.31	0.45	0.38	0.10	0.03	0.19	0.62	0.73	0.57	0.20	0.14	0.30
9, 9	0.15	0.26	0.28	1	-0.08	i	-0.03	0.49	0.39	0.48	0.31	0.15	0.16
3, 3	0.10	0.20	0.20	0.13	0.03	0.01	0.00	0.24	0.20	0.20	0.22	0.13	0.10
10, 10	0.03	0.14	0.09	-0.13	-0.29	-0.12	-0.15	-0.10	-0.06	0.02	0.11	0.10	-0.03
7, 1	-0.17	-0.21	-0.67	-0.55	-0.S6	-0.86	-0.75	-0.68	-0.45	-0.36	-0.27	-0.20	-0.50
7, 2, 9	-0.13	-0.13	-0.13	-0.19	-0.38	-0.36	-0.40	-0.25	-0.14	-0.14	-0.08	-0.14	-0.21
6, 2, 10	-0.05	-0.05	0.38	0.19	0.19	0.14	0.08	0.16	0.15	-0.02	-0.01	-0.05	0.09
Daily ext.	-0.16	-0.21	-0.23	-0.14	0.04	0.06	0.04	-0.20	-0.27	-0.32	-0.23	-0.15	-0.15

#### LX.

Sleswick. — Apenrade. Lat. 55° 3' N. Long. 9° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
25 1	0.00	0.00	0.00	1 **0	0.10	0.00	0.50	0.07	0.10	: 00	0.54	0.01	
Morn. 1	0.26	0.69	0.98 1.14	1.73 1.83	3.18 3.17	3.82 $3.90$		2.61 $2.66$	2.16 $2.29$	1.06	1	0.31	1.65 1.72
3	0.38	0.79	1.14	1.98	3.02	3.82	1	2.66	2.54	1.19		0.37	1.74
4	0.42	0.75	1.34	2.10	2.71	3.50	1	2.64	2.62	1.37	0.66	0.38	1.69
_													
5 C	0.44	0.69	1.31	2.02	2.22	2.89		2.18	2.43	1.36		0.40	1.50
6 7	$0.50 \\ 0.47$	$0.62 \\ 0.54$	1.18 0.90	1.63 1.15	1.54 0.70	1.94 0.83	0.86	$1.56 \\ 0.77$	2.02 1.18	$1.25 \\ 0.97$	0.69	$0.40 \\ 0.37$	1.18 0.73
8	0.39	0.38	0.50	0.41	-0.23	-0.34		-0.18	0.18	0.52	0.61	0.37	0.13
	0.50	0.00	0.00	0.11	0.20	0.01	0.20	0.10	0.10	0.02	0.12	0.2.	0.11
9	0.23	1	1	1	i	l	-0.87			-0.10	0.10	0.10	-0.44
10		-0.32									1	-0.15	1
11	l í	-0.78	ł							1	-0.68		-1.41
Noon	-0.62	-1.19	-1.62	-2.42	-2.86	-2.98	-2.09	-2.74	-2.79	-1.94	-0.98	-0.66	-1.91
1	-0.78	-1.40	-1.90	-2.75	-3.08	-3.24	-2.23	-2.89	-3.03	-2.15	-1.10	-0.78	-2.11
2	II	-1.34	1	1						l .		-0.75	1
3	II	-1.06		(								-0.59	1
4	-0.38	-0.64	-1.41	-2.43	-2.86	-3.62	-2.02	-2.39	-2.54	-1.23	-0.59	-0.38	-1.71
_	0.10	0.20	0.00	1.00	0 10	0.04	1 **0	2.02	7 00	0.00	0.00	0.15	7 00
5 6	-0.16					1	-1.70		-1.93		-0.29	ì	-1.30
7	-0.03 0.01	0.05	-0.42 $0.02$		-0.79	-2.57 $-1.42$	-1.18 -0.57	-1.23 $-0.47$	ł.	-0.25 $0.10$	-0.12 $0.02$	Į.	$\begin{bmatrix} -0.80 \\ -0.27 \end{bmatrix}$
8	0.03	0.18	0.02	0.66		-0.07	0.18	0.40	0.56	0.34	0.03	0.14	0.25
	0.00	0.10	0.00	0.00	0.22	0.0.	0.10	0.40	0.50	0.01	0.00	0.11	0.20
9	0.01	0.17	0.54	1.25	1.22	1.25	0.97	1.21	1.21	0.51	0.09	0.15	0.71
10	0.02	0.22	0.66	1.57	2.05	2.33	1.63	1.72	1.61	0.65	0.18	0.18	1.07
11	0.07	0.33	0.76	1.69	2.66	3.10	2.14	2.25	1.83	0.85	0.30	0.21	1.35
Midn	0.15	0.52	0.86	1.70	3.02	3.57	2.43	1.68	1.97	0.92	0.42	0.26	1.46
6. 6	0.24	0.34	0.38	0.32	-0.08	-0.32	-0.16	0.17	0.45	0.50	0.29	0.21	0.19
7. 7	0.24	0.36	0.46	0.52	-0.05	-0.30	-0.14	0.15	0.46	0.54	0.30	0.24	0.23
8. 8	0.21	0.28	0.42	0.54	-0.01	-0.21	-0.06	0.11	0.37	0.43	0.23	0.21	0.21
9. 9	0.11	0.14	0.26	0.42	0.04	-0.07	0.05	0.06	0.19	0.21	0.10	0.13	0.14
10.10	-0.02	-0.05	-0.00	0.18	0.08	0.09	0.12	-0.13	-0.05	-0.07	-0.06	0.02	0.01
7. 2. 9	-0.08	-0.21	-0.17	-0.16	-0.41	-0.47	-0.33	-0.31	-0.23	-0.20	-0.11	-0.08	-0.23
6. 2. 8	l I	-0.18					-0.41			-0.16	1		-0.23
6. 2.10	ll .	-0.17	-0.04	0.10	0.14	0.26	0.07	0.13		-0.06		ſ	0.04
6. 2. 6	ll .	-0.22		1	-1.11		-0.86			-0.36		)	-0.58
<b>*</b> 0	0.1-	0.10	0 50	0.00	7.00	1 00	0.00	1.00	0.05	0.55	0.07	0.10	0.70
7. 2 8. 2	1	-0.40								ł			-0.70 -0.98
8. 1	i I	-0.48 -0.51	,							ŀ	1		-0.95 $-0.97$
7. 1		<b>-0.31</b> <b>-0.43</b>					-0.97				J		-0.69
	0.10	0.49	0.00	0.00	1,10	1,91		2.00	0.00	0.00			
9.12.3.9	-0.25	-0.50	-0.72	-1.10	-1.47	-1.70	-1.05	-1.35		1		-0.25	
7. 2.2(9)	-0.06	-0.12	0.01	0.19	0.01	-0.04	-0.01	0.07	0.13	-0.02	-0.06	-0.02	0.01
Doil ove	-0.14	_0.31	_0.31	-0.10	0.01	0.11	0.19	_0.19	_0.22	_0.30	-0.21	-0.19	-0.20
Dail. ext.	-0.14	-0.51	_0.9T	-0.40	0.01	0.11	0.12	-0.12	-0.23	-0.59	0.21	0.13	0.20

### LXI.

## Scotland. — Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degree	s of Fal	renheit	•					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	'Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.38	0.86	1.76	3.02	3.04	3.29	4.10	2.95	2.54	1.10	1.26	0.72	2.09
2	0.61	0.77	1.98	3.92	3.47	3.62	4.28	3.20	2.77	1.19	1.53	0.65	2.33
3	0.68	0.77	2.41	4.57	3.96	3.74	4.66	3.49	3.29	1.31	1.40	0.61	2.57
4	0.95	0.95	2.59	5.31	4.41	3.98	5.11	3.71	3.65	1.33	1.46	0.70	2.84
5	1.06	1.17	2.75	5.49	4.28	3.94	4.59	3.65	3.78	1.62	1.37	0.77	2.87
6	1.06	1.31	2.79	5.36	3.51	3.04	3.56	3.26	3.51	2.03	1.28	0.59	2.61
7	0.97	1.24	2.48	3.47	2.66	2.25	2.39	2.25	2.75	1.62	1.06	0.68	1.98
8	0.88	1.26	1.80	2.18	1.40	1.10	1.15	1.08	1.46	0.97	1.04	0.54	1.24
9	0.61	0.77	0.81	-0.27	0.11	_0.18	-0.23	-0.50	-0.14	0.32	0.56	0.32	0.18
10		-0.07		-2.00							1	-0.02	
11		-0.97		-3.02			1				1	-0.86	
Noon		-1.69	1	-3.92		1	1		l		1	-1.33	1
INOUII	1.04	1.03	2.01	0.04	2.10	2.13	0.00	2.09	0.19	2.50	1,90	1.00	2.01
1	-1.42	-2.25	-2.97	-4.37	-3.35	-3.15	-3.67	-3.44	-3.92	-2.79	-2.30	-1.51	-2.93
2	-1.58	-2.23	-3.29		-3.78		1	1	J			-1.55	
3	-1.60	-2.27	-3.38	-5.09	-3.85			1	1			-1.13	
4	-1.19	-1.73				1		ł				-0.83	
	1												
5	-0.68	<b>-0.</b> 95	-2.84	-4.25	-4.03	-3.71	-4.57	-3.76	-3.56	-1.31	-1.04	-0.50	-2.60
6	-0.45	-0.47	-2.14	-3.83	-3.51	-3.29	-4.41	-3.47	-2.30	-0.59	-0.68	-0.27	-2.12
7	-0.09	-0.09	-1.17	-2.45	-2.61	-2.52	-3.58	-1.69	-0.97	0.05	-0.25	0.18	-1.27
8	0.14	0.32	-0.45	-0.81	-1.17	-0.79	-1.31	-0.41	-0.16	0.59	0.05	0.29	-0.31
9	0.23	0.61	0.25	0.38	0.32	0.50	0.43	0.59	0.59	0.72	0.32	0.36	0.44
10	0.18	0.88	0.77	1.08	0.86	1.89	1.71	1.58	1.24	1.15	0.79	0.41	1.04
11	0.32	0.99	1.31	2.18	1.69	2.16	2.52	2.23	1.67	1.60	1.19	0.54	1.53
Midn	0.38	1.01	1.44	2.68	2.32	2.68	3.44	2.77	2.27	1.49	1.42	0.59	1.87
6. 6	0.32	0.43	0.34	0.77	0.00	-0.14	-0.43	-0.11	0.61	0.72	0.32	0.16	0.25
7. 7	0.45	0.59	0.65	0.52	0.02	-0.14		0.29	0.90	0.83	0.32	0.43	0.25
8.8	0.45	0.39	0.68	0.32	0.02		<b>-0.01</b>	0.29	0.65	0.55	0.54	0.43	0.47
9. 9	0.32	0.70	0.54	0.70	0.11	0.16	0.11	0.05	0.03	0.19	0.34	0.34	0.32
10.10	0.18	0.41	0.34	-0.47	-0.11	0.10	0.11	0.05	0.23	0.16	0.23	0.34	0.15
10.10	0.10	0.41	0.47	0.47	0.11	0.23	0.10	0.10	0.07	0.10	0.20	0.20	0.10
7. 2. 9	-0.14	-0.14	-0.18	-0.29	-0.27	-0.36	-0.43	-0.27	-0.32	-0.16	-0.41	-0.18	-0.26
6. 2. 8		-0.20	l .	-0.07			-0.61			-0.07			-0.30
6. 2.10		-0.02			0.20	0.36	Į.	0.41	0.16	0.11		-0.18	0.15
6. 2. 6	1	-0.47	1	-1.06			-1.64	(	-1.01			-0.41	-0.90
7. 2	1		-0.41		)		1						
8. 2	-0.36	-0.50	-0.74										
8. 1	-0.27	-0.50	-0.59	-1.10	-0.99	-1.04	-1.26	-1.19	-1.24	-0.92	-0.63	-0.50	-0.85
7. 1	-0.23	-0.52	-0.25	-0.45	-0.36	-0.45	-0.65	-0.61	-0.59	-0.59	-0.63	-0.41	-0.47
0.10.00	0.4-	0.00		2.25	,	,	1.04	1 0 1	,	0.05	0.00	0.45	1.00
9.12.3.9	l l		-1.24										
7. 2.2(9)	-0.05	0.07	-0.09	-0.14	-0.14	-0.16	-0.20	-0.07	-0.09	0.07	-0.23	-0.05	-0.09
Dail. ext.	-0.27	-0.10	-0.20	0.20	-0.11	-0.20	0.27	-0.09	-0.25	-0.40	-0.56	-0.40	-0.20
Dan. ext.	1 -0.27	0.49	-0.29	0.20	0.11	0.20	0.27	0.03	0.20	0.40	0.00	0.40	0120

### LXII.

### Scotland. - Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
							1.00						
Morn. 1	0.17	0.38	0.78	1.34	1.35	1.46	1.82	1.31	1.13	0.49	0.56	0.32	0.93
2	0.27	0.34	0.88	1.74	1.54	1.61	1.90	1.42	1.23	0.53	0.68	0.29	1.04
3	0.30	0.34	1.07	2.03	1.76	1.66	2.07	1.55	1.46	0.58	0.62	0.27	1.14
4	0.42	0.42	1.15	2.36	1.96	1.77	2.27	1.65	1.62	0.59	0.65	0.31	1.26
5	0.47	0.52	1.22	2.44	1.90	1.75	2.04	1.62	1.68	0.72	0.61	0.34	1.28
6	0.47	0.58	1.24	2.38	1.56	1.35	1.58	1.45	1.56	0.90	0.57	0.26	1.16
7	0.43	0.55	1.10	1.54	1.18	1.00	1.06	1.00	1.22	0.72	0.47	0.30	0.88
8	0.39	0.56	0.80	0.97	0.62	0.49	0.51	0.48	0.65	0.43	0.46	0.24	0.55
	0.00	0.04	0.00	0.10	0.05	0.00	0.10	0.00	0.00	0.74	0.05	0.14	0.00
9	0.27	0.34		-0.12				-0.22		0.14	0.25	0.14	0.08
10		-0.03						-0.56					
11		-0.43						-0.90				i	1
Noon	-0.46	-0.75	-1.16	-1.74	-1.22	-1.24	-1.59	-1.33	-1.39	-1.05	-0.87	-0.59	-1.12
1	-0.63	-1.00	-1.32	-1.94	-1.49	-1.40	-1.63	-1.53	-1.74	-1.24	-1.02	-0.67	-1.30
2	-0.70	-0.99	-1.46	-2.10	-1.68	-1.70	-1.81	-1.62	-1.90	-1.26	-1.14	-0.69	-1.42
3	-0.71	-1.01	-1.50	-2.26	-1.71	-1.94	-1.94	-1.62	-1.85	-1.14	-1.17	-0.50	-1.45
4			-1.48						1				
_	0.00	0.40	1.00	1.00	1 *0	1.05	0.00	1.0*	1 50	0.50	0.10	0.00	1 15
5			-1.26										
6			-0.95										
7	-0.04		-0.52	1						0.02		ì	-0.56
8	0.06	0.14	-0.20	-0.36	-0.52	-0.35	-0.58	-0.18	-0.07	0.26	0.02	0.13	-0.14
9	0.10	0.27	0.11	0.17	0.14	0.22	0.19	0.26	0.26	0.32	0.14	0.16	0.20
10	0.08	0.39	0.34	0.48	0.38	0.84	0.76	0.70	0.55	0.51	0.35	0.18	0.46
11	0.14	0.44	0.58	0.97	0.75	0.96	1.12	0.99	0.74	0.71	0.53	0.24	0.68
Midn	0.17	0.45	0.64	1.19	1.03	1.19	1.53	1.23	1.01	0.66	0.63	0.26	0.83
			'										
6. 6	0.14	0.19	0.15	0.34	0.00	_0.06	-0.19	-0.05	0.27	0.32	0.14	0.07	0.11
7. 7	0.14	0.13	0.13	0.23		-0.06		1	1	0.37	0.13	0.19	0.16
8. 8	0.20	0.20	0.20	0.23	0.05	0.07		1	0.29	0.35	0.24	0.19	0.21
9. 9	0.19	0.31	0.34	0.03	0.10	0.07	0.05		0.10	0.23	0.20	0.15	0.14
10.10	0.08	0.18	0.24		-0.05	0.13	{	0.07	0.03	0.07	0.10	0.09	
			0.65	0.75	0.10	0.10	0.70	0.10	0.1	0.00	0.10	0.00	0.10
7. 2. 9		-0.06		-0.13		l .	-0.19		-0.14	1	-0.18	1	1
6. 2. 8			-0.14	1		1	į.	-0.12			-0.18		1
6. 2.10		-0.01	0.04	1	0.09	1	1				-0.07		
6. 2. 6	-0.14	-0.21	-0.39	-0.47	-0.56	-0.60	-0.73	-0.57	-0.45	-0.21	-0.29	-0.18	-0.40
7. 2	-0.14	-0.22	-0.18	-0.28	-0.25	-0.35	-0.38	-0.31	-0.34	-0.27	-0.34	-0.20	-0.27
8. 2			-0.33										
8. 1			-0.26										
7. 1	-0.10	-0.23	-0.11	-0.20	-0.16	-0.20	-0.29	-0.27	-0.26	-0.26	-0.28	-0.18	-0.21
0.10.20	0.00	0.00	0.55	0.00	0.00	0.70	_0.00	_0.70	_0 =0	0 (0	-0.41	_0.20	-0.57
9.12.3.9	11		-0.55								-0.41 $-0.10$		
7. 2.2(9)	-0.02	0.03	-0.04	-0.06	-0.06	-0.07	_0.09	-0.03	-0.04	0.03	-0.10	-0.02	-0.04
Dail. ext.	-0.12	-0.22	-0.13	0.09	0.05	-0.09	0.12	-0.04	-0.11	-0.18	-0.25	-0.18	-0.09
1			1				1						

### LXIII.

Scotland. — Makerstoun. Lat. 55° 36' N. Long. 2° 31' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

		77.1				~	7 .		a . I	0 .	N7	D - 1	V.o.
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.67	0.88	1.24	2.30	2.00	2.25	2.10	1.98	1.95	0.88	0.46	0.24	1.41
1	0.76	0.92	1.37	2.52	2.04	2.43	2.44	2.24	2.15	0.88	0.46	0.16	1.53
2	0.78	1.08	1.37	2.70	2.33	2.54	2.57	2.38	2.26	1.06	0.60	0.18	1.65
3	0.76	1.06	1.48	2.79	2.55	2.65	2.79	2.56	2.35	1.57	0.60	0.29	1.79
4	0.67	1.01	1.66	2.96	2.51	2.43	2.70	2.56	2.48	1.20	0.68	0.40	1.77
5	0.78	0.92	1.77	2.88	2.06	1.96	2.21	2.44	2.46	1.40	0.60	0.44	1.66
6	0.60	0.85	1.73	2.25	1.31	1.12	1.35	1.78	2.22	1.31	0.66	0.51	1.31
7	0.51	0.99	1.26	1.43	0.48	0.32	0.46	0.91	1.24	1.26	0.66	0.44	0.83
8	0.53	0.79	0.46	0.36		-0.51	-0.39	-0.09	0.00	0.62	0.66	0.40	0.22
9	0.33	0.08		-0.79		-1.11	-0.96	-1.02	-1.00		0.08	0.22	-0.47
10	-0.22				-1.52		-1.59	-1.78	-1.92	-0.96	-0.47	-0.20	-1.17
11	-0.84				-2.09			-2.33	-2.45	-1.63	-0.94	-0.62	-1.73
Noon.						-2.48	4	-2.73		-2.03	1		
1	-1.71				-2.69		-2.48			-2.25		-1.13	
2	-1.67				1	-2.57	-2.52		-3.12		-1.47		-2.34
3	-1.29		-2.32		1	ì	-2.54		1	-1.83		-0.60	
4	-0.71		-1.80				-2.28	-2.47	-2.29			-0.16 $-0.11$	1)
5	-0.13	-0.50	-1.20	-2.30	-1.76	-1.64	-1.81	-1.78	-1.49	-0.49	-0.07	-0.11	-1.11
6	0.18	-0.08	-0.40	-1.39	-0.98	-0.95	-1.34	-1.07	-0.60	-0.09	0.13	0.18	-0.53
7	0.29	0.15	0.08	-0.19	-0.18	-0.40	-0.59	-0.18	0.06	0.17	0.17	0.18	-0.04
8	0.31	0.37	0.46	0.52	0.62	0.36	0.35	0.56	0.46	0.40	0.28	0.18	0.41
9	0.29	0.52	0.73	1.21	1.15	1.00	0.95	1.09	0.95	0.64	0.37	0.24	0.76
10	0.27	0.64	0.95	1.74	1.46	1.56	1.48	1.58	1.33	0.73	0.46	0.31	1.04
11	0.22	0.79	1.06	2.08	1.77	1.94	1.70	1.89	1.51	0.73	0.40	0.36	1.20
Mean.	1.53	0.35	2.06	5.96	6.86	10.25	10.12	10.00	8.51	6.64	4.60	1.16	

### LXIV.

IRELAND. — DUBLIN. Lat. 53° 23' N. Long. 6° 20' W. Gr. — Dove.

						egrees e	1 Headin	.u.					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M.1	0.58	0.53	1.56	2.18	2.53	2.76	2.18	2.22	1.64	1.16	0.53	0.36	1.52
3	0.80	0.71	1.64	2.40	2.89	3.11	2.53	2.40	1.87	1.42	0.67	0.49	1.74
5	0.93	0.98	1.64	2.49	2.31	2.18	2.18	2.53	1.87	1.73	0.76	0.58	1.68
7	0.84	0.93	1.38	0.58	-0.22	-0.89	-0.36	0.40	1.07	1.56	0.80	0.53	0.56
9	0.36	0.18	-0.31	-1.11	-1.24	-1.38	-1.10	-1.16	-0.76	-0.09	0.27	0.36	-0.50
11	-0.98	-0.07	-1.82	-2.40	-2.18	-2.09	-2.04	-2.27	-2.13	-1.91	-0.98	-0.71	-1.71
P.M.1	-1.60	-1.78	-2.67	-2.93	-2.62	-2.40	-2.27	-2.62	-2.67	-2.44	-1.56	-1.16	-2.23
3	-1.33	-1.47	-2.44	-2.84	-2.71	-2.31	-2.27	-2.49	-2.22	-2.04	-1.11	-0.67	-1.99
5	-0.44	0.44	-1.29	-1.82	-1.82	-1.87	-1.64	-1.73	-1.29	-0.84	-0.27	-0.18	-1.14
7	0.09	0.18	0.18	0.04	-0.27	-0.44	-0.27	-0.09	0.27	0.04	0.04	0.09	-0.01
9	0.22	0.31	0.76	1.20	1.29	1.24	1.20	1.16	0.93	0.58	0.36	0.18	0.79
11	0.36	0.40	1.07	1.73	1.96	2.04	1.87	1.64	1.42	0.84	0.44	0.22	1.17
Mean.	4.09	4.75	5.10	6.66	9.51	11.86	12.48	12.31	10.79	7.73	5.99	4.88	

### LXV.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.59	0.91	1.84	1.97	3.09	3.69	3.51	2.49	1.99	0.68	0.47	0.65	1.82
2	0.58	0.89	2.09	2.41	3.52	4.15	3.76	2.93	2.27	0.84	0.42	0.67	2.04
3	0.53	0.87	2.42	2.87	3.80	4.35	3.96	3.42	2.60	1.04	0.36	0.64	2.24
4	0.48	0.89	2.80	3.21	3.82	4.17	4.01	3.78	2.89	1.23	0.35	0.61	2.35
5	0.58	0.95	3.11	3.23	3.45	3.54	3.78	3.79	2.98	1.36	0.43	0.63	2.32
6	0.54	1.00	3.15	2.83	2.67	2.49	3.18	3.30	2.74	1.36	0.55	0.72	2.04
7	0.60	0.94	2.76	1.99	1.57	1.18	2.21	2.29	2.11	1.17	0.64	0.81	1.52
8	0.56	0.71	1.90	0.84	0.31	0.17	0.98	0.94	1.16	0.80	0.60	0.80	0.79
9	0.37	0.27	0.65	-0.41	-0.88	-1.35	-0.34	-0.48	0.05	0.28	0.37	0.61	-0.07
10	l .	-0.33		ì	-1.85			ļ	i			l .	-0.93
11	1	-0.97		1	-2.53		-2.72			1		-0.34	
Noon.		-1.47	1		-2.98		-3.64	ł				-0.90	
1	-1.30	-1.75	-3.52	-3.04	-3.25	-3.35	-4.33	-3.25	-2.98	-1.62	-1.12	-1.32	-2.57
2	-1.37	-1.77	-3.62	-3.03	-3.41	-3.50	-4.78	-3.34	-3.16	-1.69	-1.13	-1.50	-2.69
3	-1.19	-1.55	-3.39	-2.88	-3.46	-3.56	-4.90	-3.36	-3.17	-1.58	-0.95	-1.40	-2.62
4	-0.84	-1.19	-2.96	-2.60	-3.33	-3.46	-4.62	-3.27	-2.98	-1.31	-0.66	-1.10	-2.36
5	-0.34	-0.79	-2.40	-2.18	-2.95	-3.09	-3.90	-2.98	-2.57	-0.96	-0.37	-0.73	-1.94
6	-0.11	-0.42	-1.77	-1.61	-2.29	-2.43	-2.77	-2.39	-1.93	-0.58	-0.14	-0.39	-1.40
7	0.11	-0.10	-1.08	-0.92	-1.41	-1.52	-1.39	-1.53	-1.12	-0.23	0.01	-0.14	-0.78
8	0.22	0.17	0.36	-0.22	-0.42	-0.48	0.03	-0.53	-0.26	0.06	0.12	0.03	0.14
9	0.30	0.42	0.32	0.42	0.53	0.56	1.28	0.43	0.52	0.26	0.22	0.15	0.45
10	0.37	0.63	1	0.91	1.35	1.51	2.22	1.20	1.13	0.40	0.33	0.28	0.95
11	0.36	0.80	1	1.29	2.03	2.35	2.84	1.74	1.52	0.48	0.42	0.43	1.30
Midn	0.55	0.89	1.62	1.61	2.59	3.07	3.23	2.12	1.77	0.56	0.48	0.57	1.59
Miun	0.55	0.03	1.02	1.01	2.00	3.07	0.20	2.12	1.,,	0.50	0.40	0.57	1.55
6. 6	0.21	0.27	0.69	0.61	0.19	0.03	0.20	0.45	0.40	0.39	0.21	0.17	0.32
7. 7	0.35	0.42	Į.	0.53	1	-0.17	0.41	0.38	0.49	0.47	0.33	0.33	0.37
8. 8	0.39	0.44		1	-0.05		0.51	0.20	0.45	0.43	0.36	0.41	0.32
9. 9	0.33	0.34	0.49	0.01	-0.17		0.47	1	0.29	0.43	0.29	0.38	0.19
10.10	0.18	0.15		í	-0.25		0.31	1	0.05	0.04	0.15	0.25	0.00
7. 2. 9	-0.16	-0.14	-0.18	_0 21	-0.44	-0.50	-0.42	-0.21	-0.19	-0.09	_0.00	-0.19	-0.20
6. 2. 8	H.	1	-0.18		1		)		1	1			
6. 2.10	ll .	-0.20 -0.05	į.	0.24		l .	1			4	1	-0.23	0.10
6. 2. 6	II.	ļ.	-0.75	(				1		-0.30	1	1	-0.68
7. 2			-0.43										
8. 2	1	1	-0.86	1	1		1		1	l .	1	1	1 1
8. 1	11		-0.81	i	1	i		1		1		1	
7. 1	-0.35	-0.41	-0.38	-0.53	-0.84	-1.09	-1.06	-0.48	-0.44	-0.23	-0.24	-0.26	-0.53
9.12.3.9	-0.38	-0.58	-1.36	-1.43	-1.70	-1.87	-1.90	-1.61	-1.30	-0.60	-0.31	-0.39	-1.12
7. 2.2(9)		1	-0.06	1	į.		1		1	1	-0.01		1
Dail.ext.	÷ 0.39	-0.39	-0.21	0.10	0.18	0.40	-0.45	0.22	0.17	-0.17	-0.25	-0.35	-0.17
Dail. CAL.	11 0.00	0.00	0.24	0.10	0.10	0.40	0.40	1 0.22	0.11	0.11	0.20		7.11

### LXVI.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.42	1.07	1.70	2.12	2.64	3.06	2.93	2.16	1.96	0.89	0.47	0.47	1.66
1	0.52	1.19	2.00	2.40	3.11	3.51	3.41	2.49	2.31	1.08	0.51	0.50	1.92
2	0.52	1.25	2.23	2.82	3.49	3.90	3.86	2.76	2.58	0.99	0.54	0.52	2.12
3	0.55	1.41	2.53	3.05	3.73	4.15	4.11	3.03	2.83	1.47	0.58	0.54	2.33
4	0.63	1.52	2.75	3.26	3.74	3.92	4.28	3.22	3.06	1.61	0.68	0.58	2.44
5	0.68	1.67	2.85	3.24	3.27	3.35	3.66	3.14	3.22	1.67	0.71	0.61	2.34
6	0.73	1.76	3.06	2.24	2.27	1.99	2.47	2.45	3.04	1.69	0.82	0.64	1.93
7	0.81	1.76	2.59	1.61	0.89	0.61	1.02	1.37	2.27	1.53	0.85	0.65	1.33
8	0.88	1.51	1.46		-0.24			0.18	0.85	0.91	0.77	0.58	0.54
9	0.67	0.73		-0.81		-1.46		-0.97	-0.57	-0.03	0.33		-0.36
10	0.13	-0.45	-1.45	-1.99	-1.94	-2.23	-2.35	-1.72	-1.68	-0.78	-0.22	-0.08	-1.23
11	-0.57	-1.44	-2.39	-2.62	-2.72	-2.93	-3.10	-2.54	-2.50	-1.46	-0.72	-0.71	-1.98
Noon.	1	1		1				-2.99				-1.19	
1	-1.39			-3.22			-3.57		-3.32	1			1
2		-2.74			-3.41		-3.55	1		1	-1.23	-1.39	
3		-2.37	_			-3.37			-3.48		-1.11		1
4	te .	-1.97				-3.05	1	-2.83		i		-0.61	
5	-0.50	-1.28	-2.20	-2.14	-2.60	-2.49	-2.67	-2.37	-2.48	-0.95	-0.47	-0.33	-1.71
6	-0.22	-0.74	-1.37	-1.46	-1.98	-1.98	-2.14	-1.66	-1.56	-0.56	-0.26	-0.11	-1.17
7	0.00	-0.25	-0.67	-0.59	-0.95	-1.17	-1.29	-0.79	-0.65	-0.22	-0.07	0.02	-0.55
8	0.10	0.08	-0.12	0.13	-0.04	-0.12	-0.16	0.11	0.07	0.06	0.06	0.11	0.02
9	0.17	0.40	0.44	0.65	0.85	0.96	0.83	0.84	0.67	0.36	0.16	0.26	0.55
10	0.24	0.65	0.94	1.13	1.53	1.88	1.67	1.39	1.25	0.53	0.27	0.39	0.99
11	0.34	0.86	1.34	1.58	2.13	2.51	2.36	1.81	1.65	0.74	0.40	0.56	1.36
Mean.	-10.76	-9.50	-5.83	0.47	6.31	12.08	14.53	10.61	6.32	1.41	-6.11	-11.68	

### LXVII.

Russia. - St. Petersburg. Lat. 59° 56' N. Long. 30° 18' E. Gr. - Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.14	0.38	0.73	1.44	2.08	1.99	1.77	1.68	1.17	0.52	0.15	0.17	1.02
1	0.21	0.44	0.99	1.68	2.43	2.29	2.05	2.02	1.38	0.60	0.17	0.21	1.21
2	0.25	0.46	1.22	1.91	2.70	2.56	2.24	2.24	1.58	0.65	0.15	0.27	1.35
3	0.30	0.52	1.38	2.11	2.91	2.73	2.43	2.48	1.75	0.73	0.25	0.34	1.49
4	0.38	0.63	1.56	2.24	2.86	2.44	2.32	2.59	1.87	0.78	0.30	0.36	1.53
5	0.43	0.72	1.71	2.28	2.38	1.97	1.92	2.40	1.96	0.84	0.34	0.34	1.44
6	0.45	0.76	1.75	1.95	1.72	1.33	1.33	1.96	1.90	0.90	0.37	0.30	1.23
7	0.41	0.78	1.57	1.32	0.93	0.63	0.64	1.19	1.47	0.82	0.37	0.29	0.87
8	0.42	0.60	1.07	0.65	0.14	-0.04	0.05	0.42	0.81	0.57	0.32	0.25	0.44
9	0.35	0.40	0.40	-0.05	-0.59	-0.69	-0.56	-0.40	0.00	0.20	0.17	0.17	-0.05
10	0.13	-0.05	-0.19	-0.78	-1.30	-1.21	-1.12	-1.07	-0.71	-0.22	0.00	0.04	-0.54
11	-0.20	-0.48	-0.86	-1.42	-1.92	-1.71	-1.58	-1.64	-1.27	-0.61	-0.20	-0.14	-1.00

### LXVII.

### Russia. — St. Petersburg, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-0.38	-0.90	-1.31	-1.93	-2.30	-1.99	-1.89	-2.10	-1.72	-0.94	-0.37	-0.30	-1.34
1	-0.63	-0.97	-1.62	-2.10	-2.41	-2.17	-2.03	-2.47	-2.26	-1.75	-0.64	-0.48	-1.63
2	-0.66	-1.04	-1.88	-2.36	-2.65	-2.32	-2.15	-2.60	-2.34	-1.29	-0.63	-0.58	-1.71
3	-0.55	-0.99	-1.94	-2.49	-2.90	-2.45	-2.29	-2.64	-2.31	-1.06	-0.46	-0.40	-1.71
4	-0.33	-0.83	-1.92	-2.65	-2.92	-2.60	-2.41	-2.80	-2.27	-0.86	-0.20	-0.31	-1.68
5	-0.25	-0.45	-1.53	-2.31	-2.48	-2.23	-2.06	-2.45	-1.76	-0.50	-0.16	-0.22	-1.37
6	-0.19	-0.26	-1.02	-1.43	-1.65	-1.41	-1.30	-1.41	-0.95	-0.25	-0.11	-0.14	-0.84
7	-0.18	-0.16	-0.55	-0.61	-0.74	-0.71	-0.63	-0 62	-0.35	-0.09	-0.05	-0.10	-0.40
S	-0.14	-0.03	-0.25	-0.03	0.06	-0.03	0.02	0.09	0.07	0.07	0.01	0.08	-0.01
9	-0.11	0.08	0.03	0.47	0.79	0.67	0.64	0.65	0.40	0.18	0.08	0.03	0.33
10	-0.03	0.17	0.24	0.84	1.22	1.25	1.18	1.05	0.66	0.33	0.08	0.02	0.58
11	0.06	0.30	0.50	1.17	1.76	1.65	1.45	1.40	0.91	0.45	0.11	0.11	0.82
Mean.	-7.41	-6.73	-3.56	1.10	7.01	11.33	13.39	13.58	8.43	3.61	<del>-0</del> 80	-3.75	

### LXVIII.

Russia. — Helsingfors. Lat. 60° 10' N. Long. 24° 57' E. Gr. — Dove.

					D	egrees of	Reaum	ur.					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.06	0.47	1.28	1.61	1.61	2.01	1.65	1.36	0.83	0.37	0.18	0.20	0.97
1	0.13	0.49	1.48	1.87	1.94	2.44	1.90	1.68	1.03	0.45	0.15	0.21	1.15
2	0.16	0.52	1.64	2.07	2.21	2.84	2.17	1.98	1.21	0.55	0.18	0.18	1.31
3	0.23	0.67	1.84	2.21	2.58	3.04	2.45	2.23	1.35	0.65	0.23	0.15	1.47
4	0.35	0.64	1.91	2.37	2.68	2.77	2.42	2.49	1.48	0.62	0.28	0.23	1.52
5	0.38	0.77	1.98	2.34	2.28	2.21	2.05	2.41	1.63	0.67	0.33	0.10	1.43
6	0.38	0.92	2.01	1.74	1.31	1.31	1.33	1.81	1.63	0.75	0.33	0.03	1.13
7	0.41	0.99	1.78	1.14	0.58	0.51	0.55	1.11	1.28	0.73	0.36	0.01	0.79
8	0.43	0.99	1.04	0.17	-0.19	-0.36	-0.10	0.26	0.58	0.57	0.35	0.00	0.31
9	0.38	0.55	0.04	-9.73	-0.86	-0.83	-0.73	-0.56	-0.09	0.33	0.25	0.06	-0.18
10	0.08	-0.20	-0.89	-1.49	-1.39	-1.29	-1.23	-1.12	-0.65	-0.15	0.13	-0.07	-0.69
11	-0.19	-0.93	-1.19	-1.93	-1.76	-1.83	-1.65	-1.59	-1.05	-0.47	-0.19	-0.32	-1.09
Noon.	-0.72	-1.25	-2.36	-2.26	-1.82	-1.76	-1.80	-2.02	-1.67	-0.90	-0.59	-0.42	-1.46
1	-0.79	-1.50	-2.62	-2.46	-2.12	-2.06	-2.13	-2.26	-1.82	-1.08	-0.70	-0.45	-1.67
2	-0.74	-1.60	-2.62	-2.56	-2.19	-2.36	-2.28	-2.31	-1.85	-1.10	-0.64	-0.42	-1.72
3	-0.49	-1.33	-2.46	-2.37	-2.16	-2.49	-2.13	-2.17	-1.75	-0.95	-0.50	-0.22	-1.58
-1	-0.24	-0.90	-2.12	-1.89	-1.82	-2.16	-1.75	-1.84	-1.52	-0.77	-0.29	-0.02	-1.28
5	-0.12	-0.43	-1.56	-1.59	-1.49	-1.89	-1.48	-1.64	-1.20	-0.43	-0.17	0.03	-1.00
6	-0.04	-0.21	-0.79	-1.09	-1.09	-1.53	-1.15	-1.19	-0.72	-0.25	-0.09	-0.02	-0.68
7	0.03	0.07	-0.29	-0.49	-0.86	-0.96	-0.68	-0.64	-0.27	-0.13	-0.04	0.01	-0.35
8	0.08	0.20	0.01	0.14	-0.16	-0.36	-0.10	-0.14	0.05	-0.03	0.00	0.11	-0.02
9	0.10	0.25	0.44	0.64	0.44	0.37	0.55	0.28	0.23	0.05	0.06	0.13	0.29
10	0.08	0.35	0.74	1.04	0.94	1.04	1.02	0.71	0.43	0.13	0.10	0.18	0.56
11	0.01	0.42	1.01	1.37	1.34	1.54	1.37	1.06	0.63	0.27	0.18	0.15	0.78
Mean.	-5.02	-7.43	-3.89	-0.06	5.11	10.84	12.75	14.11	9.23	4.55	1.13	-3.42	

### LXIX.

Russia. — Petersburg. Lat. 59° 56' N. Long. 30° 18' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of R	aumur.	·					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
75 1	0.20	0.38	0.92	1.52	2.59	2.40	1.98	2.08	1.39	0.72	0.14	0.17	1.21
Morn. 1	0.20	1	1.10		2.59		$\begin{array}{ c c c } \hline 1.98 \\ 2.26 \\ \hline \end{array}$			0.72		1	1 1
3	0.23	0.39	1.30	1	3.03	l .	2.49	2.79	1.97	0.82		0.33	
4	0.21	0.43	1.49	2.19	3.05		2.57	3.01	2.20	0.88		1	1.62
1													
5	0.26	1	1.59	2.17	2.79		2.37	2.92	2.25	0.95			1
6	0.37	0.57	1.56	1.88	2.20	1.98	1.88		2.06	0.98		0.34	1.38
7	0.51	0.56	1.36		1.27		1.15			0.92	1	0.33	1 1
8	0.59	0.46	0.99	0.68	0.41	0.24	0.34	0.79	1.01	0.72	0.16	0.31	0.56
9	0.53	0.23	0.47	-0.02	-0.47	-0.53	-0.40	-0.10	0.31	0.36	0.03	0.27	0.06
10	11	-0.09	1	f .		1		-0.86			1	l .	-0.43
11	0.01	-0.43		-1.18				-1.47				0.03	1
Noon	-0.34	-0.73	-1.28	-1.62	-2.09	-1.83	-1.67	-2.01	-1.75	-0.99	-0.49	-0.15	-1.25
	0.70	0.00	1.00	0.05	0.70	0.00	7.00	0.50	2.22			0.55	
1	II.	-0.92		)		ł	1	1	1				1
$\begin{vmatrix} 2 \\ 3 \end{vmatrix}$	11	-0.95 -0.86				l .	1						1
4	11	-0.67				i e		1			ł .		1
*	-0.40	0.01	1.10	2.00	3.50	5.12	-2.00	3.00	2.00	1.12	-0.10	0.44	-1.00
5	-0.27	-0.44	-1.44	-2.10	-3.11	-2.89	-2.46	-3.02	-2.19	-0.88	-0.02	-0.36	-1.61
6		-0.22									0.10	-0.26	-1.18
7	-0.12	-0.02						1	1		0.17	-0.19	-0.65
8	-0.13	0.13	-0.20	-0.10	<b>-0.</b> 34	-0.31	-0.29	-0.20	-0.01	-0.12	0.19	-0.14	-0.13
9	-0.14	0.24	0.14	0.54	0.69	0.61	0.49	0.66	0.53	0.11	0.10	-0.12	0.33
10	-0.14	0.32	0.14	0.96	1.47	1.30	1.07	1.24	0.87	0.33		-0.12	0.66
11	0.02	0.37	0.59	1.20	2.00	1.77	1.45	1.58	1.05	0.50		-0.02	0.89
Midn	0.12	0.38	0.75	1.35	2.33	2.11	1.73	1.81	1.20	0.63	0.16	0.07	1.05
		0.10		0.7				00					
6. 6	0.11	0.18	0.26			-0.14		0.10	0.28	0.18	0.17	0.04	0.10
7. 7	0.20	0.27	0.38			-0.10		0.23	0.45	0.28	0.20	0.07	0.18
8. 8 9. 9	0.23	0.29	0.40 0.31	0.29 0.26	0.04	-0.04	0.03	0.29 $0.28$	0.50 $0.42$	$0.30 \\ 0.24$	0.18 0.11	0.09	0.22
10.10	0.12	0.12	0.13	0.15	0.16	0.11	0.04	0.19	0.42	0.12	0.01	0.05	0.13
20,10		3712		5.13	0.10		2.03	3.10	0.22	0.12	0.01	0.00	0.12
7. 2. 9	1	-0.05		-0.15						-0.11		-0.08	1 (
6. 2. 8		-0.08						-0.25			-0.02		4
6. 2.10	-0.13		0.02	0.17	0.25	0.22	0.21	0.23			-0.03		1
6. 2. 6	-0.15	-0.20	-0.46	-0.69	-1.05	-0.97	-0.79	-0.94	-0.70	-0.33	-0.05	-0.12	-0.54
7. 2	-0.09	-0.20	-0.27	-0.49	-0.82	-0.75	-0.58	-0.66	-0.53	-0.22	-0.13	-0.06	-0.40
8. 2		-0.25										-0.07	
8. 1		-0.23											
7. 1	1	-0.18		1									
0.10.00	0.7	0.20	0.05	0.07	1.00	1.70		1.00	0.00		0 -		
9.12.3.9	1	-0.28						-1.20			-0.16		
7. 2.2(9)	-0.11	0.02	-0.06	0.03	-0.07	-0.07	-0.05	0.00	0.00	-0.06	0.03	-0.09	-0.04
Dail. ext.	-0.05	-0.19	-0.17	-0.17	-0.16	-0.11	-0.06	-0.19	-0.28	-0.19	-0.16	-0.07	-0.15
	1												

### LXX.

## Russia. — Helsingfors. Lat. 60° 10' N. Long. 24° 57' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of Re	eaumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
							1						
Morn. 1	0.47	0.85	1		1	3.37	3.16	2.58		1.06	0.64	0.34	1.67
2	0.79	1.25	1.86	3.18	2.82	3.78	3.48	2.96	2.09	1.45	0.99	0.68	2.11
3	0.99	1.55	2.28	2.79		3.74	3.45	3.11	2.48	1.70	1.22	0.91	2.26
4	1.13	1.71	2.52	2.77	2.62	3.22	3.02	2.92	2.61	1.74	1.26	0.97	2.21
5	1.06	1.66	2.49	2.41	2.06	2.32	2.25	2.39	2.40	1.51	1.09	0.84	1.87
6	0.86	1.43	2.16	1.76	1.30	1.24	1.23	1.59	1.84	1.10	0.76	0.59	1.32
7	0.58	1.07	1.57	0.92	0.49	0.20	0.17	0.64	1.06	0.59	0.38	0.31	0.67
8	0.28	0.60	0.79	0.05	-0.26	-0.65	-0.78	-0.28	0.21	0.08	0.02	0.07	0.01
9	0.01	0.10	-0.05	-0.74	-0.87	-1 26	-1.51	-1.07	-0.58	-0.38	-0.27	-0.10	-0.56
10			ł		-1.34						ł		1
11					-1.70			1	l .	1		ł	)
Noon	ł I		1		-1.98				ì			-0.43	
1	1			1	-2.19				1	ſ			
2				1 -	-2.32			t ·					
3	11		1		-2.31								
4	-0.73	-1.20	-2.01	-2.10	-2.11	-2.42	-2.27	-2.26	-1.92	-1.05	-0.68	-0.49	-1.60
5	-0.52	-0.87	-1.56	-1.73	-1.77	-2.13	-1.85	-1.80	-1.48	-0.74	-0.48	-0.33	-1.27
6	-0.32	-0.57	-1.07	-1.25	-1.30	-1.71	-1.30	-1.24	-0.95	-0.44	-0.28	-0.18	-0.88
7	-0.19	-0.38	-0.60	-0.72	-0.78	-1.20	-0.68	-0.62	-0.42	-0.22	-0.16	-0.11	-0.51
8	-0.15	-0.25	-0.20	-0.21	-0.24	-0.61	-0.04	-0.03	-0.00	-0.10	-0.12	-0.12	-0.17
9	0.10	0.70	0.70	0.00	0.00	0.00	0.03	0.50	0.01	0.00	0.10	0.00	0.10
1	-0.16		0.10	0.26		0.07	0.61	0.52		-0.03			0.12
10	-0.16		0.36	0.69	0.82	0.87	1.27	1.03	0.54		-0.10		0.42
Midn 11	-0.06	0.12	0.63 0.96	1.13	1.40	1.75	1.95	1.54	0.79	0.29		-0.19	0.78
Midn	0.16	0.44	0.90	1.60	1.97	2.63	2.61	2.08	1.14	0.63	0.28	0.02	1.21
6. 6	0.27	0.43	0.55		-0.00				0.45			0.21	0.22
7. 7	0.20	0.35	0.49		-0.15				0.32	0.19		0.10	0.08
8.8	0.07	0.18			-0.25					-0.01			-0.08
9. 9	-0.08				-0.29			-0.28		-0.21			-0.22
10.10	-0.21	-0.25	-0.26	-0.33	-0.26	-0.39	-0.38	-0.33	-0.35	-0.35	-0.29	-0.24	-0.30
7. 2. 9	-0.17	-0.24	-0.26	-0.40	-0.51	-0.75	-0.63	-0.50	-0.31	-0.29	-0.21	-0.17	-0.37
6. 2. 8		-0.14			-0.42								
6. 2.10	-0.07	-0.08	0.02		-0.07					-0.08		1	
6. 2. 6	-0.13	-0.25	-0.45	-0.62	-0.77	-0.99	-0.91	-0.77	-0.47	-0.26	-0.13	-0.07	-0.49
7. 2	-0.17	_0.9**	-0.44	_0 =0	-0.00	_1.10	_1.95	-1.01	_0.69	_0.49	-0.95	_0.15	-0.62
8. 2	1	-0.27			-0.92								
8. 1		-0.47			-1.29 -1.23								
7. 1		-0.47			-0.85								
												ļ	
9.12.3.9		-0.71			-1.22								
7. 2.2(9)	-0.17	-0.22	-0.17	-0.23	-0.31	-0.54	-0.32	-0.25	-0.16	-0.23	-0.19	-0.18	-0.25
Dail.ext.	0.11	0.06	0.04	0.41	0.29	0.62	0.41	0.23	0.16	0.16	0.19	0.18	0.19

#### LXXI.

Norway. — Christiania. Lat. 59° 55' N. Long. 10° 43' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.16	0.89	1.07	1.56	2.55	2.58	2.21	2.04	1.64	0.74	0.52	0.22	1.35
2	0.21	0.94	1.30	1.88	2.85	3.15	2.53	2.23	1.88	0.82	0.50	0.21	1.54
3	0.27	1.17	1.51	2.03	3.23	3.28	2.64	2.41	2.03	0.94	0.49	0.28	1.69
4	0.32	1.49	1.67	2.12	3.21	3.05	2.62	2.60	2.07	1.06	0.55	0.30	1.84
5	0.38	1.60	1.82	2.23	2.55	2.39	2.09	2.44	2.14	1.16	0.51	0.00	1.00
6	0.47	1.54	1.69	1.81	1.63	1	1.37	1.98	2.14	1.16			1.63 1.31
7	0.51	1.67	1.71	1.28	0.71	0.43	0.58	1.00	1.50	1.13			0.93
8	0.54	1.42	1.29	0.56	0.07			0.10	0.62	0.75	0.38	1	0.44
											0.00	0110	0.11
9 *	0.48	1.11		-0.06					0.01	0.15	0.17	0.16	-0.03
10	0.24		1	-0.67		i .				1	-0.23		-0.59
11	-0.17			-1.38	)								
Noon	-0.67	-1.32	-1.48	-1.80	-2.17	-2.29	-2.02	-2.11	-2.02	-1.30	-1.06	-0.40	-1.55
1	-0.87	-1.90	-1 71	_2 22	-2.16	-2 50	-2.21	_9 35	-2 (1	-1 50	_1.15	_0 19	_1 89
2		-2.22											
3		-2.29				3			l .			1	1
4		-2.00		1							1		1
-	0.02	2.00	1.00	2.11	2100	2.20	2.00	2.02	2.00	1100	0.55	0.12	1.00
5	-0.35	-1.42	-1.58	-1.80	-2.20	-2.14	-1.87	-1.97	-1.80	-0.90	-0.23	-0.06	-1.36
6	-0.12	-1.10	-1.10	-1.27	<b>-1.</b> 82	-1.70	-1.48	-1.48	-1.21	-0.52	-0.02	-0.03	-0.99
7	-0.01	-0.60	-0.65	-0.70	-1.35	-0.98	-0.89	-0.78	-0.57	-0.24	0.11	-0.10	-0.58
8	0.12	-0.32	-0.20	-0.14	-0.44	<b>-0.</b> 31	<b>-0.</b> 30	-0.10	0.02	0.18	0.23	-0.13	-0.12
9	0.16	0.09	0.09	0.36	0.24	0.44	0.45	0.55	0.36	0.36	0.07	-0.05	0.28
10	0.10	0.09	0.36	0.70	0.24	1.20	1.06	1.08		0.58	1	-0.03	0.28
11	0.31	0.52	0.53	0.99	1.46	1.76	1.63	1.41	0.81 $1.06$	0.55	0.43		0.03
Midn	0.33	0.86	0.77	1.20	1.90	2.31	2.00	1.75	1.38	0.95	0.48		1.17
Tradit.	0.00	0.00	0,,,	1.20	*****	2.01		1	1100	0.00	0.40	0.00	1.1.
6. 6	0.18	0.22	0.30			<b>-0.20</b>		0.25	0.45	0.32	0.29	0.04	0.16
7. 7	0.25	0.54	0.53			-0.28		0.11	0.47	0.45	0.29	0.05	0.18
8. 8	0.33	0.55	0.55			-0.32		0.00	0.32	0.47	0.31	0.01	0.16
9. 9	0.32	0.60	0.23			-0.21		-0.02	0.19	0.26	0.22	0.06	0.12
10.10	0.26	0.31	0.01	0.05	-0.13	-0.18	-0.10	-0.08	0.02	0.05	0.05	0.04	0.02
7. 2. 9	-0.12	-0.15	-0.05	-0.23	-0.50	-0.51	-0.39	-0.32	-0.23	-0.06	-0.14	-0.07	-0.23
6. 2. 8	1	-0.33		-0.22						1	-0.11		-0.23
6. 2.10	-0.10		0.03		0.03	0.04		0.19	0.12		-0.07		0.02
6. 2. 6		-0.59		-0.59							-0.19		-0.49
7. 2	1	-0.28											
8. 2		-0.40											
8. 1		-0.24											
7. 1	-0.18	-0.12	-0.02	-0.47	-0.88	-1.04	-0.82	-0.08	-0.46	-0.23	-0.35	-0.12	-0.50
9.12.3.9	-0.56	-0.60	-0.80	-0.94	-1.25	-1.29	-1.14	-1.16	-1.04	-0.59	-0.38	-0.13	-0.82
7. 2.2(9)		-0.09										-0.07	
` '													
Dail.ext.	-0.25	-0.31	-0.17	-0.05	0.35	0.39	0.22	0.05	-0.20	-0.26	-0.28	-0.06	-0.05

#### LXXII.

NORWAY. - DRONTHEIM. Lat. 63° 26' N. Long. 10° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Rea	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
M 1	0.29	0.41	0.77	1.94	2.63	2.64	2.53	2.51	1.37	0.89	0.27	0.33	1.38
Morn. 1	0.25	0.50	0.95	2.09	2.97	2.76	$\frac{2.55}{2.75}$	2.68	1.48	0.91	0.31	0.31	1.50
3	0.22	0.64	1.11	2.19	3.13	2.82	2.77	2.91	1.59	0.97	0.23	0.42	1.58
4	0.20	0.71	1.27	2.32	3.03	2.82	2.65	2.77	1.55	1.07	0.28	0.34	1.58
5	0.13	0.75	1.37	2.05	2.76	2.52	2.35	2.58	1.59	0.86		0.42	1.47
6 7	0.11	0.82	1.42	1.67	$\frac{2.30}{1.68}$	1.96 1.39	1.86	2.13 1.58	1.49 1.07	0.71	0.14	0.43	1.25
8	0.04	0.33	1.35 1.17	1.36 0.94	0.83	0.61	1.17 0.40	1.02	0.57		-0.02	0.36	$0.92 \\ 0.52$
	0.00	0.20	1.11	0.54	0.00	0.01	0.40	1.02	0.51	0.00	0.02	0.50	0.02
9	0.00	-0.08	0.41	-0.02	-0.28	-0.03	-0.14	0.22	-0.07	-0.29	-0.14	0.19	-0.02
10	-0.09	-0.48					-1.30		-0.89	-0.59	-0.16	0.02	-0.65
11		-0.78					-1.95				-0.33		1
Noon	-0.59	-1.08	-1.35	-2.57	<b>-2.</b> S1	-2.43	-2.77	-3.21	-2.05	-1.20	-0.38	-0.42	-1.75
1	-0.80	-1.22	-1.70	-2.66	-3.28	-3.25	-3.20	-3.39	-2.12	-1.14	-0.44	-0.42	-1.97
2	i	į.	-1.70										1 1
3		(	-1.54										1 1
4	-0.36	-0.56	-1.37	-1.83	-2.90	-2.78	-2.41	-2.81	-1.43	-0.86	-0.16	-0.29	-1.48
A. C. C. C. C. C. C. C. C. C. C. C. C. C.										0 70			
5	-0.29	1	-1.07					ì				-0.22	l i
6 7	0.09		-0.75 $-0.54$				-0.61			-0.51 -0.28	1	-0.23 $-0.30$	i 1
8	0.03	0.17		-0.37 -0.20		0.04	0.01	0.11		-0.23 -0.02		-0.19	
	0.21	0.11	0.21	0.20	0.01	0.01	0.01	0.11	0.00	0.02	0.11	0.15	0.02
9	0.45	0.37	0.00	0.16	0.50	0.41	0.66	0.51	0.43	0.22	0.05	-0.11	0.30
10	0.52	0.53	0.23	0.61	1.10	1.08	1.17	1.18	0.75	0.55	0.13	-0.06	0.65
11	0.47	0.50	0.43	0.90	1.61	1.63	1.48	1.67	1.02	0.74	0.11	0.02	0.88
Midn	0.45	0.49	0.63	1.27	1.92	2.07	1.88	2.13	1.28	1.14	0.19	0.02	1.12
									}				
6. 6	-0.03	0.36	0.34	0.39	0.30	0.06	0.36	0.43	0.35	0.10	0.11	0.10	0.24
7. 7	0.07	0.27	0.41	0.40	0.33	0.20	0.28	0.45	0.38	0.07	0.05	0.03	0.24
8.8	0.18	0.20	0.45	0.37	0.23	0.33	0.21	0.57	0.30	0.02	0.08	0.09	0.25
9. 9	0.23	0.15	0.21	0.07	0.11	0.19	0.26	0.37		-0.04	-0.05	0.04	0.14
10.10	0.22	0.03	0.05	-0.12	-0.10	0.08	-0.07	-0.02	-0.07	-0.02	-0.02	-0.02	0.00
7. 2. 9	-0.06	-0.07	-0.12	-0.31	-0.36	-0.51	-0.41	-0.42	-0.26	-0.15	-0.12	-0.07	-0.24
6. 2. 8			-0.12										
6. 2.10	-0.02	1	-0.02	ł			-0.01		1		-0.05	1	1
6. 2. 6	-0.25	1	-0.39	1			1			1	5		1
	0.00							}	1	1	1		
7. 2	-0.32	1	-0.18			1			}		1	1	
8. 2	$\begin{bmatrix} -0.30 \\ -0.36 \end{bmatrix}$		$\begin{bmatrix} -0.27 \\ -0.27 \end{bmatrix}$										
7. 1	1.6		-0.27 -0.18										
	1	0.02	0.10	0.03	1	0.33	1.02		0.55			0.50	
9.12.3.9	-0.16		-0.62										
7. 2.2(9)	0.07	0.04	-0.09	-0.19	-0.15	-0.28	-0.15	-0.19	-0.09	-0.16	-0.02	-0.12	-0.11
Dail.ext.	-0.11	_0.20	_0.14	-0.17	_0 00	_0.25	_0.22	-0.24	_0.25	-0.07	-0.07	-0.02	-0.16
Dan. ext.	0.14	-0.20	-0.14	-0.17	1-0.08	-0.25	-0.22	-0.24	-0.50	-0.07	-0.07	-0.02	-0.10

#### LXXIII.

# Strait of Kara. Lat. 70° 37' N. Long. 57° 47' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

-						Degree	es of Re	aumur.						
Hours.		Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn.	1	0.27	0.38	1.66	2.53	2.26	1.86	1.37	0.62	0.33	0.00	0.08	0.55	0.99
	2	0.24	0.38	1.78	2.67	2.22	1.68	1.24	0.58	0.40	0.02	0.14	0.42	0.98
	3	0.22	0.40	1.86	2.66	2.06	1.41	1.03	0.53	0.49	0.02	0.14	0.26	0.92
	4	0.23	0.42	1.88	2.44	1.82	1.12	0.79	0.47	0.58	0.06	0.15	0.11	0.84
	5	0.25	0.42	1.80	1.98	1.48	0.82	0.54	0.38	0.61	0.17	0.22	-0.00	0.72
	6	0.27	0.33	1.55	1.30	1.01	0.49	0.25	0.26	0.58	0.29		-0.15	0.55
	7	0.29	0.16	1.10	0.52	0.40	0.10	-0.05	0.10	0.42	0.35		-0.29	0.30
	8	0.30	0.08	0.42	-0.27	-0.30	-0.33	-0.35	-0.07	0.27	0.32		-0.42	0.01
	9	0.26	0.30	-0.43	-0.98	-1.01	-0.78	-0.66	-0.23	0.01	0.18	0.66	-0.54	-0.32
1	0	0.18	-0.50	-1.32	-1.58	-1.63	-1.19	-0.85	-0.36	-0.28	0.02	0.55	-0.61	-0.63
1	1	0.04	-0.64	-2.07	-2.13	-2.06	-1.48	-0.98	-0.46	-0.54	-0.25	0.33	-0.62	-0.91
Noon.		-0.12	-0.70	-2.56	-2.41	-2.27	-1.62	-1.04	-0.55	-0.72	-0.37	0.18	-0.54	-1.07
	1	-0.31	-0.70	-2.70	-2.67	-2.26	-1.62	-1.03	-0.63	-0.81	-0.43	-0.13	-0.44	-1.14
	2		1		-2.81						ļ	1	1	
	3				-2.75		l .		ł .		1		1	i I
	4				-2.46					1	i			(
	5	-0.58	-0.21	-0.98	-1.91	-1.30	-1.05	-0.78	-0.59	-0.30	0.02	-0.35	-0.04	-0.67
	6	-0.46	-0.02	-0.47	-1.18	-0.90	-0.76	-0.59	-0.38	-0.13	0.07	-0.41	0.06	-0.43
	7	-0.26	0.14	-0.04	-0.37	-0.40	-0.35	-0.29	-0.09	0.06	0.08	-0.48	0.18	-0.15
	8	-0.06	0.32	0.34	0.42	0.20	0.18	0.11	0.22	0.11	0.07	-0.52	0.33	0.14
	9	0.11	0.42	0.67	1.08	0.83	0.78	0.54	0.46	0.17	0.06	-0.49	0.48	0.43
1	0	0.22	0.46	0.98	1.59	1.42	1.31	0.94	0.62	0.20	0.06	-0.38	0.61	0.67
1	1	0.28	0.44	1.25	1.98	1.88	1.71	1.23	0.68	0.23	0.06	-0.20	0.66	0.85
Midn.		0.29	0.40	1.48	2.29	2.16	1.90	1.38	0.66	0.27	0.01	-0.03	0.64	0.95
6. 6	3	0.10	0.16	0.54	0.06		-0.14		-0.06	0.23	ſ	-0.03		0.06
7. 7	- 1	0.02	0.15	0.53			-0.13		0.01	0.24	0.22		-0.06	0.08
8. 8	- 1	0.12	0.12	0.38			-0.08		0.08	0.19	0.20		-0.05	0.08
9. 9		0.19	0.06	0.12			-0.00		0.12	0.09	0.12		-0.03	0.05
10.10	)	0.20	-0.02	-0.17	0.01	-0.11	0.06	0.05	0.13	-0.04	0.04	0.09	-0.00	0.02
7. 2.	9	-0.03	-0.02	-0.25	-0.40	-0.29	-0.22	-0.17	-0.05	-0.06	0.02	-0.07	-0.04	-0.13
6. 2.	8	-0.09	-0.00	-0.21	-0.36	-0.30	-0.29	-0.21	-0.08	-0.03	-0.00	-0.14	-0.04	-0.15
6. 2.1	0	-0.00	0.05	-0.00	0.03	0.11		0.06			-0.00			0.03
6. 2.	6	-0.23	-0.11	-0.48	-0.90	-0.67	-0.60	-0.45	-0.28	-0.11	-0.00	-0.10	-0.13	0.34
7. 2					-1.15							0.14	-0.30	-0.41
8. 2					-1.54								-0.37	l ì
8. 1					-1.47								-0.43	1
7. 1		-0.01	-0.27	-0.80	-1.08	-0.93	-0.76	-0.54	-0.27	-0.20	-0.04	0.20	-0.37	-0.42
9.12.3.	9	-0.09	-0.28	-1.11	-1.27	-1.08	-0.76	-0.53	-0.27	-0.30	-0.09	-0.01	-0.20	0.50
7. 2.20		0.01	1		-0.03		0.03	0.01		-0.01		-0.18	0.09	
Dail. e	xt.	-0.17	-0.12	-0.41	-0.07	-0.01	0.14	0.17	-0.04	-0.10	-0.04	0.07	0.02	<b>-0.0</b> 9
					1									

#### LXXIV.

NOVAIA ZEMLIA. - MATOSCHKIN SCHAR. Lat. 73° - N. Long. 57° 20' E. Gr. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

-					2 08 0	es or Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	-0.22	0.16	0.46	1.63		1	1.18	0.73			-0.14		0.70
2	-0.30	0.09	0.70	1.34	2.28	1.54	1.20	0.79	0.88	-0.47	-0.14	0.05	0.66
3	-0.31	0.01	0.91	1.15	1.89	1.26	1.11	0.80	0.62	-0.22	-0.10	0.17	0.61
4	-0.26	-0.06	1.02	1.09	1.41	0.93	0.94	0.72	0.46	0.02	-0.00	0.26	0.54
				-									
5	-0.14	-0.09	0.99	0.81	0.85	0.61	0.73	0.55	0.46	0.20	0.10	0.34	0.45
6	1	-0.09	0.86	0.63		1	0.47	0.30	0.56	0.26	0.20		0.34
11				j		ì	0.18	0.01	0.58	0.18	0.26	0.45	1
7		-0.07	0.62		-0.38								1
8	0.10	-0.05	0.34	-0.50	-1.03	-0.38	-0.13	-0.30	0.38	0.06	0.26	0.46	-0.07
	0.10	0.05	0.00	, , ,	1.05	0.00	0.10	0.50	0.00	0.00	0.04	0 10	0.00
9		-0.05						-0.58			0.24		-0.33
10		-0.06									0.18		-0.61
11	0.05	-0.10	-0.58	-2.02	-2.53	-1.45	-0.97	-0.91	-1.24	-0.14	0.15	0.28	-0.79
Noon	0.05	-0.13	-0.78	-2.09	-2.67	-1.58	-1.08	-0.93	-1.46	-0.12	0.11	0.18	-0.88
1		-0.14	1					1					-0.85
2	0.09	-0.14	-0.96	-1.62	-2.28	-1.32	-0.96	-0.70	-0.89	-0.09	0.02	-0.02	-0.74
3		-0.11										-0.11	-0.58
4		-0.07											
			0111	0.00									0.11
5	0.10	-0.03	-0.50	-0.54	-0.72	-0.57	-0.54	-0.14	-0.02	0.10	-0.18	-0.26	-0.28
6	0.10		-0.30					-0.00			-0.20		
7	0.10		-0.16	0.30		-0.16			-0.35		-0.18		
	1							1					
8	0.12	0.10	-0.09	0.70	1.04	0.19	-0.11	0.21	-0.36	0.46	-0.14	-0.48	0.13
9	0.12	0.15	-0.06	1.24	1.59	0.56	0.14	0.30	-0.12	0.26	-0.10	_0 10	0.31
10	0.08		-0.02	1.50	2.06		0.46	0.39	0.33		-0.08		0.47
11	-0.00	0.21	0.09	1.75	2.40	1.42	0.78	0.50			-0.08		0.61
Midn	-0.11	0.20	0.23	1.72	2.55	1.66	1.03	0.62	1.06	-0.39	-0.11	-0.22	0.69
6.6	0.04	0.04	0.28	0.19	0.06	-0.04	0.02	0.15	0.20	0.26	0.00	0.03	0.10
7. 7	0.08	0.01	0.23	0.20	0.04	-0.09	-0.06	0.07	0.12	0.29	0.04	0.01	0.08
8.8	0.11	0.03	0.13	0.10	0.01	-0.12	-0.12	-0.05	0.01	0.26	0.06	-0.01	0.03
9. 9	0.11		-0.02	0.05				-0.14	1	0.15		-0.03	
10.10	0.08		-0.15	-0.14				-0.20		-0.01		-0.04	
10,10	0.00	0.01	0.10	0.14	0.00	0.01		0.20		0.01	0.00	0.01	0.01
7. 2. 9	0.09	-0.02	-0.13	-0.10	-0.36	-0.26	-0.21	-0.13	-0.14	0.15	0.06	-0.02	-0.09
6. 2. 8		-0.04								0.21		-0.03	
6. 2.10		-0.04		0.17				-0.00		0.12		-0.03	0.03
11	1												
6. 2. 6	0.05	-0.07	-0.13	-0.42	-0.72	-0.47	-0.31	-0.13	-0.17	0.14	0.01	0.01	-0.18
7. 2	0.00	-0.11	_0.1**	_0 ==	_1 99	_0.6**	_0.20	_0.25	-0.16	0.05	0.14	0.99	-0.29
11										0.05	0.14		
8. 2	1 1	-0.10								-0.02	0.14		-0.40
8. 1	)	-0.10							1	-0.02	0.17		-0.46
7. 1	0.06	-0.11	-0.16	-0.92	-1.48	-0.77	-0.44	-0.42	-0.37	0.04	0.17	0.28	-0.34
0.10.00	0.0-	0.0	0.15			0 ===	0	0.1-	0 40	0.0-	0.0-	0.00	0.05
9.12.3.9		-0.04								0.03		-0.00	
7. 2.2(9)	0.10	0.02	-0.12	0.24	0.13	-0.06	-0.13	-0.02	-0.14	0.20	0.02	-0.14	0.01
~	0.50											0.00	0.00
Dail.ext.	-0.10	0.04	0.03	-0.17	-0.06	0.06	0.06	-0.07	-0.19	-0.02	0.03	-0.02	-0.09

#### LXXV.

Norway. — Bossekop. Lat. 69° 58' N. Long. 22° E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

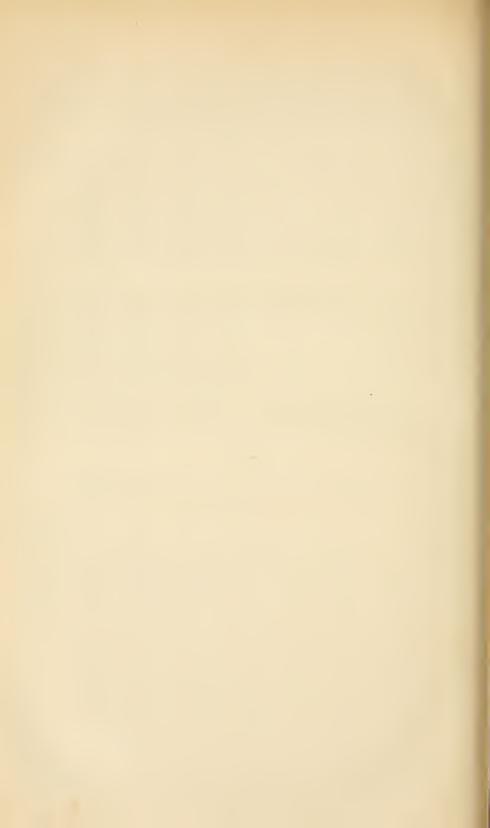
Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.26	0.36	1.37		1.20	0.66	0.04	0.35	0.04
4	-0.11	0.30	1.78		1.01	0.53	-0.03	0.42	0.10
6	0.00	0.50	1.90		1.22	0.73	0.04	0.28	0.08
8	0.09	0.26	1.18	0.36	0.62	0.41	0.07	0.10	0.02
10	-0.13	-0.19	-1.09	-0.85	-1.01	-0.29	-0.15	-0.14	-0.19
Noon.	0.18	-0.79	-2.39	-1.29	-1.66	-1.05	-0.13	-0.09	-0.03
2	0.20	-1.02	-2.85	-1.22	-1.69	-1.02	-0.09	-0.34	-0.10
4	0.30	-0.11	-2.38	-0.82	-1.54	-0.50	0.09	-0.38	0.06
6	0.18	0.06	-0.57	-0.10	-0.27	-0.17	0.18	-0.23	0.09
8	0.12	0.16	0.46	0.70	0.39	0.09	0.14	-0.26	0.02
10	-0.34	0.21	1.19	1.44	0.79	0.13	-0.03	0.14	-0.10
12	-0.27	0.22	1.39	1.83	0.89	0.49	-0.13	0.17	-0.10
Mean.	-7.67	-6.39	-7.55	-0.77	5.91	-1.62	-6.55	-5.66	-7.66

LXXV'.

NORWAY. — BOSSEKOP. Lat. 69° 58′ N. Long. 22° E. Greenw. Centigrade Degrees.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.32	0.45	1.71	• • •	1.50	0.82	0.05	0.44	0.05
4	-0.14	0.37	2.22		1.26	0.66	-0.04	0.52	0.12
6	0.00	0.62	2.37		1.52	0.91	0.05	0.35	0.10
8	0.11	0.32	1.47	0.45	0.77	0.51	0.09	0.12	0.02
10	-0.16	-0.24	-1.36	-1.06	-1.26	-0.36	-0.19	-0.17	-0.24
Noon.	0.22	-0.99	-2.98	-1.62	-2.07	-1.31	-0.16	-0.11	-0.04
2	0.25	-1.27	-3.56	-1.52	-2.11	-1.27	-0.11	-0.42	-0.12
4	0.37	-0.14	-2.97	-1.02	-1.92	-0.62	0.11	-0.47	0.07
6	0.22	0.07	-0.71	-0.12	-0.34	-0.21	0.22	-0.29	0.11
8	0.15	0.20	0.57	0.87	0.49	0.11	0.17	-0.32	0.02
10	-0.42	0.26	1.48	1.80	0.99	0.16	-0.04	0.17	-0.12
12	-0.34	0.27	1.73	2.29	1.11	0.61	-0.16	0.21	-0.12
Mean.	-9.59	-7.99	-9.44	-0.96	7.39	-2.02	-8.19	-7.07	-9.57



# HOURLY CORRECTIONS

FOR

# PERIODIC VARIATIONS.

AFRICA. — AUSTRALIA.



#### LXXVI.

Africa. - St. Helena. Lat. 15° 55' S. Long. 5° 43' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.76	0.70	0.63	0.58	0.52	0.43	0.48	0.43	0.52	0.62	0.71	0.73	0.59
1	0.85	0.76	0.71	0.66	0.61	0.48	0.53	0.48	0.56	0.71	0.78	0.81	0.66
2	0.93	0.84	0.77	0.70	0.66	0.54	0.56	0.53	0.62	0.78	0.86	0.90	0.72
3	1.03	0.92	0.86	0.76	0.73	0.59	0.62	0.63	0.69	0.86	0.95	0.98	0.80
4	1.06	1.00	0.92	0.81	0.80	0.65	0.66	0.66	0.76	0.91	0.99	1.02	0.85
5	1.11	1.04	0.93	0.86	0.83	0.67	0.69	0.73	0.79	0.94	1.02	1.08	0.89
6	1.15	1.07	0.98	0.93	0.83	0.68	0.72	0.74	0.83	0.99	1.07	1.09	0.92
7	1.16	1.08	0.97	0.94	0.89	0.71	0.75	0.79	0.81	0.96	1.03	1.06	0.93
8	0.95	0.99	0.78	0.85	0.88	0.69	0.72	0.72	0.72	0.77	0.80	0.98	0.82
9	0.53	0.63	0.52	0.49	0.46	0.42	0.41	0.43	0.42	0.38	0.40	0.48	0.46
10	-0.05	0.06	-0.07	-0.04	-0.08	-0.04	-0.04	-0.02	-0.05	-0.17	-0.16	-0.09	-0.06
11	-0.62	-0.55	-0.49	-0.51	-0.47	-0.40	-0.40	-0.40	-0.55	-0.66	-0.67	-0.56	-0.52
Noon.	-1.14	-1.06	-0.95	-1.00	-0.96	-0.73	-0.76	-0.80	-0.92	-1.11	-1.12	-1.08	-0.97
1	-1.64		-1.28			-1.04		-1.12	-1.25	-1.45	-1.60	-1.52	-1.33
2	-1.81	-1.67	-1.48	-1.46	-1.32	-1.20	-1.26	-1.25	-1.42	-1.67	-1.80	-1.80	-1.51
3	-1.76	-1.78	-1.62	-1.50	-1.35	-1.18	-1.24	-1.31	-1.38	-1.64	-1.84	-1.82	-1.54
4	-1.69	-1.66	-1.54	-1.35	-1.24	-1.03	-1.12	-1.13	-1.20	-1.37	-1.64	-1.76	-1.39
5	-1.48	-1.38	-1.27	-1.06	-0.94	-0.78	-0.84	-0.86	-0.91	-0.99	-1.24	-1.38	-1.09
6	-0.92	-0.91	-0.83	-0.61	-0.47	-0.40	-0.44	-0.42	-0.43	-0.48	-0.66	-0.82	-0.62
7	-0.27	-0.33	-0.28	-0.11	-0.23	-0.03	-0.07	-0.03	0.01	0.02	-0.04	-0.18	-0.13
8	0.26	0.21	0.18	0.20	-0.12	0.17	0.13	0.15	0.23	0.29	0.32	0.30	0.19
9	0.47	0.44	0.34	0.34	0.14	0.26	0.23	0.25	0.32	0.26	0.48	0.48	0.33
10	0.60	0.55	0.48	0.44	0.41	0.32	0.33	0.32	0.38	0.49	0.56	0.58	0.46
11	0.69	0.64	0.55	0.51	0.45	0.39	0.38	0.38	0.46	0.55	0.64	0.67	0.53
Mean.	14.21	15.04	15.22	14.93	13.80	12.48	11.55	11.19	11.14	11.66	12.37	13.23	

#### LXXVII.

Africa.—Cape of Good Hope. Lat. 33° 56′ S. Long. 19° 39′ E. Gr.—Dove.

Degrees of Reaumur.

Hour	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.69	1.50	1.51	1.37	1.00	0.88	1.04	0.85	1.07	1.45	1.62	1.85	1.32
1	2.80	1.64	1.64	1.49	1.07	1.01	1.20	1.03	1.25	1.62	1.79	2.01	1.55
2	1.89	1.74	1.81	1.61	1.14	1.09	1.33	1.14	1.39	1.72	1.98	2.16	1.58
3	2.01	1.92	1.92	1.70	1.24	1.16	1.43	1.23	1.54	1.82	2.12	2.30	1.70
4	2.10	2.00	2.05	1.88	1.34	1.30	1.53	1.37	1.63	1.92	2.21	2.42	1.81
5	1.96	2.13	2.13	1.93	1.46	1.42	1.59	1.53	1.59	1.93	1.92	2.01	1.80
6	1.06	1.53	1.97	1.98	1.59	1.48	1.73	1.55	1.62	1.26	0.85	0.86	1.46
7	0.15	0.70	1.21	1.39	1.41	1.47	1.57	1.22	0.81	0.39	-0.02	-0.20	0.84
8	-0.53	-0.01	0.16	0.36	0.53	0.86	0.77	0.64	-0.06	-0.46	-0.67	-0.81	0.06
9	-1.10	-0.80	-0.76	-0.68	-0.39	-0.12	-0.24	-0.42	-0.82	-1.24	-1.25	-1.36	-0.77
10	-1.72	-1.65	-1.66	-1.48	-1.10	-0.90	-1.09	-1.08	-1.41	-1.82	-1.80	-1.90	-1.47
11	-2.23	-2.31	-2.37	-2.10	-1.64	-1.46	-1.72	-1.63	-1.85	-2.25	-2.24	-2.25	-2.00

#### LXXVII.

### AFRICA. — CAPE OF GOOD HOPE, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-2.48	-2.72	-2.66	-2.56	-2.09	-1.92	-2.11	-1.88	-2.15	-2.45	-2.46	-2.52	-2.33
1	-2.54	-2.74	-2.95	-2.81	-2.20	-2.07	-2.33	-2.04	-2.23	-2.55	-2.48	-2.61	-2.46
2	-2.42	-2.54	-2.86	-2.79	-2.14	-2.06	-2.33	-1.97	-2.18	-2.44	-2.30	-2.44	-2.37
3	-2.16	-2.20	-2.51	-2.42	-1.84	-1.86	-2.13	-1.77	-1.82	-2.08	-2.01	-2.16	-2.08
4	-1.75	-1.70	-1.78	-1.75	-1.28	-1.28	-1.49	-1.32	-1.28	-1.52	-1.66	-1.90	-1.56
5	-1.21	-1.09	-1.03	-0.71	-0.61	-0.64	-0.76	-0.57	-0.56	-0.71	-1.05	-1.28	-0.85
6	-0.16	-0.13	-0.10	-0.03	-0.21	-0.29	-0.33	-0.17	0.00	0.20	-0.01	-0.15	-0.12
7	0.65						-0.03			0.57		)	1
8	0.95	0.79	0.61	0.48	0.36	0.19	0.26	0.32	0.51	0.86	0.92	0.96	0.60
9	1.14	1.00	0.92	0.73	0.54	0.40	0.48	0.46	0.69	1.09	1.10	1.20	0.81
10	1.30	1.14	1.14	1.00	0.78	0.61	0.69	0.65	0.97	1.26	1.31	1.46	1.03
11	1.55	1.32	1.29	1.22	0.95	0.81	0.91	0.76	1.02	1.44	1.48	1.67	1.20
Mean.	15.81	15.96	15.00	13.61	11.38	9.84	9.96	10.06	11.01	12.43	13.54	14.82	

#### LXXVIII.

Australia. — Hobarton. Lat. 42° 53′ S. Long. 147° 21′ E. Gr. — Dove.

					200	grees of	Reaum						
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	2.34	1.95	1.78	1.31	0.88	0.66	0.72	1.10	1.51	1.99	2.44	2.45	1.59
1	2.59	2.17	1.99	1.41	1.03	0.76	0.86	1.36	1.71	2.19	2.67	2.76	1.79
2	2.89	2.32	2.19	1.62	1.11	0.88	1.01	1.43	1.93	2.45	2.77	2.95	1.96
3	3.09	2.53	2.39	1.75	1.23	0.97	1.16	1.58	2.06	2.68	2.98	3.24	2.14
4	3.20	2.68	2.49	1.85	1.31	1.15	1.28	1.69	2.20	2.80	3.11	3.38	2.26
5	3.33	2.82	2.54	1.99	1.44	1.15	1.40	1.82	2.32	2.85	2.99	3.13	2.31
6	2.62	2.59	2.64	2.11	1.55	1.29	1.50	1.91	2.34	2.60	2.24	2.24	2.14
7	1.48	1.75	2.10	2.00	1.60	1.37	1.50	1.90	1.84	1.61	1.16	1.03	1.61
8	0.27	0.68	1.08	1.30	1.27	1.26	1.31	1.32	0.93	0.41	0.01	-0.24	0.80
9	-0.88	-0.56	-0.17	0.24	0.45	0.60	0.60	0.44	-0.21	-0.70	-1.13	-1.27	-0.22
10	-1.92	-1.61	-1.28	-0.85	-0.46	-0.18	-0.21	-0.52	-1.21	-1.68	-2.10	-2.16	-1.18
11	-2.75	-2.34	-2.24	-1.78	-1.29	-0.96	-1.01	-1.53	-2.09	-2.54	-2.89	-2.85	-2.02
Noon.	-3.51	-3.22	-3.03	-2.58	-2.00	-1.67	-1.67	-2.28	-2.70	-3.10	-3.43	-3.36	-2.71
1	-3.82	-3.52	-3.48	-2.95	-2.42	-2.08	-2.17	-2.73	-3.14	-3.48	-3.72	-3.67	-3.10
2	-3.91	-3.54	-3.63	-3.11	-2.53	-2.22	-2.38	-2.91	-3.25	-3.48	-3.67	-3.56	-3.18
3	-3.60	-3.36	-3.43	-2.87	-2.32	-2.02	-2.23	-2.71	-3.10	-3.32	-3.33	-3.45	-2.98
4		-2.94					-1.73	1	-2.53			-3.12	-2.51
5	-2.57	-2.22	-2.02	-1.35	-0.92	-0.73	-1.01	-1.37	-1.59	-2.02	-2.30	-2.56	-1.72
6	-1.38	-1.04	-0 84	-0.56	-0.36	-0.25	-0.48	-0.64	-0.65	-0.80	-1.01	-1.38	-1.78
7	-0.13	-0.20	-0.04	-0.05	0.01	0.00	0.12	-0.13	0.01	0.05	0.20	-0.09	-0.02
8	0.82	0.68	0.45	0.32	0.27	0.24	0.14	0.21	0.46	0.55	0.90	0.89	0.49
9	1.31	1.13	0.82	0.57	0.42	0.24	0.34	0.57	0.79	1.00	1.41	1.51	0.84
10	1.71	1.47	1.19	0.84	0.62	0.40	0.50	0.79	1.08	1.34	1.75	1.91	1.13
11	2.05	1.77	1.47	1.06	0.77	0.54	0.64	0.93	1.31	1.63	2.05	2.25	1.37
Mean.	13.38	13.96	11.96	9.41	7.69	5.93	5.21	6.24	7.97	9.39	11.38	12.95	

# CORRECTIONS FOR TEMPERATURE.

# MONTHLY AND YEARLY

# CORRECTIONS FOR NON-PERIODIC VARIATIONS,

OR

# TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS

TO THE MEANS DERIVED FROM A SERIES OF YEARS.



#### TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS TO THE MEANS DERIVED FROM A SERIES OF YEARS.

Observation shows that the monthly and annual mean temperature of a place somewhat varies from year to year. No law, however, has been as yet discovered as to the course of these oscillations. It follows that the means derived from observations carried on during a single year are but approximations to the true means. These last must be obtained from observations made for a series of years, during which these irregular variations become insensible by compensating each other; and it is obvious that their accuracy increases with the number of years which compose the series.

Professor Dove, having proved by his researches that these abnormal temperatures above and below the average of a whole month, or of a year, are apt to be felt simultaneously on extensive tracts of country, concluded that the means of a single year could be made available for obtaining the true means of the place, by being corrected for the non-periodic variations by means of normal stations in the same meteorological region, in which those elements had been more accurately determined by the observations of a long series of years. Comparing, namely, the means of a given year with the means derived from the whole series, we find a difference in + or -, which, applied, with reverse signs, to the means of the same year in the neighboring station to be corrected, will reduce, with a good degree of probability, the means of that particular year to the means which would have been obtained from a long series of years similar to that of the normal station.

The following tables, LXXIX. to XCVII., have been selected from those given by Dove in his five papers on the non-periodic variations of the atmospheric temperature, to be found in the *Memoirs of the Academy of Sciences of Berlin* for the years 1838, 1839, 1842, 1848, and 1853, to which we must refer for further details. They furnish normal stations for various latitudes; the columns contain the corrections for every month, viz. the differences, with *reverse* signs, between the monthly means in the year indicated in the first and last columns, and the means derived from the whole series, which are contained in the line at the bottom.

 $\mathbf{E}$ 

#### LXXIX.

### Region of the Monsoons. - Madras.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1796	0.00	0.24	0.00	0.36	° -0.10	° -1.48	° -1.16	° -1.15	-0.31	$\stackrel{\circ}{-0.28}$	0.47	-0.51	1796
1797			0.66	0.53	0.39	0.56	0.09	0.85	1	-0.33	0.16	1 1	1797
1798	-0.13	1.12	0.40	• •	0.55	0.39	0.53	-0.31	0.27	0.56		0.02	1798
1799	-0.13	-0.08	0.62	0.36	0.26	-0.06	-1.20		-0.36	0.38		0.25	1799
11 1	)	1	ł			1		1	1	0.33			
1800	0.40	0.41	0.57	1.20	-0.23	-0.50	-1.02	-0.40	-0.58	0.20	0.47	-0.60	1800
1801	0.44	0.01	1.77	• •	• •	-0.59	-0.67	0.63	}	-0.02	1		1801
1802	0.44	0.86	1.77	1.02	-0.36	0.65	0.58	-0.04	1.60	0.43	-0.02		1802
1803	0.22	0.24	0.80	0.53	-0.32	0.08	0.18	0.80	0.80	0.38	0.33	0.65	1803
1804	1.64	1.48	0.75	1.38	0.70	0.70	1.24	0.00	0.58	0.38	0.91	0.29	1804
1805	0.27	0.41	0.66	-0.36	0.61	0.52	-0.76	-0.22	-0.27	-0.33	0.69	0.65	1805
1806	0.00	-0.39	-0.09	0.09	-0.41	-1.61	0.00	-0.13	1.07	0.47	0.96	0.12	1806
1807	0.22	-1.54	-3.20	-5.47	-1.79	0.48	1.20	-0.17	-0.09	-0.64	-0.20	0.78	1807
1813	0.80	0.37	0.13	0.96	1.12	-0.32	0.44	-0.22			-0.38		1813
1814	-0.36	-0.39	-0.58	0.04	-2.99	1.10	1.38		1		-0.20	Į.	1814
1815	-0.98	0.32	-0.67	2.00	1.55	-1.39	-0.98	0.27	0.31	-0.73	1	-0.82	1815
1816	-1.09	-1.76	-1.56	-0.93	0.44	0.39	-0.44	-0.71	-0.67	-0.20	0.33	-0.51	1816
1817	-0.58			-0.62	0.12	-0.19	0.67	0.29		-0.55	1	1	1817
1818	0.22	0.32		-0.02	1.41	0.65	-1.33	ł	-0.18	-0.55			1818
1819		-1.28			0.48	0.88	0.44	1	-0.31	0.03	0.78		1819
1820	$\begin{bmatrix} -1.75 \\ -0.67 \end{bmatrix}$	-0.30	-0.85	0.58	-1.16	-0.32	0.18	0.23		0.47	0.69	0.10	1820
1821	1.02	0.64	1.06	-1.51	0.26	0.08	0.18	0.94		-0.02	0.03	0.20	1821
1021													1021
Means.	19.19	20.07	21.30	22.41	24.41	24.96	23.84	23.43	23.03	22.16	20.74	19.48	Means.
1822	-0.36	0.37	0.41	-0.28	0.07	-0.95	-0.76	0.72	-0.37	-0.70	-0.35	-0.19	1822
1823	0.31	0.37	-0.21	0.30	0.15	0.29	0.22	0.17	-0.60	0.72	0.27	0.97	1823
1824	0.71	0.59	0.27	0.52	-0.02	0.60	1.55	0.88	1.36	-0.93	0.14	0.26	1824
1825	-0.09	0.37	-0.21	0.12	0.24	-0.29	0.04	-0.36	0.03	0.32	0.59	-0.59	1825
1826	0.80	0.24	0.45	0.92	0.78	-1.17	0.04	-0.36	0.25	0.81	0.36	0.30	1826
1827	-0.09	-0.29	-0.17	0.17	-1.27	-0.46	-0.01	-0.09	-0.15	-0.13	0.54	0.08	1827
1828	1.07	0.51	-0.57	-0.59	-0.42	i e	-0.23	0.04		-0.17	0.81	0.21	1828
1829	0.09	-0.69	-0.35	0.08	-0.11		-0.89	-0.01	0.16	0.54	0.23	0.12	1829
1830	-0.27	-0.74	0.01	-0.32	-2.73	-0.15			0.25	1.12	0.68	0.53	1830
1831	0.31	1.49	1.66	0.48	1.89	1.36	0.04	0.67	0.70	0.41	0.41	0.53	1831
1832	-0.49	-0.29	1.26	1.73	2.51	2.65	1.64	2.40	0.34	-0.25	0.46		1832
1833	0.36	0.23	-0.19	0.97	0.83	0.83	1.33	0.40	1	0.41	0.19		1833
1834	0.18	0.60		-0.58	1.31	0.12		-0.18	1	-0.03	0.01	-0.01	1834
1835	-0.66	-0.73	-0.57	-1.07	-0.24	-0.86	-0.67	-0.45	1	-0.74	-0.48	-0.94	1835
1836	-0.75	1	-1.41	-0.72	0.60	0.12	-0.58	-1.29	ł	0.15	-0.92		1836
1837	-0.31			-0.63	-1.17	-0.41	-0.40	-0.05			-0.17		1837
1838	1	-0.69	-0.30	0.04	<b>-</b> 0.33		0.75	-0.05	0.65		-0.57	1	1838
1839		-0.69	-0.30 -0.12	-0.45	-0.35 $-0.15$	-0.24 $-0.41$	-0.49	-0.93			-0.83		1839
1840		-0.11 -0.42			0.29	1	-0.45	0.27	į.		-1.14		1840
1841	11	-0.42 $-0.16$	-0.10	-0.58	-1.17		0.35	-0.71	0.74		-0.34	1	1841
1842	11	-0.51	-0.08	-0.49	0.47	0.07		0.09	-0.86	-0.30			1842
1843	l t	-0.01	-0.03	0.22	-1.53	-1.04		0.44	0.16	-0.52		-0.32	1843
Means.		21.31	22.92			25.35		23.73	23.70	22.92	21.32	20.67	Means.
			-										

#### LXXX.

#### SICILY. — PALERMO.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees or	Reaumu	1.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1791		• •		• •			-0.52		-0.67		1.73	0.00	1791
1792	1.18	0.51	0.09		-0.48		-1.01	-1.65			-0.83		1792
1793	-1.6S	-0.38		-1.63		-1.83		-1.14	0.86	-0.54		0.44	1793
1794	-0.04	-0.69	-0.51		-0.79				-0.14		-0.29	-0.47	1794
1795	-1.62	1.27	0.78	-0.10	0.12	-0.59	-1.12	-0.34	-0.72	• •	-0.23	0.18	1795
1796	0.78	0.58					-0.39		0.40	1.11	0.00	0.98	1796
1797	-0.24	-0.29			-0.24			0.39	0.15		-0.12	0.16	1797
1798	0.03	0.20			-0.99		1	-0.41	0.00	-1.00		0.31	1798
1799	-1.75	1.38	0.52	0.64		0.08	0.37	0.75	0.48	)	-0.32	0.40	1799
1800	2.27	2.96	0.69	2.46	0.63	-0.14	0.26	-0.41	-0.58	0.02	-0.18	0.09	1800
1801	-0.11	0.76	1.45	0.24	-0.10	-0.16	1.26	-0.56	-0.07	1.04	1.04	1.64	1801
1801	1	-0.16		-1.01	ł .	$\frac{-0.10}{2.50}$	0.17	0.72	0.42	0.77	1.51	1.40	1802
1802	1.67		0.47	l l	-1.08	0.66	0.04	0.52	0.31	-0.65	1.42	0.42	1803
1804	4.63	-0.82	0.16	0.21	0.14	1.30	1.12	0.12		0.31	1.22	1.40	1804
1805	0.80	0.69	-0.68		1	1.21	1	-0.34	-1.52	0.06		-1.02	1805
1000	0.00		****	1.00	1.00	1.21	0.00	0.01	1102	0.00	1.00	1102	1000
1806	-1.15	0.64	-0.04	-0.50	0.41	0.10	-0.14	-0.85	-1.16	-0.43	-0.14	0.40	1806
1807	-1.06	0.16		-1.21	0.74	0.90	1.37	0.92	2.80	1.26	}	-0.07	1807
1808	-0.24	-1.22		-1.36	-0.48	-0.43	0.88	0.04	2.42	-1.92	-0.29	-2.31	1808
1809	0.87	-0.31	0.23	-0.50	-0.48	0.86	1.46	-0.23	-0.67	-1.67	-1.36	-0.98	1809
1810	0.01	-0.27	2.49	0.28	0.50	-0.63	-0.54	-0.19	-0.29	-0.67	0.06	-0.91	1810
1811	-0.15	0.69	-0.91	0.24	0.43	1.46	0.97	0.26	0.04	0.95	0.00	-0.76	1811
1812	-1.51	0.40	0.00	-0.39	-0.61	0.15	-1.32	-0.21	-0.69	-0.16	0.35	-0.18	1812
1813	-1.51	-1.02	-0.80	-0.52	0.79	0.32	-0.92	-1.25	-1.00	1.31	0.04	-1.18	1813
1814	0.54	-3.04	-0.88	0.04	-1.46	-0.59	-0.96	-0.56	-2.03	-0.49	-0.52	-0.42	1814
1815	-0.46	0.07	0.29	0.90	0.61	-0.63	-1.12	-2.01	-0.78	0.22	0.08	-0.78	1815
-													
1816	-0.40			-0.54		1	-0.65	1	-0.80		-0.63	1 6	1816
1817	-0.11		-0.15			ł	-0.39	l .	-0.34	0.11	1	1 1	1817
1818	-0.66	0.87	0.00	1.21			-0.25	í	0.24	-0.78	0.33	0.62	1818
1819	-1.02	0.18	1	0.97	-0.12			-0.34	ĺ	0.82	1.11	0.82	1819
1820	1.89	-0.11	-0.97	0.37	2.03	0.68	0.48	• •			-0.65	0.29	1820
1821	1.92	-0.76	0.49	0.50	0.85	-0.74	-0.30	-0.21	0.51	-0.71	-0.72	0.69	1821
1821	-1.92	1			0.68		1.48	1.46			1	0.03	1822
1823	0.52	1	-0.80	0.28	0.99	1	1	0.35			-1.63		1823
1824	-0.91	1	-1.04	1	1.25			1.86	0.13			0.51	1824
1825	-1.04	1		0.12	1	-0.45	ì	0.46	0.55	1	-0.05	1.67	1825
1020	1.01	1.02	0.11			10.10	0.10	0.10		1.00		1.01	1023
1826	-0.88	0.56	-0.29	-0.59	-1.08	-0.74	0.39	0.52	1.35	0.46	-0.87	-0.24	1826
1827	0.07	0.83			1	-1.30	0.80	1.33	-0.73	0.50	-1.76	-0.04	1827
1828	-0.16	0.20	0.23	0.29	1.99	1.28	2.48	1.10	0.74	-0.34	0.06	-0.37	1828
1829	0.79	-1.90	1.12	2.49	-0.09	-0.47	0.16	-0.12	0.41	-0.38	-0.35	-0.16	1829
Morris			-		-				7	1, -			Means.
Means.	8.35	8.27	9.40	11.52	14.35	17.12	19.25	19.48	17.60	14.78	11.69	9.44	Means.
		1						1		1		1	

### LXXXI.

### NORTH ITALY. - MILAN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1763	-1.32	0 1.58	0.60	0.27	$\begin{vmatrix} \circ \\ -2.28 \end{vmatrix}$	0.79	0.68	° 1.11	° -1.11	° -1.69	0.56	0	1763
1764	1.68	1.98	-0.70	-0.63	1.32	3	-0.12			1	-0.36	1	
1765	3.88	ļ	0.60	0.47	-1.08	0.31		$\begin{bmatrix} -1.29 \\ -1.69 \end{bmatrix}$		0.11	0.24		1764 1765
1766	-3.42	-1.52	-0.40	0.57	0.02	1.31		-0.19		-0.49	1		1766
1767	-4.22	0.38		-0.93				-0.69			1	-0.88	1767
1707	-4.44	0.00	0.10	-0.33	-1.03	-1.13	0.10	-0.03				-0.00	1707
1768	-0.82	-1.22	-1.50	0.37	-0.58	-2.19	0.68	0.51			0.64	-0.78	1768
1769	1.88	-0.42	-0.50	-1.63	-0.48	1.01	-0.52	1.51		-2.19	1.24	0.62	1769
1770	-0.52	0.98	-0.60	-0.33	-0.58	0.81	-0.72	0.01	1.99	0.51	1.04	-0.68	1770
1771	1.78	-0.52	-0.60	-1.43	1.02	-0.19	0.68	1.51	0.49	-0.69	-1.06	2.32	1771
1772	1.58	2.48	2.50	0.57	-0.58	1.61	1.38	0.41	0.29	2.01	1.94	2.02	1772
1773	1.58	-0.42	-0.80	_0.02	-0.48		-1.72	-1.29	0.69	1.61	0.34	1.82	1773
1774	0.48	0.08	0.70	}	-0.28	0.51	-0.12	1.31			-0.96		1774
1775	0.38	2.08	1.60	0.47		0.71	0.78	-0.09	[	-1.79	1	-0.88	1775
1776	-0.32	-0.02	1.30	0.97	1	0.11	0.48	0.41	-0.71	0.11	1	1	1776
1777	-1.52	-1.42	1.30			-0.79	-1.22	0.51	0.19	0.41	1.24		1777
						0.10		0.01		0111	1.21	1	1
1778	0.38	0.08	-1.90	1.47	0.62	-0.29	0.98	0.81	-0.81	-0.09	0.64	1.72	1778
1779	-3.52	1.98	0.00	1.07	1.72	-1.39	0.18	-0.19	1.59	1.81	-0.16	1.82	1779
1780	-0.62	-1.92	2.70	-0.43	1.72	1.51	0.78	0.11	-0.51	1.81	-0.16	-1.08	1780
1781	-0.12	0.38	1.90	1.47	0.22	0.01	1.78	0.41	0.39	-0.89	0.04	1.42	1781
1782	2.18	-2.42	-0.70	-1.03	-1.08	1.21	2.08	0.91	-0.31	-1.79	-2.46	-0.58	1782
1783	0.98		-0.60		0.42	-0.99	1.08	-0.29		1.51		-1.88	1783
1784	0.48	<b>-2.</b> 02		<b>-2.0</b> 3	2.62	2.11	1.38	0.61	1.49	-1.49	-0.46		1784
1785	0.58	-1.12	-3.80		0.72	1.21	0.68	0.61	2.69	0.41	0.74	2.02	1785
1786	0.18	0.68	-0.90	0.87	0.72	0.81	-0.52	-0.89	1.09	-1.89	-0.36	-0.48	1786
1787	-0.32	0.08	0.90	-0.03	-1.98	1.71	-0.02	1.61	0.09	0.81	0.84	1.72	1787
1788	2.78	1.08	2.30	1.37	-0.18	1.51	2.78	-0.39	0.99	0.21	-0.86	-2.88	1788
1789	-1.72	0.98	-1.70	1.37	2.22	-0.79	0.28	0.11	0.29	0.31	-1.26	-2.38	1789
1790	-0.12	1.48	-0.20	-1.73	1.62	0.71	-0.72	1.21	0.19	2.21	1.24	0.02	1790
1791	2.48	1.08	1.20	1.87	-0.18	-0.49	0.58	1.51	0.09	-0.29	-0.46	1.92	1791
1792	0.98	-0.12	1.30	1.87	-0.18	0.21	0.08	0.11	-0.41	0.71	0.54	-0.08	1792
1793	-1.22	-0.02	0.40	_1 19	-0.58	0.01	1.78	-0.29	9 10	7 97	1 (1	2.22	1793
1793	2.28	3.08	2.00	$\frac{-1.45}{2.37}$		0.01	1.78	0.29	2.49	1.31 $-0.49$	1.44		1793
1795	-3.72	100	-0.20	1.37		-0.79	-1.42	0.21	0.49	1.71	-0.16	1.52	1794
1796	2.48	1.18		-0.13		-0.75 -0.29	-0.12	0.51	1.39	0.41	$\frac{-0.10}{1.24}$	-1.3S	1796
1797	0.78	0.18	-1.40	0.67		-0.25 -1.59	1.18	2.51	1.09	-0.59	0.94	1.32	1797
		0.10	21.10	0.01	1,22	2.00	1.10	2.01	1.00	0.00	0.04	1,02	
1798	1.78	2.08	0.20	0.27	0.72	-0.09	0.48	0.51	0.29	-0.39	-0.86	-2.08	1798
1799	-3.22	0.88	0.60	-1.23	-0.98	-1.49	-0.62	0.41	1.39	0.51	-0.96	-1.18	1799
1800	1.78	4.58	-1.10	2.67	1.32	-1.59	0.38	-0.09	0.49	0.01	1.24	-0.08	1800
1801	1.38	1.08	1.50	0.77	0.32	-0.39	-0.62	-0.79	0.49	0.61	0.04	0.02	1801
1802	0.18	1.18	0.70	0.77		1.71	0.28	2.21	1.09	2.81	1.04	1.52	1802
1803	1	-3.82	0.30		-0.88	1.11	0.28	1.11	-0.91		0.54	0.22	1803
1000	2.00	0.02	0.50	1.47	-0.03	1.11	0.10	1.11	-0.91	0.49	0.04	0.24	1000

### LXXXI.

# NORTH ITALY. - MILAN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

,					De	grees or	Reaum	uı.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1804	0	0	0 00	0	0	0	0	0 00	0 10	0	0 26	° -0.18	1804
	3.98	}		-0.03	1		1	-0.39			1	1 1	1
1805		ł .	-0.10		-0.78	1	-0.42	1		-1.19	1	-1.58	1805
1806	0.18	1.68		-1.53	0.32		1			-0.19	1.34	1	1806
1807	0.58	6	-2.40	ł	1.32	1	1.18		1	1.71	1	1 }	1807
1808	-1.02	-1.62	-3.80	-1.23	1.62	-0.49	1.98	-0.69	0.39	-2.39	0.24	-2.08	1808
1809	0.48		-1.40	1	1.02	1	-0.52		1	1			1809
1810	0.08	1	1	-0.23		1	-2.12		1	1.11	0.34	1.82	1810
1811	-0.72	1.48	1.70		1	-0.29	1	-0.49	1	2.21			1811
1812	-3.32	1	1	-1.73	0.92		-0.82			0.11		-2.38	1812
1813	-0.12	1.08	0.50	1.07	1.52	-0.99	-2.12	-1.09	-1.11	0.21	-0.56	1.32	1813
1014	_0.19	4 49	_1 40	0.77	_1 09	_ 1 00	-0.12	_1 00	_1 01	-0.69	1.01	1.82	1814
1814 1815	1	-4.42 $-0.32$	-1.40 $1.90$	1	,		-0.12 -1.22		1	0.81	1	-1.78	1814
1816		-0.32 -2.92	1				-2.22	1	1	0.31	1	-1.88	1816
	-0.52 $-2.52$	2.08	0.30				-3.52	i .	1	-1.89		-0.18	1817
1817 1818	0.48	3.34	0.30					-0.59		0.48			1818
1010	0.45	5.04	0.70	0.57	-3.00	0.20	0.55	-0.79	0.20	0.40	1.10	-0.00	1010
1819	0.00	0.73	1.48	1.35	-0.02	-0.53	0.32	-0.50	0.48	0.46	0.93	0.30	1819
1820	-0.79	0.58	-0.56	1.60	1.03	-0.48	-0.48	1.76	-0.09	-0.30	-0.72	-0.03	1820
1821	0.80	-0.18	-0.52	0.59		-2.20		0.43	1.01	-0.29	0.78	0.35	1821
1822	1.81	1.28	2.10		1.05	3	0.53		1	0.66	1	-0.48	1822
1823	-1.92	-0.25	-0.37			-0.78		0.53	1.18	0.11	1	0.01	1823
1824	1.01	1.49	-0.40	-0.85	-0.16	-1.57	1.33	0.90	0.71	0.23	1.25	2.07	1824
1825	1.39	0.62	-2.38	1.21	-0.17	0.32	0.05	0.53	0.86	-0.81	0.82	3.92	1825
1826	-2.18	0.44	0.76	-0.72	-1.23	-0.09	0.18	1.55	0.71	1.48	-0.56	1.16	1826
1827	0.36	-1.72	1.12	0.73	0.46	-1.26	1.20	-0.60	-1.06	1.37	-1.46	0.25	1827
1828	1.38	-0.36	1.49	0.64	0.45	1.27	1.38	0.19	0.47	0.38	-0.81	0.60	1828
1829	-0.04		0.05	ì	-0.03	ì		1	-0.89		1	1 1	1829
1830	-3.72		1.66			-0.33	1.71		-0.79		1	0.60	1830
1831		-0.51	0.73		-1.12				-1.08			1.34	1831
1832	0.41	0.52	-0.21			-1.27	0.03		-1.15	-0.47	1	-1.71	1832
1833	-0.47	1.18	-0.59	-1.23	2.00	0.37	-2.28	-2.77	-3.20	-1.36	0.14	1.37	1833
1004	0.15	0.00	0.10	_1 0*	0.59	0.91	-0.23	1.10	0.41	0.70	0.99	_004	1004
1834 1835	1.03			-1.97 -0.88			-0.23 -2.59		1				1834 1835
1836	-2.51						-0.97					l i	1836
1837	-0.83			-2.41			-1.29		-2.40	1	1		1837
1838		-4.75 $-2.39$					-0.78		1	ł .		-0.80	1838
1000								1.00					1000
Means.	0.52	2.82	6.40	10.03	14.08	17.09	18.92	18.39	15.31	10.79	5.76	2.08	Means.
	1										l		

#### LXXXII.

### SWITZERLAND. - GENEVA.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1768	-0.86	-0.01	-2.38		-0.61		-0.92	-1.25	-1.42	0.99	0.77	0.08	1768
1769	0.92	0.16	l :		-0.71			-1.43	4	)	1.62	0.61	1769
1770	-1.25	-1.30	-1.72	-2.40	-1.20	-1.34	-2.97	-1.24	0.49	-0.81	0.35	0.42	1770
1771	0.53	-0.67	0.17	-2.68	0.34	-1.84	0.07	-1.45	-0.57	-0.17	-1.80	1.66	1771
1772	0.61	2.57	1.76	-0.41	-2.23	0.35	-0.72	-0.47	0.52	1.34	1.29	1.16	1772
1773	1.47	-1.84	-1.18	_1 16	-1.64	_0.87	-2 03	-1.70	_0 19	-0.35	-0.12	1.01	1773
1774	1.22	0.91	2.38		-0.94		-1.27		-1.08	1	-1.18		1773
11 11	0.89	1.89	0.99		-1.90	0.54		i	-0.02		0.33		
1775	-1.78	1.92			-1.96	0.09	0.20		-1.50		-0.26	1	1775
1776		-0.76	1.85		1	1	-1.12		-0.41	1.27	0.21	-1.72	1776
1777	-0.41	-0.76	2.46	-1.23	-1.51	-0.38	-1.12	0.45	-0.41	1.27	0.21	-1.72	1777
1778	0.03	-0.93	0.86	0.78	-0.09	-0.76	1.59	0.68	-1.85	0.32	0.76	1.85	1778
1779	-3.43	-0.28	-0.14	1.70	0.97	-1.22	-0.61	-0.45	0.48	1.77	0.57	2.70	1779
1780	-1.48	-1.63	2.35	-0.86	0.97	1.14	0.95	1.16	0.14	0.51	-1.02	-1.25	1780
1781	0.96	1.09	0.37	2.15	1.78	0.28	-1.17	0.30	0.76	-0.47	1.69	2.97	1781
1782	2.22	-3.74	-0.53	-0.95	-1.76	0.18	-1.10	-0.72	-0.97	-1.06	-1.83	-2.04	1782
	2.04		0.0-	0				!	0	0.00			
1783	2.01	1.68				-1.13		-0.94	0.17	0.93	0.81	1.03	1783
1784			-0.43		1.73	1.69		-1.62		-1.87		-3.38	1784
1785	0.58		ł			0.30		-1.75	0.94	-0.40	0.11	0.42	1785
1786	0.41	0.08		0.69	1	1.92		-1.22	1	-1.71	-0.69	0.19	1786
1787	-1.99	-1.15	1.76	-0.30	<b>-1.9</b> 8	0.79	-0.70	0.21	-0.27	0.41	0.72	2.83	1787
1788	1.01	2.06	2.19	1.04	1.13	1.04	1.61	-0.45	0.71	-0.83	-2.15	-4.48	1788
1789	-1.17	1.12	-1.97	1.19	1.71	-1.25	-0.80	-0.19	-0.57	-0.59	-1.59	-0.17	1789
1790	0.36	0.75	0.99	-0.73	1.52	0.94	-1.10	0.63	-0.84	1.95	1.13	0.78	1790
1791	2.40	0.04	-0.02	2.86	0.61	1.04	0.98	2.30	0.98	0.72	-1.37	1.30	1791
1792	1.22	-0.28	2.11	1.81	-0.12	1.14	1.03	0.83	-0.09	1.37	0.86	0.45	1792
1793	-0.52	1.05	1.77	0.08	-0.05	0.20	3.12	2.49	-0.12	1.24	0.61	1.19	1793
1794	0.14	2.21	1.91	3.26	0.76	1.10	2.11	0.39	-0.74	-0.28	0.86	1	1794
1794	-4.85	0.37	0.26	1.76	1.32	1.34	-0.73	1.34	1.54	1.92	-0.96	1.11	1795
1796	1.25	0.72	-2.15	-0.06	0.60	0.60	0.37	0.80	1.61	0.41	-0.14	-1.92	1796
1797	0.11	-1.41	-1.08	1.49	2.14	-1.28	2.21	1.28	0.71	-0.08	0.71	1.61	1797
1798	0.53	-1.17	-1.02	0.83	1.00	1.29	0.45	0.81	0.48	-0.29	0.44	-0.96	1798
1799	-1.57	1.71	-0.16	-1.73	-1.70	,	-0.13	0.67	0.21	-0.40		1	1799
1800	1.64	0.06	-1.66	2.43	2.40	-0.83	1.48	0.82	0.96	-1.55	0.63		1800
Means.	-0.43	0.75	3.08	7.19	11.21	14.03	15.44	14.85	11.49	7.32	3.34	0.57	Means.
1796	2.27	0.07			-0.91			0.16	0.70		-0.68		1796
1797		-0.85		0.97	0.67		1.27	0.71	-0.48 $0.12$	i	$0.47 \\ -0.76$	1.58 -1.36	1797 1798
1798	-1.44	-0.25 1.93			-0.22 -1.50	0.32 $-0.49$	-0.64 -0.46	-0.14 0.33	0.12		-0.76 $-1.24$		1799
1800	2.06		-0.26	$\begin{bmatrix} -1.60 \\ 2.88 \end{bmatrix}$	1.66		}	0.33	0.19		0.67	1	1800
		1							0.90	0.84	0.67	0.95	1801
1801	1.81	$\begin{bmatrix} 0.13 \\ -0.38 \end{bmatrix}$	1.43 0.94	0.74 1.18	0.43	-0.26 1.66	0.42 $-0.12$	0.15 2.68	1.72	2.51	0.67	0.58	1802
1802	1	-0.38 -2.58	0.94	2.05	-1.42	0.89	$\frac{-0.12}{2.20}$	2.08	-0.79	-0.57	1.04	1.88	1803
1803	Í	,	-0.19	0.30	Į.	2.02	,	0.47	0.59	0.22		-0.59	1804
1504	4,5	1.98	-0.19	0.30	1.50	4.02	0.01	0.47	0.59	0.22	1.00	0,3	1004

### LXXXII.

# SWITZERLAND. — GENEVA (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

_						De	grees of	Reaumi	ır.					
	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
		0	0	0	0	0	0	0	0	0	0	0	0	
l	1805	-0.41	-0.23	-0.41	-1.35	-1.22	-0.49	-0.41	-0.73	0.18		-2.19	-1.64	1805
	1806	3.23	1.83	0.12		1.33	1.66	0.08	-0.39	0.11	1.10	1.34	2.42	1806
	1807	-1.10	0.24	-2.65	-1.47	1.42	0.43	2.66	3.03	-0.58	1.42	0.39	-2.48	1807
	1808	-0.49	-3.14	-2.58	-1.87	1.14	-1.33	0.70	0.59	-0.14	-2.40	-0.28	-2.99	1808
H	1809	2.23	1.95	0.19	-3.68	-0.06	0.12	-0.43	-0.32	-1.00	-1.05	-1.76	0.70	1809
												- 0-		7070
	1810	-3.14	-3.34	1	-0.28	0.29	-0.45			1.37	1.26	1.05	1.19	1810
1	1811	-2.22	1.98	1.46	1.34	1.23	1.82	1.53		0.70	2.21	0.71	-0.85	1811
	1812	-3.92	1.40		-1.54	0.27	1		-0.69	-0.43	0.13	-1.80		1812
H	1813	-1.74	1.51	-0.69	0.53	0.54			-1.02		0.78	-0.49	0.32	1813
	1814	-1.32	-3.92	-1.44	0.96	-1.74	-0.26	0.37	-0.66	-1.74	-0.87	0.95	2.34	1814
	-01-					0.00	0.00	0.00	0.50	0 = 4	7 40	1.50	0.20	1815
	1815	-2.24	1.43	1	1.06	0.82	0.08		-0.59	0.54	1.43	-1.57	-0.39	- 11
	1816	-0.13	-1.33		-0.48		-1.41		-2.14	-0.47	0.59	-1.05		1816
	1817	2.50	2.38			-1.34	1.35		-0.71	2.16	-1.58		-0.45	1817
I	1818	0.54	0.69		-0.08	1	0.66	1.41		-0.89	-0.29	1.60		1818
I	1819	1.86	0.98	0.82	1.00	-0.21	-0.19	0.07	-0.34	0.42	0.07	-0.40	0.95	1819
ı	1820	0.10	0.54	-1.24	2.07	0.39	-0.59	-0.65	0.84	-1.93	-0.31	-2.16	0.02	1820
	1821	1.98	-1.31	0.94	0.71	-1.19	-1.54		0.62	0.26	0.27	2.34	3.36	1821
	1822	0.20	1.27	3.06	0.47	1.32		0.27	-0.85		0.69	1.60	-2.32	1822
	1823	-1.17	1.46		-0.42	0.17		1	{		-2.10	-1.97	1.04	1823
	1824	-0.78	-0.30		-2.05		1	0.17	-1.49			0.03	1.30	1824
	1825	-0.07	-0.55		1.69	1	1			0.88	0.30	0.54	2.76	1825
I	1020			1.03	1.03		0.20	0.40						
	Means.	-0.42	1.87	4.70	8.79	13.45	15.81	17.67	17.66	14.70	9.73	5.23	1.27	Means.
				ŀ		1								
H	1826	-3.23	1.12		0.34	-1.04	ì	0.90	1	1.22				1826
1	1827	1.49	-2.15	1			-0.07	1.95	I.		1	-2.02	1	1827
ı	1828	2.82	1.06	0.70	0.81	1.22	1	0.59	1			!	1	1828
	1829	-0.85	[-0.63]	0.10	0.25	-0.06	-0.83	0.15			-1.52	-1.28	1	1829
ı	1830	-4.14	-1.74	1.20	2.70	0.57	-0.49	0.53	-0.01	-0.94	-0.86	0.46	-0.90	1830
	1831	-1.10	0.46	1.67	1.54	0.53	-0.11	-0.02	-0.02	-0.29	2.16	0.58	0.90	1831
1	1832	0.10		1	1	1	1		2.29					1832
	1833	-0.06	1	-0.50	1	1		1			1 -	0.39	1	1833
	1834	5.06	1		1		1		1	1	1	0.71	1	1834
1	1835	1.15	1	-0.44			1	1					1 1	1835
	1836	0.48			1			1	1	1	1	1	1 6	1836
	1837	0.37	1	L.	-1.89			1	1			i	-0.46	1837
	1838	-3.64				i			1		1	1	-0.57	1838
	1839	0.55				1	1	1		1				1839
	1840	2.60	0.02	2 -3.22	0.71	-0.10	-0.37	-2.32	-0.01	-0.56	-1.74	1.43	-3.14	1840
	1841	0.45	-0.25	0.77	-0.69	1.82	-1.71	-1.98	-1.37	0.09	0.90	0.26	0.89	1841
	1842	-5.18					1						1	1842
	1843	1.50	1					-2.35						1843
	1844	1.50				1.00		2.00						1844
	1845	1.70					1			1			1	1845
				-		-	-	-	-	-	-	-	-	
	Means.	-0.72	0.98	8 4.16	7.08	10.77	13.61	14.96	14.58	11.84	7.98	3.98	1.30	Means.
		.11												

#### LXXXIII.

### South Germany. - VIENNA.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	egrees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1775	-1.43	1.86	1.21	-2.35	-2.77	1.32	-0.41	1.29	0.84	0.26	0.29	-1.09	1775
1776	-4.30	0.57	0.70	-1.11	-2.30	-0.42	-0.24	• 0.25	-1.42	-1.53	-1.32	-2.19	1776
1777	-1.79	-1.24	0.32	-2.93	-0.22	-0.10	-1.17	0.57	-1.38	-0.53	0.35	-1.00	1777
1778	1.92	-1.04	0.18	1.89	0.04	-0.43	1.18	0.95	-0.89	-0.54	0.87	3.61	1778
1779	-1.75	3.15	2.27	3.05	1.24	-1.32	-1.35	-0.07	0.65	1.00	0.43	3.01	1779
1780	-1.68	3.04	2.73	-1.38	-0.18	-0.92	-0.70	-0.48	-1.08	0.51	0.19	-1.99	1780
1781	-0.87	0.05	0.77	0.86	0.25	1.44	-0.06	2.31	1.40	-0.45	1.84	0.34	1781
1782	2.72	-2.63	0.60		0.54	1.82	2.74	0.85	0.86	-0.76	-1.50	0.62	1782
1783	3.59	4.12	-0.08	0.65	1.81	1.94	1.66	1.81	2.12	1.59	0.58	-2.56	1783
1784	-3.51	-1.87	-0.42	-1.36	1.69	0.86	0.47	0.49	1.98	-2.56	0.70	0.03	1784
1704	3.51					0.00			1.30			0.03	1104
1785	-0.73	-0.93	-5.63	-3.04	-0.67	-1.47	-0.83	-0.86	2.11	-0.55	0.41	0.17	1785
1786	0.52	0.16	-0.04	1.84	-1.12	0.25	-1.54	-1.85	-0.92	-2.11	-2.12	0.60	1786
1787	-0.39	1.47	0.65	-1.46		1.11	-0.40	0.35	<b>-0.7</b> 8	1.10	0.93	2.82	1787
1788	2.22	0.17	0.81	0.05	-0.36	1.18	2.28	-1.72	1.00	-0.29	-1.39	-6.79	1788
1789	-0.49	2.00	-2.43	1.19	2.15	-0.49	0.40	-0.60	0.37	0.77	0.73	0.21	1789
1790	0.86	2.87	0.31	-1.11	1.20	1.56	-1.10	0.31	-0.83	-0.76	-0.43	2.09	1790
1791	4.29	1.01	1.63	1.33		-0.33	-0.37		-0.84	-0.40		0.89	1791
1792	0.56	-1.24	0.47	0.38	-0.96	0.62	0.38		-0.93	-1.11	-0.24	0.56	1792
1793	-1.55	1.27	-1.00	-2.40	-1.23	-1.08	1.81		-0.07	1.13	0.64	1.99	1793
1794	2.24	2.99	1.95	3.74	1.35	1.55	2.92	-0.75		-0.19	0.33	-0.95	1794
1795	-4.94	-1.29	0.23	1.81	-0.05	1.44	-1.95	0.31	-0.17	2.75	ì	2.28	1795
1796	5.23	1.32	-2.73	-1.52	0.48	-0.04	0.14	0.58	1.96	0.84	l .	-1.48	1796
1797	1.58	1.02	-0.71	2.10	2.94	0.68	1.95	2.17	2.01	1.23		1.11	1797
1798	1.96	2.83	1.40	0.65	0.26	0.84	0.14	1.29	1.62	-0.47	-0.68	-3.68	1798
1799	-5.34	-2.08	-0.83	-0.43	-0.45	-1.16	-0.58	1.00	-0.50	0.45	0.58	-2.94	1799
1800	0.74	-0.19	-3.31	5.57	1.90	-1.45	-0.44	1.49	0.27	-0.40	1.57	0.10	1800
1801	1.85	-0.21	2.47	0.80	1.83	-0.85	-1.18	-1.32	1.37	1.94	1.71	0.99	1801
1802	-0.43	-1.34	0.89	0.73	-1.14	1.33	1.02	1.65	0.38	2.10	1.84	1.40	1802
1803	-2.68	-3.46	-0.50	2.49	-1.59	-0.75	0.23	0.08	-2.12	-0.45	1.24	0.27	1803
1804	3.42	-0.59	-2.44	0.05	0.29	-0.10	0.25	-0.51	0.80	0.48	-2.47	-2.40	1804
1005	0.40	1 10	_1 00	-2.16	-1.85	-0.79	-1.26	-1.61	-0.04	-2.89	-2.19	0.24	1805
1805	-0.48	-1.18	-1.28		1.84	-0.79 -0.02	-0.16	-0.62	0.56	-2.89 $-0.80$	1.60	3.48	1805
1806	4.04	2.12	1.07	-2.07	1.23				0.56	1.37	1.96	0.46	1 1
1807	1.08	1.96			1.23	0.15	1.25	1.80	1.13	-0.97	-0.32	-3.68	1807
1808	1.20	-0.51	-4.99	-1.20	0.89		1.30		0.11	-0.97 -1.31	-0.32 $-0.75$		1808
1809	-0.08	1.54	-1.13	-2.51	0.59	0.27	0.23	0.79		-1.51	-0.79	1.67	1809
1810	-0.71	-0.03	2.03	-0.74	0.50	-1.65	0.82	0.15	2.26	-0.18	-0.09	2.01	1810
1811	-3.58	-0.91	2.08	0.75	3.12	4.62	2.56	0.99	0.42	3.63	1.20	0.19	1811
1812	-2.13	0.53	0.67	-2.67	0.65	0.35	-0.87	-0.52	-1.32	2.04	-0.84	-3.96	1812
1813	-1.84	2.07	-0.76	1.56	0.36	-1.82	-1.34	-1.80		-0.37	-0.24	0.68	1813
1814	-0.34	-4.37	-0.55	1.54	-2.19	-1.76	0.66	-0.21	-2.45	-0.73	0.32	2.19	1814
1815	-1.03	2.39	2.06	0.10	0.52	0.28	-1.51	-1.29	-1.20	0.06	-1.07	-2.87	1815
1816	1.84	-0.80	-0.19	0.09		-0.73	-1.58		-0.95				1816
1817	3.24	3.78	0.51	-4.08	0.53	2.18	-0.08	-0.25	0.56	-2.29	1.09	0.16	1817
1818	2.77	0.78	1.84	2.01	-0.11	0.55	0.13		0.41	0.84	0.60	-1.31	1818
1819	1.22	2.04	1.94		-0.75	l .		-0.35		-0.12	0.51	-1.21	1819
1010	1	2.04	1.04	****	0.10	2.01	0.00	0.00					

#### LXXXIII.

# South Germany. - Vienna (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaumu	ır.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1820	-2.47	0.36	-0.86	1.78	1.97	-1.18	-0.96	2.36	-0.71	0.16	-0.36	-1.49	1820
1821	2.22	-1.56	-0.72	1.57	-0.81	-3.08	-1.83	-0.76	0.51	-0.12	1.93	2.90	1821
1822	2.85	1.63	3.44	1.05	1.21	1.50	1.16	-0.27	0.06	2.12	0.44	-0.27	1822
1823	-4.55	0.68	0.80	-0.29	0.42	-0.68	-1.35	0.15	0.36	1.13	0.29	1.35	1823
1824	1.77	2.31	0.09	-0.72	-0.74	-0.60	-0.22	-0.53	1.36	0.60	1.56	4.00	1824
1005	0.15	0.50	1.50	1.00	0.74	0.01	0.50	0.45	0.00		1	0.11	1825
1825	3.15	0.50	-1.59	1.02	-0.14	-0.31	-0.72	-0.47	-0.62	-1.71	1.74	3.11	
1826	-3.65	-2.12	0.91	-0.12	-2.42	-0.38	1.34	2.06	0.69	0.89	1	1.78	1826
1827	0.69	-2.92	1.61	1.65	1.33	1.19	1.67	-1.06		0.82		0.83	1827
1828	0.19	-2.22	0.88	1.30	-0.16	0.21	0.63		-0.70	-0.82	1 "	1.57	1828
1829	-1.66	-3.79	-1.87	-0.23	-2.26	-2.69	-0.32	-2.62	-0.31	-2.12	-3.62	-6.11	1829
1830	-5.31	-3.23	-0.44	0.94	-0.39	0.33	0.02	-0.04	-1.81	-1.68	0.76	1.13	1830
1831	-1.42	0.26	0.43	2.23	-0.90	-1.86	0.33	-1.01	-1.96	2.02		-0.04	1831
1832	0.55	0.61	0.04		-1.90	ľ			-0.86	0.04	1	-1.36	1832
1833	-3.35	2.33	0.24		2.57	1.20			-1.22	-0.55		4.03	1833
1834	4.67	0.32	-0.29	-1.17	2.24	1.65	2.61	1.26	2.85	-0.08	-0.89	1.25	1834
1835	1.71	1 40	0.46	-1.10	0.27	-0.07	0.92	0.19	0.09	-0.76	-3.77	-1.39	1835
1836	-0.08	1.46 0.29	3.84	0.00	i			-0.78	1	0.91		2.44	1836
1837						0.30			-0.89 -2.22	-0.82		-0.95	1837
11	0.20	-2.39	-1.96	-1.18	-2.57	-1.38	1 .	0.84		1	1	1	
1838	-5.10	-4.14	-0.50		-0.76	-0.74	ļ	-2.29	-0.03		l .	-0.84	1838
1839	1.12	0.73	-2.31	-3.85	-2.04	1.06	ł	-2.23	0.23	1.05	1.55	0.70	1839
1840	1.03	-0.88	-3.76	-0.55	-1.59	-1.05	1		1	-2.03	2.09	-7.72	1840
1841	0.33	-3.24	0.65	0.93	2.19	-1.02	0.55	-1.10	0.24	2.04	0.28	2.27	1841
Means.	-1.22	0.63	3.85	8.66	13.31	15.72	17.14	16.77	13.25	8.51	3.67	0.39	Means.
			LXX	XIV.	Sou	тн G	ERMAI	NY. —	RATI	SBON	,		
	1				1	1		1 0 00		1 - 22		0.05	1
1773	3.00	-0.28	1	-0.28	0.25	0.34	1	-0.60	0.47	1.20	1.06	2.35	1773
1774	1.63	0.85	2.17	1.97	-0.10			0.16	-1.29		1	-2.32	1774
1775	0.67	2.87	1.13	-2.41	-3.42	-0.51	-1.91	• •	-0.73	1	-0.14	-0.64	1775
1776	-3.04	1.19	• •	• •	• •	• •	• •	• •		• •	• •	• •	1776
1777	-1.47	-0.68	2.37	-1.29	-0.16	0.28	-1.02	1.24	0.01	1.07	1.31	-1.17	1777
1778	1.88	0.21	0.89	1.98	1.76	0.81	3.20	2.38	-1.33	-0.36	1.36	3.06	1778
1779	-2.51	1.43	2.27	2.89	1.88	-0.34	-0.38	0.95	1.40	2.18	1.47	3.74	1779
1780	-0.83	-1.52	2.87	-0.92	0.87	1.30	0.64	1.65	1.32	1.25	0.25	-0.75	1780
1781		• •	1.52	1.88	0.82	1.52	0.48	2.36	2.45	-1.03	0.53	0.56	1781
1782	2.46	-2.93	3.32	3.15	3.74	1.92	2.02	-0.28	0.80	-1.67	-2.72	-0.32	1782
1783	3.48	2.22		0.26	0.93	0.92	1.73	0.45	0.13	1.00	1	-2.38	1783
1784	-4.07	-3.45		-2.76	1.67	0.60	0.23	0.34	2.21	-2.46	0.36	1 1	1784
1785	-1.20	-2.85	-6.49	-4.37	-1.08	-0.83	-1.42	-1.91	2.05	1	0.28	0.10	1785
1786	0.66	0.04		1.32	-1.54	1.28		-1.85	-1.30	1		-0.18	1786
1787	-1.03	4.29	0.75	-1.53		0.92		0.36	0.07	1.78	0.89	2.06	1787
	1.86	$\begin{bmatrix} 4.29 \\ -0.61 \end{bmatrix}$	-0.30	1	1	0.92		-1.53	1.44			-8.30	1788
1788 1789	-1.93	1.41	-0.30 -2.90	0.64	1.62	-1.30		-0.28	-0.53	0.27	0.25	0.64	1789
	1.99	1.41	t .	Į.	1.62	$\frac{-1.30}{1.42}$		-0.28 -0.08	1	-0.37	-0.26	0.89	1790
1790		1	1	-1.21	1 -		1	1		0.50		0.84	1790
1791	3.24	0.14	1.00	1.81	-0.76	-0.35	-0.35	1.14	-0.15	0.50	-2.43	0.54	1791

### LXXXIV.

# South Germany. — Ratisbon (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees or	Reaum	uı.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	1200
1792	-0.57	-0.21	1.41	1.17	-1.12	0.87	0.66		-1.01	0.05	0.17	0.89	1792
1793	-1.17	1.26	0.53	-1.81		-0.76	1.56		-0.47	1.87	0.95	1.26	1793
1794	2.30	3.01	3.05	3.04	1.19	1.69	2.85	-0.80	-1.00	1.24	0.67	-0.78	1794
1795	-5.05	-0.89	-0.10	1.96	-0.82	1.39	-2.22	0.29	1.08	3.11	-0.98	2.26	1795
1796	4.26	1.59	-1.63	-0.77	-0.25	0.05	0.47	0.93	2.24	0.28	-0.38	-2.04	1796
1797	1.46	1.52	-0.17	2.09	2.60	-0.72	2.14	1.73	0.75	0.06	1.00	1.59	1797
1798	1.88	1.94	0.18	1.02	0.66	1.65	0.50	1.26	1.08	-0.73		1	1798
1799	-5.61	0.14	-0.29	-1.87	1	-0.83				-0.23		-3.81	1799
1800	1.15	-0.63		4.66	1.80		0.32	1.53		-0.69		0.63	1800
] [			-2.62									1	1
1801	2.72	0.10	1.82	0.76	2.45	-0.75	-0.30	0.13	1.15	1.60	1.45	0.81	1801
1802	-3.20	-0.90	0.29	0.62	0.16	1.66	-0.04	2.80	0.73	2.40	0.63	0.71	1802
1803	-1.24	-2.05	-0.06	2.70	-1.78	-0.31	1.70	1.31	-0.96	-0.33	0.29	0.93	1803
1804	3.84	-0.86	-1.18	-0.49	1.17	0.88	0.29	-0.14	1.27	1.09	-0.71	-1.68	1804
1805	-1.41	-1.00	-0.34	-1.27	-1.76	-0.88	-0.88	-1.60	0.74	-2.03	-1.81	-0.21	1805
1806	4.22	2.45	0.40	-2.24	2.47	0.16	-0.49	0.15	0.86	0.04	1.94	3.58	1806
1807	1.19	1.18	-1.17	-1.32	1.24	0.46	2.87	4.63	-0.94	1.58	1.03	1.54	1807
1808	1.08		-2.79			-0.45	1.61	1.19	0.33	1	}		1808
1809	0.33	2.19	-0.40	-2.92	0.71	-0.25	0.02	0.23	-0.31	-0.76	ì	0.93	1809
1810	-1.72	-2.39	0.86	-0.63	-0.05	-1.00	-0.41	0.17	2.72	0.52	ļ	1.89	1810
	1												
1811	-2.93	-0.16	2.09	1.48	2.23	2.85	1.75	0.24	0.43	2.24		-0.25	1811
1812	-1.33	1.05	0.28	-2.87	3	-1.15	<b>-2.1</b> S		-1.39		-1.99		1812
1813	-3.03	0.99	-1.15	0.46	-0.60					1		-0.33	1813
1814	-1.37	-4.71	-2.93	0.49	-2.79	<b>-2.39</b>	-0.12	-1.12	-2.45	-1.50	0.65	1.77	1814
1815	-1.30	1.05	1.18	-0.37	-0.46	-0.74	-2.23	-2.07	-1.35	-0.70	-1.37	-2.26	1815
1816	1.36	-1.83	<b>-1.2</b> 3	-0.93	-2.69	-2.21	-2.42	-2.56	-2.04	-0.93	-1.49	-0.75	1816
1817	2.51	2.42	-1.14	-5.01	-1.93	0.61	-1.79	-1.89	0.56	-3.22	0.63	-0.70	1817
1818	2.08		-0.16	0.27		-0.02			-1.09	1		-2.08	1818
1819	1.49	0.60	0.64		-0.76		-0.05			1		-1.34	1819
1820	-2.43	-0.35	-2.26	ļ	-0.47	-2.89	1		-2.28				1820
1821	1.17	-3.06	-1.51	0.99	į	-3.01		1	-0.06		1.51	2.53	1821
										l	1	1	
1822	2.21	0.63	1.92	0.26	0.53	2.43	0.49	-0.87	-0.56	0.73	0.48	-2.29	1822
1823	-4.17	0.86	0.11	-1.72		-0.97	1	0.43	0.38	0.02		1.05	1823
1824	0.92	0.38	-1.02	-2.10				-0.51	0.97		1.44	3.93	1824
1825	2.80	0.39	-1.05	2.12	0.93	0.56	0.51	0.32	1.31	0.21	3.09	4.15	1825
1826	-3.57	-0.34	1.39	0.17	-1.04	1.05	1.99	3.61	1.61	1.38	-0.28	0.92	1826
1827	0.09	-4.95	1.00	1.31	1.20	1.05	2.06	-0.57	0.93	1.35	-1.30	2.93	1827
1828	2.12	0.27	0.51	0.31	-0.77	0.39	0.85	-2.47	-1.95	-0.20	0.61	2.28	1828
1829	-0.85		-1.38		-1.14	-1.11	-0.20	-2.37	-1.35	-1.41	-3.79	-5.79	1829
1830	-5.98		1.17		-0.12	-0.94		-1.28		ł.	1.14	-0.58	1830
1831	-2.09		0.70	3.60		-1.36			-1.57	2.40	2.27	0.26	1831
1832	0.77	1.28	0.09	0.21	-2.45	-0.87	-1.18	0.59	-0.98	0.16	-0.71	0.25	1832
1833	-3.05	3.32	0.21	-1.45	2.29	1.06	ł		-2.01	-0.90	2.78	3.95	1833
1834	ll .	-0.43	-0.25	-1.69	0.99	0.44	4.89	2.48	1.21	0.50	0.74	1.36	1834
Means.	-2.42	-0.09	3.09	7.55	11.94	13.72	14.88	14.62	11.69	7.11	2.22	-0.71	Means.

#### LXXXV.

# South Germany. - Stuttgard.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						De	grees of	Reaum	ur.					
	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
		0	0	0	0	0	0	0	0	0	0	0	0	
11	1792	0.64	-1.23	1.78		-1.12		1.04	1	-0.70	1.30			1792
11	1793	-1.41	1.64	0.37	-1.36	1	-0.31	2.52	1	-0.84	1.71	0.66	2.10	1793
15	1794	2.02	3.72	2.76	3.26	0.41	1.30	2.75		-1.34	0.32			1794
11	1795	-4.88	0.36	0.65	2.81	0.64	1.43	-1.01	1.33	1.93	}	-0.49	3.76	1795
1	1796	6.17	1.90	-2.51	-0.67	-0.32	0.10	-0.36	0.23	2.34	0.13	-0.87	-2.18	1796
.	1797	2.46	0.08	-0.27	1.88	1.16	-1.30	2.86	1.01	1.04	0.36	1.82	3.02	1797
11	1798	0.65	1.44	0.69	1.16	0.66	1.21	0.14	0.66	i	0.53		-2.05	1798
ш	1799	-3.46	1.77		-1.30		-0.75	-0.98	0.32	-0.04			-4.70	1799
1	1800	3.03	-0.92		4.56	2.03		0.00	0.79	0.84	-0.37	1.61		1800
11	1801	3.95	0.97				-0.54	0.91	1.42	2.32	2.89	1.30	1.46	1801
				-		0.0.	0,01					1.00	1.10	1001
11	1802	H	-0.02	0.80		0.23		-0.24	2.22	0.62	2.08	0.81	1.41	1802
11	1803		-1.90		1.49	1	0.05	1	1.28		-0.90	0.46	1.36	1803
11	1804	11		-1.05		0.78	1	-0.35	Į.		0.74	0.56		1804
11	1805		-0.28	-0.60		-2.16	-1.35		-1.44		<b>-2.7</b> 3	-2.47	0.06	1805
	1806	-2.78	2.77	1.10	-1.99	1.37	-0.27	-0.62	-0.59	[-0.27]	0.03	1.67	4.85	1806
.	1807	0.76	1.58	-2.43	-1.14	-1.02	-0.21	2.15	3.23	-0.74	1.71	1.37	-0.94	1807
11	1808	1.95		-3.55			-0.98	0.54	1		-1.49	l .		1808
11	1809	1.56	3.64	1	-2.58		-0.65				-1.05		2.12	1809
11	1810	-1.56	-2.45	2.11	ł .	-0.25		i	-0.48	2.08	0.09	1.44	0.97	1810
11	1811	-3.01	0.49	2.31	0.97	1.41	1.41		-0.38		3.02	1.28		1811
11	1812	-2.36		-0.23	i .	0.64		1		-0.49		-2.28	1	1812
31	1813	-2.25		-0.42						-1.63				1813
- 11	1814	11		-3.67		-2.14				-1.56			í I	1814
11	1815	-1.92	1.26	2.15		0.71		-1.95				-2.30	1	1815
	1816	0.69	-2.37	-0.60	-0.68	-2.22	-2.63	-2.45	-2.34	-0.85	-0.17	-2.45	-0.82	1816
	1817	3.31	1.47	-0.71	-3.71	-1.78	0.92	-1.54	-0.97	1.08	-3.25	1.01	-0.49	1817
	1818	2.67	0.40			-0.82	1.06	0.15	-0.91	-0.70	-0.91	1.62	-2.04	1818
	1819	-0.61	1.54	0.89	1.21	0.29	0.36	1.02	0.36	-0.92	-0.02	-0.95	1.16	1819
	1820	-1.64	-0.06	-2.16	1.31	-0.05	-1.91	-1.37	1.10	-1.84	-1.11	-2.81	-0.66	1820
	1821	2.13	-2.72	0.19	1.52	-1.98	-2.26	-1.97	0.15	0.77	-0.62	2.42	3.25	1821
1	1822	2.11	1.58	2.61	0.51	1.43	2.90	0.00	_0.05	-0.48	1.33	1.82	-3.09	1822
11	1822 1823	-2.76	1.35		1	0.92		-1.19		-0.48 -0.38	-1.03		1.70	1823
11	1823 1824	0.79	0.79	-0.89		-1.05			-0.39	0.68	0.44	$\frac{-1.37}{2.52}$	3.81	1823
11	1824 $1825$	1.92	-0.37	-1.36		0.27	0.26	0.30	0.02	-0.61	-0.64	1.27	2.74	1825
11	1826	-4.81	1.06	1.16	0.19	-0.93	0.54	1.70	1.78	1.51	1.43		0.54	1826
	1020	7.01	1.00	1.10	0.13	0.00	0.04	1.10	1.10	1.01	1.40	1.07	9	1020
	100=	0 10	- 02	1 /-	1.00	1.00	0.00	1 10	0.45	0.00	0.0-	9.77	0.00	100
11	1827	11	-5.36	1.47	1.22	1.60	0.23		-0.45	0.08		-2.41	2.98	1827
11	1828	11	-0.35	0.61	0.54	0.43	0.97		-1.10	0.07			1.19	1828
	1829	-2.45	-3.10	-0.58	0.46	-0.36	-0.61	0.45	-1.13	-1.50	-1.06	-2.88	-5.91	1829

#### LXXXV.

### South Germany. - Stuttgard (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1830	-6.40	-3.47	1.62	2.06	0.90	-0.38	1.05	0.00	-1.43	-0.89	0.90	-0.74	1830
1831	-0.73	1.25	1.68	1.44	-0.11	-0.09	1.22	-0.10	-1.15	2.92	0.15	1.26	1831
1832	0.10	-0.76	-0.64	0.13	-0.93	-0.59	-0.22	0.75	-1.05	-0.78	-1.41	0.05	1832
1833	-2.56	2.99	-0.99	-1.31	3.38	2.06	-1.46	-2.81	-1.35	-1.03	-0.13	3.18	1833
1834	5.05	0.14	-0.60	-1.87	2.16	1.33	2.74	0.90	1.73	-0.06	0.12	-0.27	1834
1835	1.53	1.20	-0.15	-0.90	-0.53	0.28	1.62	-0.21	0.60	-1.20	-3.22	-2.85	1835
1836	0.45	-1.27	3.18	-0.90	-2.14	0.64	0.22	0.46	-1.21	0.47	-0.01	1.04	1836
1837	0.90	0.24	-2.68	-2.84	-2.23	1.16	-1.19	1.17	-1.94	-0.60	-0.40	0.04	1837
1838	-4.43	-2.08	0.21	-2.32	-0.45	-0.03	-0.36	-0.90	0.64	-0.36	1.03	-1.34	1838
1839	0.78	-0.03	-1.31	-2.71	-1.07	2.30	0.58	-1.55	0.64	0.84	1.07	1.95	1839
1840	1.82	0.15	-2.90	1.36	0.29	0.16	-1.42	-0.23	-0.26	_2.39	1.10	-5.61	1840
1841		-1.98	2.09					-0.69			i		1841
1842	-1.50			-0.47		1.74				-2.47			1842
1843	2.07	1.54	0.15		-1.06				-0.15	0.02			1843
1844		-0.91	-0.30		-1.01			-2.17				-3.18	1844
Means.	-0.80	1.64	3.97	7.80	11.87	14.03	15.48	15.02	12.05	8.05	4.11	1.25	Means.

# LXXXVI. South Germany - Carlsruhe.

1779	-3.98	1.18	1.26	2.19	1.14	-0.64	0.80	1.72	2.40	2.75	1.71	2.94	1779
1780	-2.23	-2.20	3.27	-1.17	0.52	0.41	0.27	1.39	0.18	0.83	0.00	-1.32	1780
1781	0.45	1.82	0.99	2.26	0.87	1.63	0.63	1.20	1.11	-0.94	-0.38	1.09	1781
1782	3.13	-3.95	-0.67	-1.10	-1.44	0.93	1.00	-1.62	-1.69	-2.08	-3.90	-1.07	1782
1783	3.33	1.35	-1.60	0.05	-0.14	0.47	1.69	-0.38	-0.71	-0.35	-1.04	-3.26	1783
					0.10	0.70	0.10		0.00			2	
1784			}		l		-0.48						1784
1785	-0.27	-3.06	-5.49			1	-0.46		• •		-0.63		1785
1786	• •			0.76	-1.35	1.20	-1.77	• •	• •	-1.97	<b>-3.13</b>	-0.18	1786
1788							• •		• •		• •	-8.65	1788
1789	-0.91	1.74	-3.15		2.19	-1.49	0.34	-0.14	-1.17			0.91	1789
1798							0.20	0.39	0.59	0.55	0.14	-1.90	1798
1799	-3.09	0.92	-0.59	-1.15	-1.43	-0.70	-0.60	0.20	0.01	0.12	-0.12	-4.22	1799
1800	2.53	-1.60	-2.25	3.40	1.46	-2.10	-0.26	1.20	0.89	-0.43	1.15	0.21	1800
1801	3.13	0.68	1.95	0.32	0.98	-0.98	-0.15	-0.49	0.76	0.98	1.17	2.21	1801
1802	-2.69	0.64	0.83	1.08	-0.60	1.37	-0.97	2.33	0.23	1.38	-0.38	0.53	1802
		0.00					0.00			0.00	0.50	7.00	1000
1803	H		1		1		0.63	1			1	_	1803
1804	ll .			1			-0.56	1	1	0.90	1	-2.05	1804
1805	-1.49	-0.61		1	i		-1.21					-0.39	1805
1806	4.11	1.89	0.58	-2.23	1.41	-0.09	0.03	-0.35	-0.36	-0.67	1.62	4.71	1806

### LXXXVI.

### South Germany. — Carlsruhe (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees or	Reaum	u1.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1807	0.02	1.11	-2.83	-1.34	1.19	-0.28	2.34	3.15	-1.57	1.30	1.21	-0.53	1807
1808	1.38	-1.25	-3.54	-1.63	2.40	-0.41	1.94	0.96	-0.54	-1.28	-0.24	-3.75	1808
1809	1.24	3.25	0.52	-3.16	0.41	-1.22	-0.61	-0.33	-0.80	-1.36	-1.90	1.60	1809
1810	-3.19	-2.78	1.26	-0.17	-0.60	-0.62	-0.65	-0.46	1.58	-0.05	0.84	1.69	1810
1811	-2.40	1.17	2.79	1.65	2.32	1.55	0.78	-0.29	0.53	2.92	1.21	0.48	1811
1812	$  _{-2.09}$	1.17	-0.16	-2 06	0.83	_0.50	-1.53	_0.27	_0.24	1 22	-1.42	-3 80	1812
1813	-0.84	2.15	0.57	1.50			-1.75		1	i	-0.11	-0.89	1813
1814	-1.51	-3.24	Į.	1.82		-1.66			-1.07	1		2.67	1814
11	-2.35	1					-1.75				-1.99	1 1	
1815	11	2.31	2.67	0.75			í		1		1	0.17	1815 1816
1816	1.38	-2.00	-0.27	0.27	-2.23	-2.48	-2.61	-2.10	-0.39	<del>-</del> 0.33 	-2.14	0.17	1510
1817	3.56	2.16	-0.36	-3.14	-1.63	0.87	-1.47	-1.40	1.60	-2.82	1.78	0.13	1817
1818	2.91	1.12	0.59	1.53	-1.44	1.00	0.34	-1.01		-0.63	1.49	-2.11	1818
1819	1.85	1.30	0.75	1.42	0.49	0.15	0.42	0.64		-0.15	-0.75	0.31	1819
1820	-1.09	0.55	-1.35	2.19	0.22		-0.96	0.66		-0.61	-1.80	0.00	1820
1821	2.31	-1.59	0.73	1.78	-1.87		-2.03	0.14	0.17	-0.68	2.72	3.52	1821
1021				2.,,									
1822	2.52	2.96			2.11			-0.14	0.46	1.19		1 1	1822
1823	-2.23	2.20		-0.09	1	4	-1.14	0.87	0.24	-0.27	-0.11	2.95	1823
1824	1.39	1.98	-0.10	-0.89	1	-0.65	0.32	-0.22	1.04	0.66	2.68	4.09	1824
1825	1.92	0.28	-0.76	1.43		-0.41	0.85	0.49	1.15	0.15	1.51	3.05	1825
1826	-3.48	1.35	1.13	0.20	-1.25	1.06	2.12	2.86	1.75	1.94	-0.21	0.93	1826
1827	-0.55	-5.10	1.19	1.50	1.25	1.01	2.06	0.00	1.15	1.34	-2.01	2.85	1827
1828	3.18	0.41	1.17	0.82	0.74	1.19		-1.22	0.48		-0.33	1.85	1828
1829	-2.12		-0.05	0.72	_	0.21			-0.88		-1.88		1829
1830	-5.83	-2.98	2.14	2.21	0.81	3	0.86	-0.13	1	-0.17	1.31	-0.32	1830
1831	-0.98		1.68	1.83	1	-0.61	0.38		-0.81	3.26	0.30	1.64	1831
1001	0.00	0.00	1.00	1.00	0.00	0.01	0.00	0010	0.01	0.20	0.00	1.01	1001
1832	0.10		0.23		-0.88	ł	-0.01		-0.59	ł .	-0.68	0.95	1832
1833	-2.63	3.41		-0.78			-1.24			1	0.51	4.43	1833
1834	5.74	0.29	1	-1.12	1.87	1.12	2.76	1.35		0.53	0.79	0.29	1834
1835	1.77	1.74	1	-0.90		0.13	1.46	-0.17	-0.03	-0.83	-2.92	-2.23	1835
1836	0.43	-0.85	3.27	-0.66	-1.99	0.47	0.21	0.47	1.67	0.82	0.66	1.56	1836
1837	1.30	0.80	-1.86	-2.33	-2.05	1.26	-0.86	1.24	-1.66	0.28	0.46	0.72	1837
1838	-4.35	-2.13		-2.36			-0.36	-1.24	0.44	-0.02		-0.52	1838
1839	0.88	0.67	1			2.28	0.16	-0.47	0.09	1.20	1.49	2.20	1839
1840	1.37	-0.69			1	0.23	-1.39	0.34	-0.22	-2.04	1.81	-5.32	1840
Means.	-0.17	1.95	4.39	8.31	12.40	14.43	15.80	15.41	12.60	8.30	4.16	1.35	Means.
	1										l		

# LXXXVII.

# NORTH GERMANY. - BERLIN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Keaumi	ır.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
7570	0	0	0	0 00	0	0	0	0	0	0 00	0	0	1770
1719	2.44	0.21	1.50	0.69	1.45	2.38	3.13	1.86	0.08	0.66	2.09	-1.02	1719
1720	2.27	0.40	-0.14	0.70	1.34	0.94	2.01	0.31	0.10	1.62	-0.03	1.47	1720
1721	2.38	-1.80	-1.53	2.23	-0.91	1.21	-0.67	-0.17	0.54	0.40	1.69	0.07	1721
1728	1.50	-2.28	2.39	0.65	1.24	0.26	-0.38	-1.36	-0.10	0.66	-0.58	-1.51	1728
1729	-3.18	-1.46	-3.57	-2.11	• •	• •	• •	• •	• • •	• •	• •	• •	1729
1730	1.64	0.20	0.29	0.70	0.00	0.12	-0.62	-0.03	-0.69	-2.55	1.99	-0.48	1730
1731	-2.00	-1.78	-0.67	-1.67	-1.33	-0.89	-1.44	-0.62	-0.25	1.85	0.67	0.26	1731
1732	-1.50	1.34	1.05	1.34	0.29	-1.54	-1.95	-0.98	-0.84	1.14	-0.78	-3.99	1732
1733	2.69	2.54	0.86	1.59	-1.77			-0.97	-2.02	-0.53	0.21	2.46	1733
1734	0.40	2.51	1.86	0.55		-1.26				0.65	-2.85	-1.03	1734
1735	1.79	0.30	1.81	1.49		-0.33		-0.84	0.91			-0.17	1735
1736	-0.08	-0.92	-0.73	0.85		-0.87		0.64			-0.09	1.18	1736
1737	1.83	0.55	1.57	-1.36	0.77		-0.77	-1.65		-0.39		1	1737
1738	-0.55	0.55	1.11	1.54	-0.08	-0.42	-0.79	-0.38	-0.05	0.88	-2.21	0.90	1738
1739	-0.17	2.06	1.11	-1.65	0.64	-0.96	0.99	-1.23	0.91	-2.62	-5.35	-0.01	1739
1740	-6.61	-6.54	-3.28	-3.45	-3.49	-1.70	-0.96	-0.62	1.62	<del>-3.12</del>	-2.35	-0.18	1740
1741	-0.93		-0.71	-1.38		-1.59		-0.54		1.22	1	-0.16	1741
1742	-1.23	1.08	-0.99	-2.16	-1.83	i .	-0.66	1	-1.78	0.19	0.70	1 1	1742
1743	1.32	0.99		-1.94	0.28	1.05	-1.46	1		-1.44	2.77	0.84	1743
1744	-1.98	-2.42	-0.09	2.33	0.10		0.25		0.94	2.10	1.25	1	1644
1,11	1.00	2.42	-0.03	2.00	0.10	1.11	0.20	0.00	0.04	2.10	1.20	0.05	1044
1745	-1.92	-1.26	-0.10	0.20	0.73	1.01	0.01	0.17	0.10	1.15	2.17	-2.36	1745
1746	0.12	0.03	-1.88	-0.39	0.43	-0.72	1.41	-0.43	0.44	-1.06	-0.53	1.89	1746
1747	-0.17	3.49	-2.09	0.70	-0.67	2.34	-0.33	0.18	1.43	0.43	0.21	1.04	1747
1748	-1.17	-1.70	-2.29	0.22	1.53	2.11	0.56	2.85	-0.14	0.00	1.79	3.19	1748
1749	2.28	0.47	-1.52	-0.14	1.58	0.21	0.39	1.64	0.33	0.05	-0.63	1.28	1749
1750	1.19	3.22	3.87	1.26	0.30	1.06	1.97	1.56	0.26	-0.55		-0.06	1750
1751	-0.45	-1.70	2.79	-0.86	3.59	2.39	1.78	3.12	0.42	-0.04	• •	• •	1751
Means.	-0.19	0.69	2.65	6.51	10.63	12.82	14.02	13.14	11.06	6.53	3.15	1.24	Means.
1755	-4.56	-6.47		0.54				-0.25				2.14	1755
1756	4.13	2.63	1	1.77	0.37	2.55		-0.35	1.61			-1.43	1756
1757	1.17	2.37	1.71	1	-0.39	1.47	3.25	0.33		-2.88	1.21	-1.25	1757
1758	-2.57	-0.17	0.13	-0.21	1.08	0.18	-0.86	0.55		-0.97	0.16		1758
1759	3.26	1.79	1.18	-0.01	-1.45	0.13	1.15	0.60		1.09		-3.85	1759
1,00	0.20	1.75	1.10	0.01	1.40	0.01	1.10		0.40	1.00	2.21	0.00	1.00
1760	-0.56		-0.81	0.34	0.33	0.57		0.03	0.87	0.98			1760
1761	0.97	1.65		-0.01	1.55	1.95	i .	1.88	2.30			-3.08	1761
1762	2.11	-0.01	-1.88	1.88	0.42	0.27	-0.19	-1.45	0.23	-1.34	-0.32	-1.82	1762
1763	-2.25	3.02	-0.40	-0.55	-0.34	0.17	0.92	1.32		-0.87	1	1	1763
1764	2.91	2.88	-0.10	-0.30	1.71	-1.94	1.43	-0.60	-1.70	-0.63	-1.32	-1.54	1764
1765	1.64	-2.90	1.70	0.78	-2.50	-0.88	-1.92	1.12	-1.16	1.20	0.15	0.03	1765
1766	-0.10		1	2.07	1.17	I	-0.36	l .	0.73	-0.43		-0.26	1766
1767	-5.54			1	-1.03			1	0.42	0.95		-1.75	1767
		1	10.01	1	2.00		1	, , , ,					

### LXXXVII.

# NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						51000 01	Reaum						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1768	-3.52	-0.98	° -1.25	°	-0.68	° -0.06	° 0.28	-0.0s	° -1.03	0 -0.48	o 0.54	0.47	1768
1769	1.22		0.75	0.14				-1.07	0.58	-2.26	0.26	0.84	1769
1770	-0.20		-3.16		-0.11			-0.08	0.62	0.81	0.16	1.92	1770
1771	-1.24	-3.28	-3.40		1	-0.21			-0.46	0.76		0.95	1771
1772	0.66	1.20	0.86			-0.10	-1.40		0.60	1.62	1.89	1.38	1772
1773	2.50		-0.61	0.49		-1.22		0.06	0.57	1.89		2.21	1773
Means.	-0.13	1.64	3.87	7.71	11.94	15.23	16.18	15.34	12.12	7.73	4.38	1.85	Means.
1774	1.50	2.26	2.29	1.56	-0.05	0.69	-1.56	-1.92	-1.61	0.71	-3.70	-0.75	1774
1775	0.95	3.20	2.53	-0.65	-0.72	3.26	1.88	1.61	2.00	1.23	-0.84	2.16	1775
1776	-5.55	2.42	2.10	-0.13	-2.11	1.19	1.21	0.32	0.12	-0.47	0.70	0.54	1776
1777	0.04	-1.67	0.67	-1.12	0.52	0.04	-0.60	-0.01	-1.71	0.23	2.23	0.75	1777
1778	-0.58	-1.72	1.09	1.98	0.67	0.30	1.02	0.66	-0.67	-1.69	1.44	3.84	1778
1779	0.33	3.82	2.99	2.39	0.61	-0.30	0.74	1.71	1.59	1.95	0.90	2.26	1779
1780	-1.06	-2.02	3.37	-1.27	0.72	0.24	0.45	0.99	-0.03	1.46	-0.34	-0.70	1780
1781	-0.44	0.53	2.05	1.85	1.19	1.97	2.02	2.56	1.60	-0.39	0.80	0.01	1781
1782	3.15	-2.86	-0.39	-0.87	0.33	1.78	1.52	0.21	1.75	-0.30	-1.13	0.78	1782
1783	3.19	3.67	-0.58	0.86	1.38	2.71	1.45	0.71	0.36	0.34	0.50	-1.51	1783
1784	-3.97	-3.54	-1.68	-2.30	0.58	0.20	-0.75	-1.35	0.02	-2.21	1.29	-0.94	1784
1785		-3.28		-2.54	į.		-0.70		0.61	1	1.09		1785
1786	1.81	-0.93	-2.32	1.60		i	-1.71	-1.26	-1.S6	į.	-3.64	1 1	1786
1787	-0.29	1.38	2.05	-1.31		0.99	1	-0.59		1.32	0.69	1 1	1787
1788	2.46	-1.26	-1.47	0.10	0.45	1.64	1.64	-1.21	1.20	i	-0.79		1788
1789	-1.93	1.46	-4.45	0.01	1.85	0.14	0.11	0.36	1.85	0.64	0.89	3.55	1789
1790	3.05	2.82	2.19	-1.67	1.70	0.58	-1.13	-0.54	-0.48	-0.44	-0.30	1.92	1790
1791	3.91	1.52	1.47	1.74	-1.16	0.19	0.78	1.08	-0.78	0.22	-0.89	1.35	1791
1792	0.53	-1.89	0.80	1.45	-0.81	0.83	1.59	0.46	-0.98	-0.30	-0.01	1.14	1792
1793	-0.70	2.14	0.61	-0.68	-0.58	-1.34	1.68	0.22	-0.83	1.99	0.99	2.05	1793
1794	1.18	2.56	3.66	3.12	0.18	1.77	2.79	-0.59	-1.62	0.37	1.53	-2.14	1794
1795	-5.23	-0.36	-0.84	2.88	-1.78	2.10	-0.92	-0.37	1.27	3.36	0.10	3.14	1795
1796	6.51	0.68	-1.70	-0.34	-0.46	0.38	0.48	1.33	1.74	0.07	-0.60	-1.82	1796
1797	1.60	1.89	0.66	1.09	1.41	-0.23	1.55	1.26	2.02	0.55	-0.80	1.81	1797
1798	1.79	1.57	-0.07	1.29	0.76	1.20	0.38	0.92	1.24	-0.17	-0.45	-3.54	1798
1799	$  _{-2.97}$	-4.47	-1.65	-2.12	-2.27	-1.53	-1.05	-0.32	-0.65	-0.70	0.48	-4.41	1799
1800	11	-3.61	1		i	-3.06		0.22	i	-0.41	1.47	0.00	1800
1801	1.88		1.84	1	1	-1.37	1	-0.68	1.01	1.40	0.93		1801
1802	-1.00		1.65		1	-1.01	1	1.54	1	3.04	0.78	1.81	1802
1803	-5.33		1	1		-1.46	1	1.80	1	-0.45	0.68		1803
1804	1.51		-3.11	1		-0.54		-0.73		-0.02		1	1804
1805	И	-1.94	1	-1.58		1	-1.18	1	0.55		-2.58	1.24	1805
1806	3.02		1	-2.82			-1.35	1	0.41	-0.12	1.47	4.14	1806
1807	1.62	0.18	-1.97	-1.43	-0.42	-1.50	0.42	3.72	-2.15	0.08	1.11	1.53	1807
-													

#### LXXXVII.

# NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees or	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1000	0	0	0	0	0	0	0	0	0	0	0	0	1000
1808	0.83			-2.80		-0.42				-1.56		1	1808
1809	-3.31	1.64		-3.34		-0.89		0.36		-0.99	0.02	2.23	1809
1810	-0.99	-1.66		-1.41			-0.05			-1.33	0.09	1.22	1810
1811		-0.72		-0.15	3.07	2.67	1		-0.72	2.21	0.35	1.50	1811
1812	-1.14	-0.27	-1.05	-3.98	-1.20	-0.68	-2.37	-0.78	-1.81	1.14	-1.57	-5.52	1812
1813	-1.20	2.38	0.24	1.00	-0.73	-1.23	-1.27	-2.07	-0.82	-1.30	0.05	1.02	1813
1814	-2.12	-5.52	-2.78	1	-2.92	ł			-2.23	-1.21	0.55	1.26	1814
1815	-2.81	1.14		-0.45		0.61	1	-1.57		0.42		-1.37	1815
1816	0.95	-2.27	-0.68			-1.54		-2.59	1	-1.23	1		1816
1817	2.58	1.79		-3.86	1	1.04		-0.55	1	-2.57		1	1817
1011		1	0.10	0.00	0120	1.01	1.0.	0.00	1.10	2.01		0022	1011
1818	2.54	0.19	1.56	0.53	0.22	0.95	0.72	-1.41	0.14		-0.60		1818
1819	2.51	1.57	1.59	0.85	1.00	2.28	1.42	1.60		-0.41	1	-2.61	1819
1820	-3.08	0.34	-0.02	1.52	0.91	)	-2.08	1.23		0.99		-1.88	1820
1821	1.52	-1.05	0.14	3.28	-0.48	-2.17	-1.51	<b>-0.7</b> S	0.91	1.33	3.27	3.44	1821
Means.	-1.59	0.30	2.28	6.89	11.36	13.73	15.16	15.00	11.83	7.16	2.61	-0.32	Means.
1822	3.39	3.67	3.22	1.55	0.59	0.58	0.77	-0.19	-1.24	1.36	1.58	-3.18	1822
1823	-7.56	-0.25	0.41	-1.32	-0.26	-0.78	-1.76	1.03	-0.34	0.66	1.01	1.12	1823
1824	3.67	2.45	0.29		-1.04		-0.56	-0.58	1.27	0.56	1.96	2.69	1824
1825	3.92	0.92	-2.26	0.86		-1.10	-0.47	0.05	0.54	-0.12	1.30	1	1825
1826	-3.44	1.98		-0.19	1	1.20	3.03	3.00	0.35	0.71	-0.33	1	1826
1000	0.05		,	2 20	7.00	1.00	0.00		7.00	0.00		7.70	1000
1827	0.25		1.25	2.29	1.98	1.33		-0.04	1.09	0.83		1.16	1827
1828	l .	-0.55	0.67	1.22	0.33	0.30		-0.71	1	-0.28	0.17	0.47	1828
1829		-2.67	-1.23	0.41	-0.29	0.12		1	-0.16	-1.62	1	-8.25	1829
1830	-4.21	-2.70	1.09	1.53	0.30	0.07		-0.26		-0.69	1.47	-1.79	1830
1831	-1.81	0.75	0.40	2.21	-0.94	-1.34	0.36	0.20	-1.22	1.77	-0.54	0.11	1831
1832	0.76	1.12	0.42	0.32	-1.43	-0.33	-2.40	0.22	-1.22	-0.35	-0.63	-0.24	1832
1833	-0.86	3.16	-0.18	-1.82	3.46	1.33	-0.45	-3.12	-0.48	-0.93	0.14	2.48	1833
1834	4.73	1.31	1.00	-0.68	1.82	1.23	3.65	2.34	0.74	-0.28	0.56	0.36	1834
1835	2.81	2.37	0.57	-0.91	-0.86	0.13	0.21	-0.59	1.22	-0.97	-2.71	-1.77	1835
1836	1.37	1.11	3.42	0.07	-2.55	0.20	-1.08	-1.49	-1.06	1.00	-1.10	0.26	1836
1837	1.01	0.38	_1 00	-1.68	-1.42	0.60	-1.11	1.20	-0.92	0.37	0.70	-0.87	1837
1837	$\begin{vmatrix} 1.91 \\ -6.30 \end{vmatrix}$	-3.63		-1.68 $-1.42$	-0.24		-0.22	-1.78	1.27	-0.89	-1.14		1838
1839	0.79	1		-1.42 $-2.54$		0.35			1.27	0.15		-0.55	1839
11 1	1	1.50			0.58 -0.03			-0.44 $-0.07$		0.15		-0.33	1840
1840 1841	-0.09 -0.01	0.65 $-4.03$	0.23	-0.07 1.01	2.51	0.16	-1.10		0.58	1.29	0.75	1.62	1841
1341	0.01	4.03	0.91	1.01	2.01	0.00	1.10	0.01	0.00	1.40	0.13	1.02	1041
1842	-1.34	0.39	0.93	-1.52	0.75	-0.54	-0.84	3.13	0.42	-1.55	<b>-2.</b> 82	0.71	1842
1843	2.40	2.45	-1.09	0.44	-2.01	-1.00	-0.41	1.17	-0.64	-0.66	1.42	1.96	1843
1844	1.00	-0.96	-1.50	0.48	0.56	-1.00	-2.35	-1.60	0.36	-0.24	0.56	2.41	1844
1845	1.65	-4.55	-6.24	0.28	-1.48	0.49	0.90	-0.94	-0.93	-0.18	1.26	0.33	1845
Means.	-1.90	-0.15	2.74	6.88	10.92	13.94	15.04	14.43	11.75	7.97	3.25	1.32	Means.

### LXXXVIII.

# Denmark. — Copenhagen.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.   Jan.   Feb.   March.   April.   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Year.						De	grees of	Reaum	ur.					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1768		0	0	0	0		0		0	0	0	0	0	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	ii .	11	1		1			1		1	1			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				1		1			1	1			1.66	1768
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	i	11	1		1		i			1		1	0.37	1769
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1770	0.19	1.64	1	-0.77	-0.32	-0.88	0.21	0.36	1.11	1.38	-0.48	0.69	1770
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1771	-1.20	-2.18	-3.96	-3.14	0.27	1.50	-0.33	-2.04	-0.90	0.03	-1.11	1.10	1771
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7000	0.00	7 111	0.50			0.57		0 =0		1 40	2 20		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				1			1	1		1		l .	-	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		- 11				1			4	1			1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11	1		Į.		í		4				1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$											1	1		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1776	-5.22	1.18	1.49	0.73	-0.87	1.61	2.30	1.35	0.59	0.67	0.77	0.69	1776
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		-												
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1782	2.38	-0.61	_0.90	-0.62	-0.63	3.43	0.12	0.32	0 90	-1.09	-1.49	0.07	1789
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	- 11							1					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	- 14							i .	1		1		1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11	1											
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11	1					i		1			1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1,00	0.15	0.00	2.03	0.00	1.00	1.40	-0.55	0.41	0.14	-1.21	-2.31	-0.04	1700
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1787	0.94	2.21	2.09	-0.20	0.07	0.01	0.06	-0.31	0.58	1.81	-0.40	0.26	1787
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1788	2.02	0.63	-1.14	0.95	1.00	1.28	-0.93	0.38	1.71	-0.31	-0.19	i	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1798	1.15	2.27	1.31	2.48	2.71	2.06	2.00	2.15	1.09	1.01	0.01		1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		- 11		1	-1.59		-0.44							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1800	-0.96	-2.07	-3.57	2.60	1.77	-1.69	-0.89	0.42					! !
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1801	1.28	0.75	2.82	1.44	2.93	-0.10	1.30	0.58	0.69	2.17	1.97	0.46	1801
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1802	-0.56	1.04	1.90		-1.78	-2.26	-3.12	-0.56	-0.87	0.98	0.45	0.32	1802
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1803	-3.02	-1.58	-0.39	1.86	-1.69	-2.02	-0.21	-0.14	-1.76	-0.90	-0.31	-1.36	1803
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1804	2.01	-1.47	-1.82	-0.58	0.25	-0.57	-0.30	0.12	1.23	0.77	-1.74	-2.85	1804
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1805	-1.79	-2.02	0.26	-1.03	-2.14	-3.46	-1.48	-1.03	0.77	<b>-2.</b> 53	-0.56	0.77	1805
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													Ì	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11						1					- 1	l l
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1.75			1		i	-0.17	2.54			0.19	0.77	1807
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1808	1.04						1.26	1.34	1.10	-0.14	-0.85	-2.42	1808
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	į.			1				1			1	-0.23	1.65	1809
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1810	0.60	-0.28	0.05	-1.19	-2.69	-1.01	-0.07	-0.29	0.51	-0.79	-0.22	0.10	1810
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									- 1			1	1.07	1811
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		- 11		1			- 1		- 1			1	-3.56	
1815   -0.67   1.47   1.82   0.30   -0.26   -1.26   -1.95   -0.81   -1.11   0.59   0.20   -0.66   1815			2.66		1		-1.00	0.44	-0.89	-0.53	-2.01	0.20	0.97	1813
		- 11	1										0.85	1814
1816 0.72 -1.56 -0.05 -0.49 -2.69 -1.87 -0.49 -1.86 -0.89 -0.72 -0.95 -0.31 1816	1815	-0.67	1.47	1.82	0.30	-0.26	-1.26	-1.95	-0.81	-1.11	0.59	0.20	-0.66	1815
1816   0.72 -1.56 -0.05 -0.49 -2.69 -1.87 -0.49 -1.86 -0.89 -0.72 -0.95 -0.31   1816														
1816   0.72 -1.56   -0.05   -0.49   -2.69   -1.87   -0.49   -1.86   -0.89   -0.72   -0.95   -0.31   1816	7010	0.50	7.50	0.05	0.10	0.00	1.05	0.10	7.00	0.00	0.70	0.00	0.53	
	1816	0.72	-1.56	-0.05	-0.49	-2.69	-1.87	-0.49	-1.86	-0.89	-0.72	-0.95	-0.31	1816

#### LXXXVIII.

### DENMARK. - COPENHAGEN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
101#	0 70	0	0	0 .	0	0	0	0	0 00	C	0	0	1015
1817 1818	2.79 1.99	2.98 1.73	i	-1.10 -1.05			-1.53 1.29		0.62	-2.24	1.41		1817
1819	3.46	2.30	2.39	1.56	1.25	1.69		1		0.87 $-0.79$	1.48 -1.03		1818 1819
1820	-1.67	0.51	0.52	1.55	0.25		-0.36	)	-0.60		-0.56	- 11	1820
1821	0.36	0.16	0.32					-0.86		1.62	1.68	2.47	1821
1021	0.50	0.10	0.21	2.21	0.10	1.11	1.01	0.00	0.07	1.02	1.00	21.21	1021
1822	2.56	3.82	3.64	2.28	1.59	0.87	0.24	-0.17	-0.64	1.52	2.63	0.56	1822
1823	-2.60	-0.08	0.70	-0.04	0.51	0.15	-0.94	0.41	0.47	1.02	1.88	1.74	1823
1824	3.65	2.36	0.97	0.91	0.14	1.22	-0.61	-0.48	1.62	0.09	1.20	2.18	1824
1826					4.30	5.91	7.76	6.63				2.04	1826
1827	0.16	-2.30	0.59	2.14	1.44	1.93	0.09	-0.29	1.48	1.16	-1.20	2.30	1827
1828	-0.07	0.43	1.37	0.58	1.31	1.34	1.36	0.26	0.41	0.46	0.61	0.50	1828
1829		-3.06	-0.95	-1.00	1.84			-1.01			-2.91		1829
1830	-2.26	-2.85	1.39	0.69	-0.18	-0.86	0.30	-0.81	-0.95	0.15	1.75	-0.22	1830
1831	-1.60	0.61	-0.16	1.87	0.31	0.85	2.52	1.55	-0.59	2.71	-0.65	1.91	1831
1832	1.52	1.73	1.55	1.84	-0.23	1.29	-0.94	-0.06	-0.98	0.60	-0.47	0.58	1832
1833	0.05	1.50	-0.45	-0.72	2.32	0.72	0.79	-2.27	0.08	0.63	0.77	1.32	1833
1834	2.26	1.71	2.23		1.98	0.72	1		ľ	-0.05		0.59	1834
1835	1.87	2.16		-0.02		1.17	1		;	-0.85	-1.44		1835
1836	0.29	0.63			-0.17		-0.89	1	1		-1.34		1836
1837	0.17	0.54		-1.50		ł .	-0.21	1			-0.91		1837
1838	-2.83	-4.85	-0.56	-2.63	-0.97	-0.70	-0.09	-2.25	-0.44	-1.82	-2.01	-0.25	1838
1839	1	-0.38	1	-2.80			1	4			-0.19		1839
1840	i i	-0.39				1	1				-0.51		1840
1841		-2.52		0.62			i	J.	1		-0.36	) [	1841
1842	-0.26	1	2.05	0.61			-0.99		1	-0.88		2.36	1842
10.2	0.20	11.10		0.01					0.01	0.00	2.01		
1843	1.82	0.79	-0.33	0.46	-0.96	-0.25	-0.67	1.03	-0.20	-1.23	0.86	2.99	1843
1844	1	1	-1.50	0.74			-2.17		-0.62			-1.43	1844
1845			-4.45		-1.01	0.20	1		-1.26		1.28	1	1845
Means.	-1.16	-0.80	0.55	4.45	8.98	12.45	13.81	13.50	10.86	7.05	3.12	0.68	Means.

### LXXXIX.

### France. — Paris.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	egrees o	f Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1806	3.35	1.38	0.28	-1.54	2.07	0.77	0.64	-0.38	0.53	-0.26	1.69	4.00	1806
1807	0.34	1.39	-2.74	-0.63	1.28	-0.52	1.94	2.34	-2.08	1.15	-0.74	-1.75	1807
1808	0.42	-1.42	-2.19	-2.23	2.55	-0.30	2.14	0.66	-0.78	-1.74		-1.87	1808
1809	2.95	2.91	0.42	-2.72	0.54	-1.38	-1.08	-0.36	-0.81	-1.09	-1.54	1.04	1809
1810	-2.90	-1.11	1.16	-0.42	-0.62	-0.06	-0.74	-0.70	1.75	0.25	0.80	1.30	1810
1811	-1.83	2.31	1.90	1			l .	-0.66		2.55		0.72	1811
1812	-0.32	l .	-0.82	-1.92	1	l .	-0.96		ì	0.51	Į.	i I	1812
1813	-1.18	1.33		0.71	1	l .	-1.12	1	l .	l	-0.63	-0.47	1813
1814	-1.70	-3.37	-2.30	1.30		-1.17	1	-0.91		-1.22	-0.51	2.02	1814
1815	-1.98	2.39	2.29	0.36	0.18	-0.89	-0.93	-0.54	-0.11	0.77	-2.70	-1.34	1815
								·					
1816	0.54	-1.69	1	0.10		1	-2.53	(		0.29	-2.24	0.07	1816
1817	2.48	2.22	-0.20	-2.02	1		-1.34		1	-3.16	1.80	l 1	1817
1818	1.94	-0.21	-0.15	1.20		1.75	1.14	-0.18	0.05	0.38		-1.23	1818
1819	2.43	0.95	0.16	1.31	0.02		0.30	0.78	0.58	-0.12	-1.66		1819
1820	-2.02	-0.98	-1.42	1.20	-0.30	-1.37	-0.35	0.11	-1.19	-0.93	-1.30	-0.22	1820
	- 00	2 -	A = .		- 0-	2 22	7 00		0.0=				
1821	1.02	-2.58	0.54	1.34	-1.95		-1.39	1.20	0.85	-0.14	2.70	3.10	1821
1822	1.96	1.52	2.62	1.01	1.72	3.26	0.09	0.42	0.18	1.72	1.82	-3.42	1822
1823	-1.79	0.88	-0.14	-0.62	0.50	-1.69	-1.23	0.46	0.00	-0.58	-0.84	1.58	1823
1824	0.61	0.68	-1.00	-0.54	-1.52		-0.02	-0.17	0.89	0.54	2.30	2.74	1824
1825	1.23	0.06	-0.94	1.54	-0.22	-0.05	1.24	0.70	1.77	0.75	0.40	2.18	1825
7000	0	7 =0	0	۸ ۵*	7 40	7.05	7 70	0.70		7	<b>7.0</b> 0		
1826	-2.77	1.73	0.56	0.27	-1.48	1.35	1.59	2.10	1.11		-1.08	1.72	1826
1827	-1.63 3.28	-4.14	1.14	1.14	0.18	-0.09		-0.43	0.46	1.52		2.58	1827
1828 1829	-3.16	0.80 $-0.97$	0.29 $-0.75$	0.50 $-0.08$	$0.46 \\ 0.32$	0.34		-0.74	0.74	-0.30	0.51	0.89	1828
								-1.30	-1.53	-1.01		-5.70	1829
1830	-3.42	-2.59	2.54	1.68	0.11	-0.82	0.10	-1.23	-1.50	-0.44	0.83	-0.82	1830
1831	0.13	1.53	1.85	1.20	-0.20	-0.12	0.86	0.19	-0.35	9 69	-0.10	1.50	1007
1832	-0.36	-0.59	-0.93	0.65	-1.05	0.12	0.68		-0.10		-0.10 -0.10	0.53	1831 1832
1833	-1.73	2.34	-1.82	-0.38	2.54	1.06	-0.24	-1.65	1		-0.61	3.46	1833
1834	4.34	-0.42	0.67	-0.70	1.59	0.70	1.25	0.69	1.24		-0.05	-0.02	1834
1835	1.35		-0.14			0.18	1.92	1.42	0.36		-1.10		1835
1033	1.55	1.03	0.14	0.00	0.00	0.10	1.02	1.42	0.00	-0.92	-1.10	-2.04	1555
1836	0.55	-1.03		-1.02		1.06	0.56	1	-1.24		0.66	0.36	1836
1837	0.39		-3.26	-3.34	-2.79	1.14	-0.32		-0.84	0.04	-0.62	0.60	1837
1838	-5.21	-5.03		-2.52	-0.23		-0.32		-0.12	-0.04	0.74	-1.48	1838
1839	0.75	0.73	-0.62		-0.71	1.62		-0.86	0.00		1.10	1.60	1839
1840	1.23	-0.47	-2.58	2.26	0.49	1.02	-1.08	0.98	-0.64	-1.40	0.99	-4.76	1840
												•	
1841	0.47	-1.35	1.94	0.42	2.25	-1.26	-1.68	-0.50	2.28	0.12	0.02	1.48	1841
1842	-2.65	0.33	1.30	0.26	0.05	2.66	0.52	3.18	-0.12	-2.28	-1.10	0.36	1842
1843	2.07	-0.39	1.06	0.50	-0.31	-0.86	-0.48	0.70	0.96	0.12	0.54	0.60	1843
1844	0.83	-1.31	0.18	2.22	-1.35	0.54	-1.12	-2.34	0.24	-0.36	0.26	-3.40	1844
Means.	1.53	3.35	5.33	7.90	11.59	13.66	14.96	14.82	12.52	9.00	5.41	2.92	Means.
<u></u>													

### XC.

### Holland. — Zwanenburg.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	egrees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1743	0.60		-0.15				-1.15		-0.22		1.83		1743
1744	-0.91		-0.74				-1.02	1	-0.71	0.39	0.66	0.21	1744
1745	0.15		-0.70		1		-0.92		0.02		-0.50	1	1745
1746	-0.82		-2.19		1	-0.62		-1.28	-0.65		-2.80	1.02	1746
1747	-0.47	2.16	-2.29	-0.18	-0.52	0.92	-0.65	-0.21	0.34	-0.49	1.62	1.60	1747
37.10	0.04	0.00	4.14	0.70	0.03	7.45	0.00	0.00	0.00	0.00	1.00	9.46	75.10
1748	-0.24		-4.14			1.45	0.08		-0.03		1	3.46	1748
1749	2.68	0.11	-1.09		1.11		-0.10	1			-0.45	1.65	1749
1750	-0.34	2.60		-0.06		-0.10		-0.45	0.75		-1.63	i	1750
1751	1.09			-0.60		ļ.		-0.52		1	-1.31	0.33	1751
1752	1.71	-0.56	0.72	-0.63	-1.10	0.95	-0.48	-0.09	0.39	0.07	0.90	1.37	1752
						}							
1753	-1.80		1.34		-0.30		1	-1.00			-0.88		1753
1754	0.64	-1.14	-2.23	-1.40	0.41	-0.49	-1.33	-0.16	-0.44	0.61	1	-0.36	1754
1755		-3.19	-1.24	1.72		1	-0.31			1	-0.03		1755
1756	3.20	1.32	0.38	-1.57	-1.53	0.97	0.80	-0.50	0.74	-0.31	-1.13	-2.60	1756
1757	-2.22	-0.59	0.00	1.00	-1.01	-0.11	2.37	0.36	-0.21	-1.09	1.43	-0.09	1757
1758	-1.28	0.37	0.41	-0.39	1.95	0.29	-1.41	0.99	-0.17	0.21	0.05	0.36	1758
1759	2.86	2.13	1.49	0.86	ł.	0.99	1.66	0.71		1.05	-1.54		1759
1760	-1.64	-0.69	0.15	0.77	1	1.31	-0.15	-0.40	l .	0.28	1.08		1760
1761	1.78	1.90	2.37	0.47	0.92	0.86		1.16	l	-1.75	1	-1.59	1761
1762	2.10	0.09	-1.25	2.37	0.93	0.67	0.30		1	-1.98	-1.37	1	1762
1702	2.10	0.03	1.20	2.07	0.50	0.01	0.00	1.01	0.01	1.50	1.0.	2.02	1.02
		0 ==0	0.01					0.00	0.50		0.70		17700
1763	-4.88	0.79			1	0.28		1	-0.56	1	0.56		1763
1764	3.37	2.52	0.17	0.52	1	0.02	1.43	1	-1.14	1		-1.01	1764
1765	2.24	-2.13	2.30	1.62	1	1.22	-0.84	0.85	1	1.24		-0.82	1765
1766	-0.22	-0.78	0.72	1.67	1	0.35	1	1	0.49	0.32	1	-0.68	1766
1767	-3.34	2.34	1.08	<b>-0.6</b> 3	-1.36	-0.94	-0.80	0.36	0.98	0.71	2.15	-1.33	1767
1=00		0.00	0.0=	0.00	0.00	0.54	0.05	0.00	-1.27	0.00	0.70	0.72	1768
1768	-1.94	0.93	1		-0.02	1	0.65	4			0.70		1768
1769	1.19	0.09	1	l .	-0.21	-0.53		1			0.58		1 1
1770	1.45	0.92		-1.04	1	-0.34	0.02	1.20	1.59	0.19			1770
1771	-0.50	-1.44	l .	-2.59 -0.50	1		1	-1.01 0.36	0.04	0.89	$0.69 \\ 2.36$	1	1771 1772
1772	0.11	0.21	0.08	-0.50	-1.11	1.19	0.57	0.36	0.83	2.68	2.50	1.16	1772
1000	9.00	0.5~	1.00	0.81	0.95	0.31	- 0.10	1.1~	0.66	1.79	1.51	1.76	1773
1773 1774	3.38 0.58	$\begin{bmatrix} -0.57 \\ 1.62 \end{bmatrix}$	1.36 2.18	1.30		1		1		1.79			1773
1774	1.31	3.40	2.18	1.04		1		0.51		1.25			1774
1775	-4.40	1	1	1.45	1	1	1.56	1		1.25	0.46		1776
1777	-0.23	1	1.14	1	1	1	1	0.47	0.60	0.73	1.97		1777
1777	-0.23	-1.57	1.14	-0.56	0.15	-0.19	-0.07	0.00	0.00	0.73	1.97	_0.00	1777
1778	_1 26	-1.70	-0.55	0.36	0.71	0.43	1.43	0.54	-1.58	-2.02	1.08	2.90	1778
1779	-0.28	i .		1	0.61		]	1	1.27	1.61	0.19	1	1779
1780	III .	-0.56		-0.78	1	-0.51		2.04		1.03		1	1780
1100	1 1.04	0.00	2.00	0.10	1.07	0.91	0.20	M.O.4	1.00	1.00	0.01	1.00	1.00

#### XC.

### Holland. — Zwanenburg (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					D6	egrees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1781	-0.97		1	1	1	1		1	1	)		-0.39	1781
1782	11		-0.56		-1.09	1		1	1	-0.93		-0.89	1782
1783	2.39	2.13			-0.05	0.92			1			-2.74	1783
1784		-3.01			1.23	1	-0.37	1	0.94	1	1	-1.60	1784
1785	-0.06	-2.34	-3.32	-1.54	-0.96	-0.46	-0.01	-0.59	1.14	0.40	0.41	-1.70	1785
			ŀ								1		
1786	0.35	-0.08	-3.19	0.44	-0.59	0.72	-1 80	_0.75	-1 55	_1 49	-3.59	_0.23	1786
1787	-0.23	1.24	1.82	-0.90	-1.11	i .	-0.82	1		1.40	3.33	-0.20	1787
1788	2.20	-0.42	-1.15	0.24	0.58	1	l .	-0.66			-0.73	-6.23	1788
1789	$   \frac{2.20}{-2.66}  $	0.98		-1.64	1 .		-0.58				1	1.84	1789
1790	$\frac{-2.00}{2.20}$	ł		-2.00			-0.58 -1.76		Į.	-0.86			
1790	2.20	2.51	1.95	-2.00	0.89	-0.72	-1.76	-1.23	-1.73	-0.56	-1.71	0.89	1790
1791	2.74	1.29	1.23	1.34	-1.21	-1.25	-1.20	-0,14	-0.74	-0.60	-0.79	-0.53	1791
1792	1.06	-0.38	0.03	1.70	-1.11	-0.93	-0.07	0.27	-1.53	-1.13	-0.14	1.05	1792
1793	0.52	1.59	0.03		-1.61			-0.65		l	-0.17	1.60	1793
1794	-0.21	2.09	2.58		-0.76		1.52		-1.14	-0.54	0.41		1794
1795	-4.52				-1.88			-0.08	l .	2.39	0.37	2.87	1795
1.00	1.02	1.00	0.02	0.00	1.00	0110		0.00	1.01	2.00	""	2.01	1.00
1796	4.72	1.76	-0.99	1.00	-0.63	-0.50	-0.91	0.02	0.64	-0.80	-0.46	-2.07	1796
1797	0.84	0.52	-0.18	0.81	0.52	-1.18	1.38	0.01	-0.78	-0.60	0.32	1.59	1797
1798	1.45	1.73	0.31	1.22	0.11	0.77	-0.05	0.36	0.19	0.68	-0.17	-3.49	1798
1799	-2.11	-2.00	-1.77	-2.19	-1.68	-1.83	-1.47	-1.08	-0.72	-0.63	0.59	-3.54	1799
1800	-0.65	-1.76	-1.97	2.08	1.85	-2.10	-1.32	0.04	0.50	0.02	1.12	-0.46	1800
1801	1.97	-0.59	1.61	0.26	0.68	-1.43	_0.76	0.32	0.45	1.16	0.53	0.47	1801
1802	-0.75	0.24	0.56		-1.10			1.08	0.45	1.15	0.54	1.19	1802
1802	-3.04	-2.29	0.00		-1.10 $-1.55$		1		-1.11	0.06	0.54		
1804	3.30	0.13		-0.84	1.35	0.26	1.43	0.75 $-0.20$				0.43	1803 1804
							0.03		1.57	0.62		-2.84	
1805	-1.22	-0.36	-0.07	-0.56	-2.16	-1.97	-1.18	0.05	1.47	-2.00	-1.69	0.94	1805
1806	3.14	1.58	0.25	-1.95	1.79	-0.52	0.13	0.67	1.41	0.23	2.52	4.12	1806
1807	2.36	1.74	-1.32	-0.37	1.09	-0.17	1.64	2.53	-1.40	1.63	-0.15	0.84	1807
1808	1.19	0.07	-1.71	-2.02	2.07	-0.46	2.62	1.64	0.24	-1.35	-0.05	-1.50	1808
1809				-2.53	1.30	-1.03	-0.47	0.09	-0.27	-1.32	-0.99	0.68	1809
1810	-1.94	-1.39	-0.36	-0.41	-1.76	-0.96	0.05	-0.07	0.99	-0.63	-0.03	1.06	1810
1811	-2.75	0.55	1.41	1.16					-0.49			1.05	1811
1812	0.81	1.20	-1.21	-2.48			-1.28				-2.11		1812
1813	-0.84	1.53	0.16	0.04			-0.12				-0.76		1813
1814	-3.33	-4.20	<b>-2.89</b>	1.27		-1.86			-0.72	1		0.17	1814
1815	-2.69	0.96	2.23	0.59	0.59	-0.08	-1.63	-0.77	-0.54	0.07	-0.97	-1.90	1815
1816	0.59	-1.64	-0.78	_0.20	-1 49	_2 20	-1 21	-1 95	_1.14	_0.10	-2.06	-0.45	1816
1817	2.36	$\frac{-1.04}{2.31}$			-1.48		-0.83					-0.45 -0.67	1817
1818		-0.40											1 18
1019	1.90	-0.40	0.40	-0.21	-0.56	1.69	0.99	-0.64	-0.36	-0.34	0.74	-1.22	1818

### XC.

### Holland. — Zwanenburg (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

												1	
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1819	1.47	0 1.04	0.68	0.84	0.91	0.50	0.56	0 1.12	0 55	-0.79	0 -1 18	-2.18	1819
1820		-1.49		0.72			-1.06			-0.81			1820
1821		-1.32	-0.16	1.66		i	-1.81		)	0.20		1	1821
1822	2.64	1.93	2.26		1.53		1		-0.88	0.74	1.99		1822
1823	-6.29		0.11				-0.89		-0.37				1823
1020	-0.25	-0.94	0.11	-1.13	0.44	-1.00	-0.33	0.12	-0.57	-0.00	0.30	1.05	1020
1824	2.30	0.20	-0.22	-0.78	-0.47	-0.40	-0.19	0.00	1.03	0.36	1.52	2.59	1824
1825	2.63	0.60	-1.42	0.43	0.12	0.00	-0.04	-0.36	1.20	1.04	1.03	1.70	1825
1826	-2.57	0.97	0.87	0.17	-0.59	1.52	2.12	2.01	0.30	1.95	0.16	1.99	1826
1827	-0.65	-3.83	0.58	0.93	0.40	-0.24	0.14	-0.55	-0.14	0.88	-0.91	2.79	1827
1828	0.75	-0.75	1.05	0.43	0.49	0.70	0.79	-0.64	0.43	0.24	-0.18	1.96	1828
						ł			-				
								ĺ					
1829	1		-1.43				1	}	Į.		i	-5.77	1829
1830	-2.70		0.50	1	1	-1.45	1		-1.45		i .	-1.80	1830
1831	-1.07	0.04	1.24			-0.09			[-0.14]			1	1831
1832	-0.77	-1.34	-0.43	0.55	-1.49	-0.07	-1.74	-0.12	-0.64	1	-1.37	0.72	1832
1833	-2.12	1.33	-1.62	-0.68	2.22	0.92	-0.48	-2.08	-0.99	0.11	0.44	3.07	1833
1834	4.21	0.40	1 15	-0.87	1.31	0.87	1.80	1.00	0.86	0.69	-0.31	1.42	1834
1835	1.21	1.81		į.	-1.09	ł	1	1	-0.22		1	-0.44	1835
1000	1.21	1.81	0.47	-0.76	-1.09	0.92	0.47	0.07	-0.22	-0.77	-1.44	-0.44	1000
Means.	0.99	3.14	3.86	6.80	10.19	19.45	13.97	14.19	19.20	8.61	4.84	2.16	Means.
- Lacution	0.99	9.14	3.50	0.80	10.12	12.45	13.97	14.13	12.30	0.01	4.04	2.10	1.2001101

#### XCI. ENGLAND. - LONDON.

1794	-0.96	2.72	1.23	1.64	-0.99	-0.43	1.83	-0.38	-1.35	-0.61	0.36	-1.10	1794
1795	-5.04	-2.08	-1.26	-0.23	-0.46	-1.98	-0.04	0.11	1.76	1.61	-0.88	2.46	1795
1796	4.42	0.50	-1.00	1.10	-1.26	-1.00	-1.28	-0.51	1.23	-1.45	-0.97	-3.76	1796
1797	-0.01	-1.44	-1.51	-0.45	-0.70	-1.56	0.62	-0.82	-0.97	-1.34	-0.44	0.93	1797
1798	-3.44	-0.28	-0.12	1.41	0.44	1.31	-0.10	0.88	-0.11	0.09	-1.24	-2.39	1798
							ŀ						
1500	1 00	1.0-		4 0 1	1	7.04	0 =0	7 40		1.00	0.70	0.00	1
1799	-1.00	-1.05	-1.74	-1.94	-1.39	-1.34	-0.79	-1.40	-1.19	-1.02	0.13	-2.79	1799
1800	0.59	-2.04	-1.70	1.14	0.66	-1.37	0.66	1.23	0.42	-0.86	-0.15	-0.24	1800
1801	1.64	-0.08	1.26	-0.35	-0.10	-0.09	-0.48	0.76	0.88	0.33	-1.08	-1.37	1801
1802	-1.21	0.11	-0.04	1.14	-1.50	-0.66	-2.20	1.74	0.49	0.23	-0.89	-0.56	1802
1803	-0.92	-1.03	0.51	0.88	-1.12	-0.89	0.97	0.41	-1.77	-0.40	-0.31	0.98	1803
			1										
								]					ļ
1804	3.39	-0.73	0.00	-0.95	1.80	1.07	-0.57	-0.20	1.16	0.66	0.68	-1.52	1804
1805	-0.52	0.04	0.34	-0.20	-1.38	-1.49	-0.89	0.60	1.15	-1.06	-1.17	0.08	1805
1806	2.27	1.27	-0.23	-1.21	1.00	0.64	-0.06	0.38	0.16	0.54	2.11	3.64	1806
1807	0.64	0.54	-1.80	-0.14	1.05	-0.34	1.07	1.36	-1.61	1.44	-1.60	-1.19	1807
1808	0.64	-1.01	-1.80	-1.43	1.99	0.02	1.87	0.82	-0.55	-1.76	0.58	-1.32	1808
1809	-0.11	2.36	0.65	-2.05	1.23	-0.38	-0.75	-1.09	-0.24	-0.08	-1.33	0.72	1809
	1795 1796 1797 1798 1799 1800 1801 1802 1803 1804 1805 1806 1807 1808	1795     -5.04       1796     4.42       1797     -0.01       1798     -3.44       1799     -1.00       1800     0.59       1801     1.64       1802     -1.21       1803     -0.92       1804     3.39       1805     -0.52       1806     2.27       1807     0.64       1808     0.64	$ \begin{vmatrix} 1795 \\ 1796 \\ 1797 \\ 1798 \end{vmatrix} - 5.04 \begin{vmatrix} -2.08 \\ 4.42 \\ 0.50 \\ -1.44 \\ -0.28 \end{vmatrix} $ $ \begin{vmatrix} 1799 \\ 1800 \\ 1801 \\ 164 \\ -0.08 \\ -1.21 \\ 1803 \end{vmatrix} - 0.10 $ $ \begin{vmatrix} 1804 \\ 1805 \\ -0.52 \\ 0.04 \\ 1806 \end{vmatrix}                                   $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{vmatrix} 1795 \\ 1796 \\ 4.42 \\ -0.50 \\ -1.00 \\ -0.01 \\ -1.44 \\ -0.28 \\ -0.12 \\ -0.12 \\ -1.41 \\ -0.28 \\ -0.12 \\ -0.12 \\ -1.41 \\ -0.92 \\ -1.03 \\ -0.34 \\ -0.92 \\ -1.03 \\ -0.92 \\ -1.03 \\ -0.92 \\ -1.21 \\ -0.92 \\ -1.03 \\ -0.52 \\ -0.52 \\ -0.52 \\ -0.64 \\ -0.64 \\ -0.64 \\ -1.21 \\ -0.92 \\ -1.21 \\ -0.92 \\ -1.21 \\ -0.92 \\ -1.21 \\ -0.92 \\ -1.21 \\ -0.92 \\ -1.21 \\ -0.92 \\ -1.21 \\ -0.92 \\ -1.21 \\ -0.94 \\ -1.21 \\ -0.94 \\ -1.21 \\ -0.94 \\ -1.21 \\ -0.94 \\ -1.21 \\ -0.95 \\ -0.52 \\ -0.54 \\ -0.5$	$ \begin{vmatrix} 1795 \\ 1796 \\ 4.42 \\ -0.50 \\ -1.00 \\ -3.44 \\ -0.28 \\ -0.12 \\ -0.12 \\ -3.44 \\ -0.28 \\ -0.12 \\ -0.12 \\ -3.44 \\ -0.28 \\ -0.12 \\ -0.12 \\ -3.44 \\ -0.28 \\ -0.12 \\ -3.44 \\ -0.4$	$ \begin{vmatrix} 1795 \\ 1796 \\ 4.42 \\ -0.50 \\ -1.00 \\ -0.01 \\ -1.44 \\ -0.28 \\ -0.12 \\ -0.12 \\ -0.45 \\ -0.70 \\ -0.45 \\ -0.70 \\ -0.44 \\ -0.28 \\ -0.12 \\ -0.45 \\ -0.70 \\ -0.44 \\ -0.44 \\ -0.34 \\ -0.28 \\ -0.12 \\ -0.45 \\ -0.70 \\ -0.45 \\ -0.70 \\ -0.45 \\ -0.70 \\ -0.45 \\ -0.70 \\ -0.70 \\ -0.70 \\ -0.92 \\ -1.03 \\ -0.94 \\ -0.95 \\ -1.12 \\ -0.89 \\ -0.95 \\ -0.95 \\ -0.14 \\ -0.95 \\ -0.14 \\ -0.95 \\ -0.14 \\ -0.95 \\ -0.9$	$ \begin{vmatrix} 1795 \\ 1796 \\ 1796 \\ 1797 \\ -0.01 \end{vmatrix} - \begin{vmatrix} -2.08 \\ 0.50 \\ -1.00 \\ -1.00 \\ -1.51 \\ -0.44 \end{vmatrix} - \begin{vmatrix} -0.28 \\ -1.26 \\ -1.00 \\ -1.26 \\ -1.26 \\ -0.70 \\ -0.70 \\ -1.56 \\ -0.62 \\ -0.12 \end{vmatrix} - \begin{vmatrix} -0.45 \\ -0.70 \\ -1.56 \\ -0.70 \\ -1.56 \\ -0.62 \\ -1.21 \\ -0.04 \\ -1.01 \\ -0.04 \\ -0.05 \\ -0.52 \\ -0.04 \\ -0.05 \\ -0.52 \\ -0.64 \\ -0.04 \\ -0.04 \\ -0.05 \\ -0.52 \\ -0.52 \\ -0.64 \\ -0.64 \\ -1.21 \\ -0.04 \\ -0.05 \\ -0.52 \\ -0.52 \\ -0.52 \\ -0.52 \\ -0.52 \\ -0.52 \\ -0.52 \\ -0.54 \\ -1.21 \\ -0.04 \\ -0.05 \\ -0.52 \\ -0.04 \\ -0.04 \\ -0.05 \\ -0.52 \\ -0.04 \\ -0.05 \\ -0.05 \\ -0.04 \\ -0.05 \\ -0.04 \\ -0.05 \\ -0.05 \\ -0.04 \\ -0.05 \\ -0.04 \\ -0.05 \\ -0.04 \\ -0.05 \\ -0.04 \\ -0.05 \\ -0.04 \\ -0.05 \\ -0.04 \\ -0.06 \\ -0$	$ \begin{vmatrix} 1795 \\ 1796 \\ 4.42 \end{vmatrix} \begin{vmatrix} -5.04 \\ 0.50 \\ -1.00 \end{vmatrix} \begin{vmatrix} -1.26 \\ -1.00 \\ -1.26 \\ -0.12 \end{vmatrix} \begin{vmatrix} -0.23 \\ -0.45 \\ -0.70 \\ -0.70 \end{vmatrix} \begin{vmatrix} -1.28 \\ -0.51 \\ -0.82 \end{vmatrix} \begin{vmatrix} -0.23 \\ -0.82 \\ -0.82 \end{vmatrix} \begin{vmatrix} -0.23 \\ -0.70 \\ -1.56 \\ -0.70 \end{vmatrix} \begin{vmatrix} -1.26 \\ -1.26 \\ -0.82 \end{vmatrix} \begin{vmatrix} -0.82 \\ -0.82 \end{vmatrix} \begin{vmatrix} -0.82 \\ -0.82 \end{vmatrix} \begin{vmatrix} -0.82 \\ -0.82 \end{vmatrix} \begin{vmatrix} -0.82 \\ -0.82 \end{vmatrix} \begin{vmatrix} -0.82 \\ -0.82 \end{vmatrix} \begin{vmatrix} -1.00 \\ 0.59 \\ -2.04 \\ -1.70 \\ -1.21 \end{vmatrix} \begin{vmatrix} -1.74 \\ -1.94 \\ -0.08 \\ -0.51 \\ -0.92 \end{vmatrix} \begin{vmatrix} -0.10 \\ -0.04 \\ -1.14 \\ -0.08 \end{vmatrix} \begin{vmatrix} -0.05 \\ -0.35 \\ -0.10 \\ -0.98 \end{vmatrix} \begin{vmatrix} -0.06 \\ -1.27 \\ -0.89 \end{vmatrix} \begin{vmatrix} -0.79 \\ -0.41 \\ -0.89 \end{vmatrix} \begin{vmatrix} -0.66 \\ -2.20 \\ -0.41 \\ -0.89 \end{vmatrix} \begin{vmatrix} -0.74 \\ -0.89 \\ -0.51 \\ -0.52 \end{vmatrix} \begin{vmatrix} -0.73 \\ 0.04 \\ 0.34 \\ -0.23 \\ -0.23 \\ -0.14 \end{vmatrix} \begin{vmatrix} -1.80 \\ -1.35 \\ -0.34 \\ -0.89 \end{vmatrix} \begin{vmatrix} -0.57 \\ -0.20 \\ -0.36 \\ -0.52 \\ 0.04 \\ 0.34 \\ -0.20 \\ -1.38 \\ -0.14 \\ 1.05 \\ -0.34 \\ 1.07 \\ -0.89 \\ 0.02 \end{vmatrix} \begin{vmatrix} -0.10 \\ 0.64 \\ -0.06 \\ 0.38 \\ -0.52 \\ 0.64 \\ -1.01 \\ -1.80 \\ -1.80 \\ -1.43 \\ -1.99 \\ 0.02 \end{vmatrix} \begin{vmatrix} -0.04 \\ -0.34 \\ -0.06 \\ 0.38 \\ -0.52 \\ -0.34 \\ 1.07 \\ -0.89 \\ 0.69 \end{vmatrix} \begin{vmatrix} -0.66 \\ -0.36 \\ $	$ \begin{vmatrix} 1795 \\ 1796 \\ 1796 \\ 4.42 \end{vmatrix} \begin{vmatrix} -2.08 \\ 0.50 \\ -1.00 \\ -1.00 \end{vmatrix} \begin{vmatrix} -0.23 \\ -0.45 \\ -0.70 \\ -0.01 \end{vmatrix} \begin{vmatrix} -1.26 \\ -1.00 \\ -1.26 \\ -0.70 \end{vmatrix} \begin{vmatrix} -1.28 \\ -0.51 \\ 1.23 \\ -0.92 \end{vmatrix} \begin{vmatrix} -0.01 \\ -1.44 \\ -1.51 \\ -0.45 \end{vmatrix} \begin{vmatrix} -0.45 \\ -0.70 \\ -1.41 \end{vmatrix} \begin{vmatrix} -1.56 \\ -0.70 \\ -1.56 \\ -0.70 \end{vmatrix} \begin{vmatrix} -0.02 \\ -0.82 \\ -0.97 \end{vmatrix} \begin{vmatrix} -0.97 \\ -0.10 \\ -0.88 \end{vmatrix} \begin{vmatrix} -0.97 \\ -0.11 \end{vmatrix} \begin{vmatrix} -1.39 \\ -0.10 \\ -0.88 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.88 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.88 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.88 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.88 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.88 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.88 \\ -0.11 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -0.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -1.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -1.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -1.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -1.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -1.10 \\ -0.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -1.10 \\ -1.10 \end{vmatrix} \begin{vmatrix} -1.10 \\ -1.10 \\ -1.10 \end{vmatrix} \begin{vmatrix} -1.$	$ \begin{vmatrix} 1795 \\ 1796 \\ 4.42 \end{vmatrix} \begin{vmatrix} -2.08 \\ 0.50 \\ -1.00 \end{vmatrix} \begin{vmatrix} -1.26 \\ 1.10 \\ -0.45 \\ -0.70 \end{vmatrix} \begin{vmatrix} -0.04 \\ -1.00 \\ -1.28 \\ -0.51 \end{vmatrix} \begin{vmatrix} -0.51 \\ 1.23 \\ -1.45 \\ -0.88 \end{vmatrix} \begin{vmatrix} -1.26 \\ -1.00 \\ -1.26 \\ -1.00 \end{vmatrix} \begin{vmatrix} -1.28 \\ -0.51 \\ -1.28 \\ -0.51 \end{vmatrix} \begin{vmatrix} -1.61 \\ -1.45 \\ -0.92 \\ -1.34 \end{vmatrix} \begin{vmatrix} -1.51 \\ -0.45 \\ -0.70 \\ -1.56 \\ 0.64 \end{vmatrix} \begin{vmatrix} -1.56 \\ -0.62 \\ -0.82 \\ -0.92 \end{vmatrix} \begin{vmatrix} -0.97 \\ -1.34 \\ -0.92 \\ -1.34 \end{vmatrix} \begin{vmatrix} -1.39 \\ -1.34 \\ -0.44 \end{vmatrix} \begin{vmatrix} -1.31 \\ -0.10 \\ -1.37 \\ -0.66 \end{vmatrix} \begin{vmatrix} -1.09 \\ -1.23 \\ -1.41 \end{vmatrix} \begin{vmatrix} -1.09 \\ -1.09 \\ -1.09 \end{vmatrix} \begin{vmatrix} -1.00 \\ -1.37 \\ -0.66 \end{vmatrix} \begin{vmatrix} -1.09 \\ -1.23 \\ -1.21 \\ -1.21 \\ -1.31 \end{vmatrix} \begin{vmatrix} -1.44 \\ -1.56 \\ -0.35 \\ -0.10 \end{vmatrix} \begin{vmatrix} -0.09 \\ -0.48 \\ -1.12 \end{vmatrix} \begin{vmatrix} -1.61 \\ -1.29 \\ -0.48 \end{vmatrix} \begin{vmatrix} -1.24 \\ -1.29 \\ -0.35 \end{vmatrix} \begin{vmatrix} -1.24 \\ -1.29 \\ -0.89 \end{vmatrix} \begin{vmatrix} -1.24 \\ -1.29 \\ -0.49 \end{vmatrix} \begin{vmatrix} -1.61 \\ -1.29 \\ -0.49 \end{vmatrix} \begin{vmatrix} -1.09 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.09 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.09 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.14 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.24 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.24 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.29 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.29 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.29 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.29 \\ -1.29 \\ -1.29 \end{vmatrix} \begin{vmatrix} -1.29 \\ $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$

#### XCI.

# England. — London (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaumu	ır.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
-010	0	0	0	0	0	0	0	0	0	0	0	0	1010
1810	-0.47	0.01	0.38		-1.44		-0.44		1.32	0.95		-0.03	1810
1811	-1.09	0.85	1.54	1.64	2.03	0.51		-0.51	0.83	2.50		-0.16	1811
1812	0.42	1.43	-0.68		1	-1.09				1	-0.75	0.90	1812
1813	-0.51	1.34		-0.81	0.12					-1.05		- 1	1813
1814	-3.80	-2.21	<b>-2.</b> 55	1.06	-1.66	-2.03	-0.04	-0.91	-0.72	-1.10	-0.75	0.90	1814
1815	-1.49	1.34	1.94	0.44	1.19	0.24	-0.53	-0.07	2.48	0.55	-1.42	-0.83	1815
1816	0.64	-0.70	-0.64	-0.50	-0.99	-1.27	-2.35	-1.18	0.96	0.28	-1.24	-0.48	1816
1817	1.84	2.05	0.25	-0.63	-1.75	0.77	-1.46	-2.60	-0.81	-1.76	2.14	-0.70	1817
1818	1.67	-1.32	0.03	0.04	-0.06	2.24	2.40	1.98	2.30	2.06	3.20	-0.0s	1818
1819	2.29	0.85	1.36	1.37	0.88	-0.69	0.36	1.58	0.70	3.08	-0.75	-0.74	1819
1000		0.00	0.05	1.00	0.01	0.74	0.71	1.10	0.00	0.00	0.00	0.50	1000
1820	-1.44		0.25		l	-0.74				-0.96 $0.32$	$\frac{-0.22}{2.32}$	0.59	1820
1821	1.04	-0.97 $2.19$	0.87 2.78	2.08 0.48	i e	-1.80	0.36	$0.47 \\ 0.29$	1.28 $-0.24$	1.04	2.32	2.32 -1.14	1821 1822
1822	2.16					1.57	1		i			1	1
1823	-1.40	0.19	0.16	-0.10	2.16	0.33	0.14	0.78		-0.56	0.54	0.55	1823
1824	0.78	2.41	-0.73	-0.94	-1.48	-1.40	0.00	-0.29	0.48	-0.03	1.38	1.08	1824
1825	1.31	-0.21	-1.17	1.28	0.08	-0.03	1.47	0.38	1.63	0.32	-0.84	0.59	1825
1826	-1.49	1.61		1.46	1.16	1	1.69	1.67	0.30	1.28	-1.11	1.19	1826
1827	-0.96	-3.19	0.74	0.39	-0.08	-0.40	0.74	-0.73	0.21	0.84	-0.28	1.99	1827
1828	1.73	0.54	1.00	0.28	0.70	0.88	0.36	-0.62	0.52	-0.16	0.65	2.37	1828
1829	1	-0.24	-1.08	-0.85	0.50	0.35	-0.48	-1.22	-1.41	-1.16	-1.60	-3.14	1829
1830	-2.31		1.98	1	-1.39			-1.09		0.32	0.63		1830
1831	-0.73	1.01	1.16	1.21		0.55	1.49		-0.04	2.39		1.21	1831
1832	0.13		-0.42		-0.70	1	-0.20		-0.06	1	0.47	1.08	1832
1833	-0.64	1.45	1	-0.10	2.72	0.66	į.	-1.31	-1.41	0.24	0.16	2.21	1833
1834	3.73	0.48	1.16	-0.48	1.59	1.20	1.29	0.76	0.70	0.10	0.45	0.35	1834
1835	0.82	0.81	-0.22	0.30	-0.12	0.71	0.87	1.09	0.21	-0.90	0.05	-1.76	1835
1836	0.80			-1.12	1	0.48	1	1		-1.14		0.28	1836
1837	0.73	0.74		-2.79	ł .	0.04	Į.	-0.16	1		-0.57		1837
1838	-2.93	-2.57		-1.50	1	0.02	1	1	-0.92	4	-0.68		1838
1839	0.73		-1.08	1	1	0.66	1			-0.52	1	1 1	1839
1840	11	-0.50	į.	1	0.14	1	-0.77	1	1	-1.32	1	-2.41	1840
1841	-0.38	1	2.58	0.61	2.08	2.17	1		1	-0.01	0.40		1841
1842	-1.02	0.81	1.47	-0.43	0.59	2.84	0.18	2.11	0.19	-1.70	0.36	2.50	1842
Means.	2.38	3.81	5.00	7.30	10.46	12.92	14.26	14.07	12.06	8.88	5.51	3.81	Means.
								2					

### XCII.

### SCOTLAND. - KINFAUNS CASTLE.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.   Jan.   Feb.   March.   April.   May.   June.   July.   Aug.   Sept.   Oct.   Nov.   Dec.   Year.	1					De	egrees o	Reaum	ur.					
1814	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1815		0			0				0		0	0	0	
1816							l .							1814
1817	!					1	ł.	t .						
1818			1			1	1				1			
1819						i	ł				1			
1820	1818	0.51	-1.03	-1.41	-1.59	1.03	1.43	0.85	-0.22	-0.15	2.34	2.54	0.25	1818
1820	1819	0.85	-0.88	0.67	-0.20	-0.36	-0.85	0.07	2.00	0.30	-0.32	-2.35	-2.60	1819
1822	1820	-2.43	0.95	0.33	1.10	ł	1		1	-0.36	í			
1823	1821	0.55	0.97	0.26	1.12	-1.09	-0.45	-0.01	0.84	1.44	0.83	0.38	0.73	1821
1824	1822	1.85	1.28	1.08	0.79	0.97	2.04	0.50	0.26	-0.81	0.48	1.38	-0.61	1822
1825	1823	-0.91	-1.69	-0.16	-0.60	0.63	-1.01	-0.92	-0.85	-0.15	-0.56	2.02	-0.04	1823
1825	1894	261	1 20	_0.56	0.90	0.18	0.26	0.19	0.09	0.21	9 16	0.16	0.95	1004
1827														
1828		1					1						1	
1829	l l	1					Į .		į.	ļ		1		
1830	1		ł .											
1832														
1833		1										1		
1834	1	1										ļ.		1
1835	1													!
1836	1						i						1	1
1837	1835	-0.27	0.72	-0.08	0.23	-0.58	0.20	-0.17	1.09	-0.10	-1.10	-0.31	-0.34	1835
1838	1836	0.59	-0.67	-0.70	-0.81	0.10	-0.54	-1.16	-1.09	-1.67	-0.86	-0.94	-0.05	1836
1839	1837	-0.07	0.20	-2.26	-2.35	-1.70	-0.05	0.52	-1.13	-1.32	0.23	-1.18	1.74	1837
1840	1838	-2.58	-4.61	-0.83	-1.44	-1.75	-1.03	-0.04	-0.24	-0.53	-0.55	2.73	0.48	1838
1841	1839	-0.90	-0.79	-1.56	-1.24	-1.18	-0.45	-0.34	-0.79	-0.64	-0.17	0.11	-0.35	1839
1842	1840	0.65	-0.26	-0.07	1.00	-0.72	-0.40	-1.30	0.21	-1.29	-0.63	-0.17	-0.58	1840
1842	1841	-2.19	-0.09	2.25	-0.28	0.51	-1.07	-0.83	-0.20	0.51	-1.59	-1 9.1	_0 49	18.11
Means.         1.77         2.74         3.87         5.71         8.13         10.58         11.76         11.28         9.52         6.72         4.35         2.96         Means.           XCIII. FINLAND. — TORNEÅ.           1801							1							
XCIII. FINLAND. — TORNEÅ.    1801	1012													1012
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Means.	1.77	2.74	3.87	5.71	8.13	10.58	11.76	11.28	9.52	6.72	4.35	2.96	Means.
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	ů				XCII	I. F	INLAN	D. —	Torn	ΙΕÅ.	,			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1801		1									-0.01	-1.67	1801
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-0.57	-0.17	-0.15				-2.03	-1.60					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							1	1						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1	1 1					i i							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1000		1.01											
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		,										1	- (1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	li l	1				1		1						
1810     -2.18     -2.36     -2.41     -2.45     -6.45     -0.68     -2.13     -0.68     -1.34     -1.23     -4.13     -2.20     1810       1811     2.98     -2.74     3.64     -2.04     -0.69     0.42     -0.91     -2.66     -1.05     -1.90     -0.10     -2.06     1811       1812     1.18     1.85     -3.37     -1.39     0.55     -2.94     -2.53     -1.20     -2.85     -0.78     -4.18     -1.15     1812	1												7)	_
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1												- 1	
1812   1.18   1.85   -3.37   -1.39   0.55   -2.94   -2.53   -1.20   -2.85   -0.78   -4.18   -1.15   1812													1	
		1 1				1								1
1813    1.32    1.15    1.70    1.88    -0.71    -1.58    1.87    0.08    1.88    -2.89    3.65    -1.43    1813	11	1												
	1813	1.32	1.15	1.70	1.88	-0.71	-1.5S	1.87	0.08	1.88	-2.89	3.65	-1.43	1813

#### XCIII.

## FINLAND. — TORNEÅ (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						grees of		ır.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1814	-7.01	$\overset{\circ}{2.71}$	0 -1.85	0.92	-0.59	o 2.44	o 4.65	o 4.46	2.60	c 0.44	-0.15	-4.50	1814
1815	1.22	3.16	0.66	5.27	3.22	5.58	4.70	5.03	4.02	3.38	4.30	4.82	1815
1816	2.27	-8.23	1	0.50		-0.12		-0.41	1.97	0.16	1.17	2.29	1816
1817	3.54	-2.13	-2.78	0.19	2.42		0.65	-1.34	-0.36	-1.14	-0.07	-2.85	1817
1818	3.46	-3.34	-1.07	-2.61	-3.48	-0.92	2.98	-2.55	0.09	1.08	2.89	5.83	1818
1819	4.47	-0.15	-0.50	-2.07	0.23	1.46	2.90	2.22	1.04	-4.58	-3.62	-2.15	1819
1820	-5.74	-0.22	-0.63	-1.32	-0.73	1.62	0.13	-0.17	0.18	-2.17	-1.94	-2.67	1820
1821	-2.18	1.12	0.50	0.83	1.24	-3.70	-2.44	-1.32	-0.58	3.58	-1.52	-4.13	1821
1822	0.13	6.44	5.68	4.22	1.67	1		1.75	-0.14	1	-2.05	4.46	1822
1823	-4.01	<b>-1.0</b> 8	4.15	0.66	0.87	-0.43	-0.09	-0.73	-0.86	2.06	-1.38	1.26	1823
1824	0.71	4.20	1.75	-0.22	-0.40	0.29	-0.89	-0.73	1.25	-2.18	-1.01	-0.96	1824
1825	3.99	1.42	1.83	1.78	-0.29	1	1		6.34	2.14	2.35	3.20	11 1
1826	1.99	4.70	4.99	0.50	2.65	1.56	1	í		2.67	3.23	3.74	1826
1827	0.03	0.00	0.59	í	2.39			1		-1.53		5.68	11 1
1828	-0.50	-0.84	-1.77	-0.66	2.84	0.18	-1.73	-0.73	-2.86	1.18	0.50	1.69	1828
1829	1.26	-4.27	-2.69	-2.53	1.26	1	0.30	1	0.38	ł	-0.53	2.86	
1830	0.99	0.80		1	-1.10		1	1	1		3.44	-1.22	11
1831	-3.98	-0.07		2.01	0.98	1	0.81	0.79	1	0.01	2.99	1.69	1831
1832	5.26	8.25	3.64	2.92	0.10	0.51	-1.11	-1.22	-3.67	2.86	• •	• •	1832
Means.	-12.55	-10.76	-7.19	-1.62	4.01	10.59	13.05	10.81	6.22	0.26	-6.27	-10.32	Means.
		]	XCIV.	No	RTH .	Amer	1CA	- Ale	SANY,	N. Y.	,		
						grees of							
1826	1.92	2.44	1.65	-1.02	3.23	1.07	0.72	1.09	1.57	1.46	0.81	0.35	1826
1827	-2.91	1.07	1.15	1.62	-0.02	0.05	0.55	0.08	0.43	1.14	-1.72	0.77	1827
1828	2.80	4.52	2.10	-0.88	0.76	2.66	-0.41	1.33	0.35	-0.31	0.76	3.17	1828
1829	-0.21	-2.27	-0.87	0.12	2.09	0.03	-1.54		-1.93	0.92	0.50	3.63	1829
1830	0.28	-0.11	1.41	3.64	-0.21	-0.92	0.81	0.27	0.19	1.42	3.83	4.71	1830
1831	-1.30	-1.03	2.77	1.89	1.07	2.11	0.32	1.01	1.00	1.52	0.63	-4.94	1831
1832	H	-0.87	0.16	-1.29	-1.35	0.19	-0.34		0.53	0.67	1.15	0.76	1832
1833	2.34		-1.15	1.75	1.55	-2.35	-1.06	-1.47	-0.55	-0.55	-0.61	0.18	1833
1834	-1.18		0.67	0.68	-0.05		1.59		0.27	-1.31	-0.36	-1.13	1834
1835	-1.06		-0.98	-1.59	-0.57	-0.34	-0.43		-2.14	1.45	0.31	-3.06	1835
1836	-0.35		-3.48		-0.95	1	0.20		-0.39	-3.06		l H	1836
1837	-3.40	1	-1.94	-2.02	-1.23	0.07	-0.95		-0.60	-0.89		-0.49	1837
1838 1839	3.34 -0.25	1	0.97	-3.07 $0.79$	-1.26 $-0.79$	1.78 -1.79	$0.31 \\ 0.15$	0.27 $-0.14$	0.36	-0.68 $0.99$	-1.47 $-0.94$	-2.11 -0.19	1838 1839
1840	-3.32	1	0.60	1.32	0.96		0.15	0.81	-0.91	0.99	0.28	-0.15 -1.26	1840
1	1.95		-1.19	-2.58	}	1.90	0.	1.23	0.88		-0.49	0.86	1841
1841 1842	2.03		$\frac{-1.19}{2.06}$	0.62		-0.98	0.28	0.13	-1.09	-0.12		-1.69	1841
1843	2.65	1	-4.26	-0.62	-0.62	-0.64	-0.55	0.64	0.85	-1.24	-1.11	0.93	1843
1844		-0.15	0.27	2.97	0.47	-0.29		-0.19	0.72		-0.20	0.47	1844
			-										

2.70 -1.65 Means.

Means.

-3.58 -3.08

## XCV.

## NORTH AMERICA. - SALEM, MASS.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					D	egrees o	f Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1787	0.40	° −1.37	0.24	0 -0.24	-0.61	° -0.84	0 -1.53	0.28	o -1.13	° -1.00	0.58	0.07	1787
1788	II .	-2.15		-0.47	1		1		l .	-1.00		-1.60	1788
1789	11	-2.81		-0.47			-0.31	1	-0.47	1	1	1.18	1789
1790	l i	-1.04		-1.47			-0.75	l .	-1.02	1	1	-2.82	1790
1791	III	-1.48	0.90	1	1	1	-0.08	1	-0.69		1	0.07	1791
1792	$  _{-2.94}$	-0.37	1.79	0.87	1.61	-0.84	-0.64	-0.28	-1.80	0.77	0.92	-1.15	1792
1793	1.03	0.70	1.42	1.51	2.55	2.07	0.59	0.75	0.37			-0.10	1793
1794	0.95	-0.25	1.91	1.19	1.16	0.11	0.52	0.58	0.75			4.35	1794
1795	0.20	-0.50	0.54	0.21	0.39	0.12		1.85	1.04	1.24	0.36	1.51	1795
1796	1.18	0.12	-0.37	1.17	1	0.40		Į.	-0.06			1	1796
				1		0.10	0.00	0.00	0.00	0.00	1.20	0.02	1,00
1797	-1.15	2.24	0.55	-0.26		0.41	1.40		í		-1.72		1797
1798	0.68	-0.89	0.54	0.76	1.44	0.60		2.29	0.83	0.81		-3.03	1798
1799	0.28	0.08	0.31	0.51	0.63	0.58	0.45	0.99	0.27	1	-0.53	1	1799
1800	0.31	0.24	-0.31	1.92	-0.12	1.22	1.15	0.11	0.04	Į.	-0.93	1.63	1800
1801	0.40	0.46	<b>1.</b> 51	0.21	1.69	0.08	0.35	0.49	1.41	0.96	0.17	0.30	1801
1802	3.79	-0.16	0.76	0.31	-1.34	0.13	0.13	0.88	1.19	1.87	1.23	1.19	1802
1803	1.12	2.15	0.67	0.38	-0.81	0.53	-0.08	1.09	-0.24	0.96	-0.71	1.99	1803
1804	-0.48	0.08	-0.48	-0.98	1.55	0.20	-0.25	-0.44	0.28	-1.05	0.16	-1.76	1804
1805	-1.46	1.02	1.92	1.45	0.91	0.11	1.40	0.82	1.23	-0.82	0.13	3.24	1805
1806	0.48	1.60	-1.83	-2.28	-0.44	-0.19	-1.12	-0.77	-0.52	-0.04	0.15	-0.06	1806
1807	-1.05	-1.13	-1.30	-0.31	-0.80	-0.62	0.05	0.00	-1.08	0.22	-0.65	2.45	1807
1808	0.13	1.41	1.55	0.37	-0.74	0.04	-0.15	-0.86	0.54	-0.72	0.69	0.72	1808
1809	-1.15	-1.73	-1.36	0.31	-0.24	-0.42	-1.90	-0.76	-0.95	3.00	-2.19	2.04	1809
1810	0.11	0.95	-0.68	0.70	0.84	0.04	-0.93	-0.39	0.46	-0.12	-0.24	-0.34	1810
1811	0.30	0.14	1.69	-0.01	0.65	0.43	0.16	0.14	0.58	1.74	0.67	-0.34	1811
1812	-1.51	-1.16	-2.68	-1.05	-3.22	-2.04	-2.13	-1.64	-2.07	-0.30	-0.90	-0.73	1812
1813	-1.09	-0.34				-0.95		0.44		-0.62		-0.70	1813
1814	-0.73	0.80	-0.51	1.08				-0.94				-1.78	1814
1815	-0.93	-1.98	0.28	-1.47	-1.49		1.12		-0.50	-0.69		-0.45	1815
1816	-0.16	0.07	-2.14	-0.44	-1.36	-2.36		-1.31		0.17	1.79	0.31	1816
1817	-0.71	-3.48	-1.43	-0.73	-0.44	-1.65	-0.52	-0.76	0.18	-0.70	0.78	0.68	1817
1818	-0.51	-3.56	0.14	-2.31	-0.42	1.17	0.85	-0.01	-0.84	0.61	1.92	-1.94	1818
1819	2.45	4.91		-1.06		1.33	0.64	0.59	1.63	0.64		-0.43	1819
1820	-1.51			-0.07		0.51	1.95	0.26	1.52	-0.17	-0.98		1820
1821	-2.75	1.50	-0.80	-0.97	-0.37	0.36	-1.08	0.83		-0.05	0.42	-1.31	1821
1822	-1.60	-0.50	1.64	-0.87	1.77	0.09	0.44	0.06	1.84	0.75	0.96	0.12	1822
1823	0.37	1	-0.99		-1.19	-0.42	-0.19	0.35	-1.63		-1.72	0.52	1823
1824	2.28	0.47	-0.11	0.62	-0.84	-0.59	-0.14	-1.08	0.12	0.21	-0.61	1.43	1824
1825	1.30	1.27	2.16	1.49	0.69	1.74	2.36	-0.12	-1.05		-0.14	0.62	1825
1826	0.96	1.11	0.10	-1.05	2.95	0.04	1.56	-0.13	0.78	0.23	0.19	0.55	1826
1827	-1.49	0.52	0.64	1.56	-0.03	-0.60	-0.35	-0.82	-0.28	1.13	-2.74	0.01	1827
1828	2.42	4.05	1.10			1.06	0.36	0.96	0.37	-0.19	1.17	2.04	1828
Means.	-2.84		1.54					17.17		8.56		-0.63	Means.
<u> </u>				0.00	22.00	10101	1.00	21121	20.00	0.00	0.00	0.00	

#### XCVI.

## ICELAND. — REIKIAVIK.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
,	0	0	0	0	0	0	0	0	0	0	0	0	
1823		-0.56	0.40		-0.60					-1.50		-0.86	1823
1824	-0.32	0.61	-0.05	2.16	2.95	4.63	3.12	1.53	-0.73	-2.37	-3.64	-3.99	1824
1825	-1.07	-0.40	3.04	0.98	0.50	0.33	1.70	0.66	2.34	1.68	-0.81	-0.92	1825
1826	-0.19	2.84	2.15	-0.79	1.58	-1.10	-0.75	-0.18	1.24	1.12	0.36	1.17	1826
1827	-0.72	1.93	-3.80	-0.86	0.67	0.86	0.14	1.73	0.64	2.29	2.26	0.88	1827
1828	1.98	2.48	1.54	1.29	2.37	0.53	3.15	3.98	3.07	3.26	0.94	2.77	1828
1829	1.02	-0.09	0.20	0.56	0.79	0.26	1.21	2.21	-0.20	-1.16	0.03	1.86	1829
1830	1.89	-0.58	-1.22	-0.72	2.44	0.52	-0.80	0.68	0.85	2.09	-0.35	-2.60	1830
1831	0.28	-0.95	2.58	1.39	-1.76	1.44	-1.89	-1.85	-0.37	0.95	-0.76	1.45	1831
1832	0.71	-0.48	-1.77	0.17	-2.20	ì			į.		1.22	-0.29	
													7000
													1832
1833	1.41		}		-0.57		1	l		1	1	-1.64	1833
1834	-0.43	0.20	1		-1.35			1		1		1	1834
1835	ll		-1.55		1	1	l .	1				1	1835
1836	-1.86	-3.24	-2.00	-3.01	-0.37	-0.94	-0.59	-2.68	-1.80	-1.67	-1.52	-1.95	1836
1837	-0.42	0.43	-2.23	-1.91	-2.07	-0.32	0.40		• •			• •	1837
Means.	-1.00	-1.60	-1.07	1.84	5.54	8.67	10.78	9.27	6.42	2.19	-0.60	-1.15	Means.

#### XCVII. GREENLAND. - GODTHAAB.

Degrees of Reaumur.

L							grees of	reaum	ur.					
	1796										-2.52	1.51	2.19	1796
	1797	0.91	-2.08	-0.73	-1.96	1.14	0.27	1.40	1.31	0.77	1.02	2.22	0.87	1797
	1798	-1.30	0.53	3.98	0.08	0.37	-0.39	0.39	0.07	-0.37	-0.67	0.83	-0.08	1798
	1799	-0.40	3.08	-1.87	0.47	0.37	-0.71	-0.47	-0.72	0.62	-0.43	-0.91	4.72	1799
	1800	2.75	0.22	2.32	-0.68	1.52	1.05	0.35	0.88	-0.42	0.48	0.05	0.07	1800
1														
	1801	-0.86	2.63	0.00	-1.00	-2.86	-1.61	0.89	0.92	-0.39	0.19	0.22	1.94	1801
	1802	1.85	-2.99	-3.76	-2.68	-0.44								1802
	1816							0.09	-0.98	-0.12	-0.15	-0.01	-6.91	1816
	1817	-1.55	-2.46	-4.17	0.37	-1.32	-0.79	-1.63	-0.28	-0.41	-1.65	-0.52	-1.73	1817
	1818	-5.58	<b>-5.1</b> 3	-4.00	2.56	-0.90	-0.84	0.52	0.15	-0.71	-1.97	-1.82	-0.42	1818
	1819	-2.74	0.94	-0.35	0.98	-0.91	-0.97	-3.78	-2.29	-2.30	1.78	1.38	3.15	1819
	1820	4.16	0.14	0.35	-2.15	0.97	0.66	-0.96	-1.57	-0.72	-0.06	1.60	1.19	1820
-	1821	0.04	0.42	1.30	1.00	-0.07	0.68							1827
	1841									0.45	0.14	-0.27	0.23	1841
	1842	1.13	-1.15	-1.12	1.56	2.03	0.37	0.89	0.34	1.39	1.95	-0.37	-1.37	1842
	,										1			
	1843	0.11	4.74	4.65	2.18	1.18	1.16	1.52	0.72	1.57	1.66	-2.89	-3.93	1843
	1844	-0.13	0.40	-0.51	-3.10	-1.29	0.79	0.78	1.39	1	l .	-1.08	0.01	1844
	1845	1.54	0.76	3.98	2.34	0.24	0.32							1845
-														
	Means.	-8.72	-8.64	-7.29	-4.44	0.07	3.15	4.41	3.93	1.62	-0.96	-4.47	-6.45	Means.



## CORRECTIONS

FOR

## FORCE OF VAPOR AND RELATIVE HUMIDITY.

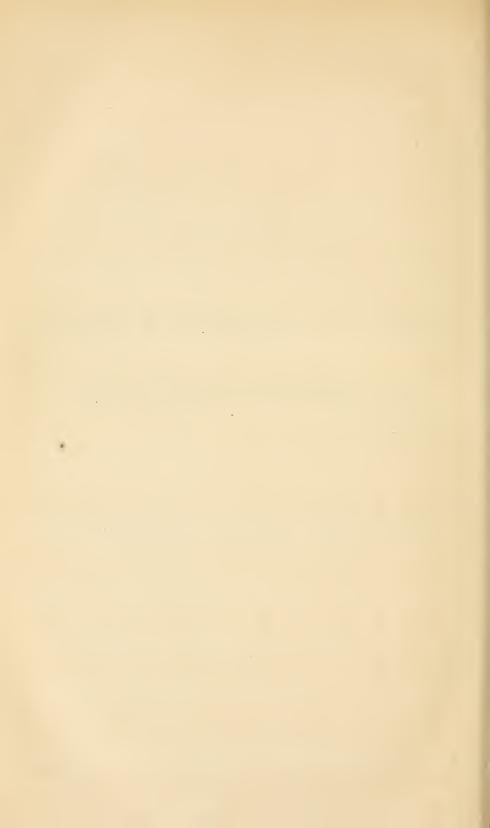
## HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

#### TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY TO THE TRUE MEAN FORCE OF VAPOR AND RELATIVE HUMIDITY OF THE DAY, OF THE MONTH, AND OF THE YEAR.

 $\mathbf{E}$ 



#### XCVIII.

## England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Force of Vapor for the respective Months. (GLAISHER.)

English Inches.

						guan inc							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
Midn	.006	.006	.008	.017	.026	.031	.028	.025	.024	.018	.010	.009	.017
1	.011	.008	.010	.021	.028	.037	.031	.031	.030	.020	.012	.010	.021
2	.015	.010	.011	.024	.031	.043	.036	.035	.035	.021	.015	.010	.024
3	.015	.011	.013	.027	.032	.048	.038	.039	.037	.023	.017	.011	.026
	1010	.011	1010	1021									
4	.015	.013	.015	.029	.031	.047	.037	.040	.040	.025	.019	.011	.027
5	.015	.014	.016	.029	.027	.037	.031	.038	.040	.023	.021	.011	.025
6	.014	.015	.016	.025	.019	.022	.019	.029	.033	.021	.021	.010	.020
7	.013	.014	.014	.016	.007	.008	.007	.014	.022	.018	.018	.009	.013
, i	.010	.014	.014			1000							
8	.010	.010	.010	.005	005	004	004	.000	.010	.011	.012	.007	.005
9	.007	.006	.005	1	ļ.	015			005	.005	.005		002
10	.002	.000	1	1	1		019	021		005			010
11	004	}		020	l	1				009	ł	1	017
11	1004	009	007	.00	.020	.000	.020	1021	.021	.505	.510		
Noon	- 007	009	- 012	026	030	-,012	029	030	030	015	017	007	021
1								032					
2	1	1	<b></b> 013	1				034					
3	1		1	)	1			031					
9	007	012	012	025	020	039	055	.051	027	014	.010	.000	.021
4	- 00=	010	- 010	020	_ 021	_ 025	_ 028	- 027	_ 021	_ 009	010	007	- 017
5		006						020					
6		004						015				003	
7		001	.002	.001			007		003	.003		001	
1	001	001	.002	•001	004	007	007	•000	.005	•000	1004	.001	.002
8	.000	.001	.004	.005	.005	.005	.004	.004	.004	.005	.006	.001	.004
9	.000	.003	.005	.007	.013	.015	.010	.010	.008	.008	.008	.004	.007
10	.001	.004	.007	.010	.017	.023	.017	.015	.013	.011	.009	.005	.011
11	.002	.005	.008	.014	.022	.029	.024	.020	.018	.014	.010	.006	.014
11	.002	.005	.003	•014	.022	1020	*024	.020	.010		1010		
	1												
6. 6	.006	.005	.007	.009	.005	.003	.001	.007	.012	.008	.010	.004	.006
7. 7	.006	.006	.008	.009	.001	.000	.000	.004	.009	.011	.011	.004	.005
8. 8	.005	.005	.007	.005	.000	.000	.000	.002	.007	.008		.004	.005
9. 9	.003	.004	.005	.006	002	.000	002	001	.002	.006	.007	.004	.003
10.10	.001	.002	.002	ł	1	l	001	1		.003	.002	.003	.000
7. 2. 9	.002	.001		001		l		003	.000	.003	.002	.002	001
6. 2. 8	.002	.000	.002	.001	001	005	004	000	.003	.003	.002	.001	.000
6. 2.10	.003	.001	.003	.003	.002	1	.001	.003	.006	.005	.003	.002	.003
6. 2. 6	.002			003	006	1	010	007	002	.000	.000	000	003
7. 2	.003	000	.000	005	011	017	014	010	003	.000	001	.000	005
8. 2	.001	002		011	017	023	019	017	009	003	004	000	009
8. 1	.001							016					009
7. 1	.002	.000						009					005
9.12.3.9	002	003	003	010	015	020	016	016	013	004	005	001	009
	U					,			·	1			

#### XCIX.

## England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours to obtain the true Mean *Humidity* for the respective Months. (Glaisher.)

Thousandths.

		<u> </u>				housand							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Midn	013	021	063	095	087	105	091	096	080	053	018	011	061
1	.002	021	065	106	100	114	095	104	080	059	009	012	064
2	.004	026	066	116	108	125	107	113	085	066	011	017	069
3	003	033	067	123	<b>11</b> 3	132	116	117	091	070	020	019	075
4		I .		126									
5	1	035		<b>125</b>			1	<b></b> 123	4				1
6	1	034	1	112				107				026	
7	020	030	055	080	059	065	<b></b> 055	061	080	058	031	025	052
8	000	000	005	000	004	015	00=	000	0.17	00=	007	070	00=
9	020	1		065	024	015	1		047	1		018	1
10	017 004	007 .009	003 .031		.018	.035	.041	.030	.042	009 .025		007 .008	.003
11	.011	.009	.060		.083	.100	.104	.102	.082	.060	ł	.022	.052
**	.011	.020	.000	.022	.003	1.100	.104	102	.502	.000	.021	.022	1000
Noon	.031	.045	.084	.070	.110	.123	.114	.127	.115	.088	.040	.033	.082
1	.054	.058	.100	.132	.126	.137	.119	.142	.131	.109		.046	.100
2	.059	.065	.106	.151	.125	.135	.123	.145	.132	.113		.048	.105
3	.048	.065	.104	.147	.118	.123	.121	.138	.126	.108	.047	.036	.098
4	.036	.053	.087	.128	.108	.113	.111	.120	.103	.089	.032	.024	.084
5	.021	.032	.063	.110	.091	.099	.095	.100	.071	.055	.018	.013	.064
6	.007	.009	.038	.088	.074	.078	.062	.071	.044	.030	1	.004	.042
7	005	010	.010	.059	.052	.049	.025	.036	.009	.007	005	003	.019
	0	000		000	000			000	015	077	0.0	005	00.
8			010		.022	i .	015	1		,		005	
9 10		029		030				038					
10				058 080				067 085					
11	015	030	000	030	075	055	050	000	071	043	020	009	055
6. 6	007	012	012	012	005	015	017	018	027	020	014	011	015
7. 7		020						012					
8. 8	017	021		022	001	003	010	010	031	024	016	011	016
9. 9		018	018	1	.000	.005	.000	004		017		007	
10.10	011	010			.000	.009	.006	.001			006		006
7. 2. 9	.008	.002	.006	.014	.016	.015	.009	.015	.004	.010	.002	.005	.009
6 2 0	000	000	07.7	070	007	0.10	004	070	010	010	000	.006	010
6. 2. 8 6. 2.10	.008	.003	.011	.019	- 0021	.013	.004	.013 009	.016 008	.010	.003	.005	.010 003
6. 2. 6	006 .015	.000	002 .027	006 .042	003 .038	010 .035	.029	.036	005 -026	.024	.000	.009	.025
0. 2. 0	•010	*0.19	.021	*042	.000	.000	•020	.000	1020		1000	.505	.020
7. 2	.019	.017	.026	.036	.033	.035	.034	.042	.026	.027	.012	.011	.026
8. 2	.019	.022	.036	.043	.050	.060	.059	.062	.042	.038	.016	.015	.039
8. 1	.017	.019	.032	.034	.051	.061	.057	.061	.042	.036	.014	.014	.037
7. 1	.017	.014	.023	.026	.033	.036	.032	.041	.025	.026	.009	.010	.024
9.12.3.9	.011	018	.038	.038	.032	.064	.059	.064	.050	.040	.016	.014	.037

# METEOROLOGICAL TABLES.

VI.

MISCELLANEOUS TABLES,

USEFUL IN

TERRESTRIAL PHYSICS AND METEOROLOGY.

F

1



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Ι.

## POSITIONS OF THE PRINCIPAL OBSERVATORIES.

[From the American Nautical Almanac.]

(North Latitudes and West Longitudes are considered as positive.)

li-		1	1	
Place.	Latitude.	Longitude from Washington in Time.	Longitude from Washington in Arc.	Longitude from Greenwich in Arc.
Åbo,	0 1 11	h. m. s.	0 1 #	0 1 11
Altona,	+60 26 56.8	- 6 37 20.0	260 40 0.6	337 42 48.6
Athens,	53 32 45.3	5 47 57.4	273 0 39.8	350 3 27.8
′	37 58 20	6 43 6.4	259 13 24.2	336 16 12.2
Berlin,	52 30 16.7	6 1 46.1	269 33 28.1	346 36 16.1
Bilk,	51 12 25	5 35 16.1	276 10 58.1	353 13 46.1
Bonn,	50 43 45.0	5 36 35.7	275 51 5.1	352 53 53.1
Breslau,	51 6 56.0	6 16 21.2	265 54 42.0	342 57 30.0
Brussels,	50 51 10.7	5 25 38.8	278 35 18.0	355 38 6.0
Cambridge (Eng.),	52 12 51.8	5 8 34.7	282 51 18.9	359 54 6.9
Cambridge (Mass.),	+42 22 48.6	0 23 41.5	354 4 36.9	71 7 24.9
Camorago (Exassi);	12 22 1010	0 20 11.0	331 1 3310	71 7 23.0
Cape of Good Hope,	-33 56 3	6 22 7.2	264 28 12.3	341 31 0.3
Christiania,	+59 54 43.7	- 5 51 6.0	272 13 30.6	349 16 18.6
Cincinnati,	39 5 54	+ 0 29 46.9	7 26 42.8	84 29 30.8
Copenhagen,	55 40 53.0	- 5 58 30.5	270 22 22.5	347 25 10.5
Cracow,	50 3 50.0	6 28 2.4	262 59 23.4	340 2 11.4
Dorpat,	58 22 47.1	6 55 5.8	256 13 33.6	333 16 21.6
Dublin,	53 23 13	4 42 49.2	289 17 42.0	6 20 30.0
Durham,	54 46 6.4	5 1 53.2	284 31 42.0	1 34 30.0
Edinburgh,	55 57 23.2	4 55 28.2	286 7 57.0	3 10 45.0
Florence,	43 46 40.8	5 53 12.9	271 41 47.1	348 44 35.1
Geneva,	46 11 58.8	- 5 32 48.9	276 47 46.8	353 50 34.8
Georgetown,	38 54 26.1	+ 0 0 6.2	0 1 33.0	77 4 21.0
Göttingen,	51 31 47.9	- 5 47 57.3	273 0 40.5	350 3 28.5
Gotha,	50 56 5.2	5 51 6.9	272 13 17.1	349 16 5.1
Greenwich,	51 28 38.2	5 8 11.2	282 57 12.0	0 0 0
**	#0 00 #	F 40 40	0#0 #0 40 0	970 1 900
Hamburg,	53 33 7	- 5 48 4.8	. 272 58 48.6	350 1 36.6
Hudson,	41 14 42.6	+ 0 17 32.1	4 23 0.9	81 25 48.9 310 52 1.1
Kasan,	55 47 23.1	- 8 24 43.1 6 30 11.6	233 49 13.1 262 27 6.6	310 52 1.1 339 29 54.6
Königsberg,	54 42 50.4 48 3 23.8	6 30 11.6 6 4 44.6	268 48 50.7	345 51 38.7
Kremsmünster,	45 3 23.5	0 4 44.0	405 45 50.7	549 91 55.7
Leipsic,	51 20 20.7	5 57 39.7	270 35 4.5	347 37 52.5
Levden,	52 9 28.2	5 26 8.6	278 27 50.6	355 30 38.6
Liverpool,	53 24 47.7	4 56 11.1	285 57 13.7	3 0 1.7
London,	51 31 29.8	5 7 34.1	283 6 28.5	0 9 16.5
Madras,	+13 4 9.2	-10 29 8.2	202 42 57.0	279 45 45.0
Ziamirao,	1 0.1	20 20 0.2		

Place.	La	titu	le.	from V	ngitu Vash Tim	ington	from V	ngitu Vash Arc	ington	from G	ngitu reen Arc.	wich in
Mannheim,	+49	20	12.9	h.		1. s. 2.7	274		19,5	351	32	7.5
Markree,			31.7	4		22.8			18.0	8	27	6.0
Marseilles,		17	49	5	-	40.2			57.2	354		45.2
Milan,		28	0.7	5		57.8	1		32.4	350	48	20.4
Modena,			52.8	5		55.2	272		12.5	349	4	0.5
Moscow,	55	45	19.8	7	38	28.5	245	22	52.7	322	25	40.7
Munich,	48	8	45	5	54	37.6	271	20	35.4	348	23	23.4
Naples,	40	51	46.6	6	5	12.1	268	41	58.1	345	44	46.1
Olmütz,	49	35	40.0	6	17	11.3	265	42	10.5	342	44	58.5
Oxford,	51	45	36.0	5	3	8.6	284	12	51.0	1	15	39.0
Padua,	45	24	2.5	5	55	40.2	271	4	56.6	348	7	44.6
Palermo,	+38	6	44	-6	1	36.7	269	35	50.1	346	38	38.1
Paramatta,	-33	48	49.8	+8	47	42.6	131	55	38.3	208	58	26.3
Paris,	+48	50	13.2	-5	17	32.7	280	36	50.1	357	39	38.1
St. Petersburg,	59	56	29.7	7	9	24.7	252	38	49.8	329	41	37.8
Philadelphia,	39	<b>57</b>	7.5	0	7	33.6	358	6	35.4	75	9	23.4
Prague,	50	5	18.5	6	5	53.2	268	31	42.6	345	34	30.6
Pulkowa,	59	46	18.7	7	9	29.9	252	37	31.9	329	40	19.9
Rome,	41	53	54	5	58	5.9	270	28	31.5	347	31	19.5
San Fernando,	+36.	27	45	4	43	22.1	289	9	29.1	6	12	17.1
Santiago,	-33	26	24.8	0	25	52.3	353	31	55.5	70	34	43.5
Senftenberg,	+50	5	10.1	6	14	1.1	266	29	43.1	343	32	31.1
Vienna,	48	12	35.5	6	13	43.7	266	34	4.1	343	36	52.1
Washington,	38	53	39.3	0	0	0	0	0	0	77	2	48.0
Wilna,	+54	40	59.1	-6	49	23.0	257	39	15.5	334	42	3.5

II. TO CONVERT PARTS OF THE EQUATOR IN ARC INTO SIDEREAL TIME, OR TO CONVERT TERRESTRIAL LONGITUDE IN ARC INTO TIME.

					D	EGREES.					
Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.
1	$\begin{bmatrix} 0 & 4 \\ 0 & 8 \end{bmatrix}$	41	2 44 2 48	81	5 24 5 28	121 122	8 4 8 8	161	10 44	201	13 24
3	0 8 0 12	42	2 48 2 52	83	5 28 5 32	123	8 8 8 8 12	162 163	10 48 10 52	202 203	13 28 13 32
4	0 16	44	2 56	84	5 36	124	8 16	164	10 56	204	13 36
5	0 20	45	3 0	85	5 40	125	8 20	165	11 0	205	13 40
6	0 24	46	3 4	86	5 44	126	8 24	166	11 4	206	13 44
7	0 28	47	3 8	87	5 48	127	8 28	167	11 8	207	13 48
8 9	0 32 0 36	48	3 12 3 16	88	5 52 5 56	128 129	8 32 8 36	168 169	11 12	208	13 52
10	0 40	50	3 20	90	6 0	130	8 36 8 40	170	11 16 11 20	210	13 56 14 U
10	0 40		5 20			100	0 40	110	11 20	210	14 0
11	0 44	51	3 24	91	6 4	131	8 44	171	11 24	211	14 4
12	0 48	52	3 28	92	6 8	132	8 48	172	11 28	212	14 8
13	0 52	53	3 32	93	6 12	133	8 52	173	11 32	213	14 12
14	0 56	54	3 36	94	6 16	134	8 56	174	11 36	214	14 16
15	1 0	55	3 40	95	6 20	135	9 0	175	11 40	215	14 20
16	1 4	56	3 44	96	6 24	136	9 4	176	11 44	216	14 24
17	1 8	57	3 48	97	6 28	137	9 8	177	11 48	217	14 28
18	1 12	58	3 52	98	6 32	138	9 12	178	11 52	218	14 32
19	1 16	59	3 56	99	6 36	139	9 16	179	11 56	219	14 36
20	1 20	60	4 0	100	6 40	140	9 20	180	12 0	220	14 40
21	1 24	61	4 4	101	6 44	141	9 24	181	12 4	221	14 44
22	1 28	62	4 8	102	6 48	142	9 28	182	12 8	222	14 48
23	1 32	63	4 12	103	6 52	143	9 32	183	12 12	223	14 52
24	1 36	64 65	4 16 4 20	104	6 56 7 0	144 145	9 36 9 40	184 185	12 16 12 20	224 225	14 56 15 0
25	1 40	00	4 40	105	, ,	149	9 40	155	12 20	229	15 0
26	1 44	66	4 24	106	7 4	146	9 44	186	12 24	226	15 4
27	1 48	67	4 28	107	7 8	147	9 48	187	12 28	227	15 8
28	1 52	68	4 32	108	7 12	148	9 52	188	12 32	228	15 12
29	1 56	69	4 36	109	7 16	149	9 56	189	12 36	229	15 16
30	2 0	70	4 40	110	7 20	150	10 0	190	12 40	230	15 20
31	2 4	71	4 44	111	7 24	151	10 4	191	12 44	231	15 24
32	2 8	72	4 48	112	7 28	152	10 8	192	12 48	232	15 28
33	2 12	73	4 52	113	7 32	153	10 12	193	12 52	233	15 32
34 35	2 16 2 20	74 75	4 56 5 0	114	7 36	154	10 16 10 20	194	12 56 13 0	234 235	15 36
30	2 20	10	5 0	115	7 40	155	10 20	195	13 0	400	15 40
36	2 24	76	5 4	116	7 44	156	10 24	196	13 4	236	15 44
37	2 28	77	5 8	117	7 48	157	10 28	197	13 8	237	15 48
38	2 32	78	5 12	118	7 52	158	10 32	198	13 12	238	15 52
39 40	2 36 2 40	79 80	5 16 5 20	119	7 56 8 0	159	10 36 10 40	199 200	13 16 13 20	239 240	15 56 16 0
40	4 40	] 00	0 20	120	0 0	160	10 40	200	15 20	240	10 0

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to convert parts of the equator in arc into sidereal time, or  $\phantom{-}2$ TO CONVERT TERRESTRIAL LONGITUDE IN ARC INTO TIME.

					DEGR	EES,					
Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.
241	16 4	261	17 24 17 28	281	18 44	301	$\begin{bmatrix} 20 & 4 \\ 20 & 8 \end{bmatrix}$	321	21 24	341	22 44 22 48
242 243	16 8	262	17 28	282	18 48 18 52	302 303	20 8 20 12	322 323	$\begin{vmatrix} 21 & 28 \\ 21 & 32 \end{vmatrix}$	342 343	$\begin{array}{ccc} 22 & 48 \\ 22 & 52 \end{array}$
244	16 12 16 16	263 264	17 32	283 284	18 56	304	20 12	324	21 36	344	22 56
245	16 20	265	17 40	285	19 0	305	20 20	325	21 40	345	23 0
240	10 20	200	1, 40	200	15 0		20 20	020	21 10	010	20 0
246	16 24	266	17 44	286	19 4	306	20 24	326	21 44	346	23 4
247	16 28	267	17 48	287	19 8	307	20 28	327	21 48	347	23 8
248	16 32	268	17 52	288	19 12	308	20 32	328	21 52	348	23 12
249	16 36	269	17 56	289	19 16	309	20 36	329	21 56	349	23 16
250	16 40	270	18 0	290	19 20	310	20 40	330	22 0	350	23 20
251	16 44	271	18 4	291	19 24	311	20 44	331	22 4	351	23 24
252	16 48	272	18 8	292	19 28	312	20 48	332	22 8	352	23 28
253	16 52	273	18 12	293	19 32	313	20 52	333	22 12	353	23 32
254	16 56	274	.18 16	294	19 36	314	20 56	334	22 16	354	23 36
255	17 0	275	18 20	295	19 40	315	21 0	335	22 20	355	23 40
256	17 4	276	18 24	296	19 44	316	21 4	336	22 24	356	23 44
257	17 8	277	18 28	297	19 48	317	21 8	337	22 28	357	23 48
258	17 12	278	18 32	298	19 52	318	21 12	338	22 32	358	23 52
259	17 16	279	18 36	299	19 56	319	21 16	339	22 36	359	23 56
260	17 20	280	18 40	300	20 0	320	21 20	340	22 40	360	24 0
					Min	UTES.					
í	m. s. 0 4	, 11	m. s. 0 44	21	m. s. 1 24	31	m. s. 2 4	41	m. s. 2 44	51	m. s. 3 24
2	0 8	12	0 48	22	1 28	32	2 8	42	2 48	52	3 28
3	0 12	13	0 52	23	1 32	33	2 12	43	2 52 -	53	3 32
4	0 16	14	0 56	24	1 36	34	2 16	44	2 56	54	3 36
5	0 20	15	1 0	25	1 40	35	2 20	45	3 0	55	3 40
6	0 24	16	1 4	26	1 44	36	2 24	46	3 4	56	3 44
7	0 28	17	1 8	27	1 48	37	2 28	47	3 8	57	3 48
8	0 32	18	1 12	28	1 52	38	2 32	48	3 12	58	3 52
9	0 36	19	1 16	29	1 56	39	2 36	49	3 16	59	3 56
10	0 40	20	1 20	30	2 0	40	2 40	50	3 20	60	4 0
		,,			Sec	onds.				1.	
" 1	s. 0.067	111	s. 0.733	21	s. 1.400	" 31	s. 2.067	" 41	s. 2.733	" 51	s. 3.400
2	0.133	12	0.800	22	1.467	32	2.133	42	2.800	52	3.467
3	0.200	13	0.867	23	1.533	33	2.200	43	2.867	53	3.533
4	0.267	14	0.933	24	1.600	34	2.267	44	2.933	54	3.600
5	0.333	15	1.000	25	1.667	35	2.333	45	3.000	55	3.667
6	0.400	16	1.067	26	1.733	36	2.400	46	3.067	56	3.733
7	0.467	17	1.133	27	1.800	37	2.467	47	3.133	57	3.800
8	0.533	18	1.200	28	1.867	38	2.533	48	3.200	58	3.867
9	0.600	19	1.267	29	1.933	39	2.600	49	3.267	59	3.933
10	0.667	20	1.333	30	2.000	40	2.667	50	3.333	60	4.000

III. TO CONVERT SIDEREAL TIME INTO PARTS OF THE EQUATOR IN ARC, OR TO CONVERT TIME INTO TERRESTRIAL LONGITUDE IN ARC.

					Hot	TRS.			<del></del>		1
Time.	Arc.	Time.	Arc	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.
h.	0	h.	0	h.	0	h.	0	h.	0	h.	0
1	15	5	75	9	135	13	195	17	255	21	315
2 3	30 45	6 7	90 105	10	150 165	14 15	210 225	18 19	$\frac{270}{285}$	22 23	330 345
4	60	8	120	12	180	16	240	20	300	24	360
-	00 1		120			UTES.	2 10	20	000		
m,	0 /	m.	0 /	m.	0 /	m.	0 /	m.	0 /	m.	0 /
1	0 15	11	2 45	21	5 15	31	7 45	41	10 15	51	12 45
2	0 30	12	3 0	22	5 30	32	8 0	42	10 30	52	13 0
3	0 45	13	3 15	23	5 45	33	8 15	43	10 45	53	13 15
4	1 0	14	3 30	24	6 0	34	8 30	44	11 0	54	13 30
5	1 15	15	3 45	25	6 15	35	8 45	45	11 15	55	13 45
6	1 30	16	4 0	26	6 30	36	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	37	9 15	47	11 45	57	14 15
8	$\begin{array}{c c} 2 & 0 \\ 2 & 15 \end{array}$	18 19	4 30 4 45	28 29	7 0 7 15	38	9 30 9 45	48	$\begin{array}{ccc} 12 & 0 \\ 12 & 15 \end{array}$	58 59	14 30 14 45
10	2 30	20	5 0	30	7 30	40	10 0	50	12 13	60	15 0
	<u>'</u>	11		<u>'</u>	SEC	ONDS.		1		'}	
S.	1 , ,,	s.	, ,,	8.	, ,,	s.	, ,,	s.	, ,,	s.	, ,,
1	0 15	11	2 45	21	5 15	31	7 45	41	10 15	51	12 45
2	0 30	12	3 0	22	5 30	32	8 0	42	10 30	52	13 0
3	0 45	13	3 15	23	5 45	33	8 15	43	10 45	53	13 15
4	1 0	14	3 30	24	6 0	34 35	8 30 8 45	44 45	11 0 11 15	54	13 30 13 45
5	1 15	15	3 45	25	6 15					-	
6	1 30	16	4 0	26	6 30	36	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	37	9 15	47	11 45	57	14 15
8 9	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	18 19	4 30 4 45	28 29	7 0 7 15	38	9 30 9 45	48 49	$12   0 \\ 12   15$	58	14 30 14 45
10	2 30	20	5 0	30	7 30	40	10 0	50	12 13	60	15 0
	1	11			Tenths o	F SECON	DS.	JI	·	1	1
S.		s.	1 //	8.	l "	s.	"	S.	"	s.	
0.01	0.15	0.18	2.70	0.35	5.25	0.52	7.80	0.69	10.35	0.86	12.90
0.02	0.30	0.19	2.85	0.36	5.40	0.53	7.95	0.70	10.50	0.87	13.05
0.03	0.45	0.20	3.00	0.37	5.55	0.54	8.10 8.25	$0.71 \\ 0.72$	10.65	0.88	13.20
0.04	0.60	$\begin{array}{c c} 0.21 \\ 0.22 \end{array}$	3.15	0.38	5.85	0.55	8.40	0.72	10.50	0.89	13.50
0.06	0.73	0.22	3.45	0.40	6.00	0.57	8.55	0.74	11.10	0.91	13.65
0.07	1.05	0.24	3.60	0.41	6.15	0.58	8.70	0.75	11.25	0.92	13.80
0.08	1.20	0.25	3.75	0.42	6.30	0.59	8.85	0.76	11.40	0.93	13.95
0.09	1.35	0.26	3.90	0.43	6.45	0.60	9.00	0.77	11.55	0.94	14.10
0.10		0.27	4.05	0.44	6.60	0.61	9.15	0.78	11.70	0.95	14.25
0.11		0.28	4.20	0.45	6.75	0.62	9.30	0.79	11.85	0.96	14.40
0.12	1	0.29	4.35	0.46	6.90 7.05	0.63	9.45	0.80	12.00 12.15	0.97	14.55 14.70
0.13	1	$\begin{vmatrix} 0.30 \\ 0.31 \end{vmatrix}$	4.50 4.65	0.47	7.05	0.65	9.75	0.81	12.15	0.99	14.85
0.15	1	0.31	4.80	0.49	7.35	0.66	9.90	0.83	12.45	1.00	15.00
0.16		0.33	4.95	0.50	7.50	0.67	10.05	0.84	12.60		
0.17	2.55	0.34		0.51	7.65	0.68	10.20	0.85	12.75		

# IV. FOR CONVERTING SIDEREAL TIME INTO MEAN SOLAR TIME, AND MEAN TIME INTO SIDEREAL TIME.

	HOURS				MINU	SECONDS.						
Hours	Mean Time.	Sidereal Time.	Min- utes.	Mean Time.	Sidereal Time.	Min- utes.	Mean Time.	Sidereal Time.	Sec- onds.	Mean or Sidereal Time.	Sec- onds.	Mean or Sidereal Time
	m s.	m. s.		s.	S.		s.	s.		g.		s.
1	0 9.83	0 9.86	1	0.16	0.16	31	5.08	5.09	1	0.00	31	0.09
2	0 19.66	0 19.71	2	0.33	0.33	32	5.24	5.26	2	0.01	32	0.09
3	0 29.49	0 29.57	3	0.49	0.49	33	5.41	5.42	3	0.01	33	0.09
4	0 39.32	0 39.43	4	0.66	0.66	34	5.57	5.59	5	0.01	34 35	0.09
5	0 49.15	0 49.28	5	0.82	0.82	35	5.75	5.75	9	0.01	99	0.10
6	0 58.98	0 59.14	6	0.98	0.99	36	5.90	5.91	6	0.02	36	0.10
7	1 8.81	1 9.00	7	1.15	1.15	37	6.06	6.08	7	0.02	37	0.10
8	1 18.64	1 18.85	8	1.31	1.31	38	6.23	6.24	8	0.02	38	0.10
9	1 28.47	1 28.71	9	1.47	1.48	39	6.39	6.41	9	0.03	39	0.11
10	1 38.30	1 38.57	10	1.64	1.64	40	6.55	6.57	10	0.03	40	0.11
13	1 48.13	1 48.42	11	1.80	1.81	41	6.72	6.74	11	0.03	41	0.11
11 12	1 57.96	1 58.42	12	1.97	1.97	41	6.88	6.90	12	0.03	42	0.11
13	2 7.78	2 8.13	13	2 13	2.14	43	7.05	7.06	13	0.04	43	0.12
14	2 17.61	2 17.99	14	2.29	2.30	44	7.21	7.23	14	0.04	44	0.12
15	2 27.44	2 27.85	15	2.46	2.46	45	7.37	7.39	15	0.04	45	0.12
16	2 37.27	2 37.70	16	2.62	2.63	46	7.54	7.56	16	0.04	46	0.13
17	2 47.10	2 47.56	17	2.79	2.79	47	7.70	7.72	17	0.05	47	0.13
18	2 56.93	2 57.42	18	2.95	2.96	48	7.86	7.89	18	0.05	48	0.13
19	3 6.76	3 7.27	19	3.11	3.12	49	8.03	8 05	19	0.05	49	0.13
20	3 16.59	3 17.13	20	3.28	3.29	50	8.19	8.21	20	0.06	50	0.14
21	3 26.42	3 26.99	21	3.44	3.45	51	8.36	8.38	21	0.06	51	0.14
22	3 36.25	3 36.84	22	3.60	3.61	52	8.52	8.54	22	0.06	52	0.14
23	3 46.03	3 46.70	23	3.77	3.79	53	8.68	8.71	23	0.06	53	0.15
24	3 55.91	3 56.56	24	3.93	3.94	54	8.85	8.87	24	0.07	54	0.15
25	4 5.74	4 6.41	25	4.10	4.11	55	9.01	9.04	25	0.07	55	0.15
26	4 15.57	4 16.27	26	4.26	4.27	56	9.17	9.20	26	0.07	56	0.15
27	4 25.40	4 26.13	27	4.42	4.43	57	9.34	9.36	27	0.07	57	0.16
28	4 35.23	4 35.98	28	4.59	4.60	58	9.50	9.53	28	0.08	58	0.16
29	4 45.06	4 45.84	29	4.75	4.76	59	9.67	9.69	29	0.08	59	0.16
30	4 54.89	4 55.69	30	4.92	4.93	60	9.83	9.86	30	0.08	60	0.16

V.

# CORRECTION OF THE TIME OBTAINED BY OBSERVATION OF THE SUN, IN ORDER TO HAVE THE TRUE TIME OF THE CLOCK.

		1	1 1							1	1	1	1			
Day of	Jan.	Feb.	Mar.	Apr.	Apr.	May.	June.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Dec.	Day of
Month.	Add.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Subt.	Add.	Month.
	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	
1	4	14	13	4		3	3		3	6	0	10	16	11		1
2	4	14	12	4		3	2		4	6	0	11	16	10		2
3	5	14	12	3		3	2		4	6	1	11	16	10		3
4	5	14	12	3		3	2	• •	4	6	1	11	16	10		4
5	6	14	12	3		4	2		4	6	1	12	16	9		5
6	6	14	12	2	٠.	4	2		4	6	2	12	16	9		6
7	7	14	11	2		4	2		4	5	2	12	16	8		7
8	7	15	11	2		4	1		5	5	2	12	16	8		8
9	8	15	11	2		4	1		5	5	3	13	16	7		9
10	8	15	11	1		4	1		5	5	3	13	16	7		10
11	9	15	10	1		4	1		5	5	3	13	16	6		11
12	9	15	10	1		4	1		5	5	4	13	16	6		12
13	9	15	10	1		4	0		5	5	4	14	16	5	• •	13
14	10	14	9	0		4	0		5	4	5	14	15	5		14
15	10	14	9	0		4	0		6	4	5	14	15	4		15
16	10	14	9	0		4	0	• •	6	4	5	14	15	4		16
17	11	14	9	0		4	0		6	4	6	15	15	3	• •	17
18	11	14	8		1	4	• •	1	6	4	6	15	15	3	• •	18
19	11	14	8		1	4	• •	1	6	3	6	15	14	2		19
20	11	14	8		1	4		1	6	3	7	15	14	2	• •	20
21	12	14	7		1	4	• •	1	6	3	7	15	14	1		21
22	12	14	7		2	4	• •	2	6	3	7	15	14	1		22
23	12	14	7		2	4		2	6	2	8	16	13	0	• •	23
24	12	13	6		2	3	• •	2	6	2	8	16	13	0	• •	24
25	13	13	6		2	3	• •	2	6	2	8	16	13	0	• •	25
26	13	13	6		2	3	• •	2	6	2	9	16	12	٠.	1	26
27	13	13	5		2	3	• •	3	6	1	9	16	12	• •	1	27
28	13	13	5		3	3	• •	3	6	1	9	16	12	• •	2	28
29	14	13	5		3	3		3	6	1	10	16	11	• •	2	29
30	14	• •	4	• •	3	3	• •	3	6	0	10	16	11	• •	3	30
31	14		4		• •	3	• •	• •	6	0	• •	16	• •	• •	3	31
T.			1					0								

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#### TABLE FOR COMPUTING TERRESTRIAL SURFACES.

The tables under No. VI. were published by Delcros in the Annuaire Météorologique de la France pour 1850, p. 65 et seq.

The formula from which they have been computed reads as follows: —

$$\mathbf{S} = \frac{a \, b \, \pi}{90} \begin{cases} \sin \frac{1}{2} \phi \cos \left(\mathbf{L} + \frac{1}{2} \phi\right) \\ -\frac{1}{3} \left[ 2 \cdot \left(\frac{a - b}{a + b}\right) + \left(\frac{a - b}{a + b}\right)^{2} \right] \sin \left(\phi + \frac{1}{2} \phi\right) \cos \left[3 \, \mathbf{L} + \left(\phi + \frac{1}{2} \phi\right)\right] \\ +\frac{1}{5} \left[3 \cdot \left(\frac{a - b}{a + b}\right)^{2} + \left(\frac{a - b}{a + b}\right)^{3} \right] \sin \left(2 \phi + \frac{1}{2} \phi\right) \cos \left[5 \, \mathbf{L} + \left(2 \phi + \frac{1}{2} \phi\right)\right] \\ - \text{etc.} ; \end{cases}$$

in which  $a=\frac{1}{2}$  great axis of the globe;  $b=\frac{1}{2}$  small axis; L= the latitude of the lower limit of a quadrilateral surface; L'= the latitude of the upper limit of the same;  $\phi=L'-L$ ; S= the area of a quadrilateral surface of one degree in longitude;  $\pi=$  the ratio of the circumference to the diameter.

Substituting the numerical values, the quarter of the meridian being = 10,000,724 legal metres; the  $\frac{1}{2}$  great axis, or  $a_1 = 6,376,989$  metres; the  $\frac{1}{2}$  small axis, or  $b_1 = 6,356,323$  metres; the ratio of the axis  $\frac{1}{30\frac{1}{2}\cdot64}$ ; and making  $\phi = 1^{\circ}$  nonagesimal, the

formula becomes,

$$\mathbf{S} = \begin{cases} 224.996360 \cos \left( \begin{array}{c} \mathbf{L} + 0^{\circ} \ 30' \right) \\ -0.730851 \cos \left( 3 \ \mathbf{L} + 1^{\circ} \ 30' \right) \\ +0.001784 \cos \left( 5 \ \mathbf{L} + 2^{\circ} \ 30' \right) \\ -0.000004 \cos \left( 7 \ \mathbf{L} + 3^{\circ} \ 30' \right) \\ + \ \text{etc.} \end{cases}$$

The first three terms of the formula give the results with sufficient accuracy.

In order to avoid too large a number of figures, the results are given in square miles, the linear base of which is a mile equal to  $\frac{1}{15}$  of the mean degree of the meridian. That mile is thus  $=\left(\frac{10000724}{90\times15}\right)=7407.942$  metres. In order to convert the results into new geographical miles, of which  $60=1^\circ$ , multiply by 16,  $\log=1.2041200$ ; into common French leagues,  $25=1^\circ$ , multiply by 2.777778,  $\log=0.4436975$ ; into nautical leagues,  $20=1^\circ$ , multiply by 1.777778,  $\log=0.2498775$ ; into English statute miles,  $69.163=1^\circ$ , by 21.711034,  $\log=1.3366868$ .

## Use of the Tables.

Table I., which gives the number of square miles contained in the quadrilateral surfaces of one degree in latitude and longitude, successively from the equator to the pole, will be more frequently used. Table II. has been computed for maps on a smaller scale; and Tables III. and IV. for maps of very small scale, covering large areas, in which surfaces of one degree could not be estimated with sufficient accuracy. If the scale is large enough to have the minutes traced on, then Table V. is to be used.

For computing a surface by Table I., which may serve as an example for all the others, find first the lowest parallel circle which crosses, on the map, the surface to be estimated; suppose it is 40° lat. N., and the zone within 40° and 41° lat. N. contains four integral degrees of longitude, that is, four surfaces of one degree each way; then in the first column of the table, on the line beginning with latitude 40°, and in the vertical column headed 4, take the value of these four surfaces, viz. 685.88. Then take likewise the value of the number of surfaces between 41° and 42° lat. N., and so on. The fractional parts left outside of the integral degrees are best estimated, with the compass, in decimals, the values of which can be found in the columns of the multiples, by properly moving the decimal point to the left. Having taken them in that way, and summing them up with all the integral surfaces, we obtain the total surface required.

F

TABLE I. QUADRILATERAL SURFACES OF 1 DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

	Limiting Multiples of these Quadrilateral Surfaces from 1 to 9.													
Limi LATIT	ting UDES.			Multiples	of these Qu	adrilateral S	Surfaces fro	m 1 to 9.						
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	1	224.259	448.52	672.78	897.04	1121.29	1345.55	1569.81	1794.07	2018.33				
1	2	224.192	448.38	672.58	896.77	1120.96	1345.15	1569.35	1793.54	2017.73				
2	3	224.059	448.12	672.18	896.24	1120.30	1344.36	1568.42	1792.47	2016.53				
3	4	223.860	447.72	671.58	895.44	1119.30	1343.16	1567.02	1790.88	2014.74				
4	5	223.594	447.19	670.78	894.37	1117.97	1341.56	1565.16	1788.75	2012.34				
5	6	223.261	446.52	669.78	893.05	1116.31	1339.57	1562.83	1786.09	2009.35				
6	7	222.863	445.73	668.59	891.45	1114.31	1337.18	1560.04	1782.90	2005.76				
7	8	222.398	444.80	667.19	889.59	1111.99	1334.39	1556.78	1779.18	2001.58				
8	9	221.867	443.73	665.60	887.47	1109.33	1331.20	1553.07	1774.93	1996.80				
9	10	221.270	442.54	663.81	885.08	1106.35	1327.62	1548.89	1770.16	1991.43				
10	11	220.607	441.21	661.82	882.43	1103.03	1323.64	1544.25	1764.85	1985.46				
11	12	219.878	439.76	659.63	879.51	1099.39	1319.27	1539.15	1759.02	1978.90				
12	13	219.084	433.17	657.25	876.34	1095.42	1314.50	1533.59	1752.67	1971.76				
13	14	218.225	436.45	654.67	872.90	1091.12	1309.35	1527.57	1745.80	1964.02				
14	15	217.300	434.60	651.90	869.20	1086.50	1303.80	1521.10	1738.40	1955.70				
15	16	216.311	432.62	648.93	865.24	1081.55	1297.86	1514.17	1730.48	1946.80				
16	17	215.257	430.51	645.77	861.03	1076.28	1291.54	1506.80	1722.05	1937.31				
17	18	214.138	428.28	642.41	856.55	1070.69	1284.83	1498.97	1713.10	1927.24				
18	19	212.955	425.91	638.87	851.82	1064.78	1277.73	1490.69	1703.64	1916.60				
19	20	211.709	423.42	636.13	846.84	1058.54	1270.25	1481.96	1693.67	1905.38				
20	21	210.399	420.80	631.20	841.59	1051.99	1262.39	1472.79	1683.19	1893.59				
21	22	209.025	418.05	627.08	836.10	1045.13	1254.15	1463.18	1672.20	1881.23				
22	23	207.589	415.18	622.77	830.36	1037.95	1245.54	1453.12	1660.71	1868.30				
23	24	206.090	412.18	618.27	824.36	1030.45	1236.54	1442.63	1648.72	1854.81				
24	25	204.529	409.06	613.59	818.12	1022.65	1227.18	1431.71	1636.24	1840.76				
25	26	202.907	405.81	608.72	811.63	1014.53	1217.44	1420.35	1623.25	1826.16				
26	27	201.223	402.45	603.67	804.89	1006.11	1207.34	1408.56	1609.78	1811.00				
27	28	199.477	398.95	598.43	797.91	997.39	1196.86	1396.34	1595.82	1795.30				
28	29	197.672	395.34	593.02	790.69	988.36	1186.03	1383.70	1581.38	1779.05				
29	30	195.806	391.61	587.42	783.23	979.03	1174.84	1370.64	1566.45	1762.26				
30	31	193.881	387.76	581.64	775.52	969.40	1163.29	1357.17	1551.05	1744.93				
31	32	191.897	383.79	575.69	767.59	959.48	1151.38	1343.28	1535.17	1727.07				
32	33	189.854	379.71	569.56	759.41	949.27	1139.12	1328.98	1518.83	1708.68				
33	34	187.753	375.51	563.26	750.01	938.76	1126.52	1314.27	1502.02	1689.77				
34	35	185.594	371.19	556.78	742.38	927.97	1113.57	1299.16	1484.75	1670.35				
35	36	183.379	366.76	550.14	733.52	916.89	1100.27	1283.65	1467.03	1650.41				
36	37	181.107	362.21	543.32	724.43	905.53	1086.64	1267.75	1448.86	1629.96				
37	38	178.780	357.56	536.34	715.12	893.90	1072.68	1251.46	1430.24	1609.02				
38	39	176.397	352.79	529.19	705.59	881.98	1058.38	1234.78	1411.18	1587.57				
39	40	173.960	347.92	521.88	695.84	869.80	1043.76	1217.72	1391.68	1565.64				
40	41	171.469	342.94	514.41	685.88	857.34	1028.81	1200.28	1371.75	1543.22				
41	42	168.925	337.85	506.77	675.70	844.62	1013.55	1182.47	1351.40	1520.22				
42	43	166.328	332.66	498.98	665.31	831.64	997.97	1164.30	1330.62	1496.95				
43	44	163.680	327.36	491.04	654.72	818.40	982.08	1145.76	1309.44	1473.12				
44	45	160.980	321.96	482.94	643.92	804.90	965.88	1126.86	1287.84	1448.82				

TABLE I. (Continued.) QUADRILATERAL SURFACES OF 1 DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT	ting UDES.			Multiples	of these Qu	adrilateral S	Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
45	46	158.231	316.46	474.69	632.92	791.15	949.39	1107.62	1265.85	1424.08
46	47	155.432	310.86	466.30	621.73	777.16	932.59	1088.02	1243.46	1398.89
47	48	152.584	305.17	457.75	610.34	762.92	915.51	1068.09	1220.67	1373.26
48	49	149.689	299.38	449.07	598.75	748.44	899.13	1047.82	1197.51	1347.20
49	50	146.746	293.49	440.24	586.98	733.73	880.48	1027.22	1173.97	1320.71
50	51	143.757	287.51	431.27	575.03	718.78	862.54	1006.30	1150.06	1293.81
51	52	140.723	281.45	422.17	562.89	703.61	844.34	985.06	1125.78	1266.51
52	53	137.644	275.29	412.93	550.58	688.22	825.86	963.51	1101.15	1238.80
53	54	134.522	269.04	403.57	538.09	672.61	807.13	941.65	1076.17	1210.70
54	55	131.357	262.71	394.07	525.43	656.78	788.14	919.50	1050.86	1182.21
55	56	128.150	256.30	384.45	512.60	640.75	768.90	897.05	1025.20	1153.35
56	57	124.903	249.81	374.71	499.61	624.51	749.42	874.32	999.22	1124.13
57	58	121.616	243.23	364.85	486.46	608.08	729.69	851.31	972.92	1094.54
58	59	118.289	236.58	354.87	473.16	591.45	709.74	828.03	946.32	1064.61
59	60	114.926	.229.85	344.78	459.70	574.63	689.55	804.48	919.41	1034.33
60	61	111.525	223.05	334.58	446.10	557.63	669.15	780.68	892.20	1003.78
61	62	108.089	216.18	324.27	432.35	540.44	648.53	756.62	864.71	972.80
62	63	104.618	209.24	313.85	418.47	523.09	627.71	732.32	836.94	941.56
63	64	101.113	202.23	303.34.	404.45	505.56	606.68	707.79	808.90	910.0
64	65	97.575	195.15	292.73	<b>3</b> 90 <b>.</b> 30	487.88	585.45	683.03	780.60	878.18
65	66	94.007	188.01	282.02	376.03	470.03	564.04	658.05	752.05	846.06
66	67	90.408	180.82	271.22	361.63	452.04	542.45	632.85	723.26	813.67
67	68	86.779	173.56	260.34	347.12	433.90	520.68	607.46	694.23	781.01
68	69	83.123	166.25	249.37	332.49	415.61	498.74	581.86	664.98	748.1
69	70	79.439	158.88	238.32	317.76	397.20	476.64	556.08	635.52	714.93
70	71	75.730	151.46	227.19	302.92	378.65	454.38	530.11	605.S4	681.5
71	72	71.996	143.99	215.99	287.99	359.98	431.98	503.98	575.97	647.97
72	73	68.239	136.48	204.72	272.96	341.20	409.44	477.68	545.91	614.13
73	74	64.460	128.92	193.38	257.84	322.30	386.76	451.22	515.68	580.1
74	75	60.659	121.32	181.98	242.64	303.30	363.96	424.62	485.28	545.9
75	76	56.839	113.68	170.52	227.36	284.20	341.04	397.88	454.72	511.5
76	77	53.001	106.00	159.00	212.00	265.00	318.00	371.00	424.00	477.0
77	78	49.145	98.29	147.43	196.58	245.72	294.87	344.01	393.16	442.30
<b>7</b> 8	79	45.272	90.54	135.82	181.09	226.36	271.63	316.91	362.18	407.4
79	80	41.386	82.77	124.16	165.54	<b>2</b> 06 <b>.</b> 93	248.31	289.70	331.08	372.4
80	81	37.485	74.97	112.46	149.94	187.43	224.91	262.40	299.88	337.3
81	82	33.572	67.14	100.72	134.29	167.86	201.43	235.01	268.58	302.13
82	83	29.649	59.30	88.95	118.59	148.24	177.89	207.54	237.19	266.8
83	84	25.715	51.43	77.15	102.86	128.58	154.29	180.01	205.72	231.4
84	85	21.773	43.55	65.32	87.09	108.87	130.64	152.41	174.19	195.96
85	86	17.824	35.65	53.47	71.30	89.12	106.95	124.77	142.59	160.43
86	87	13.869	27.74	41.61	55.48	69.35	83.22	97.09	110.96	124.82
87	SS	9.910	19.82	29.73	39.64	49.55	59.46	69.37	79.28	89.19
ss	89	5.947	11.89	17.84	23.79	29.74	35.68	41.63	47.58	53.58
89	90	1.983	3.97	5.95	7.93	9.91	11.90	13.88	15.86	17.8

TABLE II. QUADRILATERAL SURFACES OF 2 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT	iting						Surfaces fro			
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	2	896.903	1793.81	2690.71	3587.61	4484.51	5381.42	6278.32	7175.22	8072.13
2	4	895.838	1791.68	2687.51	3583.35	4479.19	5375.03	6270.87	7166.71	8062.54
4	6	893.710	1787.42	2681.13	3574.84	4468.55	5362.26	6255.97	7149.68	8043.39
6	8	890.520	1781.04	2671.56	3562.08	4452.60	5343.12	6233.64	7124.16	8014.68
8	10	886.272	1772.54	2658.82	3545.09	4431.36	5317.63	6203.91	7090.18	7976.45
10	12	880.969	1761.94	2642.91	3523.88	4404.85	5285.82	6166.79	7047.76	7928.72
12	14	874.617	1749.23	2623.85	3498.47	4373.09	5247.70	6122.32	6996.94	7871.55
14	16	867.221	1734.44	2601.66	3468.88	4336.11	5203.33	6070.55	6937.77	7804.99
16	18	858.789	1717.58	2576.37	3435.16	4293.95	5152.74	6011.52	6870.31	7729.10
18	20	849.328	1698.66	2547.98	3397.31	4246.64	5095.97	5945.30	6794.63	7643.95
20	22	838.848	1677.70	2516.54	3355.39	4194.24	5033.09	5871.94	6710.78	7549.63
22	. 24	827.359	1654.72	2482.08	3309.44	4136.80	4964.16	5791.51	6618.87	7446.23
24	26	814.872	1629.74	2444.62	3259.49	4074.36	4889.23	5704.11	6518.98	7333.85
26	28	811.400	1602.80	2404.20	3205.60	4007.00	4808.40	5609.80	6411.20	7212.60
28	30	786.956	1573.91	2360.87	3147.83	3934.78	4721.74	5508.69	6295.65	7082.61
30	32	771.555	1543.11	2314.67	3086.22	3857.78	4629.33	5400.89	6172.44	6944.00
32	34	755.213	1510.43	2265.64	3020.85	3776.06	4531.28	5286.49	6041.70	6796.92
34	36	737.946	1475.89	2213.84	2951.78	3689.73	4427.68	5165.62	5903.57	6641.51
36	38	719.773	1439.55	2159.32	2879.09	3598.87	4318.64	5038.41	5758.19	6477.96
38	40	700.713	1401.43	2102.14	2802.85	3503.57	4204.28	4904.99	5605.71	6306.42
40	42	680.787	1361.57	2042.36	2723.15	3403.93	4084.72	4765.51	5446.29	6127.08
42	44	660.016	1320.03	1980.05	2640.06	3300.08	3960.09	4620.11	5280.13	5940.14
44	46	638.423	1276.85	1915.27	2553.69	3192.11	3830.54	4468.96	5107.38	5745.81
46	48	616.032	1232.06	1848.10	2464.13	3080.16	3696.19	4312.23	4928.26	5544.29
48	50	592.869	1185.74	1778.61	2371.48	2964.34	3557.21	4150.08	4742.95	5335.82
50	52	568.960	1137.92	1706.88	2275.84	2844.80	3413.76	3982.72	4551.68	5120.64
52	54	544.332	1088.66	1632.99	2177.33	2721.66	3265.99	3810.32	4354.65	4898.99
54	56	519.014	1038.03	1557.04	2076.06	2595.07	3114.09	3633.10	4152.11	4671.13
56	58	493.037	986.07	1479.11	1972.15	2465.18	2958.22	3451.26	3944.29	4437.33
58	60	466.430	932.86	1399.29	1865.72	2332.15	2798.58	3265.01	3731.44	4197.87
60	62	439.228	878.46	1317.68	1756.91	2196.14	2635.37	3074.59	3513.82	3953.05
62	64	411.461	822.92	1234.38	1645.84	2057.30	2468.76	2880.23	3291.69	3703.15
64	66	383.164	766.33	1149.49	1532.66	1915.82	2298.99	2682.15	3065.32	3448.48
66	68	354.374	708.75	1063.12	1417.50	1771.87	2126.24	2480.62	2834.99	3189.36
68	70	325.124	650.25	975.37	1300.50	1625.62	1950.75	2275.87	2601.00	2926.12
70	72	295.453	590.91	886.36	1181.81	1477.27	1772.72	2068.17	2363.63	2659.08
72	74	265.398	530.80	796.20	1061.59	1326.99	1592.39	1857.79	2123.19	2388.59
74	76	234.998	469.99	704.99	939.99	1174.99	1409.99	1644.98	1879.98	2114.98
76	78	204.290	408.58	612.87	817.16	1021.45	1225.74	1430.03	1634.32	1838.61
78	80	173.316	346.63	519.95	693.26	866.58	1039.90	1213.21	1386.53	1559.85
80	82	142.115	284.23	426.34	568.46	710.57	852.69	994.80	1136.92	1279.03
82	84	110.728	221.46	332.18	442.91	553.64	664.37	775.09	885.82	996.55
84	86	79.195	168.39	237.59	316.78	395.98	475.17	554.37	633.56	712.76
86	88	47.559	95.12	142.68	190.24	237.79	285.35	332.91	380.47	428.03
88	90	15.860	31.72	47.58	63.44	79.30	95.16	111.02	126.88	142.74

TABLE III. QUADRILATERAL SURFACES OF 5 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT	ting UDES.			Multiple	es of these (	Quadrilatera	l Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	5	5599.821	11199.64	16799.46	22399.29	27999.11	33598.93	39198.75	44798.57	50398.39
5	10	5558.288	11116.58	16674.87	22233.15	27791.44	33349.73	38908.02	44466.31	50024.60
10	15	5475.466	10950.93	16426.40	21901.87	27377.33	32852.80	38328.27	43803.73	49279.20
15	20	5351.846	10703.69	16055.54	21407.39	26759.23	32111.08	37462.93	42814.77	48166.62
20	25	5188.165	10376.33	15564.49	20752.66	25940.82	31128.99	36317.15	41505.32	46693.48
25	30	4985.425				24927.12	29912.55	34897.97	39883.40	44868.82
30	35	4744.891			18979.57		28469.35	33214.24		42704.02
35	40	4468.110	1			22340.55	26808.66	31276.77		40212.99
40	45	4156.909	1			20784.54	24941.45	29098.36	33255.27	37412.18
45	50	3813.408	7626.82	11440.22	15253.63	19067.04	22880.45	26693.86	30507.26	34320.67
50	55	3440.013	6880.03	10320.04	13760.05	17200.06	20640.08	24080.09	27520.10	30960.12
55	60	3039.419	6078.84	9118.26	12157.68	15197.09	18236.51	21275.93	24315.35	27354.77
60	65	2614.598	5229.20	7843.80	10458.39	13072.99	15687.59	18302.19	20916.79	23531.39
65	70	2168.779	4337.56	6506.34	8675.12	10843.89	13012.67	15181.45	17350.23	19519.01
70	<b>7</b> 5	1705.427	3410.85	5116.28	6821.71	8527.13	10232.56	11937.99	13643.42	15348-84
75	80	1228.213	2456.43	3684.64	4912.85	6141.07	7369.28	8597.49	9825.71	11053.92
80	85	740.973	1481.95	2222.92	2963.89	3704.86	4445.84	5186.81	5927.78	6668.76
85	90	247.668	495.34	743.00	990.67	1238.34	1486.01	1733.68	1981.34	2229.01

TABLE IV. QUADRILATERAL SURFACES OF 10 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT			. Multiples of these Quadrilateral Surfaces from 1 to 9.												
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
0	10	22316.220	44632.44	66948.66	89264.88	111581.10	133897.32	156213.54	178529.76	200845.98					
10	20	21654.626	43309.25	64963.88	86618.50	108273.13	129927.76	151582.38	173237.01	194891.63					
20	30	20347.180	40694.36	61041.54	81388.72	101735.90	122083.08	142430.26	162777.44	183124.62					
30	40	18426.004	36852.01	55278.01	73704.02	92130.02	110556.02	128982.03	147408.03	165834.04					
40	50	15940.634	31881.27	47821.90	63762.54	79703.17	95643.80	111584.44	127525.07	143465.71					
50	60	12958.864	25917.73	38876.59	51835.46	64794.32	77753.18	90712.05	103670.91	116629.78					
60	70	1	19133.51			47833.77	57400.53								
70	80				23469.12		35203.69								
80	90	1977.282	3954.56	5931.85	7909.13	9886.41	11863.69	13840.97	15818.26	17795.54					

TABLE V. Mean Quadrilateral Surfaces of 1, 10, 20, and 30 Minutes in Latituda and in Longitude deduced from each Quadrilateral of 1 Degree in Table I.

Limi LATIT	ting UDES.	Mean Su	and in L	asuring in ongitude.	Latitude	Limi LATIT	ting UDES.	Mean Su	rfaces mea and in L	suring in I	Latitude
Inf.	Sup.	1/.	10%	20′.	30%	Inf.	Sup.	1'.	10'.	20′.	30%
0	1	0.0623	6.229	24.918	56.065	45	46	0.0440	4.395	17.581	39.558
1	2	0.0623	6.228	24.910	56.048	46	47	0.0432	4.318	17.270	38.858
2	3	0.0622	6.224	24.895	56.015	47	48	0.0424	4.238	16.954	38.146
3	4	0.0622	6.218	24.873	55.965	48	49	0.0416	4.158	16.632	37.422
4	5	0.0621	6.211	24.844	55.898	49	50	0.0408	4.076	16.305	36.686
5	6	0.0620	6,202	24.807	55.815	50	51	0.0399	3.993	15.973	35.939
6	7	0.0619	6.191	24.763	55.716	51	52	0.0391	3.909	15.636	35.181
7	8	0.0618	6.178	24.711	55.599	52	53	0.0382	3.823	15.294	34.411
8	9	0.0616	6.163	24.652	55.467	53	54	0.0374	3.737	14.947	33.630
9	10	0.0615	6.146	24.586	55.317	54	55	0.0365	3.649	14.595	32.839
10	11	0.0613	6.128	24.512	55.152	55	56	0.0356	3.560	14.239	32.038
11	12	0.0611	6.108	24.431	54.970	56	57	0.0347	3.470	13.878	31.226
12	13	0.0609	6.086	24.343	54.771	57	58	0.0338	3.378	13.513	30.404
	14	0.0606	6.062	24.247	54.556	58	59	0.0329	3.286	13.143	29.572
13		0.0604	6.036	24.247	54.325	59	60	0.0329	3.192	12.770	28.731
14	15		1			i i					
15	16	0.0601	6.009	24.035	54.078	60	61	0.0310	3.098	12.392	27.881
16	17	0.0598	5.979	23.917	53.814	61	62	0.0300	3.002	12.010	27.022
17	18	0.0595	5.948	23.793	53.534	62	63	0.0291	2.906	11.624	26.154
18	19	0.0592	5.915	23.662	53.239	63	64	0.0281	2.809	11.235	25.278
19	20	0.0588	5.881	23.523	52.927	64	65	0.0271	2.710	10.842	24.394
20	21	0.0584	5.844	23.378	52.600	65	66	0.0261	2.611	10.445	23.502
21	22	0.0581	5.806	23.225	52.256	66	67	0.0251	2.511	10.045	22.602
22	23	0.0577	5.766	23.065	51.897	67	68	0.0241	2.411	9.642	21.695
23	24	0.0572	5.725	22.899	51.523	68	69	0.0231	2.309	9.236	20.781
24	25	0.0568	5.681	22.725	51.132	69	70	0.0221	2.207	8.827	19.860
25	26	0.0564	5.636	22.545	50.727	70	71	0.0210	2.104	8.414	18.933
26	27	0.0559	5.590	22.358	50.306	71	72	0.0200	2.000	8.000	17.999
27	28	0.0554	5.541	22.164	49,869	72	73	0.0190	1.896	7.582	17.060
28	29	0.0549	5.491	21.964	49.418	73	74	0.0179	1.791	7.162	16.115
29	30	0.0544	5.439	21.756	48.952	74	75	0.0168	1.685	6.740	15.165
30	31	0.0539	5.386	21.542	48.470	75	76	0.0158	1.579	6.315	14.210
31	32	0.0533	5.330	21.322	47.974	76	77	0.0147	1.472	5.889	13.250
32	33	0.0527	5.274	21.095	47.463	77	78	0.0137	1.365	5.461	12.280
33	34	0.0522	5.214	20.861	46.938	78	79	0.0126	1.258	5.030	11.318
34	35	0.0522	5.155	20.622	46.399	79	80	0.0125	1.150	4.598	10.346
				1	1	80			1		9.37
35	36	0.0509	5.094	20.375	45.845	80	81	0.0104	1.041 0.933	4.165 3.730	8.39
36	37	0.0503	5.031	20.123	45.277	81	82	0.0093 $0.0082$	0.933	3.730	7.415
37	38	0.0497	4.966	19.864	44.695		83	1			
38	39 40	0.0490	4.900	19.600 19.329	44.099	83	84	0.0071	0.714	2.857	6.429
		II.	1								
40	41	0.0476	4.763	19.052	42.867	85	S6	0.0049	0.495	1.980	4.450
41	42	0.0469	4.692	18.769	42.231	86	87	0.0039	0.385	1.541	3.46
42	43	0.0462	4.620	18.481	41.582	87	88	0.0028	0.275	1.101	2.47
43	41	0.0455	4.547	18.187	40.920	88	89	0.0017	0.165	0.661	1.48
44	45	0.0447	4.472	17.SS7	40.245	89	90	0.0006	0.055	0.220	0.49

#### ERRATA IN THE FIRST EDITION.

A, page 7, line below the title, instead of  $(32 + \frac{4}{5}x^{\circ})$  read  $(32 + \frac{9}{5}x^{\circ})$ . A, "21, on the line beginning with 30, in the last four columns,

instead of 100.75 100.97 101.20 101.42 read 100.85 101.07 101.30 101.52.

- B, "7, on the line beginning with 23°, second column, instead of 20.410, read 20.888.
- B, "23, on the line beginning with 12°, third column, instead of 5 87, read 5.37.
- B, "30-32, at the head of each first column, Temperature of the Air, add "in Centigrade degrees."
- B, "40, Table II., first part, on the line beginning with 60, column headed 7, instead of 24.11,01, read 24.9,01.
- B, " Table II., first part, on the line beginning with 70, column headed 5, instead of 27.4,47, read 27.8,47; and column headed 8, instead of 28.11,77, read 28.9,77.
- B, " Table II., second part, on the line beginning with 70, column headed 5, instead of 328.47, read 332.47.
- B, "41, Table III., line beginning with 20, the five last columns, instead of 63.54 66.08 68 62 71.16 73.70, read 63.50 66.04 68.58 71.12 73.66.
- B, " Table III, line beginning with 200, column headed 3, instead of 515.11, read 515.61.
- B, "42, Table V., line beginning with 180, column headed 7, instead of 516.21, read 506.21.
- B, "43, Table VI., first part, on line beginning with 70, column headed 2, instead of 76.635, read 76.735.
- В, Table VI., second part, on line beginning with 7, the last eight columns, instead of 0.6483 0.6572 0 6661 0 6750 0.6839 0.6927 0.7016 0.7105, 0.6395 0.6483 0.6572 0 6661 0.6750 0.6839 0.6927 0.7016.
- B, "43, Table VI., second part, on line beginning with 12, column headed 5, instead of 1.1018, read 1.1102.
- C, "11, on line beginning with 26.5 inches, column headed 6, instead of 674.41, read 674.61.
- C, " on line of 27.1 inches, column headed 1, instead of 688.38, read 688.58.
- C, "12, on line of 30.5 inches, column headed 2, instead of 778.20, read 775.19.
- C, "39 and 41, at the head of table, instead of "Tenths of Degrees," read "English Inches."
- D, "28, 29, and 30, head of page, instead of "Tenths of a Degree," read "Hundredths of a Degree."
- D, " 35, note at the bottom, instead of "Geology," read "Geodesy."
- D, " 36, on line beginning with 160, columns headed 8 and 9, instead of 550.19 and 553.47, read 551.19 and 554.47.
- D, ". 36, on line beginning with 260, columns headed 2, 3, 5, and 6,

instead of 860.59 863.87 879.43 882.72, read 859.60 862.88 869.44 872.72.

- D, " 37, on line beginning with 620, column headed 4, instead of 2048.28, read 2047.28.
- D, """ " " " 770, " 0, " 2526.39, " 2526.29.
- D, "38, " " 880, " 5, " 2903.69, " 2903.60.
- D, " " " " 890, " 6, " 2939.79, " 2939.69.
- D, " " " " " 930, " 5, " 3069.64, " 3067.64.
- D, " " " " " 990, " 4, " 3261.71, " 3261.21.
- D, "" " " " 990, " 5, " 3264.59, " 3264.49.
- D, " 39, on line beginning with 1380, columns headed 3, 4, 5, 6, 7, 8,

instead of 4537.28 4540.56 4543.85 4547.13 4550.41 4553.69, read 4537.48 4540.76 4544.05 4547.33 4550.61 4553.89.

- D, "40, on line beginning with 1610, column headed 5, instead of 5292.65, read 5298.65.
- D, "44, Table X., on line beginning with 3, column headed 6, instead of 21.0205, read 23 0205.
- D, "45, Table XII., on line beginning with column 0, column headed 5, instead of 0.83333, read 0.08333.



















